
STORMWATER POLLUTION PREVENTION PLAN

AMS BUCHANAN

**ALBANY POST ROAD & CRAFT LANE
VILLAGE OF BUCHANAN, NEW YORK**

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JMC Project 22062

Date: 11/08/2023

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| C-100 | Site Layout Plan | 10/17/2023 |
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| C-300 | Site Utilities Plan | 10/17/2023 |
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| C-905 | Construction Details | 10/17/2023 |
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| L-100 | Site Landscaping Plan | 10/17/2023 |

I. INTRODUCTION

This Stormwater Pollution Prevention Plan has been prepared for the 5.96-acre AMS Buchanan site, located in the Village of Buchanan, Westchester County, New York (hereinafter referred to as the "Site"). The site is bordered by Craft Lane to the north, commercial properties to the south and east, and ConEdison to the west. The development has been designed in accordance with the following:

- Requirements of the New York State Department of Environmental Conservation (NYSDEC) SPDES General Permit No. GP-0-20-001, effective January 29, 2020.
- Chapter 166 "Stormwater Management" of the Village of Buchanan Zoning Code
- New York State Stormwater Management Design Manual

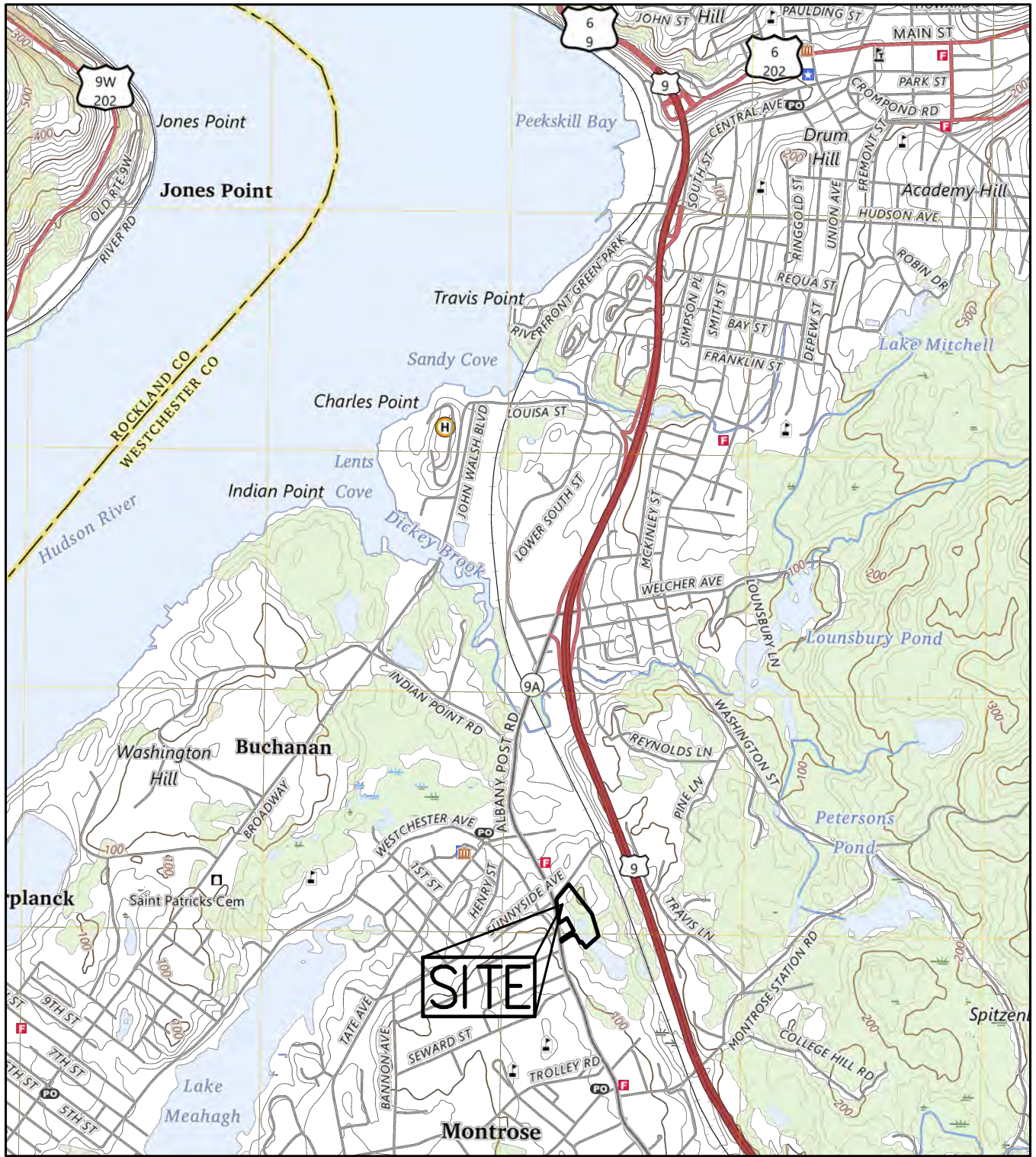
The proposed improvements on the Site consist of a multi-family apartment building comprised of four residential stories above a one-story parking structure. The building will contain 148 two- and one-bedroom dwelling units and 223 parking spaces. 149 of the parking spaces will be located within the structure and the remaining 74 will be in a parking area northwest of the building.

II. STORMWATER MANAGEMENT PLANNING

In order to be eligible for coverage under the NYSDEC SPDES General Permit No. GP-0-20-001 for Stormwater Discharges from Construction Activities, the Stormwater Pollution Prevention Plan (SWPPP) includes stormwater management practices (SMP's) from the publication "New York State Stormwater Management Design Manual," last revised January 2015.

A Stormwater Pollution Prevention Plan has been prepared for this project because it is a construction activity that involves:

- Soil disturbances of one (1) or more acres of land.



AMS BUCHANAN

ALBANY POST ROAD & CRAFT LANE VILLAGE OF BUCHANAN, NEW YORK

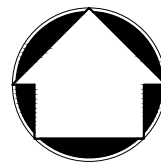
SITE LOCATION MAP

DATE: 11/01/2023

JMC PROJECT: 22062

FIGURE: 01

SCALE: 1" = 2,000'



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The proposed stormwater facilities have been designed such that the quantity and quality of stormwater runoff during and after construction are not adversely altered or are enhanced when compared to pre-development conditions.

Based on the GIS information provided by the website of the New York State Office of Parks, Recreation and Historic Places, the site does not contain, nor is it immediately adjacent to any properties listed on the State or National Register of Historic Places.

The Six Step Process for Stormwater Site Planning and Practice Selection

Stormwater management using green infrastructure is summarized in the six-step process described below. The six-step process was adhered to when developing this SWPPP. Information is provided in this SWPPP which documents compliance with the required process as follows:

Step 1: Site Planning

Implement planning practices that protect natural resources and utilize the hydrology of the site. Strong consideration must be given to reducing impervious cover to aid in the preservation of natural resources including protecting natural areas, avoiding sensitive areas and minimizing grading and soil disturbance.

Step 2: Determine Water Quality Treatment Volume (WQv)

Determine the required WQv for the site based on the site layout, impervious areas and sub-catchments. This initial calculation of WQv will have to be revised after green infrastructure techniques are applied. The following method has been used to calculate the WQv.

- **90% Rule** - According to the New York State Stormwater Design Manual, Section 4.1, the water quality volume is determined from the 90% rule. The method is based on 90% of the average annual stormwater runoff volume which must be provided due to

impervious surfaces. The Water Quality Volume (denoted as the WQv) is designed to improve water quality sizing to capture and treat 90% of the average annual stormwater runoff volume. The WQv is directly related to the amount of impervious cover created at a site. The average rainfall storm depth for 90% of storms in New York State in one year is used to calculate a volume of runoff. The rainfall depth depends on the location of the site within the state. From this depth of rainfall, the required water quality volume is calculated.

Due to the physical constraints of the site such as bedrock, groundwater, and urban fill, some of the proposed stormwater BMP's proposed to treat water quality are limited to proprietary/alternative practices rather than standard practices. The alternative practices are designed to treat stormwater runoff and/or provide water quantity control. The SWPPP proposes Water Quality Treatment Option III which implements the use of alternative practices to treat 75 % of the water quality volume from the disturbed, impervious area as well as any additional runoff from tributary areas that are not within the disturbed, impervious area.

Step 3: Runoff Reduction Volumes (RRv) by Applying Green Infrastructure Techniques and Standard SMP's

RRv is required for this project since it is a new development.

Green infrastructure techniques or standard SMP's with RRv capacity can potentially reduce the required WQv by incorporating combinations of green infrastructure techniques and standard SMP's within each drainage area on the site.

Green infrastructure techniques are grouped into two categories:

- Practices resulting in a reduction of contributing area such as preservation/restoration of conservation areas, vegetated channels, etc.
- Practices resulting in a reduction of contributing volume such as green roofs, stormwater planters, and rain gardens.

Apply a combination of green infrastructure techniques and standard SMPs with RRv capacity to provide 100% of the WQv calculated in Step 2. If the RRv calculated in this step is greater than or equal to the WQv in Step 2, the RRv requirement has been met and Step 4 can be skipped. If the RRv provided cannot meet or exceed 100% of the WQv, the project must, at a minimum, reduce a percentage of the runoff from impervious areas to be constructed on the site. The percent reduction is based on the Hydrologic Soil Group(s) (HSG) of the site and is defined as Specific Reduction Factor (S).

The Minimum RRv capacity required must be provided by green infrastructure techniques to verify that the RRv requirement has been met. The RRv that is provided by the green infrastructure techniques can then be subtracted from the Total Required WQv that must be provided by the SMP's.

Step 4: Determine the minimum RRv Required

The minimum RRv is calculated similar to the WQV. However, it is determined using only the new impervious cover and accounts for the hydrologic soil group present. In no case shall the runoff reduction achieved from the newly constructed impervious area be less than the minimum runoff reduction volume (RRv_{min}).

Step 5: Apply Standard Stormwater Management Practices to Address Remaining Water Quality Volume

Apply the standard SMP's to meet additional water quality volume requirements that cannot be addressed by applying the green infrastructure techniques. The standard SMP's with RRv capacity must be implemented to verify that the RRv requirement has been met.

Step 6: Apply Volume and Peak Rate Control Practices to Meet Water Quantity Requirements

The Channel Protection Volume (CPv), Overbank Flood Control (Qp) and Extreme Flood Control (Qf) must be met for the plan to be completed. This is accomplished by using practices

such as infiltration basins, dry detention basins, etc. to meet water quantity requirements. The following standards must be met:

1. Stream Channel Protection (CPv)

Stream Channel Protection Volume Requirements (CPv) are designed to protect stream channels from erosion. In New York State this goal is accomplished by providing 24-hour extended detention of the one-year, 24-hour storm event, remained from runoff reduction. Reduction of runoff for meeting stream channel protection objectives, where site conditions allow, is encouraged and the volume reduction achieved through green infrastructure can be deducted from CPv. Trout waters may be exempted from the 24-hour ED requirement, with only 12 hours of extended detention required to meet this criterion. Detention time may be calculated using either a center of mass method or plug flow calculation method.

- CPv is not required for this site because the 1-year post-development peak discharge is less than or equal to 2.0 cfs.

2. Overbank Flood (Qp) which is the 10 year storm.

Overbank control requires storage to attenuate the post development 10-year, 24-hour peak discharge rate (Qp) to predevelopment rates.

3. Extreme Storm (Qf) which is the 100 year storm.

100 Year Control requires storage to attenuate the post development 100-year, 24-hour peak discharge rate (Qf) to predevelopment rates.

Based on the foregoing, this project is eligible for coverage under NYSDEC SPDES General Permit No. GP-0-20-001.

III. STUDY METHODOLOGY

Runoff rates were calculated based upon the standards set forth by the United States Department of Agriculture Natural Resources Conservation Service Technical Release 55, Urban Hydrology for Small Watersheds (TR-55), dated June 1986. The methodology set forth in TR-55 considers a multitude of characteristics for watershed areas including soil types, soil permeability, vegetative cover, time of concentration, topography, rainfall intensity, ponding areas, etc.

The 1, 10, 25, 100-year storm recurrence intervals were reviewed in the design of the stormwater management facilities (see Appendix A - Existing & Proposed Hydrologic Calculations).

Anticipated drainage conditions were analyzed taking into account the rate of runoff which will result from the construction of buildings, parking areas and other impervious surfaces associated with the site development.

Base Data and Design Criteria

For the stormwater management analysis, the following base information and methodology were used:

1. The site drainage patterns and outfall facilities were reviewed by JMC personnel for the purpose of gathering background data and confirming existing mapping of the watershed areas.
2. An Existing Drainage Area Map was developed from the topographical survey. The drainage area map reflects the existing conditions within and around the project area.
3. A Proposed Drainage Area Map was developed from the proposed grading design superimposed over the topographical survey. The drainage area map reflects the proposed

conditions within the project area and the existing conditions to remain in the surrounding area.

4. The United States Department of Agriculture (USDA) Web Soil Survey of the site available on its website at <http://websoilsurvey.nrcd.usda.gov>.
5. The United States Department of Agriculture Natural Resources Conservation Service National Engineering Handbook, Section 4 - Hydrology", dated March 1985.
6. The United States Department of Agriculture Natural Resources Conservation Service Technical Report No. 55, Urban Hydrology for Small Watersheds (TR-55), dated June 1986.
7. United States Department of Commerce Weather Bureau Technical Release No. 40 Rainfall Frequency Atlas of the United States.

The time of concentration was calculated using the methods described in Chapter 3 of TR-55, Second Edition, June 1986. Manning's kinematics wave equation was used to determine the travel time of sheet flow. The 2-year 24-hour precipitation amount of 3.37 inches was used in the equation for all storm events. The travel time for shallow concentrated flow was computed using Figure 3-1 and Table 3-1 of TR-55. Manning's Equation was used to determine the travel time for channel reaches.

8. All hydrologic calculations were performed with the Bentley PondPack software package version 10.0.
9. The New York State Stormwater Management Design Manual, revised January 2015.
10. New York Standards and Specifications for Erosion and Sediment Control, November 2016.

11. The storm flows for the 1-, 10-, 25-, & 100-year recurrence interval storms were analyzed for the total watershed areas. The Type III distribution design storm for a 24-hour duration was used and the mass rainfall for each design storm was taken from the Extreme Precipitation in New York & New England developed by the Natural Resource Conservation Service (NRCS) and the Northeast Regional Climate Center (NRCC) as follows:

24 Hour Rainfall Amounts

| Design Storm Recurrence Interval | Inches of Rainfall |
|----------------------------------|--------------------|
| 1 Year | 2.75 |
| 10 Year | 5.08 |
| 25 Year | 6.44 |
| 100 Year | 9.23 |

IV. EXISTING CONDITIONS

The existing conditions of the project site consists of an existing gravel drive and forested area over a previously developed quarry site. After stormwater runoff exits the project site, it flows to a stormwater pipe underneath the intersection of Albany Post Road and Craft Lane, with a portion of the site running into a pond on the south end of the site.

The following natural features, conservation areas, resource areas and drainage patterns of the project site have been identified and utilized to develop Drawing DA-1 “Existing Drainage Area Map” which is included in Appendix F:

- Wetlands (jurisdictional, wetland of special concern)
- Buffers (stream, wetland, forest, etc.)
- Forest, vegetative cover
- Topography (contour lines, existing flow paths, steep slopes, etc.)
- Soil (hydrologic soil groups, highly erodible soils, etc.)

Based on the USDA Web soil survey, all on-site soils belong to hydrological group D or are not rated. The soil types, boundaries and drainage areas/designations are depicted on Drawing DA-1 within Appendix F.

Three separate Design Points (DP-1 through DP-3) were identified for comparing peak rates of runoff in existing and proposed conditions. Similarly, three separate drainage areas were identified in existing conditions based on the existing drainage divides at the site. The numbers included in the name of each drainage area correspond to the Design Point they drain towards.

The following is a description of each of the drainage areas analyzed in the existing conditions analysis:

Existing Drainage Area 1 (EDA-1) is 0.52 acres in size and is located on the eastern portion of the site along the property line. This area consists of wooded area. This drainage area drains overland towards the property to the east. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 77 and 10 minutes, respectively.

Existing Drainage Area 2 (EDA-2) is 1.42 acres in size and is located on the southern portion of the site along the property line. This area consists of wooded area and an existing pond. This drainage area drains overland towards the pond. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 80 and 28 minutes, respectively.

Existing Drainage Area 3 (EDA-3) is 4.03 acres in size and is located on the northwestern portion of the site. This area consists of an existing gravel entrance road and wooded area. This drainage area drains towards an inlet at the property corner, which is connected to a collapsed pipe underneath Craft Lane. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 78 and 34 minutes, respectively.

The peak rates of runoff to the design points from the drainage areas for each storm are shown in the table below:

Table I
Summary of Peak Rates of Runoff in Existing Conditions
(Cubic Feet per Second)

| Storm Recurrence Interval | DP-1 | DP-2 | DP-3 |
|----------------------------------|-------------|-------------|-------------|
| 1 year | 0.43 | 0.99 | 2.27 |
| 10 year | 1.33 | 2.82 | 6.86 |
| 25 year | 1.90 | 3.96 | 9.79 |
| 100 year | 0.90 | 6.33 | 15.93 |

V. PROPOSED CONDITIONS

The proposed improvements on the Site consist of a multi-family apartment building comprised of four residential stories above a one-story parking structure. The building will contain 148 two- and one-bedroom dwelling units and 223 parking spaces. 149 of the parking spaces will be located within the structure and the remaining 74 will be in a parking area northwest of the building.

The proposed drainage improvements include a variety of stormwater practices, such as stormwater planters, green roof areas, JellyFish Filter systems and subsurface storage. This section describes the design and analysis of the proposed conditions used to demonstrate that the SWPPP meets the requirements of the General Permit.

The Six Step Process For Stormwater Site Planning and Practice Selection

Step 1: Site Planning

The following practices and site features were incorporated in the site design:

- Preserving hydrology - Maintaining drainage divides
- Wetlands and buffers – The site includes 0.16 acres of wetlands and 0.59 acres of wetland buffers. The project requires the disturbance of 0 acres of wetlands and 0.25 acres of wetland buffers.

- Floodplain considerations - The site doesn't lie within the 100 year flood zone according to the National Flood Insurance Program Flood Insurance Rate Map (FIRM) No. 36119C0018F, effective date 09/28/2007.
- Forest, vegetative cover – The maximum amount of forest and vegetative cover has been maintained and/or provided.
- Critical areas have been preserved.
- Topography (contour lines, existing flow paths, steep slopes, etc.) has been maintained or disturbed to the minimum extent practicable.
- Soil (hydrologic soil groups, highly erodible soils, etc.)
- Bedrock, significant geology features have been accounted for.

Step 2: Determine Water Quality Treatment Volume (WQv)

Step 3: Runoff Reduction Volumes (RRv) by Applying Green Infrastructure Techniques and Standard SMP's

- **Green Roofs**
- **Stormwater Planters**

Step 4: Determine the minimum RRv Required

RRv_{min} calculations can be found in Appendix 'B'. RRv_{min} was met through

- **Green Roofs**
- **Stormwater Planters**

Step 5: Apply Standard Stormwater Management Practices to Address Remaining Water Quality Volume

Non Standard/Alternative SMP's to Address Remaining Water Quality Volume (for Redevelopment Projects)

- **Hydrodynamic Separators**
- **Media Filters**

Step 6: Apply Volume and Peak Rate Control Practices to Meet Water Quantity Requirements

- **Subsurface Detention Systems**

All practices exceed the required elements of SMP criteria as outlined in Chapter 6 of the NYS Stormwater Management Design Manual. A summary of each category is provided below.

1. Feasibility – Stormwater practices are designed based upon unique physical environmental considerations noted in the NYS Stormwater Management Design Manual (NYSSMDM).
2. Conveyance – The design conveys runoff to the designed stormwater practice in a manner that is safe, minimizes erosion and disruption to natural drainage channel and promotes filtering and infiltration.
3. Pretreatment – All stormwater practices provide pretreatment as required in accordance with NYSSMDM design guidelines.
4. Treatment Geometry – The plan provides water quality treatment in accordance with NYSSMDM guidelines.
5. Environmental/Landscaping – Extensive landscaping has been provided for each proposed stormwater practice to enhance pollutant removal and provide aesthetic enhancement to the property.
6. Maintenance – Maintenance for the environment practices has been provided and is detail the SWPPP Report as required. Maintenance access is provided in the design plans.

In order to determine the post-development rates of runoff generated on-site, the following drainage areas were analyzed in the post-development conditions. These areas are graphically depicted on Drawing DA-2 "Proposed Drainage Area Map" located in Appendix "F".

Three separate Design Points (DP-1 through DP-3) were identified for comparing peak rates of runoff in existing and proposed conditions. Similarly, seven separate drainage areas were identified in proposed conditions based on the proposed drainage divides at the site. The numbers included in the name of each drainage area correspond to the Design Point they drain towards.

The following is a description of each of the drainage areas analyzed in the proposed conditions analysis:

Proposed Drainage Area 1 (PDA-1) is 0.25 acres in size and is located on the eastern portion of the site along the property line. This area consists of wooded area. This drainage area drains overland towards the property to the east. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 77 and 9 minutes, respectively.

Proposed Drainage Area 2A (PDA-2A) is 0.99 acres in size and is located on the southern portion of the site along the property line. This area consists of existing wooded area, an existing pond, and landscaped area. This drainage area drains overland towards the pond. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 81 and 22 minutes, respectively.

Proposed Drainage Area 2B (PDA-2B) is 0.43 acres in size and is comprised of portions of the building roof and courtyard area. This area is directed into stormwater planters along the south side of the building. After being treated by the planters, the runoff is directed into a subsurface detention system, which slowly releases the water into the existing pond. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 98 and 10 minutes, respectively.

Proposed Drainage Area 2C (PDA-2C) is 0.42 acres in size and is comprised of portions of the

building roof surrounding the courtyard area. This area is directed into intensive green roof planters along the edge of the courtyard. After being treated by the planters, the runoff is directed into a subsurface detention system, which slowly releases the water into the existing pond. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 98 and 10 minutes, respectively.

Proposed Drainage Area 2D (PDA-2D) is 0.18 acres in size and is comprised of portions of the courtyard area which drain into the planters. This area is directed into intensive green roof planters within the courtyard. After being treated by the planters, the runoff is directed into a subsurface detention system, which slowly releases the water into the existing pond. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 98 and 10 minutes, respectively.

Proposed Drainage Area 2E (PDA-2E) is 0.09 acres in size and is located on the southeastern corner of the site. This area consists of existing wooded area and landscaped area. This drainage area is collected by a drain inlet and directed to the subsurface detention system, which slowly releases the water into the existing pond. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 81 and 22 minutes, respectively.

Proposed Drainage Area 3 (EDA-3) is 3.61 acres in size and is located on the northwestern portion of the site. This area consists of existing wooded area, portions of the building roof area along with the proposed driveway and parking surfaces. This drainage area drains towards a JellyFish filter and subsurface detention system located under the parking area. The subsurface system slowly releases the stormwater into a new storm sewer, replacing the existing pipe underneath Craft Lane. The Curve Number (CN) and Time of Concentration (Tc) for this drainage area are 87 and 9 minutes, respectively.

The peak rates of runoff to the design point of each of the analyzed drainage areas for each storm are shown on the table below:

Table 2
Summary of Proposed Peak Rates of Runoff in Proposed Conditions
(Cubic Feet per Second)

| Storm Recurrence Interval | DP-1 | DP-2 | DP-3 |
|----------------------------------|-------------|-------------|-------------|
| 1 year | 0.21 | 0.99 | 2.00 |
| 10 year | 0.63 | 2.49 | 5.48 |
| 25 year | 0.90 | 3.62 | 8.01 |
| 100 year | 1.47 | 5.97 | 15.14 |

The reductions in peak rates of runoff from proposed to existing conditions are shown on the table below:

Table 3
Percent Reductions in Peak Rates of Runoff (Existing vs. Proposed Conditions)
(Cubic Feet per Second)

| Design Point | Storm Recurrence Frequency (Years) | Existing Peak Runoff Rate (cfs) | Proposed Peak Runoff Rate (cfs) | Percent Reduction (%) |
|---------------------|---|--|--|------------------------------|
| 1 | 1 year | 0.43 | 0.21 | 51.16% |
| | 10 year | 1.33 | 0.63 | 52.63% |
| | 25 year | 1.90 | 0.90 | 52.63% |
| | 100 year | 3.08 | 1.47 | 52.27% |
| 2 | 1 year | 0.99 | 0.99 | 0.00% |
| | 10 year | 2.82 | 2.49 | 11.70% |
| | 25 year | 3.96 | 3.62 | 8.59% |
| | 100 year | 6.33 | 5.97 | 5.69% |
| 3 | 1 year | 2.27 | 2.00 | 11.89% |
| | 10 year | 6.86 | 5.48 | 20.12% |
| | 25 year | 9.79 | 8.01 | 18.18% |
| | 100 year | 15.93 | 15.14 | 4.96% |

As demonstrated in Table 3, the proposed stormwater improvements will result in reductions of peak rates of runoff for all storms and design points analyzed.

VI. SOIL EROSION & SEDIMENT CONTROL

A potential impact of the proposed development on any soils or slopes will be that of erosion and transport of sediment during construction. An Erosion and Sediment Control Management Program will be established for the proposed development, beginning at the start of construction and continuing throughout its course, as outlined in the "New York State Standards and Specifications for Erosion and Sediment Control," November 2016. A continuing maintenance program will be implemented for the control of sediment transport and erosion control after construction and throughout the useful life of the project.

The Operator shall have a qualified professional conduct an assessment of the site prior to the commencement of construction and certify that the appropriate erosion and sediment controls, as shown on the Sediment & Erosion Control Plans, have been adequately installed to ensure overall preparedness of the site for the commencement of construction. In addition, the Operator shall have a qualified professional conduct one site inspection at least every seven calendar days and at least two site inspections every seven calendar days when greater than five acres of soil is disturbed at any one time.

Prior to the commencement of construction activity, the owner or operator must identify the contractor(s) and subcontractor(s) that will be responsible for installing, constructing, repairing, replacing, inspecting and maintaining the erosion and sediment control practices included in the SWPPP; and the contractor(s) and subcontractor(s) that will be responsible for constructing the post-construction stormwater management practices included in the SWPPP. The owner or operator shall have each of the contractors and subcontractors identify at least one person from their company that will be responsible for implementation of the SWPPP. This person shall be known as the trained contractor. The owner or operator shall ensure that at least one trained contractor is on site on a daily basis when soil disturbance activities are being performed. The owner or operator shall have each of the contractors and subcontractors identified above sign a copy of the certification statement provided in Appendix E before they commence any construction activity.

Soil Description

As provided by the United States Department of Agriculture, Soil Conservation Service "Web Soil Survey," soil classifications which exist on the subject site are described below.

Soils are placed into four hydrologic groups: A, B, C, and D. In the definitions of the classes, infiltration rate is the rate at which water enters the soil at the surface and is controlled by the surface conditions. Transmission rate is the rate at which water moves in the soil and is controlled by soil properties. Definitions of the classes are as follows:

- A. (Low runoff potential). The soils have a high infiltration rate even when thoroughly wetted. They chiefly consist of deep, well drained to excessively drained sands or gravels. They have a high rate of water transmission.
- B. The soils have a moderate infiltration rate when thoroughly wetted. They chiefly are moderately deep to deep, moderately well drained to well drained soils that have moderately fine to moderately coarse textures. They have a moderate rate of water transmission.
- C. The soils have a slow infiltration rate when thoroughly wetted. They chiefly have a layer that impedes downward movement of water or have moderately fine to fine texture. They have a slow rate of water transmission.
- D. (High runoff potential). The soils have a very slow infiltration rate when thoroughly wetted. They chiefly consist of clay soils that have a high swelling potential, soils that have a permanent high water table, soils that have a claypan or clay layer at or near the surface, and shallow soils over nearly impervious material. They have a very slow rate of water transmission.

A soil's tendency to erode is also described in the USDA web soil survey. The ratings in this interpretation indicate the hazard of soil loss from unsurfaced areas. The ratings are based on soil erosion factor K, slope, and content of rock fragments. The hazard is described as "slight," "moderate," or "SEVERE." A rating of "slight" indicates that little or no erosion is likely; "moderate" indicates that some erosion is likely, that the temporarily unsurfaced / unstabilized

during construction may require occasional maintenance, and that simple erosion-control measures are needed; and "SEVERE" indicates that significant erosion is expected, that the roads or trails require frequent maintenance, and that erosion-control measures are needed.

Per the Soil Survey, the following soils listed below are present at the site. Following this list is a detailed description of each soil type found on the property:

| SYM. | HYDRO. | SOIL GROUP | DESCRIPTION |
|-------------|------------------|-------------------|---|
| Pv | Not Rated | | Pits, quarry |
| W | Not Rated | | Water |
| CuD | D | | Chatfield-Hollis-Rock, outcrop complex, 0-15% |
| CtC | D | | Chatfield-Hollis-Rock complex, 0-15%, very rocky |
| HrF | D | | Hollis-Rock outcrop complex, 35-60% |
| UIC | Not Rated | | Urban land-Charlton-Chatfield complex, rolling |
| UmC | Not Rated | | Urban land-Chatfield-Rock outcrop complex, rolling |

Pv, Pits, quarry

This soil is comprised of 80 percent quarry pits and 3 percent minor components. It typically has unweathered bedrock. There is no soil group or drainage capacity ratings for this soil.

Hydrologic group: **NOT RATED**

W, Water

This soil is surface water. There is no soil group or drainage capacity ratings for this soil.

Hydrologic group: **NOT RATED**

CuD, Chatfield-Hollis-Rock, outcrop complex, 0 to 15 percent slopes

This soil is comprised of 35% Chatfield, 30% Hollis, and 20% rock outcrop. The landform is typically ridges and hills with a coarse-loamy melt-out till derived from granite, gneiss, and/or schist. The soil is well drained with a high class of runoff and low water table.

Hydrologic group: **D**

CtC, Chatfield-Hollis-Rock complex, 0 to 15 percent slopes, very rocky

This soil is comprised of 39% Chatfield, 26% Hollis, and 17% rock outcrop. The landform is typically ridges and hills with a coarse-loamy melt-out till derived from granite, gneiss, and/or schist. The soil is well drained with a high class of runoff and low water table.

Hydrologic group: **D**

HrF, Hollis-Rock outcrop complex, 35 to 60 percent slopes

This soil is comprised of 60% Hollis, 20% rock outcrop, and 4% minor components. The landform is typically ridges and hills with a coarse-loamy melt-out till derived from granite, gneiss, and/or schist. The soil is somewhat excessively drained with a very high class of runoff and low water table.

Hydrologic group: **D**

UIC, Urban land-Charlton-Chatfield complex, rolling, very rocky

This soil is comprised of 40% Urban land, 20% Charlton and similar soils, 15% Chatfield and similar soils and 3% minor components. The landform is typically till plains, ridges and hills with an acid loamy till derived mainly from schist, gneiss, or granite. The soil is well drained with a low water table.

Hydrologic group: **Not Rated**

UmC, Urban land-Chatfield-Rock outcrop complex, rolling

This soil is comprised of 50% Urban land, 20% Chatfield and similar soils, 15% rock outcrop and 1% minor components. The landform is typically ridges and hills with a loamy till derived mainly from granite, gneiss, or schist. The soil is well drained with a low water table.

Hydrologic group: **Not Rated**

On-Site Pollution Prevention

There are temporary pollution prevention measures used to control litter and construction debris on site, such as:

- Silt Fence

- Manufactured Insert Inlet Protection
- Excavated Drop Inlet Protection

There will be inlet protection provided for all storm drains and inlets with the use of curb gutter inlet protection structures and stone & block drop inlet protection, which keep silt, sediment and construction litter and debris out of the on-site stormwater drainage system.

Temporary Control Measures

Temporary control measures and facilities will include silt fences, construction ditches, stabilized construction access, temporary seeding, mulching and sediment traps with temporary riser and anti-vortex devices.

Throughout the construction of the proposed development, temporary control facilities will be implemented to control on-site erosion and sediment transfer. Construction ditches, if required, will be used to direct stormwater runoff to temporary sediment traps for settlement. The sediment traps will be constructed as part of this project will serve as temporary sediment basins to remove sediment and pollutants from the stormwater runoff produced during construction. Descriptions of the temporary sediment & erosion controls that will be used during the development of the site including silt fence, stabilized construction access, seeding, mulching and inlet protection are as follows:

1. Silt Fence is constructed using a geotextile fabric. The fence will be either 18 inches or 30 inches high. The height of the fence can be increased in the event of placing these devices on uncompacted fills or extremely loose undisturbed soils. The fences will not be placed in areas which receive concentrated flows such as ditches, swales and channels nor will the filter fabric material be placed across the entrance to pipes, culverts, spillway structures, sediment traps or basins.
2. Stabilized Construction Access consists of AASHTO No. 1 rock. The rock entrance will be a minimum of 50 feet in length by 24 feet in width by 8 inches in depth.

3. Seeding will be used to create a vegetative surface to stabilize disturbed earth until at least 80% of the disturbed area has a perennial vegetative cover. This amount is required to adequately function as a sediment and erosion control facility. Grass lining will also be used to line temporary channels and the surrounding disturbed areas.
4. Mulching is used as an anchor for seeding and disturbed areas to reduce soil loss due to storm events. These areas will be mulched with straw at a rate of 3 tons per acre such that the mulch forms a continuous blanket. Mulch must be placed after seeding or within 48 hours after seeding is completed.
5. Inlet Protection will be provided for all stormwater basins and inlets with the use of curb & gutter inlet protection and stone & block inlet protection structures, which will keep silt, sediment and construction debris out of the storm system. Existing structures within existing paved areas will be protected using “Manufactured Inlet Protection” inside the structures.

The contractor shall be responsible for maintaining the temporary sediment and erosion control measures throughout construction. This maintenance will include, but not be limited to, the following tasks:

1. For dust control purposes, moisten all exposed graded areas with water at least twice a day in those areas where soil is exposed and cannot be planted with a temporary cover due to construction operations or the season (December through March).
2. Inspection of erosion and sediment control measures shall be performed at the end of each construction day and immediately following each rainfall event. All required repairs shall be immediately executed by the contractor.
3. Sediment deposits shall be removed when they reach approximately $\frac{1}{3}$ the height of the silt fence. All such sediment shall be properly disposed of in fill areas on the site, as directed by the Owner’s Field Representative. Fill shall be protected following disposal with mulch,

temporary and/or permanent vegetation and be completely circumscribed on the downhill side by silt fence.

4. Rake all exposed areas parallel to the slope during earthwork operations.
5. Following final grading, the disturbed area shall be stabilized with a permanent surface treatment (i.e. turf grass, pavement or sidewalk). During rough grading, areas which are not to be disturbed for seven or more days shall be stabilized with the temporary seed mixture, as defined on the plans. Seed all piles of dirt in exposed soil areas that will not receive a permanent surface treatment.

Concrete Material and Equipment Management

Concrete washouts shall be used to contain concrete and liquids when the chutes of concrete mixers and hoppers of concrete pumps are rinsed out after delivery. The washout facilities consolidate solid for easier disposal and prevent runoff of liquids. The wash water is alkaline and contains high levels of chromium, which can leach into the ground and contaminate groundwater. It can also migrate to a storm drain, which can increase the pH of area waters and harm aquatic life. Solids that are improperly disposed of can clog storm drain pipes and cause flooding. Installing concrete washout facilities not only prevents pollution but also is a matter of good housekeeping at your construction site.

Prefabricated concrete washout containers can be delivered to the site to provide maintenance and disposal of materials. Regular pick-ups of solid and liquid waste materials will be necessary. To prevent leaks on the job site, ensure that prefabricated washout containers are watertight. A self installed concrete washout facility can be utilized although they are much less reliable than prefabricated containers and are prone to leaks. There are many design options for the washout, but they are preferably built below-grade to prevent breaches and reduce the likelihood of runoff. Above-grade structures can also be used if they are sized and constructed correctly and are diligently maintained. One of the most common problems with self-installed concrete washout facilities is that they can leak or be breached as a result of constant use,

therefore the contractor shall be sure to use quality materials and inspect the facilities on a daily basis.

Washouts must be sized to handle solids, wash water, and rainfall to prevent overflow. Concrete Washout Systems, Inc. estimates that 7 gallons of wash water are used to wash one truck chute and 50 gallons are used to wash out the hopper of a concrete pump truck.

For larger sites, a below-grade washout should be at least 10 feet wide and sized to contain all liquid and solid waste expected to be generated in between cleanout periods. A minimum of 12-inches of freeboard must be provided. The pit must be lined with plastic sheeting of at least 10-mil thickness without holes or tears to prevent leaching of liquids into the ground. Concrete wash water should never be placed in a pit that is connected to the storm drain system or that drains to nearby waterways.

An above-grade washout can be constructed at least 10 feet wide by 10 feet long and sized to contain all liquid and solid waste expected to be generated in between cleanout periods. A minimum of 4-inches of freeboard must be provided. The washout structures can be constructed with staked straw bales or sandbags double-or triple lined with plastic sheeting of at least 10-mil thickness without holes or tears.

Concrete washout facilities shall not be located within 100 feet of storm drains, open ditches, or water bodies and should be placed in locations that allow for convenient access for concrete trucks. The contractor shall check all concrete washout facilities daily to determine if they have been filled to 75 percent capacity, which is when materials need to be removed. Both above-and below-ground self-installed washouts should be inspected daily to ensure that plastic linings are intact and sidewalls have not been damaged by construction activities. Prefabricated washout containers should be inspected daily as well as to ensure the container is not leaking or nearing 75 percent capacity. Inspectors should also note whether the facilities are being used regularly. Additional signage for washouts may be needed in more convenient locations if concrete truck operators are not utilizing them.

The washout structures must be drained or covered prior to predicted rainstorms to prevent overflows. Hardened solids either whole or broken must be removed and then they may be reused onsite or hauled away for recycling.

Once materials are removed from the concrete washout, a new structure must be built or excavated, or if the previous structure is still intact, inspect it for signs of weakening or damage and make any necessary repairs. Line the structure with new plastic that is free of holes or tears and replace signage if necessary. It is very important that new plastic be used after every cleaning because pumps and concrete removal equipment can damage the existing liner.

Construction Site Chemical Control

The purpose of this management measure is to prevent the generation of nonpoint source pollution from construction sites due to improper handling and usage of nutrients and toxic substances, and to prevent the movement of toxic substances from the construction site.

Many potential pollutants other than sediment are associated with construction activities. These pollutants include pesticides; fertilizers used for vegetative stabilization; petrochemicals; construction chemicals such as concrete products, sealers, and paints; wash water associated with these products; paper; wood; garbage; and sanitary waste.

Disposal of excess pesticides and pesticide-related wastes should conform to registered label directions for the disposal and storage of pesticides and pesticide containers set forth in applicable Federal, State and local regulations that govern their usage, handling, storage, and disposal.

Pesticides should be disposed of through either a licensed waste management firm or a treatment, storage and disposal (TSD) facility. Containers should be triple-rinsed before disposal, and rinse waters should be reused as product.

Other practices include setting aside a locked storage area, tightly closing lids, storing in a cool, dry place, checking containers periodically for leaks or deterioration, maintaining a list of

products in storage, using plastic sheeting to line the storage areas, and notifying neighboring property owners prior to spraying.

When storing petroleum products, follow these guidelines:

- Create a shelter around the area with cover and wind protection;
- Line the storage area with a double layer of plastic sheeting or similar material;
- Create an impervious berm around the perimeter with a capacity of 110 percent greater than that of the largest container;
- Clearly label all products;
- Keep tanks off the ground; and
- Keep lids securely fastened.

Post spill procedure information and have persons trained in spill handling on site or on call at all times. Materials for cleaning up spills should be kept on site and easily available. Spills should be cleaned up immediately and the contaminated material properly disposed of. Maintain and wash equipment and machinery in confined areas specifically designed to control runoff.

Thinners or solvents should not be discharged into sanitary or storm systems when cleaning machinery. Use alternative methods for cleaning larger equipment parts, such as high-pressure, high-temperature water washes, or steam cleaning. Equipment-washing detergents can be used, and wash water may be discharged into sanitary sewers if solids are removed from the solution first. (This practice should be verified with the local sewer authority.) Small parts can be cleaned with degreasing solvents, which can then be reused or recycled.

Solid Waste Management and Portable Sanitary Management

The purpose of this management measure is to prevent the potential for solid waste such as construction debris, trash, etc. from construction sites due to improper handling and storage. Debris and litter should be removed periodically from the BMP's and surrounding areas to prevent clogging of pipes and structures. All construction material shall be stored in designated

staging areas. Roll-off containers shall be placed on site and all empty containers, construction debris and litter shall be placed in the containers.

Portable sanitary units may be utilized on-site or bathrooms will be provided within construction trailers. A sanitation removal company will be hired to pump/remove any sanitary waste. In the event that portable sanitary units are used and then cleaned after being emptied, the rinse water may not be disposed of to the storm drain system. It shall be contained for later disposal if it can't be disposed of on-site. Remove paper and trash before cleaning the portable sanitary units. The portable sanitary units shall be located away from the storm drain system if possible. Provide over head cover for wash areas if possible. Maintain spill response material and equipment on site to eliminate the potential for contaminants and wash water from entering the storm drain system.

Permanent Control Measures and Facilities for Long Term Protection

Towards the completion of construction, permanent sediment and erosion control measures will be developed for long term erosion protection. The following permanent control measures and facilities have been proposed to be implemented for the project:

- I. Stormwater Planters are proposed along the south side of the building to collect and filter runoff from portions of the building rooftops. Small drainage areas, less than 15,000 square feet will be collected by gutters and roof drain leaders and discharged into stormwater planters that will infiltrate the smaller storms and then discharge the higher storms through risers/standpipes directly into the underground storm pipes to the proposed stormwater management basins. Stormwater Planters act as small basins that treat stormwater as it flows through plant material and a soil matrix and is discharged to the storm drain system. These practices are elevated above the existing grade, surrounded by a concrete wall and consist of a reservoir with a depth of 12 inches, grass/landscaping with a layer of mulch, 12 inches of sandy loam topsoil and a sand/gravel layer a minimum of 24 inches wide that extends down to the native soil. Filtration through these layers will enable removal of pollutants and sediment generated by the rooftop and other small impervious areas. Refer to Appendix 'B' for the Runoff Reduction and Water Quality Volume Sizing Calculations.

2. Catch Basins will be used to remove some of the coarse sand and grit sediment before entering the drainage system. Each catch basin will be constructed with an 18 inch deep sump.
3. Rip-Rap Energy Dissipators At discharge points from the stormwater drainage system into the stormwater management basins, rip-rap pads consisting of angular rocks will be placed to dissipate velocity and reduce the risk of erosion.
4. Seeding of at least 80% perennial vegetative cover will be used to produce a permanent uniform erosion resistant surface. The seeded areas will be mulched with straw at a rate of 2 tons per acre such that the mulch forms a continuous blanket.
5. Green Roof - The proposed building will be constructed with an intensive green roof which will provide hydrologic source control and water quality volume for the rooftop runoff. The green roof must provide volume reduction equal to or greater than the required minimum RRv. This reduction is achieved when runoff is captured, routed through green infrastructure, infiltrated to the ground, reused, reduced by evapotranspiration and eventually removed from the stormwater discharge from the site. After determining the minimum RRv required, which depends on factors such as the Hydrologic Soil Group (HSG) and the amount of impervious area within the targeted drainage area, the remaining water quality volume is directed to a standard practice.
6. Subsurface Detention Systems – Two subsurface detention systems are proposed to detain and slowly release stormwater runoff using an outlet control structure.

Specifications for Soil Restoration

Prior to the final stabilization of the disturbed areas, soil restoration will be required for all vegetated areas to recover the original properties and porosity of the soil. Soil Restoration Requirements are provided on Table 7 below:

Table 7

Soil Restoration Requirements

| Type of Soil Disturbance | Soil Restoration Requirement | | Comments/Examples |
|--|--|---------------------------------------|--|
| No soil disturbance | Restoration not permitted | | Preservation of Natural Features |
| Minimal soil disturbance | Restoration not required | | Clearing and grubbing |
| Areas where topsoil is stripped only – no change in grade | HSG A&B | HSG C&D | Protect area from any ongoing construction activities |
| | apply 6 inches of topsoil | Aerate* and apply 6 inches of topsoil | |
| Areas of cut or fill | HSG A&B | HSG C&D | Clearing and grubbing |
| | Aerate and apply 6 inches of topsoil | Apply full Soil Restoration** | |
| Heavy traffic areas on site (especially) in a zone 5-25 feet around buildings but not within a 5 foot perimeter around foundation walls) | Apply full Soil Restoration (decompaction and compost enhancement) | | |
| Areas where Runoff Reduction and/or Infiltration practices are applied | Restoration not required, but may be applied to enhance the reduction specified for appropriate practices. | | Keep construction equipment from crossing these areas. To protect newly installed practice from any ongoing construction activities construct a single phase operation fence area. |
| Redevelopment projects | Soil Restoration is required on redevelopment projects in areas where existing impervious area will be converted to pervious area. | | |

* Aeration includes the use of machines such as tractor-drawn implements with coulters making a narrow slit in the soil, a roller with many spikes making indentations in the soil, or prongs which function like a mini-subsoiler.

** Per "Deep Ripping and De-compaction, DEC 2008."

During periods of relatively low to moderate subsoil moisture, the disturbed subsoils are returned to rough grade and the following full soil restoration steps applied:

1. Apply 3 inches of compost over subsoil.
2. Till compost into subsoil to a depth of at least 12 inches using a cat-mounted ripper, tractor-mounted disc, or tiller, mixing, and circulating air and compost into subsoils.
3. Rock-pick until uplifted stone/rock materials of four inches and larger size are cleaned off the site.

Specifications for Final Stabilization of Graded Areas

Final stabilization of graded areas consists of the placement of topsoil and installation of landscaping (unless the area is to be paved, or a building is to be constructed in the location). Topsoil is to be spread as soon as grading operations are completed. Topsoil is to be placed to a minimum depth of six inches on all embankments, planting areas and seeding/sod areas. The subgrade is to be scarified to a depth of two inches to provide a bond of the topsoil with the subsoil. Topsoil is to be raked to an even surface and cleared of all debris, roots, stones and other unsatisfactory material.

Planting operations shall be conducted under favorable weather conditions as follows:

- Permanent Lawns - April 15 (provided soil is frost-free and not excessively moist) to May 15; August 15 to October 15.
- Temporary Lawn Seeding - if outside of the time periods noted above, the areas shall be seeded immediately on completion of topsoil operations with annual ryegrass (Italian rye) at a rate of six pounds per 1,000 square feet. Temporary lawn installation is permitted provided the soil is frost-free and not excessively moist. The permanent lawn is to be installed the next planting season.

On slopes with a grade of 3 horizontal to 1 vertical or greater, and in swales, a geotextile netting or mat shall be installed for stabilization purposes as shown on the Plans. Seeded areas are to be mulched with straw or hay at an application rate of 70-90 pounds per 1,000 s.f. Straw or hay mulch must be spread uniformly and anchored immediately after spreading to prevent wind blowing. Mulches must be inspected periodically and in particular after rainstorms to check for erosion. If erosion is observed, additional mulch must be applied. Netting shall be inspected after rainstorms for dislocation or failure; any damage shall be repaired immediately.

All denuded surfaces which will be exposed for a period of over two months or more shall be temporarily hydroseeded with (a) perennial ryegrass at a rate of 40 lbs per acre (1.0 lb per 1000 square feet); (b) Certified "Aroostook" winter rye (cereal rye) @ 100 lb per acre (2.5 lb/1000 s.f.) to be used in the months of October and November.

Permanent turfgrass cover is to consist of a seed mixture as follows:

(a) Sunny sites

| | |
|--------------------|---------------------------------|
| Kentucky Bluegrass | 2.0-2.6 pounds/1000 square feet |
| Perennial Ryegrass | 0.6-0.7 pounds/1000 square feet |
| Fine Fescue | 0.4-0.6 pounds/1000 square feet |

(b) Shady sites

| | |
|--------------------|---------------------------------|
| Kentucky Bluegrass | 0.8-1.0 pounds/1000 square feet |
| Perennial Ryegrass | 0.6-0.7 pounds/1000 square feet |
| Fine Fescue | 2.6-3.3 pounds/1000 square feet |

All plant materials shall comply with the standards of the American Association Of Nurserymen with respect to height and caliper as described in its publication American Standard for Nursery Stock, latest edition.

VII. CONSTRUCTION PHASE AND POST-CONSTRUCTION MAINTENANCE

During the construction phase and following construction of the project, a number of maintenance measures will be taken with respect to the site maintenance. Measures to be taken included the following:

I. During Construction

A comprehensive sediment and erosion control plan will be in place during the construction period. Maintenance measures for sediment and erosion controls will include:

A qualified professional acceptable to the municipality will be hired by the owner or operator to monitor the installation and maintenance of the sediment and erosion control plans. The qualified professional shall report directly to the Engineering Consultant and shall be responsible for ensuring compliance with the design of the sediment and erosion control plans.

The qualified professional so hired will inspect all sediment and erosion control measures at least every seven calendar days. In the event that there has been a variance with the design of the sediment and erosion control measures so that the ability of the measures to adequately perform the intended function is lessened or compromised and/or the facilities are not adequately maintained, the qualified professional shall be required to report such variance to the Engineering Consultant within 48 hours and shall be empowered to order immediate repairs to the sediment and erosion control measures.

The qualified professional will also be responsible for observing the adequacy of the vegetation growth (trees, shrubs, groundcovers and turfgrasses) in newly graded areas and for ordering additional plantings in the event that the established plant materials do not adequately protect the ground surface from erosion.

2. Following Construction

Site maintenance activities on the property will include:

- Grounds maintenance, including mowing of lawns;
- Planting of trees, shrubs and groundcovers; pruning of trees and shrubs;
- Application of fertilizer and herbicides;
- Maintenance of stormwater management area;

Grounds maintenance on the site will be performed by landscaping contractor.

Fertilizer is typically applied twice in the year - once in the spring and once in the fall. The application of fertilizer is usually necessary to maintain healthy lawn growth due to competition for nutrients with trees and shrubs and since the clippings are often removed. It is not recommended that fertilizer be applied during the summer. It is at this time that lawns are typically dormant.

Fertilizers come in three basic types: (1) Organic; (2) Soluble synthetic and (3) Slow release.

Organic fertilizers are derived from plant or animal waste. Since they are heavier and bulkier than other fertilizers, it is necessary to apply a much greater amount at one time. Soluble synthetic fertilizers are predictable with determining the exact impact on a lawn. However more applications are necessary since their effect is often short term. Slow release fertilizers have a high percentage of nitrogen so quantities that need be handled at one time are smaller. Slow release fertilizers will be utilized by the project.

A complete fertilizer contains all three of the primary nutrients - nitrogen (N), phosphorus (P) and potassium in the form of potash (K). Typically, a 3-1-2 ratio of nutrients (N-P-K) is used for lawn applications.

Fertilizer shall be applied by the landscape contractor in accordance with the manufacturer's instructions. The application of fertilizer does require some skill on the part of the operator. Should there be a spill of fertilizer, the landscape contractor shall be required to scrape or

vacuum it up. The area will then be watered in accordance with the manufacturer's instructions to ensure that the fertilizer becomes soluble and available to plants and does not run off.

Buchanan Dev AMS LLC will be responsible for the long-term operation and maintenance of the permanent stormwater management practices. The permanent stormwater management practices shall be maintained in accordance with the Maintenance Inspection Checklists provided in Appendix D.

VIII. CONCLUSION

This Stormwater Pollution Prevention Plan has been prepared to describe the project's pre and post-development stormwater management improvements and its sediment and erosion control improvements to be utilized during construction. The proposed permanent improvements and the interim improvements to be utilized during construction have been designed in accordance with the requirements of the:

- New York State Department of Environmental Conservation (NYSDEC) SPDES General Permit No. GP-0-20-001, effective January 29, 2020.
- Chapter 166 "Stormwater Management" of the Village of Buchanan Zoning Code
- New York State Stormwater Management Design Manual.

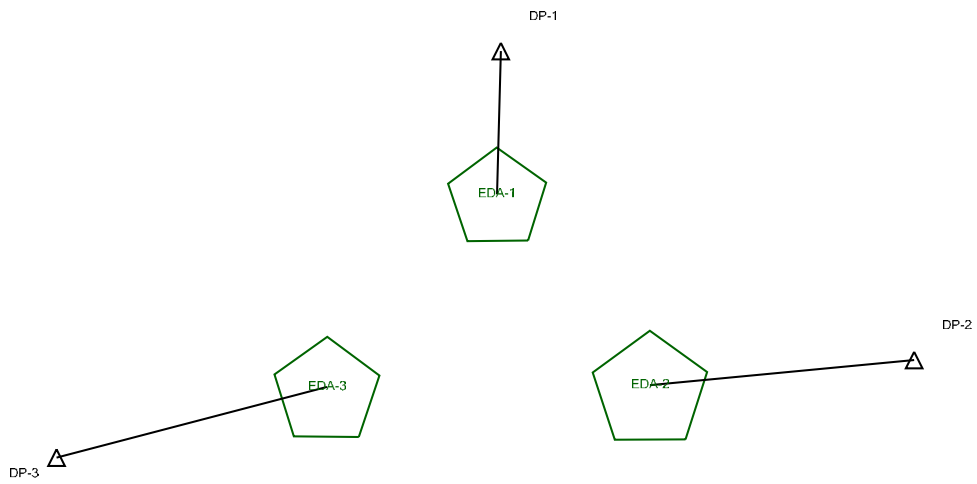
The project employs a variety of practices to enhance stormwater quality and reduce peak rates of runoff associated with the proposed building and parking improvements. These measures include green roofs, stormwater planters, JellyFish filter, and subsurface detention systems. These improvements will also mitigate runoff volumes from the proposed improvements as runoff volumes will be slightly reduced or maintained in all the analyzed storms.

Based on the foregoing, it is our professional opinion that the proposed improvements will provide water quantity and quality enhancements which exceed the above mentioned requirements and are not anticipated to have any adverse impacts to the site or any surrounding areas.

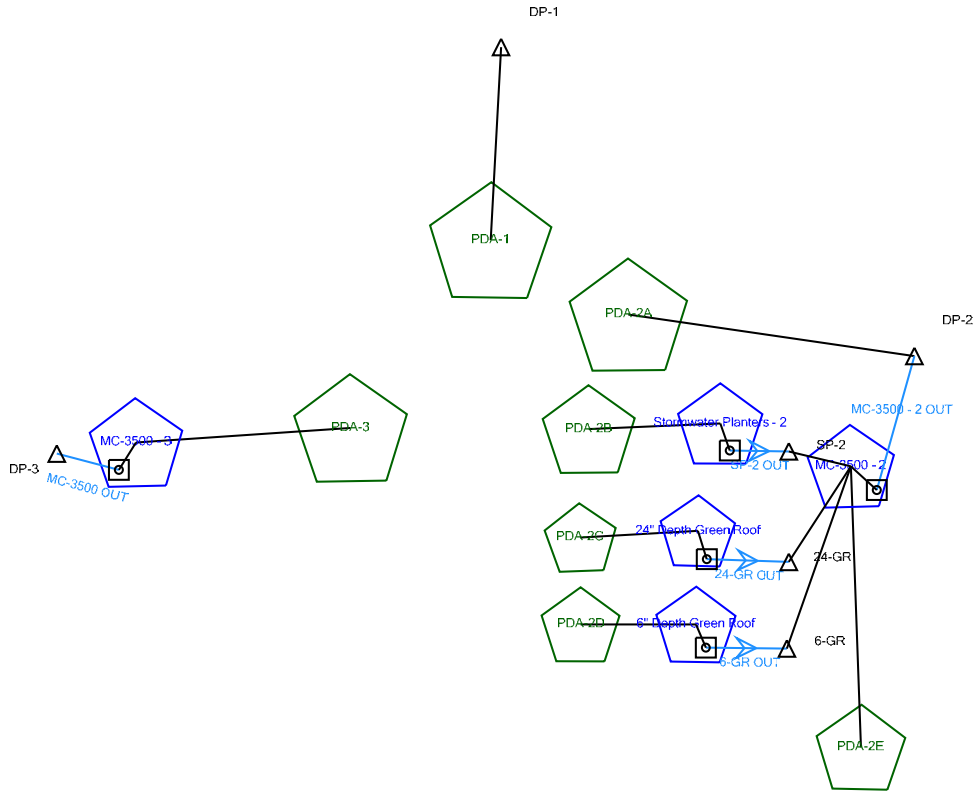
APPENDIX A

***EXISTING & PROPOSED HYDROLOGIC
CALCULATIONS***

Scenario: Pre-Development 1 year



Scenario: Post-Development 1 year



Existing and Proposed Hydrologic Calculations

Project Summary

| | |
|----------|-------------------------|
| Title | AMS Buchanan |
| Engineer | Michael Thompson, PE |
| Company | JMC, PLLC |
| Date | 11/8/2023 |

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Existing and Proposed Hydrologic Calculations

Subsection: Master Network Summary

Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|--------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|
| EDA-1 | Pre-Development 1 year | 1 | 1,699 | 12.150 | 0.43 |
| EDA-1 | Pre-Development 10 year | 10 | 5,072 | 12.150 | 1.33 |
| EDA-1 | Pre-Development 25 year | 25 | 7,291 | 12.150 | 1.90 |
| EDA-1 | Pre-Development 100 year | 100 | 12,096 | 12.150 | 3.08 |
| EDA-3 | Pre-Development 1 year | 1 | 13,836 | 12.450 | 2.27 |
| EDA-3 | Pre-Development 10 year | 10 | 40,363 | 12.400 | 6.86 |
| EDA-3 | Pre-Development 25 year | 25 | 57,674 | 12.400 | 9.79 |
| EDA-3 | Pre-Development 100 year | 100 | 95,023 | 12.400 | 15.93 |
| EDA-2 | Pre-Development 1 year | 1 | 5,442 | 12.350 | 0.99 |
| EDA-2 | Pre-Development 10 year | 10 | 15,146 | 12.350 | 2.82 |
| EDA-2 | Pre-Development 25 year | 25 | 21,378 | 12.350 | 3.96 |
| EDA-2 | Pre-Development 100 year | 100 | 34,717 | 12.300 | 6.33 |
| PDA-1 | Post-Development 1 year | 1 | 808 | 12.150 | 0.21 |
| PDA-1 | Post-Development 10 year | 10 | 2,413 | 12.150 | 0.63 |
| PDA-1 | Post-Development 25 year | 25 | 3,468 | 12.150 | 0.90 |
| PDA-1 | Post-Development 100 year | 100 | 5,754 | 12.150 | 1.47 |
| PDA-2A | Post-Development 1 year | 1 | 4,040 | 12.300 | 0.81 |
| PDA-2A | Post-Development 10 year | 10 | 10,989 | 12.250 | 2.24 |
| PDA-2A | Post-Development 25 year | 25 | 15,418 | 12.250 | 3.13 |
| PDA-2A | Post-Development 100 year | 100 | 24,861 | 12.250 | 4.97 |
| PDA-3 | Post-Development 1 year | 1 | 19,897 | 12.150 | 5.21 |
| PDA-3 | Post-Development 10 year | 10 | 47,606 | 12.150 | 12.08 |
| PDA-3 | Post-Development 25 year | 25 | 64,556 | 12.100 | 16.18 |

Existing and Proposed Hydrologic Calculations

Subsection: Master Network Summary

Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|--------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|
| PDA-3 | Post-Development 100 year | 100 | 100,006 | 12.100 | 24.51 |
| PDA-2B | Post-Development 1 year | 1 | 3,907 | 12.100 | 0.97 |
| PDA-2B | Post-Development 10 year | 10 | 7,510 | 12.100 | 1.81 |
| PDA-2B | Post-Development 25 year | 25 | 9,617 | 12.100 | 2.30 |
| PDA-2B | Post-Development 100 year | 100 | 13,940 | 12.100 | 3.30 |
| PDA-2C | Post-Development 1 year | 1 | 3,814 | 12.100 | 0.94 |
| PDA-2C | Post-Development 10 year | 10 | 7,332 | 12.100 | 1.76 |
| PDA-2C | Post-Development 25 year | 25 | 9,388 | 12.100 | 2.24 |
| PDA-2C | Post-Development 100 year | 100 | 13,610 | 12.100 | 3.22 |
| PDA-2D | Post-Development 1 year | 1 | 1,605 | 12.100 | 0.40 |
| PDA-2D | Post-Development 10 year | 10 | 3,085 | 12.100 | 0.74 |
| PDA-2D | Post-Development 25 year | 25 | 3,951 | 12.100 | 0.94 |
| PDA-2D | Post-Development 100 year | 100 | 5,727 | 12.100 | 1.35 |
| PDA-2E | Post-Development 1 year | 1 | 305 | 12.150 | 0.08 |
| PDA-2E | Post-Development 10 year | 10 | 909 | 12.100 | 0.24 |
| PDA-2E | Post-Development 25 year | 25 | 1,306 | 12.100 | 0.35 |
| PDA-2E | Post-Development 100 year | 100 | 2,167 | 12.100 | 0.57 |

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|-------|-------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|
| DP-1 | Pre-Development 1 year | 1 | 1,699 | 12.150 | 0.43 |
| DP-1 | Post-Development 1 year | 1 | 808 | 12.150 | 0.21 |
| DP-1 | Pre-Development 10 year | 10 | 5,072 | 12.150 | 1.33 |

Existing and Proposed Hydrologic Calculations

Subsection: Master Network Summary

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) |
|-------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|
| DP-1 | Post-Development 10 year | 10 | 2,413 | 12.150 | 0.63 |
| DP-1 | Pre-Development 25 year | 25 | 7,291 | 12.150 | 1.90 |
| DP-1 | Post-Development 25 year | 25 | 3,468 | 12.150 | 0.90 |
| DP-1 | Pre-Development 100 year | 100 | 12,096 | 12.150 | 3.08 |
| DP-1 | Post-Development 100 year | 100 | 5,754 | 12.150 | 1.47 |
| DP-3 | Pre-Development 1 year | 1 | 13,836 | 12.450 | 2.27 |
| DP-3 | Post-Development 1 year | 1 | 19,594 | 12.450 | 2.00 |
| DP-3 | Pre-Development 10 year | 10 | 40,363 | 12.400 | 6.86 |
| DP-3 | Post-Development 10 year | 10 | 46,990 | 12.400 | 5.48 |
| DP-3 | Pre-Development 25 year | 25 | 57,674 | 12.400 | 9.79 |
| DP-3 | Post-Development 25 year | 25 | 63,759 | 12.350 | 8.01 |
| DP-3 | Pre-Development 100 year | 100 | 95,023 | 12.400 | 15.93 |
| DP-3 | Post-Development 100 year | 100 | 98,845 | 12.300 | 15.14 |
| DP-2 | Pre-Development 1 year | 1 | 5,442 | 12.350 | 0.99 |
| DP-2 | Post-Development 1 year | 1 | 13,437 | 12.300 | 0.99 |
| DP-2 | Pre-Development 10 year | 10 | 15,146 | 12.350 | 2.82 |
| DP-2 | Post-Development 10 year | 10 | 27,448 | 12.250 | 2.49 |
| DP-2 | Pre-Development 25 year | 25 | 21,378 | 12.350 | 3.96 |
| DP-2 | Post-Development 25 year | 25 | 36,524 | 12.250 | 3.62 |
| DP-2 | Pre-Development 100 year | 100 | 34,717 | 12.300 | 6.33 |
| DP-2 | Post-Development 100 year | 100 | 55,900 | 12.250 | 5.97 |

Pond Summary

Existing and Proposed Hydrologic Calculations

Subsection: Master Network Summary

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ft ³) |
|-------------------------------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|--------------------------------------|---|
| Stormwater Planters - 2 (IN) | Post-Development 1 year | 1 | 3,907 | 12.100 | 0.97 | (N/A) | (N/A) |
| Stormwater Planters - 2 (OUT) | Post-Development 1 year | 1 | 3,912 | 11.600 | 0.14 | 79.20 | 1,189 |
| Stormwater Planters - 2 (IN) | Post-Development 10 year | 10 | 7,510 | 12.100 | 1.81 | (N/A) | (N/A) |
| Stormwater Planters - 2 (OUT) | Post-Development 10 year | 10 | 7,515 | 10.850 | 0.14 | 79.77 | 2,931 |
| Stormwater Planters - 2 (IN) | Post-Development 25 year | 25 | 9,617 | 12.100 | 2.30 | (N/A) | (N/A) |
| Stormwater Planters - 2 (OUT) | Post-Development 25 year | 25 | 9,621 | 12.450 | 0.70 | 79.90 | 3,336 |
| Stormwater Planters - 2 (IN) | Post-Development 100 year | 100 | 13,940 | 12.100 | 3.30 | (N/A) | (N/A) |
| Stormwater Planters - 2 (OUT) | Post-Development 100 year | 100 | 13,345 | 12.200 | 2.47 | 80.06 | 3,800 |
| 24" Depth Green Roof (IN) | Post-Development 1 year | 1 | 3,814 | 12.100 | 0.94 | (N/A) | (N/A) |
| 24" Depth Green Roof (OUT) | Post-Development 1 year | 1 | 3,817 | 11.250 | 0.09 | 94.46 | 1,398 |
| 24" Depth Green Roof (IN) | Post-Development 10 year | 10 | 7,332 | 12.100 | 1.76 | (N/A) | (N/A) |
| 24" Depth Green Roof (OUT) | Post-Development 10 year | 10 | 6,928 | 12.200 | 1.34 | 95.24 | 2,253 |
| 24" Depth Green Roof (IN) | Post-Development 25 year | 25 | 9,388 | 12.100 | 2.24 | (N/A) | (N/A) |
| 24" Depth Green Roof (OUT) | Post-Development 25 year | 25 | 8,686 | 12.100 | 2.71 | 95.27 | 2,322 |
| 24" Depth Green Roof (IN) | Post-Development 100 year | 100 | 13,610 | 12.100 | 3.22 | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Master Network Summary

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ft ³) |
|----------------------------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|--------------------------------------|---|
| 24" Depth Green Roof (OUT) | Post-Development 100 year | 100 | 12,417 | 12.100 | 3.20 | 95.29 | 2,346 |
| 6" Depth Green Roof (IN) | Post-Development 1 year | 1 | 1,605 | 12.100 | 0.40 | (N/A) | (N/A) |
| 6" Depth Green Roof (OUT) | Post-Development 1 year | 1 | 1,610 | 11.800 | 0.13 | 93.29 | 282 |
| 6" Depth Green Roof (IN) | Post-Development 10 year | 10 | 3,085 | 12.100 | 0.74 | (N/A) | (N/A) |
| 6" Depth Green Roof (OUT) | Post-Development 10 year | 10 | 3,090 | 11.650 | 0.13 | 93.68 | 819 |
| 6" Depth Green Roof (IN) | Post-Development 25 year | 25 | 3,951 | 12.100 | 0.94 | (N/A) | (N/A) |
| 6" Depth Green Roof (OUT) | Post-Development 25 year | 25 | 3,955 | 12.250 | 0.53 | 93.72 | 950 |
| 6" Depth Green Roof (IN) | Post-Development 100 year | 100 | 5,727 | 12.100 | 1.35 | (N/A) | (N/A) |
| 6" Depth Green Roof (OUT) | Post-Development 100 year | 100 | 5,731 | 12.150 | 1.27 | 93.75 | 1,017 |
| MC-3500 - 3 (IN) | Post-Development 1 year | 1 | 19,897 | 12.150 | 5.21 | (N/A) | (N/A) |
| MC-3500 - 3 (OUT) | Post-Development 1 year | 1 | 19,594 | 12.450 | 2.00 | 64.50 | 6,135 |
| MC-3500 - 3 (IN) | Post-Development 10 year | 10 | 47,606 | 12.150 | 12.08 | (N/A) | (N/A) |
| MC-3500 - 3 (OUT) | Post-Development 10 year | 10 | 46,990 | 12.400 | 5.48 | 65.76 | 13,858 |
| MC-3500 - 3 (IN) | Post-Development 25 year | 25 | 64,556 | 12.100 | 16.18 | (N/A) | (N/A) |
| MC-3500 - 3 (OUT) | Post-Development 25 year | 25 | 63,759 | 12.350 | 8.01 | 66.49 | 17,897 |

Existing and Proposed Hydrologic Calculations

Subsection: Master Network Summary

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ft ³) | Time to Peak (hours) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ft ³) |
|-------------------|---------------------------|----------------------|--------------------------------------|----------------------|--------------------------------|--------------------------------------|---|
| MC-3500 - 3 (IN) | Post-Development 100 year | 100 | 100,006 | 12.100 | 24.51 | (N/A) | (N/A) |
| MC-3500 - 3 (OUT) | Post-Development 100 year | 100 | 98,845 | 12.300 | 15.14 | 68.23 | 24,465 |
| MC-3500 - 2 (IN) | Post-Development 1 year | 1 | 9,644 | 12.150 | 0.44 | (N/A) | (N/A) |
| MC-3500 - 2 (OUT) | Post-Development 1 year | 1 | 9,398 | 16.500 | 0.23 | 72.74 | 2,429 |
| MC-3500 - 2 (IN) | Post-Development 10 year | 10 | 18,443 | 12.200 | 1.81 | (N/A) | (N/A) |
| MC-3500 - 2 (OUT) | Post-Development 10 year | 10 | 16,459 | 13.550 | 0.42 | 73.13 | 3,552 |
| MC-3500 - 2 (IN) | Post-Development 25 year | 25 | 23,569 | 12.100 | 3.33 | (N/A) | (N/A) |
| MC-3500 - 2 (OUT) | Post-Development 25 year | 25 | 21,106 | 12.900 | 0.73 | 73.86 | 5,580 |
| MC-3500 - 2 (IN) | Post-Development 100 year | 100 | 33,660 | 12.150 | 7.23 | (N/A) | (N/A) |
| MC-3500 - 2 (OUT) | Post-Development 100 year | 100 | 31,039 | 12.700 | 1.28 | 76.44 | 10,803 |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 1 years

Label: Time-Depth - 1

Storm Event: 1 year

Scenario: Pre-Development 1 year

Time-Depth Curve: 1 year

| | |
|--------------|--------------|
| Label | 1 year |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 1 years |

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|-----------------|---------------|---------------|---------------|---------------|---------------|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 3.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 3.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 4.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 4.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 5.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 5.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 6.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 6.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 7.000 | 0.2 | 0.3 | 0.3 | 0.3 | 0.3 |
| 7.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 8.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 8.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 9.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 9.500 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 10.000 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 |
| 10.500 | 0.6 | 0.6 | 0.6 | 0.6 | 0.7 |
| 11.000 | 0.7 | 0.7 | 0.7 | 0.8 | 0.8 |
| 11.500 | 0.8 | 0.9 | 0.9 | 1.0 | 1.1 |
| 12.000 | 1.4 | 1.6 | 1.7 | 1.8 | 1.9 |
| 12.500 | 1.9 | 2.0 | 2.0 | 2.0 | 2.0 |
| 13.000 | 2.1 | 2.1 | 2.1 | 2.1 | 2.1 |
| 13.500 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| 14.000 | 2.2 | 2.2 | 2.3 | 2.3 | 2.3 |
| 14.500 | 2.3 | 2.3 | 2.3 | 2.3 | 2.3 |
| 15.000 | 2.3 | 2.4 | 2.4 | 2.4 | 2.4 |
| 15.500 | 2.4 | 2.4 | 2.4 | 2.4 | 2.4 |
| 16.000 | 2.4 | 2.4 | 2.5 | 2.5 | 2.5 |
| 16.500 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 1 years

Label: Time-Depth - 1

Storm Event: 1 year

Scenario: Pre-Development 1 year

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|--------------|------------|------------|------------|------------|------------|
| 17.000 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |
| 17.500 | 2.5 | 2.5 | 2.5 | 2.5 | 2.5 |
| 18.000 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 |
| 18.500 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 |
| 19.000 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 |
| 19.500 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 |
| 20.000 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 |
| 20.500 | 2.6 | 2.7 | 2.7 | 2.7 | 2.7 |
| 21.000 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| 21.500 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| 22.000 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| 22.500 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| 23.000 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| 23.500 | 2.7 | 2.7 | 2.7 | 2.7 | 2.7 |
| 24.000 | 2.8 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 10 years

Label: Time-Depth - 1

Storm Event: 10 year

Scenario: Pre-Development 10 year

Time-Depth Curve: 10 year

| | |
|--------------|--------------|
| Label | 10 year |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 10 years |

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|-----------------|---------------|---------------|---------------|---------------|---------------|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 3.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 4.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 4.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 5.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 5.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 |
| 6.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 6.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 7.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 7.500 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 |
| 8.000 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 8.500 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 |
| 9.000 | 0.7 | 0.8 | 0.8 | 0.8 | 0.8 |
| 9.500 | 0.8 | 0.9 | 0.9 | 0.9 | 0.9 |
| 10.000 | 1.0 | 1.0 | 1.0 | 1.0 | 1.1 |
| 10.500 | 1.1 | 1.1 | 1.2 | 1.2 | 1.2 |
| 11.000 | 1.3 | 1.3 | 1.4 | 1.4 | 1.5 |
| 11.500 | 1.5 | 1.6 | 1.7 | 1.9 | 2.1 |
| 12.000 | 2.5 | 3.0 | 3.2 | 3.4 | 3.5 |
| 12.500 | 3.6 | 3.6 | 3.7 | 3.7 | 3.8 |
| 13.000 | 3.8 | 3.8 | 3.9 | 3.9 | 3.9 |
| 13.500 | 4.0 | 4.0 | 4.0 | 4.1 | 4.1 |
| 14.000 | 4.1 | 4.1 | 4.2 | 4.2 | 4.2 |
| 14.500 | 4.2 | 4.3 | 4.3 | 4.3 | 4.3 |
| 15.000 | 4.3 | 4.4 | 4.4 | 4.4 | 4.4 |
| 15.500 | 4.4 | 4.4 | 4.5 | 4.5 | 4.5 |
| 16.000 | 4.5 | 4.5 | 4.5 | 4.5 | 4.6 |
| 16.500 | 4.6 | 4.6 | 4.6 | 4.6 | 4.6 |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 10 years

Label: Time-Depth - 1

Storm Event: 10 year

Scenario: Pre-Development 10 year

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|--------------|------------|------------|------------|------------|------------|
| 17.000 | 4.6 | 4.6 | 4.6 | 4.7 | 4.7 |
| 17.500 | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| 18.000 | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| 18.500 | 4.8 | 4.8 | 4.8 | 4.8 | 4.8 |
| 19.000 | 4.8 | 4.8 | 4.8 | 4.8 | 4.8 |
| 19.500 | 4.8 | 4.8 | 4.8 | 4.8 | 4.9 |
| 20.000 | 4.9 | 4.9 | 4.9 | 4.9 | 4.9 |
| 20.500 | 4.9 | 4.9 | 4.9 | 4.9 | 4.9 |
| 21.000 | 4.9 | 4.9 | 4.9 | 4.9 | 4.9 |
| 21.500 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 22.000 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 22.500 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 23.000 | 5.0 | 5.0 | 5.0 | 5.0 | 5.1 |
| 23.500 | 5.1 | 5.1 | 5.1 | 5.1 | 5.1 |
| 24.000 | 5.1 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 100 years

Label: Time-Depth - 1

Storm Event: 100 year

Scenario: Pre-Development 100 year

Time-Depth Curve: 100 year

| | |
|--------------|--------------|
| Label | 100 year |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 100 years |

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|-----------------|---------------|---------------|---------------|---------------|---------------|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.2 | 0.2 | 0.2 |
| 2.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 |
| 3.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 3.500 | 0.3 | 0.4 | 0.4 | 0.4 | 0.4 |
| 4.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 4.500 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 5.000 | 0.5 | 0.5 | 0.6 | 0.6 | 0.6 |
| 5.500 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 6.000 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 |
| 6.500 | 0.7 | 0.8 | 0.8 | 0.8 | 0.8 |
| 7.000 | 0.8 | 0.9 | 0.9 | 0.9 | 0.9 |
| 7.500 | 0.9 | 1.0 | 1.0 | 1.0 | 1.0 |
| 8.000 | 1.1 | 1.1 | 1.1 | 1.1 | 1.2 |
| 8.500 | 1.2 | 1.2 | 1.2 | 1.3 | 1.3 |
| 9.000 | 1.3 | 1.4 | 1.4 | 1.5 | 1.5 |
| 9.500 | 1.5 | 1.6 | 1.6 | 1.7 | 1.7 |
| 10.000 | 1.7 | 1.8 | 1.8 | 1.9 | 1.9 |
| 10.500 | 2.0 | 2.1 | 2.1 | 2.2 | 2.2 |
| 11.000 | 2.3 | 2.4 | 2.5 | 2.5 | 2.6 |
| 11.500 | 2.8 | 2.9 | 3.1 | 3.4 | 3.8 |
| 12.000 | 4.6 | 5.4 | 5.8 | 6.1 | 6.3 |
| 12.500 | 6.5 | 6.6 | 6.7 | 6.8 | 6.9 |
| 13.000 | 6.9 | 7.0 | 7.1 | 7.1 | 7.2 |
| 13.500 | 7.2 | 7.3 | 7.3 | 7.4 | 7.4 |
| 14.000 | 7.5 | 7.5 | 7.6 | 7.6 | 7.7 |
| 14.500 | 7.7 | 7.7 | 7.8 | 7.8 | 7.8 |
| 15.000 | 7.9 | 7.9 | 8.0 | 8.0 | 8.0 |
| 15.500 | 8.0 | 8.1 | 8.1 | 8.1 | 8.2 |
| 16.000 | 8.2 | 8.2 | 8.2 | 8.2 | 8.3 |
| 16.500 | 8.3 | 8.3 | 8.3 | 8.4 | 8.4 |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 100 years

Label: Time-Depth - 1

Storm Event: 100 year

Scenario: Pre-Development 100 year

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|--------------|------------|------------|------------|------------|------------|
| 17.000 | 8.4 | 8.4 | 8.4 | 8.5 | 8.5 |
| 17.500 | 8.5 | 8.5 | 8.5 | 8.5 | 8.6 |
| 18.000 | 8.6 | 8.6 | 8.6 | 8.6 | 8.6 |
| 18.500 | 8.6 | 8.7 | 8.7 | 8.7 | 8.7 |
| 19.000 | 8.7 | 8.7 | 8.7 | 8.7 | 8.8 |
| 19.500 | 8.8 | 8.8 | 8.8 | 8.8 | 8.8 |
| 20.000 | 8.8 | 8.8 | 8.9 | 8.9 | 8.9 |
| 20.500 | 8.9 | 8.9 | 8.9 | 8.9 | 8.9 |
| 21.000 | 8.9 | 9.0 | 9.0 | 9.0 | 9.0 |
| 21.500 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 |
| 22.000 | 9.1 | 9.1 | 9.1 | 9.1 | 9.1 |
| 22.500 | 9.1 | 9.1 | 9.1 | 9.1 | 9.1 |
| 23.000 | 9.1 | 9.2 | 9.2 | 9.2 | 9.2 |
| 23.500 | 9.2 | 9.2 | 9.2 | 9.2 | 9.2 |
| 24.000 | 9.2 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 25 years

Label: Time-Depth - 1

Storm Event: 25 year

Scenario: Pre-Development 25 year

Time-Depth Curve: 25 year

| | |
|--------------|--------------|
| Label | 25 year |
| Start Time | 0.000 hours |
| Increment | 0.100 hours |
| End Time | 24.000 hours |
| Return Event | 25 years |

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|-----------------|---------------|---------------|---------------|---------------|---------------|
| 0.000 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.500 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 |
| 1.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 1.500 | 0.1 | 0.1 | 0.1 | 0.1 | 0.1 |
| 2.000 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 |
| 2.500 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.000 | 0.2 | 0.2 | 0.2 | 0.2 | 0.2 |
| 3.500 | 0.2 | 0.2 | 0.3 | 0.3 | 0.3 |
| 4.000 | 0.3 | 0.3 | 0.3 | 0.3 | 0.3 |
| 4.500 | 0.3 | 0.3 | 0.3 | 0.3 | 0.4 |
| 5.000 | 0.4 | 0.4 | 0.4 | 0.4 | 0.4 |
| 5.500 | 0.4 | 0.4 | 0.4 | 0.4 | 0.5 |
| 6.000 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| 6.500 | 0.5 | 0.5 | 0.5 | 0.6 | 0.6 |
| 7.000 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 |
| 7.500 | 0.7 | 0.7 | 0.7 | 0.7 | 0.7 |
| 8.000 | 0.7 | 0.8 | 0.8 | 0.8 | 0.8 |
| 8.500 | 0.8 | 0.8 | 0.9 | 0.9 | 0.9 |
| 9.000 | 0.9 | 1.0 | 1.0 | 1.0 | 1.0 |
| 9.500 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 |
| 10.000 | 1.2 | 1.2 | 1.3 | 1.3 | 1.4 |
| 10.500 | 1.4 | 1.4 | 1.5 | 1.5 | 1.6 |
| 11.000 | 1.6 | 1.7 | 1.7 | 1.8 | 1.8 |
| 11.500 | 1.9 | 2.0 | 2.2 | 2.4 | 2.7 |
| 12.000 | 3.2 | 3.8 | 4.0 | 4.3 | 4.4 |
| 12.500 | 4.5 | 4.6 | 4.7 | 4.7 | 4.8 |
| 13.000 | 4.8 | 4.9 | 4.9 | 5.0 | 5.0 |
| 13.500 | 5.0 | 5.1 | 5.1 | 5.2 | 5.2 |
| 14.000 | 5.2 | 5.3 | 5.3 | 5.3 | 5.3 |
| 14.500 | 5.4 | 5.4 | 5.4 | 5.5 | 5.5 |
| 15.000 | 5.5 | 5.5 | 5.5 | 5.6 | 5.6 |
| 15.500 | 5.6 | 5.6 | 5.7 | 5.7 | 5.7 |
| 16.000 | 5.7 | 5.7 | 5.7 | 5.8 | 5.8 |
| 16.500 | 5.8 | 5.8 | 5.8 | 5.8 | 5.8 |

Existing and Proposed Hydrologic Calculations

Subsection: Time-Depth Curve

Return Event: 25 years

Label: Time-Depth - 1

Storm Event: 25 year

Scenario: Pre-Development 25 year

CUMULATIVE RAINFALL (in)

Output Time Increment = 0.100 hours

Time on left represents time for first value in each row.

| Time (hours) | Depth (in) | Depth (in) | Depth (in) | Depth (in) | Depth (in) |
|--------------|------------|------------|------------|------------|------------|
| 17.000 | 5.9 | 5.9 | 5.9 | 5.9 | 5.9 |
| 17.500 | 5.9 | 5.9 | 5.9 | 6.0 | 6.0 |
| 18.000 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 18.500 | 6.0 | 6.0 | 6.0 | 6.1 | 6.1 |
| 19.000 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 |
| 19.500 | 6.1 | 6.1 | 6.1 | 6.1 | 6.2 |
| 20.000 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 |
| 20.500 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 |
| 21.000 | 6.2 | 6.3 | 6.3 | 6.3 | 6.3 |
| 21.500 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |
| 22.000 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |
| 22.500 | 6.3 | 6.4 | 6.4 | 6.4 | 6.4 |
| 23.000 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |
| 23.500 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 |
| 24.000 | 6.4 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: EDA-1

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.160 ft/ft |
| 2 Year 24 Hour Depth | 3.4 in |
| Average Velocity | 0.18 ft/s |
| Segment Time of Concentration | 0.152 hours |

Segment #2: TR-55 Shallow Concentrated Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 55.00 ft |
| Is Paved? | False |
| Slope | 0.018 ft/ft |
| Average Velocity | 2.16 ft/s |
| Segment Time of Concentration | 0.007 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.159 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: EDA-1

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

Where:

$$(L_f / V) / 3600$$

R= Hydraulic radius
A_q= Flow area, square feet
W_p= Wetted perimeter, feet
V= Velocity, ft/sec
S_f= Slope, ft/ft
n= Manning's n
T_c= Time of concentration, hours
L_f= Flow length, feet

==== SCS TR-55 Shallow Concentration Flow

$$T_c = \frac{\text{Unpaved surface:}}{V = 16.1345 * (S_f^{0.5})}$$

$$\text{Paved Surface:}$$
$$V = 20.3282 * (S_f^{0.5})$$

Where:

$$(L_f / V) / 3600$$

V= Velocity, ft/sec
S_f= Slope, ft/ft
T_c= Time of concentration, hours
L_f= Flow length, feet

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: EDA-2

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.010 ft/ft |
| 2 Year 24 Hour Depth | 3.4 in |
| Average Velocity | 0.06 ft/s |
| Segment Time of Concentration | 0.458 hours |

Segment #2: TR-55 Shallow Concentrated Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Is Paved? | False |
| Slope | 0.065 ft/ft |
| Average Velocity | 4.11 ft/s |
| Segment Time of Concentration | 0.007 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.465 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: EDA-2

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

$$\text{Where: } (L_f / V) / 3600$$

R= Hydraulic radius
Aq= Flow area, square feet
Wp= Wetted perimeter, feet
V= Velocity, ft/sec
Sf= Slope, ft/ft
n= Manning's n
Tc= Time of concentration, hours
Lf= Flow length, feet

==== SCS TR-55 Shallow Concentration Flow

$$T_c = \frac{\text{Unpaved surface:}}{V = 16.1345 * (S_f^{0.5})}$$

$$\text{Paved Surface:}$$
$$V = 20.3282 * (S_f^{0.5})$$

$$\text{Where: } (L_f / V) / 3600$$

V= Velocity, ft/sec
Sf= Slope, ft/ft
Tc= Time of concentration, hours
Lf= Flow length, feet

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: EDA-3

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.007 ft/ft |
| 2 Year 24 Hour Depth | 3.4 in |
| Average Velocity | 0.05 ft/s |
| Segment Time of Concentration | 0.528 hours |

Segment #2: TR-55 Shallow Concentrated Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 419.00 ft |
| Is Paved? | False |
| Slope | 0.027 ft/ft |
| Average Velocity | 2.65 ft/s |
| Segment Time of Concentration | 0.044 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.572 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: EDA-3

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

$$\text{Where: } \frac{(L_f / V) / 3600}{R = \text{Hydraulic radius}} \\ A_q = \text{Flow area, square feet} \\ W_p = \text{Wetted perimeter, feet} \\ V = \text{Velocity, ft/sec} \\ S_f = \text{Slope, ft/ft} \\ n = \text{Manning's n} \\ T_c = \text{Time of concentration, hours} \\ L_f = \text{Flow length, feet}$$

==== SCS TR-55 Shallow Concentration Flow

$$T_c = \frac{\text{Unpaved surface:}}{V = 16.1345 * (S_f^{0.5})}$$

$$\text{Paved Surface:} \\ V = 20.3282 * (S_f^{0.5})$$

$$\text{Where: } \frac{(L_f / V) / 3600}{V = \text{Velocity, ft/sec}} \\ S_f = \text{Slope, ft/ft} \\ T_c = \text{Time of concentration, hours} \\ L_f = \text{Flow length, feet}$$

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-1

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.160 ft/ft |
| 2 Year 24 Hour Depth | 3.4 in |
| Average Velocity | 0.18 ft/s |
| Segment Time of Concentration | 0.151 hours |

Segment #2: TR-55 Shallow Concentrated Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 55.00 ft |
| Is Paved? | False |
| Slope | 0.018 ft/ft |
| Average Velocity | 2.16 ft/s |
| Segment Time of Concentration | 0.007 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.158 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-1

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

Where: $(L_f / V) / 3600$
R= Hydraulic radius
A_q= Flow area, square feet
W_p= Wetted perimeter, feet
V= Velocity, ft/sec
S_f= Slope, ft/ft
n= Manning's n
T_c= Time of concentration, hours
L_f= Flow length, feet

==== SCS TR-55 Shallow Concentration Flow

$$T_c = \frac{\text{Unpaved surface:}}{V = 16.1345 * (S_f^{0.5})}$$

$$\text{Paved Surface:}$$
$$V = 20.3282 * (S_f^{0.5})$$

Where: $(L_f / V) / 3600$
V= Velocity, ft/sec
S_f= Slope, ft/ft
T_c= Time of concentration, hours
L_f= Flow length, feet

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2A

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.018 ft/ft |
| 2 Year 24 Hour Depth | 3.4 in |
| Average Velocity | 0.08 ft/s |
| Segment Time of Concentration | 0.364 hours |

Segment #2: TR-55 Shallow Concentrated Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 75.00 ft |
| Is Paved? | False |
| Slope | 0.093 ft/ft |
| Average Velocity | 4.92 ft/s |
| Segment Time of Concentration | 0.004 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.368 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Return Event: 1 years

Label: PDA-2A

Storm Event: 1 year

Scenario: Post-Development 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

Where: $(L_f / V) / 3600$
R= Hydraulic radius
A_q= Flow area, square feet
W_p= Wetted perimeter, feet
V= Velocity, ft/sec
S_f= Slope, ft/ft
n= Manning's n
T_c= Time of concentration, hours
L_f= Flow length, feet

==== SCS TR-55 Shallow Concentration Flow

$$T_c = \frac{\text{Unpaved surface:}}{V = 16.1345 * (S_f^{0.5})}$$

$$\text{Paved Surface:}$$
$$V = 20.3282 * (S_f^{0.5})$$

Where: $(L_f / V) / 3600$
V= Velocity, ft/sec
S_f= Slope, ft/ft
T_c= Time of concentration, hours
L_f= Flow length, feet

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2B

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

| | |
|-----------------------------|-------------|
| Segment #1: User Defined Tc | |
| Time of Concentration | 0.100 hours |

| | |
|--------------------------------------|-------------|
| Time of Concentration (Composite) | |
| Time of Concentration (Composite) | 0.100 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2B

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== User Defined

Tc = Value entered by user

Where: Tc= Time of concentration, hours

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2C

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: User Defined Tc

| | |
|-----------------------|-------------|
| Time of Concentration | 0.100 hours |
|-----------------------|-------------|

Time of Concentration (Composite)

| | |
|--------------------------------------|-------------|
| Time of Concentration (Composite) | 0.100 hours |
|--------------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2C

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== User Defined

Tc = Value entered by user

Where: Tc= Time of concentration, hours

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Return Event: 1 years

Label: PDA-2D

Storm Event: 1 year

Scenario: Post-Development 1 year

Time of Concentration Results

| | |
|-----------------------------|-------------|
| Segment #1: User Defined Tc | |
| Time of Concentration | 0.100 hours |

| | |
|--------------------------------------|-------------|
| Time of Concentration (Composite) | |
| Time of Concentration (Composite) | 0.100 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2D

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== User Defined

Tc = Value entered by user

Where: Tc= Time of concentration, hours

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2E

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.230 ft/ft |
| 2 Year 24 Hour Depth | 3.4 in |
| Average Velocity | 0.21 ft/s |
| Segment Time of Concentration | 0.131 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.131 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-2E

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

$$\text{Where: } T_c = \frac{(L_f / V) / 3600}{R = \text{Hydraulic radius}} \\ A_q = \text{Flow area, square feet} \\ W_p = \text{Wetted perimeter, feet} \\ V = \text{Velocity, ft/sec} \\ S_f = \text{Slope, ft/ft} \\ n = \text{Manning's n} \\ T_c = \text{Time of concentration, hours} \\ L_f = \text{Flow length, feet}$$

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Label: PDA-3

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Time of Concentration Results

Segment #1: TR-55 Sheet Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 100.00 ft |
| Manning's n | 0.400 |
| Slope | 0.230 ft/ft |
| 2 Year 24 Hour Depth | 2.8 in |
| Average Velocity | 0.19 ft/s |
| Segment Time of Concentration | 0.144 hours |

Segment #2: TR-55 Shallow Concentrated Flow

| | |
|-------------------------------|-------------|
| Hydraulic Length | 233.00 ft |
| Is Paved? | False |
| Slope | 0.120 ft/ft |
| Average Velocity | 5.59 ft/s |
| Segment Time of Concentration | 0.012 hours |

Time of Concentration (Composite)

| | |
|-----------------------------------|-------------|
| Time of Concentration (Composite) | 0.156 hours |
|-----------------------------------|-------------|

Existing and Proposed Hydrologic Calculations

Subsection: Time of Concentration Calculations

Return Event: 1 years

Label: PDA-3

Storm Event: 1 year

Scenario: Post-Development 1 year

==== SCS Channel Flow

$$T_c = \frac{R = Q_a / W_p}{V = (1.49 * (R^{2/3}) * (S_f^{-0.5})) / n}$$

$$\text{Where: } \frac{(L_f / V) / 3600}{R = \text{Hydraulic radius}} \\ A_q = \text{Flow area, square feet} \\ W_p = \text{Wetted perimeter, feet} \\ V = \text{Velocity, ft/sec} \\ S_f = \text{Slope, ft/ft} \\ n = \text{Manning's n} \\ T_c = \text{Time of concentration, hours} \\ L_f = \text{Flow length, feet}$$

==== SCS TR-55 Shallow Concentration Flow

$$T_c = \frac{\text{Unpaved surface:}}{V = 16.1345 * (S_f^{0.5})}$$

$$\text{Paved Surface:} \\ V = 20.3282 * (S_f^{0.5})$$

$$\text{Where: } \frac{(L_f / V) / 3600}{V = \text{Velocity, ft/sec}} \\ S_f = \text{Slope, ft/ft} \\ T_c = \text{Time of concentration, hours} \\ L_f = \text{Flow length, feet}$$

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: EDA-1
 Scenario: Pre-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|-----------------------------------|--------|----------------------------|----------|-----------|-------------|
| Woods - good - Soil D | 77.000 | 22,667 | 0.0 | 0.0 | 77.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 22,667 | (N/A) | (N/A) | 77.000 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: EDA-2
 Scenario: Pre-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|-----------------------------------|---------|----------------------------|----------|-----------|-------------|
| Woods - good - Soil D | 77.000 | 54,880 | 0.0 | 0.0 | 77.000 |
| POND | 100.000 | 6,764 | 0.0 | 0.0 | 100.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 61,644 | (N/A) | (N/A) | 79.524 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: EDA-3
 Scenario: Pre-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|--|--------|----------------------------|----------|-----------|-------------|
| Woods - good - Soil D | 77.000 | 167,198 | 0.0 | 0.0 | 77.000 |
| Impervious Areas - Gravel (w/ right-of-way) - Soil D | 91.000 | 8,159 | 0.0 | 0.0 | 91.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 175,357 | (N/A) | (N/A) | 77.651 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-1
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|-----------------------------------|--------|----------------------------|----------|-----------|-------------|
| Woods - good - Soil D | 77.000 | 10,780 | 0.0 | 0.0 | 77.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 10,780 | (N/A) | (N/A) | 77.000 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-2A
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|---|---------|----------------------------|----------|-----------|-------------|
| POND | 100.000 | 6,764 | 0.0 | 0.0 | 100.000 |
| Woods - good - Soil D | 77.000 | 24,245 | 0.0 | 0.0 | 77.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil D | 80.000 | 12,308 | 0.0 | 0.0 | 80.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 43,317 | (N/A) | (N/A) | 81.444 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-2B
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|---|--------|----------------------------|----------|-----------|-------------|
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil D | 98.000 | 18,622 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 18,622 | (N/A) | (N/A) | 98.000 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-2C
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|---|--------|----------------------------|----------|-----------|-------------|
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil D | 98.000 | 18,180 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 18,180 | (N/A) | (N/A) | 98.000 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-2D
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|---|--------|----------------------------|----------|-----------|-------------|
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil D | 98.000 | 7,650 | 0.0 | 0.0 | 98.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 7,650 | (N/A) | (N/A) | 98.000 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-2E
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|---|--------|----------------------------|----------|-----------|-------------|
| Woods - good - Soil D | 77.000 | 3,388 | 0.0 | 0.0 | 77.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil D | 80.000 | 672 | 0.0 | 0.0 | 80.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 4,060 | (N/A) | (N/A) | 77.497 |

Existing and Proposed Hydrologic Calculations

Subsection: Runoff CN-Area
 Label: PDA-3
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Runoff Curve Number Data

| Soil/Surface Description | CN | Area (ft ²) | C (%) | UC (%) | Adjusted CN |
|---|--------|----------------------------|----------|-----------|-------------|
| Impervious Areas - Paved parking lots, roofs, driveways, Streets and roads - Soil D | 98.000 | 69,329 | 0.0 | 0.0 | 98.000 |
| Woods - good - Soil D | 77.000 | 44,908 | 0.0 | 0.0 | 77.000 |
| Open space (Lawns,parks etc.) - Good condition; grass cover > 75% - Soil D | 80.000 | 42,822 | 0.0 | 0.0 | 80.000 |
| COMPOSITE AREA & WEIGHTED CN ---> | (N/A) | 157,059 | (N/A) | (N/A) | 87.088 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: EDA-1

Storm Event: 1 year

Scenario: Pre-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.159 hours |
| Area (User Defined) | 22,667 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.137 hours |
| Flow (Peak, Computed) | 0.43 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 0.43 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 22,667 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 0.9 in |
| Runoff Volume (Pervious) | 1,703 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 1,699 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.159 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-1

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.71 ft ³ /s |
| Unit peak time, T_p | 0.106 hours |
| Unit receding limb, T_r | 0.424 hours |
| Total unit time, T_b | 0.530 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: EDA-1

Storm Event: 10 year

Scenario: Pre-Development 10 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.159 hours |
| Area (User Defined) | 22,667 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.137 hours |
| Flow (Peak, Computed) | 1.34 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 1.33 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 22,667 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.7 in |
| Runoff Volume (Pervious) | 5,081 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 5,072 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.159 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-1

Scenario: Pre-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 3.71 ft ³ /s |
| Unit peak time, Tp | 0.106 hours |
| Unit receding limb, Tr | 0.424 hours |
| Total unit time, Tb | 0.530 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: EDA-1

Storm Event: 25 year

Scenario: Pre-Development 25 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.159 hours |
| Area (User Defined) | 22,667 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.137 hours |
| Flow (Peak, Computed) | 1.92 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 1.90 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 22,667 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 3.9 in |
| Runoff Volume (Pervious) | 7,303 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 7,291 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.159 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-1

Scenario: Pre-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.71 ft ³ /s |
| Unit peak time, T_p | 0.106 hours |
| Unit receding limb, T_r | 0.424 hours |
| Total unit time, T_b | 0.530 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: EDA-1

Storm Event: 100 year

Scenario: Pre-Development 100 year

| | |
|--|-------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.159 hours |
| Area (User Defined) | 22,667 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.137 hours |
| Flow (Peak, Computed) | 3.14 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 3.08 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 22,667 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.4 in |
| Runoff Volume (Pervious) | 12,114 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 12,096 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.159 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-1

Scenario: Pre-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.71 ft ³ /s |
| Unit peak time, T_p | 0.106 hours |
| Unit receding limb, T_r | 0.424 hours |
| Total unit time, T_b | 0.530 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: EDA-2

Storm Event: 1 year

Scenario: Pre-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.465 hours |
| Area (User Defined) | 61,644 ft ² |
| <hr/> | |
| Computational Time Increment | 0.062 hours |
| Time to Peak (Computed) | 12.335 hours |
| Flow (Peak, Computed) | 0.99 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.350 hours |
| Flow (Peak Interpolated Output) | 0.99 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 80.000 |
| Area (User Defined) | 61,644 ft ² |
| Maximum Retention (Pervious) | 2.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 1.1 in |
| Runoff Volume (Pervious) | 5,475 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 5,442 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.465 hours |
| Computational Time Increment | 0.062 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-2

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.45 ft ³ /s |
| Unit peak time, T_p | 0.310 hours |
| Unit receding limb, T_r | 1.240 hours |
| Total unit time, T_b | 1.550 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: EDA-2

Storm Event: 10 year

Scenario: Pre-Development 10 year

| | |
|---|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.465 hours |
| Area (User Defined) | 61,644 ft ² |
| <hr/> | |
| Computational Time Increment | 0.062 hours |
| Time to Peak (Computed) | 12.335 hours |
| Flow (Peak, Computed) | 2.84 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.350 hours |
| Flow (Peak Interpolated Output) | 2.82 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 80.000 |
| Area (User Defined) | 61,644 ft ² |
| Maximum Retention (Pervious) | 2.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 3.0 in |
| Runoff Volume (Pervious) | 15,220 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 15,146 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.465 hours |
| Computational Time Increment | 0.062 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-2

Scenario: Pre-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 3.45 ft ³ /s |
| Unit peak time, Tp | 0.310 hours |
| Unit receding limb, Tr | 1.240 hours |
| Total unit time, Tb | 1.550 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: EDA-2

Storm Event: 25 year

Scenario: Pre-Development 25 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.465 hours |
| Area (User Defined) | 61,644 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.062 hours |
| Time to Peak (Computed) | 12.335 hours |
| Flow (Peak, Computed) | 3.99 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.350 hours |
| Flow (Peak Interpolated Output) | 3.96 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 80.000 |
| Area (User Defined) | 61,644 ft ² |
| Maximum Retention (Pervious) | 2.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |

| | |
|---------------------------------------|------------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.2 in |
| Runoff Volume (Pervious) | 21,475 ft ³ |

| | |
|--|------------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 21,378 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.465 hours |
| Computational Time Increment | 0.062 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-2

Scenario: Pre-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 3.45 ft ³ /s |
| Unit peak time, Tp | 0.310 hours |
| Unit receding limb, Tr | 1.240 hours |
| Total unit time, Tb | 1.550 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: EDA-2

Storm Event: 100 year

Scenario: Pre-Development 100 year

| | |
|--|-------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.465 hours |
| Area (User Defined) | 61,644 ft ² |
| <hr/> | |
| Computational Time Increment | 0.062 hours |
| Time to Peak (Computed) | 12.335 hours |
| Flow (Peak, Computed) | 6.38 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.300 hours |
| Flow (Peak Interpolated Output) | 6.33 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 80.000 |
| Area (User Defined) | 61,644 ft ² |
| Maximum Retention (Pervious) | 2.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.8 in |
| Runoff Volume (Pervious) | 34,862 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 34,717 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.465 hours |
| Computational Time Increment | 0.062 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-2

Scenario: Pre-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 3.45 ft ³ /s |
| Unit peak time, Tp | 0.310 hours |
| Unit receding limb, Tr | 1.240 hours |
| Total unit time, Tb | 1.550 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: EDA-3

Storm Event: 1 year

Scenario: Pre-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.572 hours |
| Area (User Defined) | 175,357 ft ² |
| <hr/> | |
| Computational Time Increment | 0.076 hours |
| Time to Peak (Computed) | 12.438 hours |
| Flow (Peak, Computed) | 2.28 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.450 hours |
| Flow (Peak Interpolated Output) | 2.27 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 78.000 |
| Area (User Defined) | 175,357 ft ² |
| Maximum Retention (Pervious) | 2.8 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 1.0 in |
| Runoff Volume (Pervious) | 13,947 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 13,836 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.572 hours |
| Computational Time Increment | 0.076 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-3

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 7.97 ft ³ /s |
| Unit peak time, Tp | 0.382 hours |
| Unit receding limb, Tr | 1.526 hours |
| Total unit time, Tb | 1.908 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: EDA-3

Storm Event: 10 year

Scenario: Pre-Development 10 year

| | |
|--|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.572 hours |
| Area (User Defined) | 175,357 ft ² |
| <hr/> | |
| Computational Time Increment | 0.076 hours |
| Time to Peak (Computed) | 12.438 hours |
| Flow (Peak, Computed) | 6.89 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.400 hours |
| Flow (Peak Interpolated Output) | 6.86 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 78.000 |
| Area (User Defined) | 175,357 ft ² |
| Maximum Retention (Pervious) | 2.8 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.8 in |
| Runoff Volume (Pervious) | 40,621 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 40,363 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.572 hours |
| Computational Time Increment | 0.076 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-3

Scenario: Pre-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 7.97 ft ³ /s |
| Unit peak time, Tp | 0.382 hours |
| Unit receding limb, Tr | 1.526 hours |
| Total unit time, Tb | 1.908 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: EDA-3

Storm Event: 25 year

Scenario: Pre-Development 25 year

| | |
|--------------------------------------|-------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.572 hours |
| Area (User Defined) | 175,357 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.076 hours |
| Time to Peak (Computed) | 12.438 hours |
| Flow (Peak, Computed) | 9.80 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.400 hours |
| Flow (Peak Interpolated Output) | 9.79 ft ³ /s |

| | |
|---|-------------------------|
| Drainage Area | |
| SCS CN (Composite) | 78.000 |
| Area (User Defined) | 175,357 ft ² |
| Maximum Retention (Pervious) | 2.8 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|------------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.0 in |
| Runoff Volume (Pervious) | 58,016 ft ³ |

| | |
|--|------------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 57,674 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.572 hours |
| Computational Time Increment | 0.076 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-3

Scenario: Pre-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 7.97 ft ³ /s |
| Unit peak time, T_p | 0.382 hours |
| Unit receding limb, T_r | 1.526 hours |
| Total unit time, T_b | 1.908 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: EDA-3

Storm Event: 100 year

Scenario: Pre-Development 100 year

| | |
|--|--------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.572 hours |
| Area (User Defined) | 175,357 ft ² |
| <hr/> | |
| Computational Time Increment | 0.076 hours |
| Time to Peak (Computed) | 12.362 hours |
| Flow (Peak, Computed) | 15.99 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.400 hours |
| Flow (Peak Interpolated Output) | 15.93 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 78.000 |
| Area (User Defined) | 175,357 ft ² |
| Maximum Retention (Pervious) | 2.8 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.5 in |
| Runoff Volume (Pervious) | 95,540 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 95,023 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.572 hours |
| Computational Time Increment | 0.076 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: EDA-3

Scenario: Pre-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|------------------------|-------------------------|
| Unit peak, qp | 7.97 ft ³ /s |
| Unit peak time, Tp | 0.382 hours |
| Unit receding limb, Tr | 1.526 hours |
| Total unit time, Tb | 1.908 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-1

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.158 hours |
| Area (User Defined) | 10,780 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.149 hours |
| Flow (Peak, Computed) | 0.21 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 0.21 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 10,780 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 0.9 in |
| Runoff Volume (Pervious) | 810 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 808 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.158 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-1

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.77 ft ³ /s |
| Unit peak time, T_p | 0.105 hours |
| Unit receding limb, T_r | 0.422 hours |
| Total unit time, T_b | 0.527 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-1

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.158 hours |
| Area (User Defined) | 10,780 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.128 hours |
| Flow (Peak, Computed) | 0.64 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 0.63 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 10,780 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.7 in |
| Runoff Volume (Pervious) | 2,417 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 2,413 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.158 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-1

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.77 ft ³ /s |
| Unit peak time, T_p | 0.105 hours |
| Unit receding limb, T_r | 0.422 hours |
| Total unit time, T_b | 0.527 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-1

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|---|-------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.158 hours |
| Area (User Defined) | 10,780 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.128 hours |
| Flow (Peak, Computed) | 0.91 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 0.90 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 10,780 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 3.9 in |
| Runoff Volume (Pervious) | 3,473 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 3,468 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.158 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-1

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.77 ft ³ /s |
| Unit peak time, T_p | 0.105 hours |
| Unit receding limb, T_r | 0.422 hours |
| Total unit time, T_b | 0.527 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-1

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.158 hours |
| Area (User Defined) | 10,780 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.128 hours |
| Flow (Peak, Computed) | 1.49 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 1.47 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 10,780 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.4 in |
| Runoff Volume (Pervious) | 5,761 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 5,754 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.158 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-1

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.77 ft ³ /s |
| Unit peak time, T_p | 0.105 hours |
| Unit receding limb, T_r | 0.422 hours |
| Total unit time, T_b | 0.527 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-2A

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.368 hours |
| Area (User Defined) | 43,317 ft ² |
| <hr/> | |
| Computational Time Increment | 0.049 hours |
| Time to Peak (Computed) | 12.267 hours |
| Flow (Peak, Computed) | 0.82 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.300 hours |
| Flow (Peak Interpolated Output) | 0.81 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 81.000 |
| Area (User Defined) | 43,317 ft ² |
| Maximum Retention (Pervious) | 2.3 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 1.1 in |
| Runoff Volume (Pervious) | 4,059 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 4,040 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.368 hours |
| Computational Time Increment | 0.049 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2A

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.06 ft ³ /s |
| Unit peak time, T_p | 0.245 hours |
| Unit receding limb, T_r | 0.981 hours |
| Total unit time, T_b | 1.227 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-2A

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.368 hours |
| Area (User Defined) | 43,317 ft ² |
| <hr/> | |
| Computational Time Increment | 0.049 hours |
| Time to Peak (Computed) | 12.267 hours |
| Flow (Peak, Computed) | 2.26 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.250 hours |
| Flow (Peak Interpolated Output) | 2.24 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 81.000 |
| Area (User Defined) | 43,317 ft ² |
| Maximum Retention (Pervious) | 2.3 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 3.1 in |
| Runoff Volume (Pervious) | 11,032 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 10,989 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.368 hours |
| Computational Time Increment | 0.049 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2A

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.06 ft ³ /s |
| Unit peak time, T_p | 0.245 hours |
| Unit receding limb, T_r | 0.981 hours |
| Total unit time, T_b | 1.227 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-2A

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|--|-------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.368 hours |
| Area (User Defined) | 43,317 ft ² |
| <hr/> | |
| Computational Time Increment | 0.049 hours |
| Time to Peak (Computed) | 12.267 hours |
| Flow (Peak, Computed) | 3.15 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.250 hours |
| Flow (Peak Interpolated Output) | 3.13 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 81.000 |
| Area (User Defined) | 43,317 ft ² |
| Maximum Retention (Pervious) | 2.3 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.3 in |
| Runoff Volume (Pervious) | 15,474 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 15,418 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.368 hours |
| Computational Time Increment | 0.049 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2A

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.06 ft ³ /s |
| Unit peak time, T_p | 0.245 hours |
| Unit receding limb, T_r | 0.981 hours |
| Total unit time, T_b | 1.227 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-2A

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--|-------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.368 hours |
| Area (User Defined) | 43,317 ft ² |
| <hr/> | |
| Computational Time Increment | 0.049 hours |
| Time to Peak (Computed) | 12.267 hours |
| Flow (Peak, Computed) | 4.98 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.250 hours |
| Flow (Peak Interpolated Output) | 4.97 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 81.000 |
| Area (User Defined) | 43,317 ft ² |
| Maximum Retention (Pervious) | 2.3 in |
| Maximum Retention (Pervious, 20 percent) | 0.5 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.9 in |
| Runoff Volume (Pervious) | 24,945 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 24,861 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.368 hours |
| Computational Time Increment | 0.049 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2A

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 3.06 ft ³ /s |
| Unit peak time, T_p | 0.245 hours |
| Unit receding limb, T_r | 0.981 hours |
| Total unit time, T_b | 1.227 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-2B

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,622 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.97 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.97 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,622 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.5 in |
| Runoff Volume (Pervious) | 3,910 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 3,907 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2B

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.84 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-2B

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,622 ft ² |
| <hr/> | |
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 1.81 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 1.81 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,622 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.8 in |
| Runoff Volume (Pervious) | 7,516 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 7,510 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2B

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.84 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-2B

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,622 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 2.30 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 2.30 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,622 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.2 in |
| Runoff Volume (Pervious) | 9,624 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 9,617 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2B

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.84 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-2B

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,622 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.093 hours |
| Flow (Peak, Computed) | 3.30 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 3.30 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,622 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|------------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 9.0 in |
| Runoff Volume (Pervious) | 13,950 ft ³ |

| | |
|--|------------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 13,940 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2B

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.84 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-2C

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,180 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.94 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.94 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,180 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.5 in |
| Runoff Volume (Pervious) | 3,817 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 3,814 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2C

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.73 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-2C

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,180 ft ² |
| <hr/> | |
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 1.76 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 1.76 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,180 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.8 in |
| Runoff Volume (Pervious) | 7,337 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 7,332 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2C

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.73 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-2C

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,180 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 2.24 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 2.24 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,180 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.2 in |
| Runoff Volume (Pervious) | 9,395 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 9,388 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2C

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.73 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-2C

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 18,180 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.093 hours |
| Flow (Peak, Computed) | 3.22 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 3.22 ft ³ /s |

| | |
|---|------------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 18,180 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|------------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 9.0 in |
| Runoff Volume (Pervious) | 13,619 ft ³ |

| | |
|--|------------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 13,610 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2C

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 4.73 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-2D

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 7,650 ft ² |
| <hr/> | |
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.40 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.40 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 7,650 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.5 in |
| Runoff Volume (Pervious) | 1,606 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 1,605 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2D

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.99 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-2D

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--|-------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 7,650 ft ² |
| <hr/> | |
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.74 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.74 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 7,650 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.8 in |
| Runoff Volume (Pervious) | 3,087 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 3,085 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2D

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.99 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-2D

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|--|-------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 7,650 ft ² |
| <hr/> | |
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.107 hours |
| Flow (Peak, Computed) | 0.94 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.94 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 7,650 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.2 in |
| Runoff Volume (Pervious) | 3,953 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 3,951 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2D

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.99 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-2D

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|-----------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.100 hours |
| Area (User Defined) | 7,650 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.013 hours |
| Time to Peak (Computed) | 12.093 hours |
| Flow (Peak, Computed) | 1.35 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 1.35 ft ³ /s |

| | |
|---|-----------------------|
| Drainage Area | |
| SCS CN (Composite) | 98.000 |
| Area (User Defined) | 7,650 ft ² |
| Maximum Retention (Pervious) | 0.2 in |
| Maximum Retention (Pervious, 20 percent) | 0.0 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 9.0 in |
| Runoff Volume (Pervious) | 5,731 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 5,727 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.100 hours |
| Computational Time Increment | 0.013 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2D

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 1.99 ft ³ /s |
| Unit peak time, T_p | 0.067 hours |
| Unit receding limb, T_r | 0.267 hours |
| Total unit time, T_b | 0.333 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-2E

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--------------------------------------|-----------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.131 hours |
| Area (User Defined) | 4,060 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.018 hours |
| Time to Peak (Computed) | 12.131 hours |
| Flow (Peak, Computed) | 0.08 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 0.08 ft ³ /s |

| | |
|---|-----------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 4,060 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|---------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 0.9 in |
| Runoff Volume (Pervious) | 305 ft ³ |

| | |
|--|---------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 305 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.131 hours |
| Computational Time Increment | 0.018 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2E

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 0.80 ft ³ /s |
| Unit peak time, T_p | 0.088 hours |
| Unit receding limb, T_r | 0.350 hours |
| Total unit time, T_b | 0.438 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-2E

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--------------------------------------|-----------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.131 hours |
| Area (User Defined) | 4,060 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.018 hours |
| Time to Peak (Computed) | 12.131 hours |
| Flow (Peak, Computed) | 0.25 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.24 ft ³ /s |

| | |
|---|-----------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 4,060 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|---------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 2.7 in |
| Runoff Volume (Pervious) | 910 ft ³ |

| | |
|--|---------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 909 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.131 hours |
| Computational Time Increment | 0.018 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2E

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 0.80 ft ³ /s |
| Unit peak time, T_p | 0.088 hours |
| Unit receding limb, T_r | 0.350 hours |
| Total unit time, T_b | 0.438 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-2E

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|--------------------------------------|-----------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.131 hours |
| Area (User Defined) | 4,060 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.018 hours |
| Time to Peak (Computed) | 12.114 hours |
| Flow (Peak, Computed) | 0.36 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.35 ft ³ /s |

| | |
|---|-----------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 4,060 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 3.9 in |
| Runoff Volume (Pervious) | 1,308 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 1,306 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.131 hours |
| Computational Time Increment | 0.018 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2E

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 0.80 ft ³ /s |
| Unit peak time, T_p | 0.088 hours |
| Unit receding limb, T_r | 0.350 hours |
| Total unit time, T_b | 0.438 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-2E

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|-----------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.131 hours |
| Area (User Defined) | 4,060 ft ² |

| | |
|--|-------------------------|
| Computational Time Increment | 0.018 hours |
| Time to Peak (Computed) | 12.114 hours |
| Flow (Peak, Computed) | 0.58 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 0.57 ft ³ /s |

| | |
|---|-----------------------|
| Drainage Area | |
| SCS CN (Composite) | 77.000 |
| Area (User Defined) | 4,060 ft ² |
| Maximum Retention (Pervious) | 3.0 in |
| Maximum Retention (Pervious, 20 percent) | 0.6 in |

| | |
|---------------------------------------|-----------------------|
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 6.4 in |
| Runoff Volume (Pervious) | 2,170 ft ³ |

| | |
|--|-----------------------|
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 2,167 ft ³ |

| | |
|---------------------------------------|-------------|
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.131 hours |
| Computational Time Increment | 0.018 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-2E

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|-------------------------|
| Unit peak, q_p | 0.80 ft ³ /s |
| Unit peak time, T_p | 0.088 hours |
| Unit receding limb, T_r | 0.350 hours |
| Total unit time, T_b | 0.438 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 1 years

Label: PDA-3

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|--|-------------------------|
| Storm Event | 1 year |
| Return Event | 1 years |
| Duration | 24.000 hours |
| Depth | 2.8 in |
| Time of Concentration (Composite) | 0.156 hours |
| Area (User Defined) | 157,059 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.138 hours |
| Flow (Peak, Computed) | 5.29 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 5.21 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 87.000 |
| Area (User Defined) | 157,059 ft ² |
| Maximum Retention (Pervious) | 1.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.3 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 1.5 in |
| Runoff Volume (Pervious) | 19,931 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 19,897 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.156 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-3

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|--------------------------|
| Unit peak, q_p | 26.25 ft ³ /s |
| Unit peak time, T_p | 0.104 hours |
| Unit receding limb, T_r | 0.415 hours |
| Total unit time, T_b | 0.519 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 10 years

Label: PDA-3

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|--|--------------------------|
| Storm Event | 10 year |
| Return Event | 10 years |
| Duration | 24.000 hours |
| Depth | 5.1 in |
| Time of Concentration (Composite) | 0.156 hours |
| Area (User Defined) | 157,059 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.138 hours |
| Flow (Peak, Computed) | 12.30 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.150 hours |
| Flow (Peak Interpolated Output) | 12.08 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 87.000 |
| Area (User Defined) | 157,059 ft ² |
| Maximum Retention (Pervious) | 1.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.3 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 3.6 in |
| Runoff Volume (Pervious) | 47,677 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 47,606 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.156 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-3

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|--------------------------|
| Unit peak, q_p | 26.25 ft ³ /s |
| Unit peak time, T_p | 0.104 hours |
| Unit receding limb, T_r | 0.415 hours |
| Total unit time, T_b | 0.519 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 25 years

Label: PDA-3

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|--|--------------------------|
| Storm Event | 25 year |
| Return Event | 25 years |
| Duration | 24.000 hours |
| Depth | 6.4 in |
| Time of Concentration (Composite) | 0.156 hours |
| Area (User Defined) | 157,059 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.117 hours |
| Flow (Peak, Computed) | 16.44 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 16.18 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 87.000 |
| Area (User Defined) | 157,059 ft ² |
| Maximum Retention (Pervious) | 1.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.3 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 4.9 in |
| Runoff Volume (Pervious) | 64,647 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 64,556 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.156 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-3

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|--------------------------|
| Unit peak, q_p | 26.25 ft ³ /s |
| Unit peak time, T_p | 0.104 hours |
| Unit receding limb, T_r | 0.415 hours |
| Total unit time, T_b | 0.519 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Return Event: 100 years

Label: PDA-3

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--|--------------------------|
| Storm Event | 100 year |
| Return Event | 100 years |
| Duration | 24.000 hours |
| Depth | 9.2 in |
| Time of Concentration (Composite) | 0.156 hours |
| Area (User Defined) | 157,059 ft ² |
| <hr/> | |
| Computational Time Increment | 0.021 hours |
| Time to Peak (Computed) | 12.117 hours |
| Flow (Peak, Computed) | 24.86 ft ³ /s |
| Output Increment | 0.050 hours |
| Time to Flow (Peak Interpolated Output) | 12.100 hours |
| Flow (Peak Interpolated Output) | 24.51 ft ³ /s |
| <hr/> | |
| Drainage Area | |
| SCS CN (Composite) | 87.000 |
| Area (User Defined) | 157,059 ft ² |
| Maximum Retention (Pervious) | 1.5 in |
| Maximum Retention (Pervious, 20 percent) | 0.3 in |
| <hr/> | |
| Cumulative Runoff | |
| Cumulative Runoff Depth (Pervious) | 7.7 in |
| Runoff Volume (Pervious) | 100,139 ft ³ |
| <hr/> | |
| Hydrograph Volume (Area under Hydrograph curve) | |
| Volume | 100,006 ft ³ |
| <hr/> | |
| SCS Unit Hydrograph Parameters | |
| Time of Concentration (Composite) | 0.156 hours |
| Computational Time Increment | 0.021 hours |
| Unit Hydrograph Shape Factor | 483.432 |
| K Factor | 0.749 |
| Receding/Rising, Tr/Tp | 1.670 |

Existing and Proposed Hydrologic Calculations

Subsection: Unit Hydrograph Summary

Label: PDA-3

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

SCS Unit Hydrograph Parameters

| | |
|---------------------------|--------------------------|
| Unit peak, q_p | 26.25 ft ³ /s |
| Unit peak time, T_p | 0.104 hours |
| Unit receding limb, T_r | 0.415 hours |
| Total unit time, T_b | 0.519 hours |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-1 | 808 | 12.150 | 0.21 |
| Flow (In) | DP-1 | 808 | 12.150 | 0.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-1 | 1,699 | 12.150 | 0.43 |
| Flow (In) | DP-1 | 1,699 | 12.150 | 0.43 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-1 | 2,413 | 12.150 | 0.63 |
| Flow (In) | DP-1 | 2,413 | 12.150 | 0.63 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Pre-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-1 | 5,072 | 12.150 | 1.33 |
| Flow (In) | DP-1 | 5,072 | 12.150 | 1.33 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-1 | 3,468 | 12.150 | 0.90 |
| Flow (In) | DP-1 | 3,468 | 12.150 | 0.90 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Pre-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-1 | 7,291 | 12.150 | 1.90 |
| Flow (In) | DP-1 | 7,291 | 12.150 | 1.90 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Return Event: 100 years

Label: DP-1

Storm Event: 100 year

Scenario: Post-Development 100 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-1 | 5,754 | 12.150 | 1.47 |
| Flow (In) | DP-1 | 5,754 | 12.150 | 1.47 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-1

Scenario: Pre-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Summary for Hydrograph Addition at 'DP-1'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-1 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-1 | 12,096 | 12.150 | 3.08 |
| Flow (In) | DP-1 | 12,096 | 12.150 | 3.08 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2A |
| MC-3500 - 2 OUT | MC-3500 - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|--------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2A | 4,040 | 12.300 | 0.81 |
| Flow (From) | MC-3500 - 2 OUT | 9,398 | 16.500 | 0.23 |
| Flow (In) | DP-2 | 13,437 | 12.300 | 0.99 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-2 | 5,442 | 12.350 | 0.99 |
| Flow (In) | DP-2 | 5,442 | 12.350 | 0.99 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2A |
| MC-3500 - 2 OUT | MC-3500 - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|--------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2A | 10,989 | 12.250 | 2.24 |
| Flow (From) | MC-3500 - 2 OUT | 16,459 | 13.550 | 0.42 |
| Flow (In) | DP-2 | 27,448 | 12.250 | 2.49 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Pre-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-2 | 15,146 | 12.350 | 2.82 |
| Flow (In) | DP-2 | 15,146 | 12.350 | 2.82 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2A |
| MC-3500 - 2 OUT | MC-3500 - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|--------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2A | 15,418 | 12.250 | 3.13 |
| Flow (From) | MC-3500 - 2 OUT | 21,106 | 12.900 | 0.73 |
| Flow (In) | DP-2 | 36,524 | 12.250 | 3.62 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Pre-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-2 | 21,378 | 12.350 | 3.96 |
| Flow (In) | DP-2 | 21,378 | 12.350 | 3.96 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Return Event: 100 years

Label: DP-2

Storm Event: 100 year

Scenario: Post-Development 100 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2A |
| MC-3500 - 2 OUT | MC-3500 - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|--------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2A | 24,861 | 12.250 | 4.97 |
| Flow (From) | MC-3500 - 2 OUT | 31,039 | 12.700 | 1.28 |
| Flow (In) | DP-2 | 55,900 | 12.250 | 5.97 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-2

Scenario: Pre-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Summary for Hydrograph Addition at 'DP-2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-2 | 34,717 | 12.300 | 6.33 |
| Flow (In) | DP-2 | 34,717 | 12.300 | 6.33 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|---------------|---------------|
| MC-3500 OUT | MC-3500 - 3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | MC-3500 OUT | 19,594 | 12.450 | 2.00 |
| Flow (In) | DP-3 | 19,594 | 12.450 | 2.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Pre-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-3 | 13,836 | 12.450 | 2.27 |
| Flow (In) | DP-3 | 13,836 | 12.450 | 2.27 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|---------------|---------------|
| MC-3500 OUT | MC-3500 - 3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | MC-3500 OUT | 46,990 | 12.400 | 5.48 |
| Flow (In) | DP-3 | 46,990 | 12.400 | 5.48 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Pre-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-3 | 40,363 | 12.400 | 6.86 |
| Flow (In) | DP-3 | 40,363 | 12.400 | 6.86 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|---------------|---------------|
| MC-3500 OUT | MC-3500 - 3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | MC-3500 OUT | 63,759 | 12.350 | 8.01 |
| Flow (In) | DP-3 | 63,759 | 12.350 | 8.01 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Pre-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-3 | 57,674 | 12.400 | 9.79 |
| Flow (In) | DP-3 | 57,674 | 12.400 | 9.79 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|---------------|---------------|
| MC-3500 OUT | MC-3500 - 3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | MC-3500 OUT | 98,845 | 12.300 | 15.14 |
| Flow (In) | DP-3 | 98,845 | 12.300 | 15.14 |

Existing and Proposed Hydrologic Calculations

Subsection: Addition Summary

Label: DP-3

Scenario: Pre-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Summary for Hydrograph Addition at 'DP-3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | EDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------|---------------------------|----------------------|----------------------------------|
| Flow (From) | EDA-3 | 95,023 | 12.400 | 15.93 |
| Flow (In) | DP-3 | 95,023 | 12.400 | 15.93 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.250 | 93.02 | 93.02 | 93.03 | 93.03 | 93.04 |
| 11.500 | 93.05 | 93.07 | 93.09 | 93.12 | 93.16 |
| 11.750 | 93.21 | 93.25 | 93.30 | 93.36 | 93.44 |
| 12.000 | 93.55 | 93.69 | 93.84 | 93.98 | 94.09 |
| 12.250 | 94.17 | 94.24 | 94.29 | 94.33 | 94.37 |
| 12.500 | 94.40 | 94.42 | 94.43 | 94.44 | 94.45 |
| 12.750 | 94.45 | 94.46 | 94.46 | 94.46 | 94.46 |
| 13.000 | 94.46 | 94.46 | 94.46 | 94.46 | 94.46 |
| 13.250 | 94.46 | 94.46 | 94.46 | 94.45 | 94.45 |
| 13.500 | 94.45 | 94.44 | 94.44 | 94.44 | 94.43 |
| 13.750 | 94.43 | 94.42 | 94.42 | 94.41 | 94.41 |
| 14.000 | 94.40 | 94.40 | 94.39 | 94.39 | 94.38 |
| 14.250 | 94.37 | 94.37 | 94.36 | 94.35 | 94.35 |
| 14.500 | 94.34 | 94.33 | 94.33 | 94.32 | 94.31 |
| 14.750 | 94.30 | 94.30 | 94.29 | 94.28 | 94.27 |
| 15.000 | 94.26 | 94.26 | 94.25 | 94.24 | 94.23 |
| 15.250 | 94.22 | 94.21 | 94.20 | 94.20 | 94.19 |
| 15.500 | 94.18 | 94.17 | 94.16 | 94.15 | 94.14 |
| 15.750 | 94.13 | 94.12 | 94.11 | 94.10 | 94.09 |
| 16.000 | 94.08 | 94.07 | 94.06 | 94.05 | 94.04 |
| 16.250 | 94.02 | 94.01 | 94.00 | 93.99 | 93.98 |
| 16.500 | 93.97 | 93.96 | 93.95 | 93.94 | 93.93 |
| 16.750 | 93.91 | 93.90 | 93.89 | 93.88 | 93.87 |
| 17.000 | 93.86 | 93.85 | 93.83 | 93.82 | 93.81 |
| 17.250 | 93.80 | 93.79 | 93.77 | 93.76 | 93.75 |
| 17.500 | 93.74 | 93.73 | 93.71 | 93.70 | 93.69 |
| 17.750 | 93.68 | 93.66 | 93.65 | 93.64 | 93.63 |
| 18.000 | 93.61 | 93.60 | 93.59 | 93.58 | 93.56 |
| 18.250 | 93.55 | 93.54 | 93.53 | 93.51 | 93.50 |
| 18.500 | 93.49 | 93.47 | 93.46 | 93.45 | 93.44 |
| 18.750 | 93.42 | 93.41 | 93.40 | 93.38 | 93.37 |
| 19.000 | 93.36 | 93.35 | 93.33 | 93.32 | 93.31 |
| 19.250 | 93.29 | 93.28 | 93.27 | 93.25 | 93.24 |
| 19.500 | 93.23 | 93.21 | 93.20 | 93.18 | 93.16 |
| 19.750 | 93.14 | 93.12 | 93.10 | 93.07 | 93.04 |
| 20.000 | 93.02 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 24.000 | 93.00 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.02 |
| 9.750 | 93.02 | 93.02 | 93.02 | 93.02 | 93.02 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 93.03 | 93.03 | 93.04 | 93.04 | 93.05 |
| 10.250 | 93.05 | 93.06 | 93.07 | 93.08 | 93.09 |
| 10.500 | 93.10 | 93.11 | 93.12 | 93.13 | 93.14 |
| 10.750 | 93.16 | 93.17 | 93.18 | 93.20 | 93.21 |
| 11.000 | 93.22 | 93.23 | 93.24 | 93.25 | 93.27 |
| 11.250 | 93.29 | 93.30 | 93.32 | 93.34 | 93.37 |
| 11.500 | 93.39 | 93.42 | 93.46 | 93.50 | 93.56 |
| 11.750 | 93.64 | 93.73 | 93.84 | 93.97 | 94.13 |
| 12.000 | 94.35 | 94.63 | 94.92 | 95.18 | 95.24 |
| 12.250 | 95.23 | 95.23 | 95.23 | 95.22 | 95.22 |
| 12.500 | 95.22 | 95.22 | 95.21 | 95.21 | 95.21 |
| 12.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.20 |
| 15.250 | 95.20 | 95.20 | 95.20 | 95.20 | 95.19 |
| 15.500 | 95.19 | 95.19 | 95.19 | 95.18 | 95.18 |
| 15.750 | 95.18 | 95.17 | 95.17 | 95.16 | 95.16 |
| 16.000 | 95.15 | 95.15 | 95.14 | 95.14 | 95.13 |
| 16.250 | 95.13 | 95.12 | 95.12 | 95.11 | 95.11 |
| 16.500 | 95.10 | 95.10 | 95.09 | 95.08 | 95.08 |
| 16.750 | 95.07 | 95.06 | 95.05 | 95.05 | 95.04 |
| 17.000 | 95.03 | 95.02 | 95.01 | 95.01 | 95.00 |
| 17.250 | 94.99 | 94.98 | 94.97 | 94.96 | 94.96 |
| 17.500 | 94.95 | 94.94 | 94.93 | 94.92 | 94.91 |
| 17.750 | 94.90 | 94.89 | 94.88 | 94.87 | 94.86 |
| 18.000 | 94.85 | 94.84 | 94.83 | 94.82 | 94.81 |
| 18.250 | 94.80 | 94.79 | 94.78 | 94.77 | 94.76 |
| 18.500 | 94.75 | 94.74 | 94.73 | 94.72 | 94.71 |
| 18.750 | 94.70 | 94.69 | 94.68 | 94.67 | 94.66 |
| 19.000 | 94.65 | 94.64 | 94.63 | 94.62 | 94.61 |
| 19.250 | 94.60 | 94.59 | 94.58 | 94.57 | 94.56 |
| 19.500 | 94.55 | 94.53 | 94.52 | 94.51 | 94.50 |
| 19.750 | 94.49 | 94.48 | 94.47 | 94.46 | 94.45 |
| 20.000 | 94.44 | 94.43 | 94.42 | 94.40 | 94.39 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 94.38 | 94.37 | 94.36 | 94.35 | 94.34 |
| 20.500 | 94.33 | 94.31 | 94.30 | 94.29 | 94.28 |
| 20.750 | 94.27 | 94.26 | 94.25 | 94.24 | 94.22 |
| 21.000 | 94.21 | 94.20 | 94.19 | 94.18 | 94.17 |
| 21.250 | 94.16 | 94.14 | 94.13 | 94.12 | 94.11 |
| 21.500 | 94.10 | 94.09 | 94.07 | 94.06 | 94.05 |
| 21.750 | 94.04 | 94.03 | 94.02 | 94.00 | 93.99 |
| 22.000 | 93.98 | 93.97 | 93.96 | 93.94 | 93.93 |
| 22.250 | 93.92 | 93.91 | 93.90 | 93.88 | 93.87 |
| 22.500 | 93.86 | 93.85 | 93.84 | 93.82 | 93.81 |
| 22.750 | 93.80 | 93.79 | 93.78 | 93.76 | 93.75 |
| 23.000 | 93.74 | 93.73 | 93.71 | 93.70 | 93.69 |
| 23.250 | 93.68 | 93.66 | 93.65 | 93.64 | 93.63 |
| 23.500 | 93.61 | 93.60 | 93.59 | 93.58 | 93.56 |
| 23.750 | 93.55 | 93.54 | 93.53 | 93.51 | 93.50 |
| 24.000 | 93.49 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.02 | 93.02 | 93.02 |
| 9.000 | 93.02 | 93.02 | 93.02 | 93.03 | 93.03 |
| 9.250 | 93.04 | 93.04 | 93.05 | 93.05 | 93.06 |
| 9.500 | 93.07 | 93.08 | 93.08 | 93.09 | 93.10 |
| 9.750 | 93.11 | 93.12 | 93.13 | 93.14 | 93.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 93.16 | 93.17 | 93.18 | 93.19 | 93.20 |
| 10.250 | 93.21 | 93.22 | 93.23 | 93.24 | 93.25 |
| 10.500 | 93.26 | 93.28 | 93.29 | 93.30 | 93.32 |
| 10.750 | 93.33 | 93.35 | 93.36 | 93.38 | 93.40 |
| 11.000 | 93.41 | 93.43 | 93.45 | 93.47 | 93.49 |
| 11.250 | 93.52 | 93.55 | 93.58 | 93.61 | 93.64 |
| 11.500 | 93.68 | 93.72 | 93.77 | 93.83 | 93.91 |
| 11.750 | 94.02 | 94.14 | 94.28 | 94.45 | 94.66 |
| 12.000 | 94.94 | 95.22 | 95.27 | 95.26 | 95.25 |
| 12.250 | 95.24 | 95.23 | 95.23 | 95.23 | 95.22 |
| 12.500 | 95.22 | 95.22 | 95.22 | 95.22 | 95.22 |
| 12.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.750 | 95.21 | 95.21 | 95.21 | 95.20 | 95.20 |
| 16.000 | 95.20 | 95.20 | 95.20 | 95.19 | 95.19 |
| 16.250 | 95.19 | 95.19 | 95.18 | 95.18 | 95.18 |
| 16.500 | 95.17 | 95.17 | 95.16 | 95.16 | 95.16 |
| 16.750 | 95.15 | 95.15 | 95.14 | 95.14 | 95.14 |
| 17.000 | 95.13 | 95.13 | 95.12 | 95.12 | 95.11 |
| 17.250 | 95.11 | 95.10 | 95.10 | 95.09 | 95.08 |
| 17.500 | 95.08 | 95.07 | 95.06 | 95.05 | 95.05 |
| 17.750 | 95.04 | 95.03 | 95.02 | 95.02 | 95.01 |
| 18.000 | 95.00 | 94.99 | 94.98 | 94.98 | 94.97 |
| 18.250 | 94.96 | 94.95 | 94.94 | 94.93 | 94.93 |
| 18.500 | 94.92 | 94.91 | 94.90 | 94.89 | 94.88 |
| 18.750 | 94.87 | 94.86 | 94.86 | 94.85 | 94.84 |
| 19.000 | 94.83 | 94.82 | 94.81 | 94.80 | 94.79 |
| 19.250 | 94.78 | 94.78 | 94.77 | 94.76 | 94.75 |
| 19.500 | 94.74 | 94.73 | 94.72 | 94.71 | 94.70 |
| 19.750 | 94.69 | 94.68 | 94.67 | 94.66 | 94.65 |
| 20.000 | 94.64 | 94.63 | 94.62 | 94.61 | 94.60 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 94.59 | 94.58 | 94.58 | 94.57 | 94.56 |
| 20.500 | 94.55 | 94.54 | 94.53 | 94.52 | 94.51 |
| 20.750 | 94.50 | 94.49 | 94.48 | 94.47 | 94.45 |
| 21.000 | 94.44 | 94.43 | 94.42 | 94.41 | 94.40 |
| 21.250 | 94.39 | 94.38 | 94.37 | 94.36 | 94.35 |
| 21.500 | 94.34 | 94.33 | 94.32 | 94.31 | 94.30 |
| 21.750 | 94.29 | 94.28 | 94.27 | 94.26 | 94.25 |
| 22.000 | 94.24 | 94.22 | 94.21 | 94.20 | 94.19 |
| 22.250 | 94.18 | 94.17 | 94.16 | 94.15 | 94.14 |
| 22.500 | 94.13 | 94.12 | 94.10 | 94.09 | 94.08 |
| 22.750 | 94.07 | 94.06 | 94.05 | 94.04 | 94.03 |
| 23.000 | 94.01 | 94.00 | 93.99 | 93.98 | 93.97 |
| 23.250 | 93.96 | 93.95 | 93.93 | 93.92 | 93.91 |
| 23.500 | 93.90 | 93.89 | 93.88 | 93.87 | 93.85 |
| 23.750 | 93.84 | 93.83 | 93.82 | 93.81 | 93.80 |
| 24.000 | 93.78 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.02 |
| 7.750 | 93.02 | 93.02 | 93.02 | 93.02 | 93.02 |
| 8.000 | 93.02 | 93.03 | 93.03 | 93.03 | 93.04 |
| 8.250 | 93.04 | 93.05 | 93.06 | 93.06 | 93.07 |
| 8.500 | 93.08 | 93.09 | 93.10 | 93.11 | 93.12 |
| 8.750 | 93.13 | 93.14 | 93.15 | 93.17 | 93.18 |
| 9.000 | 93.19 | 93.20 | 93.21 | 93.22 | 93.23 |
| 9.250 | 93.24 | 93.26 | 93.27 | 93.28 | 93.29 |
| 9.500 | 93.30 | 93.32 | 93.33 | 93.34 | 93.36 |
| 9.750 | 93.37 | 93.39 | 93.40 | 93.42 | 93.43 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 93.45 | 93.47 | 93.49 | 93.50 | 93.52 |
| 10.250 | 93.54 | 93.56 | 93.58 | 93.61 | 93.63 |
| 10.500 | 93.65 | 93.68 | 93.70 | 93.73 | 93.76 |
| 10.750 | 93.79 | 93.81 | 93.84 | 93.88 | 93.91 |
| 11.000 | 93.94 | 93.97 | 94.01 | 94.04 | 94.08 |
| 11.250 | 94.13 | 94.17 | 94.22 | 94.28 | 94.33 |
| 11.500 | 94.39 | 94.46 | 94.54 | 94.63 | 94.76 |
| 11.750 | 94.91 | 95.10 | 95.22 | 95.25 | 95.25 |
| 12.000 | 95.27 | 95.28 | 95.29 | 95.28 | 95.26 |
| 12.250 | 95.25 | 95.24 | 95.24 | 95.24 | 95.23 |
| 12.500 | 95.23 | 95.22 | 95.22 | 95.22 | 95.22 |
| 12.750 | 95.22 | 95.22 | 95.22 | 95.22 | 95.22 |
| 13.000 | 95.22 | 95.22 | 95.21 | 95.21 | 95.21 |
| 13.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 13.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 14.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 15.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 16.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 16.250 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 16.500 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 16.750 | 95.21 | 95.21 | 95.21 | 95.21 | 95.21 |
| 17.000 | 95.21 | 95.21 | 95.21 | 95.21 | 95.20 |
| 17.250 | 95.20 | 95.20 | 95.20 | 95.20 | 95.20 |
| 17.500 | 95.20 | 95.19 | 95.19 | 95.19 | 95.19 |
| 17.750 | 95.18 | 95.18 | 95.18 | 95.17 | 95.17 |
| 18.000 | 95.17 | 95.16 | 95.16 | 95.15 | 95.15 |
| 18.250 | 95.15 | 95.14 | 95.14 | 95.13 | 95.13 |
| 18.500 | 95.12 | 95.12 | 95.12 | 95.11 | 95.11 |
| 18.750 | 95.10 | 95.10 | 95.09 | 95.09 | 95.08 |
| 19.000 | 95.07 | 95.07 | 95.06 | 95.06 | 95.05 |
| 19.250 | 95.04 | 95.04 | 95.03 | 95.03 | 95.02 |
| 19.500 | 95.01 | 95.01 | 95.00 | 94.99 | 94.99 |
| 19.750 | 94.98 | 94.97 | 94.97 | 94.96 | 94.95 |
| 20.000 | 94.95 | 94.94 | 94.93 | 94.92 | 94.92 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 94.91 | 94.90 | 94.90 | 94.89 | 94.88 |
| 20.500 | 94.87 | 94.87 | 94.86 | 94.85 | 94.84 |
| 20.750 | 94.84 | 94.83 | 94.82 | 94.81 | 94.81 |
| 21.000 | 94.80 | 94.79 | 94.78 | 94.78 | 94.77 |
| 21.250 | 94.76 | 94.75 | 94.74 | 94.74 | 94.73 |
| 21.500 | 94.72 | 94.71 | 94.70 | 94.70 | 94.69 |
| 21.750 | 94.68 | 94.67 | 94.66 | 94.65 | 94.65 |
| 22.000 | 94.64 | 94.63 | 94.62 | 94.61 | 94.60 |
| 22.250 | 94.59 | 94.59 | 94.58 | 94.57 | 94.56 |
| 22.500 | 94.55 | 94.54 | 94.53 | 94.52 | 94.51 |
| 22.750 | 94.51 | 94.50 | 94.49 | 94.48 | 94.47 |
| 23.000 | 94.46 | 94.45 | 94.44 | 94.43 | 94.42 |
| 23.250 | 94.41 | 94.40 | 94.39 | 94.38 | 94.37 |
| 23.500 | 94.36 | 94.36 | 94.35 | 94.34 | 94.33 |
| 23.750 | 94.32 | 94.31 | 94.30 | 94.29 | 94.28 |
| 24.000 | 94.27 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation
 Label: 6" Depth Green Roof (OUT)
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation
 Label: 6" Depth Green Roof (OUT)
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 10.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.750 | 93.00 | 93.02 | 93.03 | 93.04 | 93.06 |
| 12.000 | 93.11 | 93.16 | 93.21 | 93.24 | 93.26 |
| 12.250 | 93.27 | 93.28 | 93.29 | 93.29 | 93.29 |
| 12.500 | 93.29 | 93.28 | 93.27 | 93.26 | 93.25 |
| 12.750 | 93.24 | 93.23 | 93.22 | 93.21 | 93.20 |
| 13.000 | 93.18 | 93.17 | 93.15 | 93.13 | 93.11 |
| 13.250 | 93.09 | 93.06 | 93.04 | 93.00 | 93.00 |
| 13.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 13.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 14.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 14.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 14.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 14.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 15.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 15.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 15.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 15.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation
 Label: 6" Depth Green Roof (OUT)
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 20.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 24.000 | 93.00 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.500 | 93.00 | 93.00 | 93.00 | 93.02 | 93.04 |
| 11.750 | 93.06 | 93.09 | 93.13 | 93.17 | 93.22 |
| 12.000 | 93.28 | 93.35 | 93.43 | 93.50 | 93.56 |
| 12.250 | 93.60 | 93.62 | 93.64 | 93.66 | 93.67 |
| 12.500 | 93.67 | 93.68 | 93.68 | 93.67 | 93.67 |
| 12.750 | 93.67 | 93.66 | 93.66 | 93.65 | 93.65 |
| 13.000 | 93.64 | 93.64 | 93.63 | 93.62 | 93.62 |
| 13.250 | 93.61 | 93.60 | 93.60 | 93.59 | 93.58 |
| 13.500 | 93.57 | 93.56 | 93.55 | 93.54 | 93.53 |
| 13.750 | 93.52 | 93.51 | 93.50 | 93.49 | 93.48 |
| 14.000 | 93.47 | 93.46 | 93.45 | 93.44 | 93.43 |
| 14.250 | 93.42 | 93.40 | 93.39 | 93.38 | 93.37 |
| 14.500 | 93.36 | 93.35 | 93.34 | 93.32 | 93.31 |
| 14.750 | 93.30 | 93.29 | 93.28 | 93.27 | 93.25 |
| 15.000 | 93.24 | 93.23 | 93.22 | 93.20 | 93.19 |
| 15.250 | 93.17 | 93.15 | 93.13 | 93.11 | 93.08 |
| 15.500 | 93.06 | 93.03 | 93.00 | 93.00 | 93.00 |
| 15.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 20.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 24.000 | 93.00 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.500 | 93.00 | 93.02 | 93.03 | 93.04 | 93.07 |
| 11.750 | 93.11 | 93.15 | 93.20 | 93.24 | 93.29 |
| 12.000 | 93.37 | 93.46 | 93.57 | 93.65 | 93.71 |
| 12.250 | 93.72 | 93.72 | 93.72 | 93.72 | 93.72 |
| 12.500 | 93.71 | 93.71 | 93.71 | 93.71 | 93.71 |
| 12.750 | 93.71 | 93.71 | 93.71 | 93.71 | 93.70 |
| 13.000 | 93.70 | 93.70 | 93.69 | 93.69 | 93.69 |
| 13.250 | 93.68 | 93.67 | 93.67 | 93.66 | 93.66 |
| 13.500 | 93.65 | 93.65 | 93.64 | 93.63 | 93.63 |
| 13.750 | 93.62 | 93.61 | 93.61 | 93.60 | 93.59 |
| 14.000 | 93.58 | 93.57 | 93.57 | 93.56 | 93.55 |
| 14.250 | 93.54 | 93.53 | 93.52 | 93.51 | 93.50 |
| 14.500 | 93.49 | 93.48 | 93.47 | 93.46 | 93.45 |
| 14.750 | 93.44 | 93.43 | 93.42 | 93.40 | 93.39 |
| 15.000 | 93.38 | 93.37 | 93.36 | 93.35 | 93.34 |
| 15.250 | 93.33 | 93.32 | 93.30 | 93.29 | 93.28 |
| 15.500 | 93.27 | 93.26 | 93.25 | 93.23 | 93.22 |
| 15.750 | 93.21 | 93.20 | 93.18 | 93.16 | 93.14 |
| 16.000 | 93.12 | 93.10 | 93.07 | 93.04 | 93.02 |
| 16.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 16.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 20.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 24.000 | 93.00 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 0.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 1.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 2.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 3.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 4.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 5.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 6.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 7.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 8.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 9.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 10.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 10.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 11.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.02 |
| 11.250 | 93.02 | 93.03 | 93.03 | 93.04 | 93.05 |
| 11.500 | 93.07 | 93.08 | 93.11 | 93.14 | 93.18 |
| 11.750 | 93.22 | 93.27 | 93.32 | 93.39 | 93.47 |
| 12.000 | 93.58 | 93.70 | 93.75 | 93.75 | 93.74 |
| 12.250 | 93.73 | 93.73 | 93.72 | 93.72 | 93.72 |
| 12.500 | 93.72 | 93.71 | 93.71 | 93.71 | 93.71 |
| 12.750 | 93.71 | 93.71 | 93.71 | 93.71 | 93.71 |
| 13.000 | 93.71 | 93.71 | 93.71 | 93.71 | 93.71 |
| 13.250 | 93.71 | 93.71 | 93.71 | 93.70 | 93.70 |
| 13.500 | 93.70 | 93.70 | 93.70 | 93.69 | 93.69 |
| 13.750 | 93.69 | 93.68 | 93.68 | 93.67 | 93.67 |
| 14.000 | 93.66 | 93.66 | 93.66 | 93.65 | 93.64 |
| 14.250 | 93.64 | 93.63 | 93.63 | 93.62 | 93.62 |
| 14.500 | 93.61 | 93.61 | 93.60 | 93.59 | 93.59 |
| 14.750 | 93.58 | 93.57 | 93.56 | 93.55 | 93.54 |
| 15.000 | 93.54 | 93.53 | 93.52 | 93.51 | 93.50 |
| 15.250 | 93.49 | 93.48 | 93.47 | 93.47 | 93.46 |
| 15.500 | 93.45 | 93.44 | 93.43 | 93.42 | 93.41 |
| 15.750 | 93.40 | 93.39 | 93.38 | 93.37 | 93.35 |
| 16.000 | 93.34 | 93.33 | 93.32 | 93.31 | 93.30 |
| 16.250 | 93.29 | 93.28 | 93.27 | 93.25 | 93.24 |
| 16.500 | 93.23 | 93.22 | 93.21 | 93.19 | 93.18 |
| 16.750 | 93.16 | 93.14 | 93.12 | 93.10 | 93.08 |
| 17.000 | 93.05 | 93.03 | 93.00 | 93.00 | 93.00 |
| 17.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 17.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 18.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 19.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 20.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 21.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 22.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.000 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.250 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.500 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 23.750 | 93.00 | 93.00 | 93.00 | 93.00 | 93.00 |
| 24.000 | 93.00 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 71.50 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.250 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.500 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.750 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.000 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.250 | 71.51 | 71.50 | 71.50 | 71.50 | 71.50 |
| 1.500 | 71.50 | 71.50 | 71.50 | 71.50 | 71.50 |
| 1.750 | 71.50 | 71.50 | 71.50 | 71.50 | 71.50 |
| 2.000 | 71.50 | 71.50 | 71.51 | 71.51 | 71.51 |
| 2.250 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 2.500 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 2.750 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 3.000 | 71.52 | 71.52 | 71.52 | 71.52 | 71.52 |
| 3.250 | 71.52 | 71.52 | 71.52 | 71.52 | 71.52 |
| 3.500 | 71.52 | 71.52 | 71.53 | 71.53 | 71.53 |
| 3.750 | 71.53 | 71.53 | 71.53 | 71.53 | 71.53 |
| 4.000 | 71.53 | 71.53 | 71.54 | 71.54 | 71.54 |
| 4.250 | 71.54 | 71.54 | 71.54 | 71.54 | 71.54 |
| 4.500 | 71.54 | 71.55 | 71.55 | 71.55 | 71.55 |
| 4.750 | 71.55 | 71.55 | 71.55 | 71.55 | 71.56 |
| 5.000 | 71.56 | 71.56 | 71.56 | 71.56 | 71.56 |
| 5.250 | 71.56 | 71.56 | 71.56 | 71.57 | 71.57 |
| 5.500 | 71.57 | 71.57 | 71.57 | 71.57 | 71.57 |
| 5.750 | 71.57 | 71.58 | 71.58 | 71.58 | 71.58 |
| 6.000 | 71.58 | 71.58 | 71.58 | 71.58 | 71.59 |
| 6.250 | 71.59 | 71.59 | 71.59 | 71.59 | 71.59 |
| 6.500 | 71.59 | 71.60 | 71.60 | 71.60 | 71.60 |
| 6.750 | 71.60 | 71.60 | 71.61 | 71.61 | 71.61 |
| 7.000 | 71.61 | 71.61 | 71.62 | 71.62 | 71.62 |
| 7.250 | 71.62 | 71.62 | 71.63 | 71.63 | 71.63 |
| 7.500 | 71.63 | 71.63 | 71.64 | 71.64 | 71.64 |
| 7.750 | 71.64 | 71.65 | 71.65 | 71.65 | 71.65 |
| 8.000 | 71.66 | 71.66 | 71.66 | 71.66 | 71.67 |
| 8.250 | 71.67 | 71.67 | 71.67 | 71.68 | 71.68 |
| 8.500 | 71.68 | 71.69 | 71.69 | 71.69 | 71.70 |
| 8.750 | 71.70 | 71.70 | 71.71 | 71.71 | 71.72 |
| 9.000 | 71.72 | 71.73 | 71.73 | 71.73 | 71.74 |
| 9.250 | 71.74 | 71.75 | 71.75 | 71.76 | 71.76 |
| 9.500 | 71.77 | 71.77 | 71.78 | 71.78 | 71.79 |
| 9.750 | 71.79 | 71.80 | 71.80 | 71.81 | 71.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 71.82 | 71.82 | 71.83 | 71.83 | 71.84 |
| 10.250 | 71.85 | 71.85 | 71.86 | 71.87 | 71.87 |
| 10.500 | 71.88 | 71.89 | 71.89 | 71.90 | 71.91 |
| 10.750 | 71.92 | 71.93 | 71.93 | 71.94 | 71.95 |
| 11.000 | 71.96 | 71.97 | 71.98 | 71.99 | 72.00 |
| 11.250 | 72.01 | 72.02 | 72.03 | 72.04 | 72.05 |
| 11.500 | 72.06 | 72.07 | 72.08 | 72.09 | 72.11 |
| 11.750 | 72.13 | 72.14 | 72.16 | 72.18 | 72.20 |
| 12.000 | 72.22 | 72.24 | 72.26 | 72.29 | 72.31 |
| 12.250 | 72.33 | 72.35 | 72.37 | 72.39 | 72.40 |
| 12.500 | 72.42 | 72.44 | 72.45 | 72.47 | 72.48 |
| 12.750 | 72.49 | 72.51 | 72.52 | 72.53 | 72.54 |
| 13.000 | 72.55 | 72.56 | 72.57 | 72.58 | 72.59 |
| 13.250 | 72.60 | 72.61 | 72.61 | 72.62 | 72.63 |
| 13.500 | 72.63 | 72.64 | 72.64 | 72.64 | 72.64 |
| 13.750 | 72.65 | 72.65 | 72.65 | 72.66 | 72.66 |
| 14.000 | 72.66 | 72.66 | 72.66 | 72.67 | 72.67 |
| 14.250 | 72.67 | 72.67 | 72.68 | 72.68 | 72.68 |
| 14.500 | 72.68 | 72.68 | 72.69 | 72.69 | 72.69 |
| 14.750 | 72.69 | 72.69 | 72.70 | 72.70 | 72.70 |
| 15.000 | 72.70 | 72.70 | 72.70 | 72.71 | 72.71 |
| 15.250 | 72.71 | 72.71 | 72.71 | 72.71 | 72.72 |
| 15.500 | 72.72 | 72.72 | 72.72 | 72.72 | 72.72 |
| 15.750 | 72.72 | 72.72 | 72.73 | 72.73 | 72.73 |
| 16.000 | 72.73 | 72.73 | 72.73 | 72.73 | 72.73 |
| 16.250 | 72.73 | 72.73 | 72.74 | 72.74 | 72.74 |
| 16.500 | 72.74 | 72.74 | 72.73 | 72.73 | 72.72 |
| 16.750 | 72.72 | 72.71 | 72.70 | 72.70 | 72.69 |
| 17.000 | 72.69 | 72.68 | 72.67 | 72.67 | 72.66 |
| 17.250 | 72.66 | 72.65 | 72.64 | 72.64 | 72.63 |
| 17.500 | 72.63 | 72.62 | 72.61 | 72.61 | 72.60 |
| 17.750 | 72.60 | 72.59 | 72.59 | 72.58 | 72.57 |
| 18.000 | 72.57 | 72.56 | 72.56 | 72.55 | 72.55 |
| 18.250 | 72.54 | 72.53 | 72.53 | 72.52 | 72.52 |
| 18.500 | 72.51 | 72.51 | 72.50 | 72.50 | 72.49 |
| 18.750 | 72.48 | 72.47 | 72.47 | 72.46 | 72.45 |
| 19.000 | 72.45 | 72.44 | 72.43 | 72.43 | 72.42 |
| 19.250 | 72.41 | 72.41 | 72.40 | 72.39 | 72.39 |
| 19.500 | 72.38 | 72.38 | 72.37 | 72.36 | 72.36 |
| 19.750 | 72.35 | 72.35 | 72.34 | 72.34 | 72.33 |
| 20.000 | 72.33 | 72.32 | 72.31 | 72.29 | 72.28 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 72.27 | 72.26 | 72.25 | 72.24 | 72.23 |
| 20.500 | 72.22 | 72.21 | 72.20 | 72.19 | 72.18 |
| 20.750 | 72.17 | 72.16 | 72.15 | 72.14 | 72.13 |
| 21.000 | 72.12 | 72.11 | 72.10 | 72.09 | 72.08 |
| 21.250 | 72.07 | 72.06 | 72.05 | 72.04 | 72.04 |
| 21.500 | 72.03 | 72.02 | 72.01 | 72.00 | 71.99 |
| 21.750 | 71.98 | 71.97 | 71.95 | 71.94 | 71.93 |
| 22.000 | 71.92 | 71.91 | 71.90 | 71.89 | 71.88 |
| 22.250 | 71.87 | 71.86 | 71.86 | 71.85 | 71.84 |
| 22.500 | 71.83 | 71.82 | 71.82 | 71.81 | 71.80 |
| 22.750 | 71.80 | 71.79 | 71.78 | 71.78 | 71.77 |
| 23.000 | 71.77 | 71.76 | 71.76 | 71.75 | 71.75 |
| 23.250 | 71.74 | 71.74 | 71.73 | 71.73 | 71.72 |
| 23.500 | 71.72 | 71.72 | 71.71 | 71.71 | 71.70 |
| 23.750 | 71.70 | 71.70 | 71.69 | 71.69 | 71.69 |
| 24.000 | 71.68 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 71.50 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.250 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.500 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.750 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.000 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.250 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.500 | 71.51 | 71.51 | 71.52 | 71.52 | 71.52 |
| 1.750 | 71.52 | 71.52 | 71.52 | 71.53 | 71.53 |
| 2.000 | 71.53 | 71.53 | 71.53 | 71.53 | 71.54 |
| 2.250 | 71.54 | 71.54 | 71.54 | 71.54 | 71.54 |
| 2.500 | 71.55 | 71.55 | 71.55 | 71.55 | 71.56 |
| 2.750 | 71.56 | 71.56 | 71.56 | 71.56 | 71.57 |
| 3.000 | 71.57 | 71.57 | 71.57 | 71.57 | 71.58 |
| 3.250 | 71.58 | 71.58 | 71.58 | 71.59 | 71.59 |
| 3.500 | 71.59 | 71.59 | 71.60 | 71.60 | 71.60 |
| 3.750 | 71.60 | 71.60 | 71.61 | 71.61 | 71.61 |
| 4.000 | 71.61 | 71.62 | 71.62 | 71.62 | 71.62 |
| 4.250 | 71.63 | 71.63 | 71.63 | 71.63 | 71.64 |
| 4.500 | 71.64 | 71.64 | 71.64 | 71.64 | 71.65 |
| 4.750 | 71.65 | 71.65 | 71.65 | 71.66 | 71.66 |
| 5.000 | 71.66 | 71.66 | 71.67 | 71.67 | 71.67 |
| 5.250 | 71.67 | 71.67 | 71.68 | 71.68 | 71.68 |
| 5.500 | 71.68 | 71.69 | 71.69 | 71.69 | 71.69 |
| 5.750 | 71.69 | 71.70 | 71.70 | 71.70 | 71.70 |
| 6.000 | 71.71 | 71.71 | 71.71 | 71.71 | 71.71 |
| 6.250 | 71.72 | 71.72 | 71.72 | 71.72 | 71.73 |
| 6.500 | 71.73 | 71.73 | 71.74 | 71.74 | 71.74 |
| 6.750 | 71.75 | 71.75 | 71.75 | 71.76 | 71.76 |
| 7.000 | 71.76 | 71.77 | 71.77 | 71.77 | 71.78 |
| 7.250 | 71.78 | 71.79 | 71.79 | 71.79 | 71.80 |
| 7.500 | 71.80 | 71.81 | 71.81 | 71.81 | 71.82 |
| 7.750 | 71.82 | 71.83 | 71.83 | 71.83 | 71.84 |
| 8.000 | 71.84 | 71.85 | 71.85 | 71.86 | 71.86 |
| 8.250 | 71.87 | 71.87 | 71.88 | 71.88 | 71.89 |
| 8.500 | 71.90 | 71.90 | 71.91 | 71.92 | 71.92 |
| 8.750 | 71.93 | 71.94 | 71.94 | 71.95 | 71.96 |
| 9.000 | 71.97 | 71.97 | 71.98 | 71.99 | 72.00 |
| 9.250 | 72.01 | 72.01 | 72.02 | 72.02 | 72.03 |
| 9.500 | 72.04 | 72.04 | 72.05 | 72.06 | 72.06 |
| 9.750 | 72.07 | 72.08 | 72.08 | 72.09 | 72.10 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 72.11 | 72.11 | 72.12 | 72.13 | 72.14 |
| 10.250 | 72.15 | 72.16 | 72.16 | 72.17 | 72.18 |
| 10.500 | 72.19 | 72.20 | 72.21 | 72.22 | 72.23 |
| 10.750 | 72.24 | 72.25 | 72.26 | 72.28 | 72.29 |
| 11.000 | 72.30 | 72.31 | 72.32 | 72.33 | 72.34 |
| 11.250 | 72.35 | 72.36 | 72.38 | 72.39 | 72.40 |
| 11.500 | 72.41 | 72.43 | 72.44 | 72.46 | 72.48 |
| 11.750 | 72.49 | 72.51 | 72.52 | 72.54 | 72.55 |
| 12.000 | 72.57 | 72.59 | 72.62 | 72.64 | 72.70 |
| 12.250 | 72.78 | 72.85 | 72.90 | 72.95 | 72.99 |
| 12.500 | 73.02 | 73.04 | 73.05 | 73.07 | 73.08 |
| 12.750 | 73.09 | 73.09 | 73.10 | 73.11 | 73.11 |
| 13.000 | 73.12 | 73.12 | 73.12 | 73.12 | 73.12 |
| 13.250 | 73.13 | 73.13 | 73.13 | 73.13 | 73.13 |
| 13.500 | 73.13 | 73.13 | 73.13 | 73.13 | 73.13 |
| 13.750 | 73.13 | 73.13 | 73.13 | 73.13 | 73.12 |
| 14.000 | 73.12 | 73.12 | 73.12 | 73.12 | 73.12 |
| 14.250 | 73.11 | 73.11 | 73.11 | 73.11 | 73.11 |
| 14.500 | 73.10 | 73.10 | 73.10 | 73.10 | 73.10 |
| 14.750 | 73.09 | 73.09 | 73.09 | 73.09 | 73.09 |
| 15.000 | 73.08 | 73.08 | 73.08 | 73.08 | 73.08 |
| 15.250 | 73.08 | 73.08 | 73.07 | 73.07 | 73.07 |
| 15.500 | 73.07 | 73.07 | 73.07 | 73.06 | 73.05 |
| 15.750 | 73.05 | 73.04 | 73.03 | 73.02 | 73.02 |
| 16.000 | 73.01 | 73.01 | 73.00 | 72.99 | 72.99 |
| 16.250 | 72.98 | 72.98 | 72.97 | 72.97 | 72.96 |
| 16.500 | 72.96 | 72.95 | 72.95 | 72.94 | 72.94 |
| 16.750 | 72.94 | 72.93 | 72.93 | 72.92 | 72.92 |
| 17.000 | 72.92 | 72.91 | 72.91 | 72.91 | 72.90 |
| 17.250 | 72.90 | 72.90 | 72.89 | 72.89 | 72.89 |
| 17.500 | 72.88 | 72.88 | 72.88 | 72.88 | 72.87 |
| 17.750 | 72.87 | 72.87 | 72.87 | 72.86 | 72.86 |
| 18.000 | 72.86 | 72.86 | 72.86 | 72.85 | 72.85 |
| 18.250 | 72.85 | 72.85 | 72.85 | 72.84 | 72.84 |
| 18.500 | 72.84 | 72.84 | 72.84 | 72.83 | 72.83 |
| 18.750 | 72.83 | 72.83 | 72.83 | 72.83 | 72.83 |
| 19.000 | 72.82 | 72.82 | 72.82 | 72.82 | 72.82 |
| 19.250 | 72.82 | 72.82 | 72.82 | 72.82 | 72.81 |
| 19.500 | 72.81 | 72.81 | 72.81 | 72.81 | 72.81 |
| 19.750 | 72.81 | 72.81 | 72.81 | 72.81 | 72.80 |
| 20.000 | 72.80 | 72.80 | 72.80 | 72.80 | 72.80 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 72.80 | 72.80 | 72.80 | 72.80 | 72.80 |
| 20.500 | 72.80 | 72.80 | 72.80 | 72.80 | 72.79 |
| 20.750 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 21.000 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 21.250 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 21.500 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 21.750 | 72.78 | 72.78 | 72.78 | 72.78 | 72.78 |
| 22.000 | 72.78 | 72.78 | 72.78 | 72.78 | 72.78 |
| 22.250 | 72.78 | 72.78 | 72.78 | 72.78 | 72.78 |
| 22.500 | 72.78 | 72.77 | 72.76 | 72.75 | 72.75 |
| 22.750 | 72.74 | 72.73 | 72.73 | 72.72 | 72.71 |
| 23.000 | 72.71 | 72.70 | 72.70 | 72.69 | 72.68 |
| 23.250 | 72.68 | 72.67 | 72.66 | 72.66 | 72.65 |
| 23.500 | 72.64 | 72.64 | 72.63 | 72.63 | 72.62 |
| 23.750 | 72.61 | 72.61 | 72.60 | 72.60 | 72.59 |
| 24.000 | 72.58 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 71.50 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.250 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.500 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.750 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.000 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 1.250 | 71.52 | 71.52 | 71.52 | 71.52 | 71.52 |
| 1.500 | 71.53 | 71.53 | 71.53 | 71.53 | 71.54 |
| 1.750 | 71.54 | 71.54 | 71.54 | 71.55 | 71.55 |
| 2.000 | 71.55 | 71.55 | 71.56 | 71.56 | 71.56 |
| 2.250 | 71.56 | 71.57 | 71.57 | 71.57 | 71.57 |
| 2.500 | 71.58 | 71.58 | 71.58 | 71.59 | 71.59 |
| 2.750 | 71.59 | 71.60 | 71.60 | 71.60 | 71.60 |
| 3.000 | 71.61 | 71.61 | 71.61 | 71.62 | 71.62 |
| 3.250 | 71.62 | 71.62 | 71.63 | 71.63 | 71.63 |
| 3.500 | 71.64 | 71.64 | 71.64 | 71.65 | 71.65 |
| 3.750 | 71.65 | 71.66 | 71.66 | 71.66 | 71.66 |
| 4.000 | 71.67 | 71.67 | 71.67 | 71.68 | 71.68 |
| 4.250 | 71.68 | 71.69 | 71.69 | 71.69 | 71.69 |
| 4.500 | 71.70 | 71.70 | 71.70 | 71.71 | 71.71 |
| 4.750 | 71.71 | 71.71 | 71.72 | 71.72 | 71.72 |
| 5.000 | 71.73 | 71.73 | 71.73 | 71.73 | 71.74 |
| 5.250 | 71.74 | 71.74 | 71.75 | 71.75 | 71.75 |
| 5.500 | 71.75 | 71.76 | 71.76 | 71.76 | 71.77 |
| 5.750 | 71.77 | 71.77 | 71.77 | 71.78 | 71.78 |
| 6.000 | 71.78 | 71.78 | 71.79 | 71.79 | 71.79 |
| 6.250 | 71.80 | 71.80 | 71.80 | 71.80 | 71.81 |
| 6.500 | 71.81 | 71.82 | 71.82 | 71.82 | 71.83 |
| 6.750 | 71.83 | 71.84 | 71.84 | 71.84 | 71.85 |
| 7.000 | 71.85 | 71.86 | 71.86 | 71.87 | 71.87 |
| 7.250 | 71.88 | 71.88 | 71.89 | 71.89 | 71.90 |
| 7.500 | 71.90 | 71.91 | 71.91 | 71.92 | 71.92 |
| 7.750 | 71.93 | 71.93 | 71.94 | 71.94 | 71.95 |
| 8.000 | 71.95 | 71.96 | 71.97 | 71.97 | 71.98 |
| 8.250 | 71.98 | 71.99 | 72.00 | 72.00 | 72.01 |
| 8.500 | 72.01 | 72.02 | 72.02 | 72.03 | 72.04 |
| 8.750 | 72.04 | 72.05 | 72.06 | 72.06 | 72.07 |
| 9.000 | 72.08 | 72.09 | 72.09 | 72.10 | 72.11 |
| 9.250 | 72.12 | 72.13 | 72.13 | 72.14 | 72.15 |
| 9.500 | 72.16 | 72.17 | 72.18 | 72.19 | 72.19 |
| 9.750 | 72.20 | 72.21 | 72.22 | 72.23 | 72.24 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 72.25 | 72.26 | 72.27 | 72.28 | 72.29 |
| 10.250 | 72.30 | 72.31 | 72.32 | 72.33 | 72.34 |
| 10.500 | 72.35 | 72.36 | 72.37 | 72.39 | 72.40 |
| 10.750 | 72.41 | 72.42 | 72.43 | 72.44 | 72.45 |
| 11.000 | 72.46 | 72.47 | 72.48 | 72.49 | 72.50 |
| 11.250 | 72.51 | 72.52 | 72.53 | 72.54 | 72.55 |
| 11.500 | 72.56 | 72.57 | 72.59 | 72.60 | 72.61 |
| 11.750 | 72.62 | 72.64 | 72.65 | 72.67 | 72.69 |
| 12.000 | 72.71 | 72.75 | 72.87 | 73.03 | 73.16 |
| 12.250 | 73.27 | 73.37 | 73.47 | 73.57 | 73.65 |
| 12.500 | 73.72 | 73.77 | 73.80 | 73.82 | 73.84 |
| 12.750 | 73.85 | 73.86 | 73.86 | 73.86 | 73.86 |
| 13.000 | 73.86 | 73.85 | 73.85 | 73.84 | 73.83 |
| 13.250 | 73.82 | 73.81 | 73.80 | 73.79 | 73.77 |
| 13.500 | 73.76 | 73.75 | 73.74 | 73.73 | 73.71 |
| 13.750 | 73.70 | 73.69 | 73.67 | 73.66 | 73.65 |
| 14.000 | 73.63 | 73.62 | 73.60 | 73.59 | 73.57 |
| 14.250 | 73.56 | 73.55 | 73.53 | 73.52 | 73.50 |
| 14.500 | 73.49 | 73.48 | 73.47 | 73.45 | 73.44 |
| 14.750 | 73.43 | 73.42 | 73.41 | 73.40 | 73.39 |
| 15.000 | 73.38 | 73.37 | 73.36 | 73.35 | 73.34 |
| 15.250 | 73.33 | 73.32 | 73.31 | 73.30 | 73.29 |
| 15.500 | 73.29 | 73.28 | 73.27 | 73.26 | 73.25 |
| 15.750 | 73.25 | 73.24 | 73.23 | 73.23 | 73.22 |
| 16.000 | 73.21 | 73.21 | 73.20 | 73.20 | 73.19 |
| 16.250 | 73.18 | 73.17 | 73.16 | 73.15 | 73.14 |
| 16.500 | 73.13 | 73.12 | 73.11 | 73.10 | 73.09 |
| 16.750 | 73.09 | 73.08 | 73.07 | 73.06 | 73.05 |
| 17.000 | 73.05 | 73.04 | 73.03 | 73.02 | 73.02 |
| 17.250 | 73.01 | 73.01 | 73.00 | 72.99 | 72.99 |
| 17.500 | 72.98 | 72.98 | 72.97 | 72.97 | 72.96 |
| 17.750 | 72.96 | 72.95 | 72.95 | 72.94 | 72.94 |
| 18.000 | 72.93 | 72.93 | 72.93 | 72.92 | 72.92 |
| 18.250 | 72.92 | 72.91 | 72.91 | 72.90 | 72.90 |
| 18.500 | 72.90 | 72.90 | 72.89 | 72.89 | 72.89 |
| 18.750 | 72.88 | 72.88 | 72.88 | 72.88 | 72.87 |
| 19.000 | 72.87 | 72.87 | 72.87 | 72.86 | 72.86 |
| 19.250 | 72.86 | 72.86 | 72.86 | 72.85 | 72.85 |
| 19.500 | 72.85 | 72.85 | 72.85 | 72.84 | 72.84 |
| 19.750 | 72.84 | 72.84 | 72.84 | 72.84 | 72.84 |
| 20.000 | 72.83 | 72.83 | 72.83 | 72.83 | 72.83 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 72.83 | 72.83 | 72.82 | 72.82 | 72.82 |
| 20.500 | 72.82 | 72.82 | 72.82 | 72.82 | 72.82 |
| 20.750 | 72.82 | 72.82 | 72.81 | 72.81 | 72.81 |
| 21.000 | 72.81 | 72.81 | 72.81 | 72.81 | 72.81 |
| 21.250 | 72.81 | 72.81 | 72.81 | 72.81 | 72.80 |
| 21.500 | 72.80 | 72.80 | 72.80 | 72.80 | 72.80 |
| 21.750 | 72.80 | 72.80 | 72.80 | 72.80 | 72.80 |
| 22.000 | 72.80 | 72.80 | 72.80 | 72.80 | 72.80 |
| 22.250 | 72.80 | 72.79 | 72.79 | 72.79 | 72.79 |
| 22.500 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 22.750 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 23.000 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 23.250 | 72.79 | 72.79 | 72.79 | 72.79 | 72.79 |
| 23.500 | 72.79 | 72.79 | 72.78 | 72.78 | 72.78 |
| 23.750 | 72.78 | 72.78 | 72.77 | 72.76 | 72.76 |
| 24.000 | 72.75 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 71.50 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.250 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.500 | 71.51 | 71.51 | 71.51 | 71.51 | 71.51 |
| 0.750 | 71.51 | 71.51 | 71.52 | 71.52 | 71.52 |
| 1.000 | 71.52 | 71.53 | 71.53 | 71.53 | 71.54 |
| 1.250 | 71.54 | 71.55 | 71.55 | 71.55 | 71.56 |
| 1.500 | 71.56 | 71.57 | 71.57 | 71.58 | 71.58 |
| 1.750 | 71.58 | 71.59 | 71.59 | 71.60 | 71.60 |
| 2.000 | 71.61 | 71.61 | 71.62 | 71.62 | 71.62 |
| 2.250 | 71.63 | 71.63 | 71.64 | 71.64 | 71.65 |
| 2.500 | 71.65 | 71.66 | 71.66 | 71.66 | 71.67 |
| 2.750 | 71.67 | 71.68 | 71.68 | 71.69 | 71.69 |
| 3.000 | 71.70 | 71.70 | 71.70 | 71.71 | 71.71 |
| 3.250 | 71.72 | 71.72 | 71.73 | 71.73 | 71.74 |
| 3.500 | 71.74 | 71.74 | 71.75 | 71.75 | 71.76 |
| 3.750 | 71.76 | 71.77 | 71.77 | 71.77 | 71.78 |
| 4.000 | 71.78 | 71.79 | 71.79 | 71.79 | 71.80 |
| 4.250 | 71.80 | 71.81 | 71.81 | 71.82 | 71.82 |
| 4.500 | 71.82 | 71.83 | 71.83 | 71.84 | 71.84 |
| 4.750 | 71.84 | 71.85 | 71.85 | 71.86 | 71.86 |
| 5.000 | 71.86 | 71.87 | 71.87 | 71.87 | 71.88 |
| 5.250 | 71.88 | 71.89 | 71.89 | 71.89 | 71.90 |
| 5.500 | 71.90 | 71.90 | 71.91 | 71.91 | 71.92 |
| 5.750 | 71.92 | 71.92 | 71.93 | 71.93 | 71.93 |
| 6.000 | 71.94 | 71.94 | 71.94 | 71.95 | 71.95 |
| 6.250 | 71.96 | 71.96 | 71.97 | 71.97 | 71.97 |
| 6.500 | 71.98 | 71.99 | 71.99 | 72.00 | 72.00 |
| 6.750 | 72.00 | 72.01 | 72.01 | 72.02 | 72.02 |
| 7.000 | 72.03 | 72.03 | 72.03 | 72.04 | 72.04 |
| 7.250 | 72.05 | 72.06 | 72.06 | 72.07 | 72.07 |
| 7.500 | 72.08 | 72.08 | 72.09 | 72.10 | 72.10 |
| 7.750 | 72.11 | 72.12 | 72.12 | 72.13 | 72.14 |
| 8.000 | 72.14 | 72.15 | 72.16 | 72.17 | 72.17 |
| 8.250 | 72.18 | 72.19 | 72.20 | 72.20 | 72.21 |
| 8.500 | 72.22 | 72.23 | 72.24 | 72.25 | 72.26 |
| 8.750 | 72.27 | 72.28 | 72.28 | 72.29 | 72.31 |
| 9.000 | 72.32 | 72.33 | 72.34 | 72.35 | 72.36 |
| 9.250 | 72.37 | 72.38 | 72.39 | 72.40 | 72.41 |
| 9.500 | 72.42 | 72.43 | 72.44 | 72.45 | 72.46 |
| 9.750 | 72.47 | 72.48 | 72.49 | 72.50 | 72.51 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 72.51 | 72.52 | 72.53 | 72.54 | 72.54 |
| 10.250 | 72.55 | 72.56 | 72.57 | 72.58 | 72.59 |
| 10.500 | 72.59 | 72.60 | 72.61 | 72.62 | 72.63 |
| 10.750 | 72.64 | 72.65 | 72.66 | 72.66 | 72.67 |
| 11.000 | 72.68 | 72.69 | 72.70 | 72.71 | 72.72 |
| 11.250 | 72.73 | 72.75 | 72.76 | 72.77 | 72.78 |
| 11.500 | 72.79 | 72.80 | 72.81 | 72.82 | 72.83 |
| 11.750 | 72.85 | 72.86 | 72.89 | 72.98 | 73.10 |
| 12.000 | 73.25 | 73.46 | 73.77 | 74.19 | 74.61 |
| 12.250 | 74.97 | 75.28 | 75.54 | 75.82 | 76.03 |
| 12.500 | 76.21 | 76.33 | 76.39 | 76.43 | 76.44 |
| 12.750 | 76.43 | 76.42 | 76.39 | 76.36 | 76.33 |
| 13.000 | 76.28 | 76.23 | 76.18 | 76.12 | 76.06 |
| 13.250 | 76.00 | 75.95 | 75.89 | 75.84 | 75.79 |
| 13.500 | 75.73 | 75.68 | 75.62 | 75.57 | 75.51 |
| 13.750 | 75.47 | 75.43 | 75.39 | 75.35 | 75.31 |
| 14.000 | 75.26 | 75.22 | 75.18 | 75.14 | 75.10 |
| 14.250 | 75.06 | 75.01 | 74.98 | 74.94 | 74.91 |
| 14.500 | 74.87 | 74.83 | 74.80 | 74.76 | 74.73 |
| 14.750 | 74.70 | 74.66 | 74.63 | 74.59 | 74.56 |
| 15.000 | 74.53 | 74.49 | 74.46 | 74.43 | 74.40 |
| 15.250 | 74.37 | 74.34 | 74.31 | 74.29 | 74.26 |
| 15.500 | 74.23 | 74.20 | 74.17 | 74.14 | 74.12 |
| 15.750 | 74.09 | 74.06 | 74.04 | 74.01 | 73.98 |
| 16.000 | 73.96 | 73.94 | 73.91 | 73.89 | 73.87 |
| 16.250 | 73.84 | 73.82 | 73.80 | 73.78 | 73.76 |
| 16.500 | 73.74 | 73.72 | 73.70 | 73.68 | 73.66 |
| 16.750 | 73.64 | 73.62 | 73.60 | 73.58 | 73.57 |
| 17.000 | 73.55 | 73.53 | 73.51 | 73.49 | 73.47 |
| 17.250 | 73.45 | 73.43 | 73.41 | 73.40 | 73.38 |
| 17.500 | 73.36 | 73.34 | 73.33 | 73.31 | 73.30 |
| 17.750 | 73.28 | 73.27 | 73.25 | 73.24 | 73.23 |
| 18.000 | 73.21 | 73.20 | 73.19 | 73.18 | 73.17 |
| 18.250 | 73.16 | 73.15 | 73.13 | 73.12 | 73.12 |
| 18.500 | 73.11 | 73.10 | 73.09 | 73.08 | 73.07 |
| 18.750 | 73.06 | 73.06 | 73.05 | 73.04 | 73.03 |
| 19.000 | 73.03 | 73.02 | 73.01 | 73.01 | 73.00 |
| 19.250 | 73.00 | 72.99 | 72.99 | 72.98 | 72.97 |
| 19.500 | 72.97 | 72.97 | 72.96 | 72.96 | 72.95 |
| 19.750 | 72.95 | 72.94 | 72.94 | 72.94 | 72.93 |
| 20.000 | 72.93 | 72.92 | 72.92 | 72.92 | 72.91 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 72.91 | 72.91 | 72.90 | 72.90 | 72.90 |
| 20.500 | 72.90 | 72.89 | 72.89 | 72.89 | 72.88 |
| 20.750 | 72.88 | 72.88 | 72.88 | 72.88 | 72.87 |
| 21.000 | 72.87 | 72.87 | 72.87 | 72.87 | 72.86 |
| 21.250 | 72.86 | 72.86 | 72.86 | 72.86 | 72.85 |
| 21.500 | 72.85 | 72.85 | 72.85 | 72.85 | 72.85 |
| 21.750 | 72.85 | 72.84 | 72.84 | 72.84 | 72.84 |
| 22.000 | 72.84 | 72.84 | 72.84 | 72.83 | 72.83 |
| 22.250 | 72.83 | 72.83 | 72.83 | 72.83 | 72.83 |
| 22.500 | 72.83 | 72.83 | 72.83 | 72.82 | 72.82 |
| 22.750 | 72.82 | 72.82 | 72.82 | 72.82 | 72.82 |
| 23.000 | 72.82 | 72.82 | 72.82 | 72.82 | 72.81 |
| 23.250 | 72.81 | 72.81 | 72.81 | 72.81 | 72.81 |
| 23.500 | 72.81 | 72.81 | 72.81 | 72.81 | 72.81 |
| 23.750 | 72.81 | 72.81 | 72.81 | 72.81 | 72.81 |
| 24.000 | 72.80 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 6.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 6.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 6.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 6.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 7.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 7.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 7.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 7.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 8.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 8.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 8.500 | 63.15 | 63.16 | 63.16 | 63.16 | 63.16 |
| 8.750 | 63.16 | 63.16 | 63.16 | 63.16 | 63.17 |
| 9.000 | 63.17 | 63.17 | 63.17 | 63.17 | 63.17 |
| 9.250 | 63.18 | 63.18 | 63.18 | 63.18 | 63.18 |
| 9.500 | 63.19 | 63.19 | 63.19 | 63.19 | 63.20 |
| 9.750 | 63.20 | 63.20 | 63.21 | 63.21 | 63.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 63.22 | 63.22 | 63.22 | 63.23 | 63.23 |
| 10.250 | 63.23 | 63.24 | 63.24 | 63.25 | 63.25 |
| 10.500 | 63.26 | 63.26 | 63.27 | 63.27 | 63.28 |
| 10.750 | 63.28 | 63.29 | 63.29 | 63.30 | 63.31 |
| 11.000 | 63.31 | 63.32 | 63.33 | 63.34 | 63.34 |
| 11.250 | 63.35 | 63.36 | 63.38 | 63.39 | 63.40 |
| 11.500 | 63.42 | 63.43 | 63.45 | 63.48 | 63.51 |
| 11.750 | 63.55 | 63.61 | 63.67 | 63.72 | 63.78 |
| 12.000 | 63.87 | 63.99 | 64.13 | 64.24 | 64.33 |
| 12.250 | 64.40 | 64.45 | 64.48 | 64.49 | 64.50 |
| 12.500 | 64.50 | 64.49 | 64.47 | 64.45 | 64.42 |
| 12.750 | 64.40 | 64.37 | 64.35 | 64.32 | 64.30 |
| 13.000 | 64.27 | 64.25 | 64.23 | 64.21 | 64.19 |
| 13.250 | 64.17 | 64.14 | 64.12 | 64.10 | 64.07 |
| 13.500 | 64.05 | 64.03 | 64.01 | 63.99 | 63.97 |
| 13.750 | 63.96 | 63.94 | 63.92 | 63.91 | 63.89 |
| 14.000 | 63.88 | 63.87 | 63.85 | 63.84 | 63.83 |
| 14.250 | 63.82 | 63.81 | 63.80 | 63.79 | 63.78 |
| 14.500 | 63.77 | 63.76 | 63.75 | 63.74 | 63.73 |
| 14.750 | 63.73 | 63.72 | 63.71 | 63.71 | 63.70 |
| 15.000 | 63.69 | 63.69 | 63.68 | 63.68 | 63.67 |
| 15.250 | 63.66 | 63.66 | 63.65 | 63.65 | 63.64 |
| 15.500 | 63.63 | 63.63 | 63.62 | 63.61 | 63.60 |
| 15.750 | 63.60 | 63.59 | 63.58 | 63.58 | 63.57 |
| 16.000 | 63.56 | 63.56 | 63.55 | 63.54 | 63.54 |
| 16.250 | 63.53 | 63.52 | 63.52 | 63.51 | 63.51 |
| 16.500 | 63.50 | 63.50 | 63.49 | 63.49 | 63.48 |
| 16.750 | 63.48 | 63.47 | 63.47 | 63.46 | 63.46 |
| 17.000 | 63.45 | 63.45 | 63.45 | 63.44 | 63.44 |
| 17.250 | 63.43 | 63.43 | 63.43 | 63.42 | 63.42 |
| 17.500 | 63.42 | 63.41 | 63.41 | 63.41 | 63.40 |
| 17.750 | 63.40 | 63.40 | 63.39 | 63.39 | 63.39 |
| 18.000 | 63.38 | 63.38 | 63.38 | 63.37 | 63.37 |
| 18.250 | 63.37 | 63.37 | 63.36 | 63.36 | 63.36 |
| 18.500 | 63.36 | 63.35 | 63.35 | 63.35 | 63.35 |
| 18.750 | 63.34 | 63.34 | 63.34 | 63.34 | 63.34 |
| 19.000 | 63.34 | 63.33 | 63.33 | 63.33 | 63.33 |
| 19.250 | 63.33 | 63.33 | 63.32 | 63.32 | 63.32 |
| 19.500 | 63.32 | 63.32 | 63.32 | 63.32 | 63.32 |
| 19.750 | 63.31 | 63.31 | 63.31 | 63.31 | 63.31 |
| 20.000 | 63.31 | 63.31 | 63.31 | 63.31 | 63.30 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 63.30 | 63.30 | 63.30 | 63.30 | 63.30 |
| 20.500 | 63.30 | 63.30 | 63.30 | 63.30 | 63.29 |
| 20.750 | 63.29 | 63.29 | 63.29 | 63.29 | 63.29 |
| 21.000 | 63.29 | 63.29 | 63.29 | 63.29 | 63.29 |
| 21.250 | 63.29 | 63.29 | 63.28 | 63.28 | 63.28 |
| 21.500 | 63.28 | 63.28 | 63.28 | 63.28 | 63.28 |
| 21.750 | 63.28 | 63.28 | 63.28 | 63.28 | 63.28 |
| 22.000 | 63.28 | 63.28 | 63.27 | 63.27 | 63.27 |
| 22.250 | 63.27 | 63.27 | 63.27 | 63.27 | 63.27 |
| 22.500 | 63.27 | 63.27 | 63.27 | 63.27 | 63.27 |
| 22.750 | 63.27 | 63.27 | 63.27 | 63.26 | 63.26 |
| 23.000 | 63.26 | 63.26 | 63.26 | 63.26 | 63.26 |
| 23.250 | 63.26 | 63.26 | 63.26 | 63.26 | 63.26 |
| 23.500 | 63.26 | 63.26 | 63.26 | 63.26 | 63.26 |
| 23.750 | 63.25 | 63.25 | 63.25 | 63.25 | 63.25 |
| 24.000 | 63.25 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 5.750 | 63.15 | 63.15 | 63.15 | 63.16 | 63.16 |
| 6.000 | 63.16 | 63.16 | 63.16 | 63.16 | 63.16 |
| 6.250 | 63.16 | 63.16 | 63.17 | 63.17 | 63.17 |
| 6.500 | 63.17 | 63.17 | 63.17 | 63.17 | 63.18 |
| 6.750 | 63.18 | 63.18 | 63.18 | 63.18 | 63.18 |
| 7.000 | 63.19 | 63.19 | 63.19 | 63.19 | 63.20 |
| 7.250 | 63.20 | 63.20 | 63.20 | 63.21 | 63.21 |
| 7.500 | 63.21 | 63.21 | 63.22 | 63.22 | 63.22 |
| 7.750 | 63.23 | 63.23 | 63.23 | 63.23 | 63.24 |
| 8.000 | 63.24 | 63.24 | 63.25 | 63.25 | 63.26 |
| 8.250 | 63.26 | 63.26 | 63.27 | 63.27 | 63.28 |
| 8.500 | 63.28 | 63.29 | 63.29 | 63.30 | 63.30 |
| 8.750 | 63.31 | 63.31 | 63.32 | 63.32 | 63.33 |
| 9.000 | 63.34 | 63.34 | 63.35 | 63.36 | 63.36 |
| 9.250 | 63.37 | 63.38 | 63.39 | 63.39 | 63.40 |
| 9.500 | 63.41 | 63.42 | 63.43 | 63.43 | 63.44 |
| 9.750 | 63.45 | 63.46 | 63.47 | 63.48 | 63.49 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 63.50 | 63.51 | 63.52 | 63.53 | 63.54 |
| 10.250 | 63.55 | 63.56 | 63.57 | 63.59 | 63.60 |
| 10.500 | 63.61 | 63.63 | 63.64 | 63.65 | 63.66 |
| 10.750 | 63.67 | 63.68 | 63.69 | 63.70 | 63.71 |
| 11.000 | 63.72 | 63.73 | 63.74 | 63.75 | 63.77 |
| 11.250 | 63.78 | 63.80 | 63.81 | 63.83 | 63.85 |
| 11.500 | 63.87 | 63.90 | 63.92 | 63.96 | 64.01 |
| 11.750 | 64.08 | 64.16 | 64.24 | 64.33 | 64.44 |
| 12.000 | 64.59 | 64.80 | 65.04 | 65.29 | 65.50 |
| 12.250 | 65.63 | 65.71 | 65.75 | 65.76 | 65.74 |
| 12.500 | 65.70 | 65.65 | 65.58 | 65.51 | 65.44 |
| 12.750 | 65.36 | 65.29 | 65.22 | 65.16 | 65.10 |
| 13.000 | 65.04 | 64.99 | 64.94 | 64.89 | 64.84 |
| 13.250 | 64.79 | 64.75 | 64.71 | 64.68 | 64.64 |
| 13.500 | 64.61 | 64.58 | 64.55 | 64.52 | 64.49 |
| 13.750 | 64.46 | 64.44 | 64.41 | 64.39 | 64.37 |
| 14.000 | 64.34 | 64.32 | 64.30 | 64.28 | 64.26 |
| 14.250 | 64.25 | 64.23 | 64.21 | 64.20 | 64.18 |
| 14.500 | 64.17 | 64.15 | 64.14 | 64.12 | 64.10 |
| 14.750 | 64.09 | 64.07 | 64.06 | 64.04 | 64.03 |
| 15.000 | 64.01 | 64.00 | 63.99 | 63.98 | 63.97 |
| 15.250 | 63.95 | 63.94 | 63.93 | 63.92 | 63.91 |
| 15.500 | 63.90 | 63.89 | 63.88 | 63.87 | 63.87 |
| 15.750 | 63.86 | 63.85 | 63.84 | 63.83 | 63.82 |
| 16.000 | 63.82 | 63.81 | 63.80 | 63.79 | 63.78 |
| 16.250 | 63.78 | 63.77 | 63.76 | 63.76 | 63.75 |
| 16.500 | 63.75 | 63.74 | 63.73 | 63.73 | 63.72 |
| 16.750 | 63.72 | 63.71 | 63.71 | 63.71 | 63.70 |
| 17.000 | 63.70 | 63.69 | 63.69 | 63.68 | 63.68 |
| 17.250 | 63.68 | 63.67 | 63.67 | 63.66 | 63.66 |
| 17.500 | 63.66 | 63.65 | 63.65 | 63.65 | 63.64 |
| 17.750 | 63.63 | 63.63 | 63.62 | 63.62 | 63.61 |
| 18.000 | 63.61 | 63.60 | 63.60 | 63.59 | 63.59 |
| 18.250 | 63.58 | 63.58 | 63.57 | 63.57 | 63.56 |
| 18.500 | 63.56 | 63.56 | 63.55 | 63.55 | 63.54 |
| 18.750 | 63.54 | 63.54 | 63.53 | 63.53 | 63.53 |
| 19.000 | 63.52 | 63.52 | 63.52 | 63.51 | 63.51 |
| 19.250 | 63.51 | 63.51 | 63.50 | 63.50 | 63.50 |
| 19.500 | 63.49 | 63.49 | 63.49 | 63.49 | 63.49 |
| 19.750 | 63.48 | 63.48 | 63.48 | 63.48 | 63.47 |
| 20.000 | 63.47 | 63.47 | 63.47 | 63.47 | 63.46 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 63.46 | 63.46 | 63.46 | 63.46 | 63.45 |
| 20.500 | 63.45 | 63.45 | 63.45 | 63.45 | 63.45 |
| 20.750 | 63.44 | 63.44 | 63.44 | 63.44 | 63.44 |
| 21.000 | 63.44 | 63.43 | 63.43 | 63.43 | 63.43 |
| 21.250 | 63.43 | 63.43 | 63.42 | 63.42 | 63.42 |
| 21.500 | 63.42 | 63.42 | 63.42 | 63.42 | 63.42 |
| 21.750 | 63.41 | 63.41 | 63.41 | 63.41 | 63.41 |
| 22.000 | 63.41 | 63.41 | 63.40 | 63.40 | 63.40 |
| 22.250 | 63.40 | 63.40 | 63.40 | 63.40 | 63.40 |
| 22.500 | 63.39 | 63.39 | 63.39 | 63.39 | 63.39 |
| 22.750 | 63.39 | 63.39 | 63.39 | 63.38 | 63.38 |
| 23.000 | 63.38 | 63.38 | 63.38 | 63.38 | 63.38 |
| 23.250 | 63.38 | 63.37 | 63.37 | 63.37 | 63.37 |
| 23.500 | 63.37 | 63.37 | 63.37 | 63.37 | 63.36 |
| 23.750 | 63.36 | 63.36 | 63.36 | 63.36 | 63.36 |
| 24.000 | 63.36 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 4.750 | 63.15 | 63.15 | 63.15 | 63.16 | 63.16 |
| 5.000 | 63.16 | 63.16 | 63.16 | 63.16 | 63.16 |
| 5.250 | 63.16 | 63.16 | 63.17 | 63.17 | 63.17 |
| 5.500 | 63.17 | 63.17 | 63.17 | 63.18 | 63.18 |
| 5.750 | 63.18 | 63.18 | 63.18 | 63.19 | 63.19 |
| 6.000 | 63.19 | 63.19 | 63.19 | 63.20 | 63.20 |
| 6.250 | 63.20 | 63.20 | 63.20 | 63.21 | 63.21 |
| 6.500 | 63.21 | 63.21 | 63.22 | 63.22 | 63.22 |
| 6.750 | 63.23 | 63.23 | 63.23 | 63.24 | 63.24 |
| 7.000 | 63.24 | 63.25 | 63.25 | 63.25 | 63.26 |
| 7.250 | 63.26 | 63.27 | 63.27 | 63.27 | 63.28 |
| 7.500 | 63.28 | 63.29 | 63.29 | 63.30 | 63.30 |
| 7.750 | 63.30 | 63.31 | 63.31 | 63.32 | 63.32 |
| 8.000 | 63.33 | 63.33 | 63.34 | 63.34 | 63.35 |
| 8.250 | 63.36 | 63.36 | 63.37 | 63.37 | 63.38 |
| 8.500 | 63.39 | 63.40 | 63.40 | 63.41 | 63.42 |
| 8.750 | 63.43 | 63.44 | 63.44 | 63.45 | 63.46 |
| 9.000 | 63.47 | 63.48 | 63.49 | 63.50 | 63.51 |
| 9.250 | 63.52 | 63.53 | 63.54 | 63.55 | 63.56 |
| 9.500 | 63.58 | 63.59 | 63.60 | 63.61 | 63.62 |
| 9.750 | 63.64 | 63.65 | 63.66 | 63.66 | 63.67 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 63.68 | 63.69 | 63.70 | 63.71 | 63.71 |
| 10.250 | 63.72 | 63.73 | 63.74 | 63.75 | 63.76 |
| 10.500 | 63.77 | 63.78 | 63.79 | 63.80 | 63.82 |
| 10.750 | 63.83 | 63.84 | 63.85 | 63.87 | 63.88 |
| 11.000 | 63.89 | 63.90 | 63.92 | 63.93 | 63.95 |
| 11.250 | 63.97 | 63.99 | 64.01 | 64.04 | 64.06 |
| 11.500 | 64.09 | 64.12 | 64.16 | 64.20 | 64.25 |
| 11.750 | 64.32 | 64.40 | 64.51 | 64.63 | 64.78 |
| 12.000 | 64.99 | 65.27 | 65.60 | 65.93 | 66.20 |
| 12.250 | 66.38 | 66.46 | 66.49 | 66.47 | 66.43 |
| 12.500 | 66.35 | 66.26 | 66.15 | 66.04 | 65.93 |
| 12.750 | 65.82 | 65.72 | 65.63 | 65.54 | 65.46 |
| 13.000 | 65.39 | 65.32 | 65.25 | 65.18 | 65.12 |
| 13.250 | 65.07 | 65.01 | 64.97 | 64.92 | 64.88 |
| 13.500 | 64.83 | 64.80 | 64.76 | 64.72 | 64.69 |
| 13.750 | 64.66 | 64.63 | 64.60 | 64.57 | 64.55 |
| 14.000 | 64.52 | 64.50 | 64.47 | 64.45 | 64.43 |
| 14.250 | 64.41 | 64.39 | 64.37 | 64.35 | 64.33 |
| 14.500 | 64.31 | 64.30 | 64.28 | 64.27 | 64.25 |
| 14.750 | 64.24 | 64.22 | 64.21 | 64.20 | 64.19 |
| 15.000 | 64.17 | 64.16 | 64.15 | 64.14 | 64.12 |
| 15.250 | 64.11 | 64.10 | 64.08 | 64.07 | 64.06 |
| 15.500 | 64.05 | 64.03 | 64.02 | 64.01 | 64.00 |
| 15.750 | 63.99 | 63.98 | 63.97 | 63.96 | 63.95 |
| 16.000 | 63.94 | 63.93 | 63.92 | 63.91 | 63.90 |
| 16.250 | 63.89 | 63.88 | 63.87 | 63.86 | 63.85 |
| 16.500 | 63.85 | 63.84 | 63.83 | 63.83 | 63.82 |
| 16.750 | 63.81 | 63.81 | 63.80 | 63.79 | 63.79 |
| 17.000 | 63.78 | 63.78 | 63.77 | 63.77 | 63.76 |
| 17.250 | 63.76 | 63.75 | 63.75 | 63.74 | 63.74 |
| 17.500 | 63.73 | 63.73 | 63.72 | 63.72 | 63.72 |
| 17.750 | 63.71 | 63.71 | 63.70 | 63.70 | 63.70 |
| 18.000 | 63.69 | 63.69 | 63.68 | 63.68 | 63.68 |
| 18.250 | 63.67 | 63.67 | 63.67 | 63.66 | 63.66 |
| 18.500 | 63.66 | 63.65 | 63.65 | 63.65 | 63.64 |
| 18.750 | 63.64 | 63.64 | 63.63 | 63.63 | 63.62 |
| 19.000 | 63.62 | 63.62 | 63.61 | 63.61 | 63.61 |
| 19.250 | 63.60 | 63.60 | 63.60 | 63.60 | 63.59 |
| 19.500 | 63.59 | 63.59 | 63.58 | 63.58 | 63.58 |
| 19.750 | 63.58 | 63.57 | 63.57 | 63.57 | 63.56 |
| 20.000 | 63.56 | 63.56 | 63.56 | 63.55 | 63.55 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 63.55 | 63.55 | 63.55 | 63.54 | 63.54 |
| 20.500 | 63.54 | 63.54 | 63.53 | 63.53 | 63.53 |
| 20.750 | 63.53 | 63.53 | 63.52 | 63.52 | 63.52 |
| 21.000 | 63.52 | 63.52 | 63.51 | 63.51 | 63.51 |
| 21.250 | 63.51 | 63.51 | 63.50 | 63.50 | 63.50 |
| 21.500 | 63.50 | 63.50 | 63.50 | 63.49 | 63.49 |
| 21.750 | 63.49 | 63.49 | 63.49 | 63.49 | 63.48 |
| 22.000 | 63.48 | 63.48 | 63.48 | 63.48 | 63.48 |
| 22.250 | 63.47 | 63.47 | 63.47 | 63.47 | 63.47 |
| 22.500 | 63.47 | 63.46 | 63.46 | 63.46 | 63.46 |
| 22.750 | 63.46 | 63.46 | 63.45 | 63.45 | 63.45 |
| 23.000 | 63.45 | 63.45 | 63.45 | 63.44 | 63.44 |
| 23.250 | 63.44 | 63.44 | 63.44 | 63.44 | 63.44 |
| 23.500 | 63.43 | 63.43 | 63.43 | 63.43 | 63.43 |
| 23.750 | 63.43 | 63.42 | 63.42 | 63.42 | 63.42 |
| 24.000 | 63.42 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 0.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 1.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 2.750 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.000 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.250 | 63.15 | 63.15 | 63.15 | 63.15 | 63.15 |
| 3.500 | 63.15 | 63.15 | 63.15 | 63.15 | 63.16 |
| 3.750 | 63.16 | 63.16 | 63.16 | 63.16 | 63.16 |
| 4.000 | 63.17 | 63.17 | 63.17 | 63.17 | 63.17 |
| 4.250 | 63.18 | 63.18 | 63.18 | 63.18 | 63.19 |
| 4.500 | 63.19 | 63.19 | 63.19 | 63.20 | 63.20 |
| 4.750 | 63.20 | 63.21 | 63.21 | 63.21 | 63.22 |
| 5.000 | 63.22 | 63.22 | 63.23 | 63.23 | 63.23 |
| 5.250 | 63.24 | 63.24 | 63.24 | 63.25 | 63.25 |
| 5.500 | 63.25 | 63.26 | 63.26 | 63.26 | 63.27 |
| 5.750 | 63.27 | 63.28 | 63.28 | 63.28 | 63.29 |
| 6.000 | 63.29 | 63.30 | 63.30 | 63.30 | 63.31 |
| 6.250 | 63.31 | 63.32 | 63.32 | 63.33 | 63.33 |
| 6.500 | 63.34 | 63.34 | 63.35 | 63.35 | 63.36 |
| 6.750 | 63.36 | 63.37 | 63.37 | 63.38 | 63.39 |
| 7.000 | 63.39 | 63.40 | 63.41 | 63.41 | 63.42 |
| 7.250 | 63.43 | 63.43 | 63.44 | 63.45 | 63.46 |
| 7.500 | 63.46 | 63.47 | 63.48 | 63.49 | 63.49 |
| 7.750 | 63.50 | 63.51 | 63.52 | 63.53 | 63.54 |
| 8.000 | 63.54 | 63.55 | 63.56 | 63.57 | 63.58 |
| 8.250 | 63.59 | 63.60 | 63.61 | 63.62 | 63.63 |
| 8.500 | 63.64 | 63.65 | 63.66 | 63.67 | 63.68 |
| 8.750 | 63.69 | 63.69 | 63.70 | 63.71 | 63.72 |
| 9.000 | 63.73 | 63.74 | 63.75 | 63.76 | 63.77 |
| 9.250 | 63.78 | 63.79 | 63.80 | 63.81 | 63.82 |
| 9.500 | 63.83 | 63.84 | 63.85 | 63.86 | 63.87 |
| 9.750 | 63.88 | 63.89 | 63.90 | 63.91 | 63.92 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 63.93 | 63.94 | 63.95 | 63.97 | 63.98 |
| 10.250 | 63.99 | 64.00 | 64.02 | 64.03 | 64.05 |
| 10.500 | 64.06 | 64.08 | 64.10 | 64.11 | 64.13 |
| 10.750 | 64.15 | 64.16 | 64.17 | 64.19 | 64.20 |
| 11.000 | 64.22 | 64.23 | 64.25 | 64.26 | 64.28 |
| 11.250 | 64.30 | 64.33 | 64.35 | 64.38 | 64.41 |
| 11.500 | 64.44 | 64.48 | 64.52 | 64.58 | 64.66 |
| 11.750 | 64.77 | 64.90 | 65.07 | 65.26 | 65.49 |
| 12.000 | 65.81 | 66.25 | 66.79 | 67.40 | 67.96 |
| 12.250 | 68.21 | 68.23 | 68.12 | 67.93 | 67.71 |
| 12.500 | 67.47 | 67.23 | 67.02 | 66.82 | 66.64 |
| 12.750 | 66.48 | 66.34 | 66.20 | 66.08 | 65.97 |
| 13.000 | 65.87 | 65.78 | 65.69 | 65.61 | 65.53 |
| 13.250 | 65.46 | 65.39 | 65.33 | 65.28 | 65.22 |
| 13.500 | 65.17 | 65.13 | 65.08 | 65.04 | 65.00 |
| 13.750 | 64.97 | 64.93 | 64.90 | 64.86 | 64.83 |
| 14.000 | 64.80 | 64.77 | 64.75 | 64.72 | 64.69 |
| 14.250 | 64.67 | 64.65 | 64.62 | 64.60 | 64.58 |
| 14.500 | 64.56 | 64.55 | 64.53 | 64.51 | 64.49 |
| 14.750 | 64.48 | 64.46 | 64.44 | 64.43 | 64.41 |
| 15.000 | 64.40 | 64.39 | 64.37 | 64.36 | 64.35 |
| 15.250 | 64.33 | 64.32 | 64.31 | 64.30 | 64.28 |
| 15.500 | 64.27 | 64.26 | 64.25 | 64.24 | 64.23 |
| 15.750 | 64.22 | 64.21 | 64.20 | 64.18 | 64.17 |
| 16.000 | 64.16 | 64.15 | 64.14 | 64.13 | 64.12 |
| 16.250 | 64.10 | 64.09 | 64.08 | 64.07 | 64.06 |
| 16.500 | 64.05 | 64.04 | 64.03 | 64.02 | 64.01 |
| 16.750 | 64.00 | 63.99 | 63.98 | 63.97 | 63.97 |
| 17.000 | 63.96 | 63.95 | 63.94 | 63.93 | 63.93 |
| 17.250 | 63.92 | 63.91 | 63.91 | 63.90 | 63.89 |
| 17.500 | 63.89 | 63.88 | 63.87 | 63.87 | 63.86 |
| 17.750 | 63.85 | 63.85 | 63.84 | 63.84 | 63.83 |
| 18.000 | 63.82 | 63.82 | 63.81 | 63.81 | 63.80 |
| 18.250 | 63.80 | 63.79 | 63.79 | 63.78 | 63.78 |
| 18.500 | 63.77 | 63.77 | 63.77 | 63.76 | 63.76 |
| 18.750 | 63.76 | 63.75 | 63.75 | 63.75 | 63.74 |
| 19.000 | 63.74 | 63.74 | 63.73 | 63.73 | 63.73 |
| 19.250 | 63.73 | 63.72 | 63.72 | 63.72 | 63.72 |
| 19.500 | 63.71 | 63.71 | 63.71 | 63.71 | 63.71 |
| 19.750 | 63.70 | 63.70 | 63.70 | 63.70 | 63.70 |
| 20.000 | 63.69 | 63.69 | 63.69 | 63.69 | 63.69 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 63.68 | 63.68 | 63.68 | 63.68 | 63.68 |
| 20.500 | 63.68 | 63.68 | 63.67 | 63.67 | 63.67 |
| 20.750 | 63.67 | 63.67 | 63.67 | 63.66 | 63.66 |
| 21.000 | 63.66 | 63.66 | 63.66 | 63.66 | 63.66 |
| 21.250 | 63.66 | 63.65 | 63.65 | 63.65 | 63.65 |
| 21.500 | 63.65 | 63.65 | 63.64 | 63.64 | 63.64 |
| 21.750 | 63.64 | 63.64 | 63.63 | 63.63 | 63.63 |
| 22.000 | 63.63 | 63.63 | 63.62 | 63.62 | 63.62 |
| 22.250 | 63.62 | 63.62 | 63.61 | 63.61 | 63.61 |
| 22.500 | 63.61 | 63.60 | 63.60 | 63.60 | 63.60 |
| 22.750 | 63.60 | 63.59 | 63.59 | 63.59 | 63.59 |
| 23.000 | 63.58 | 63.58 | 63.58 | 63.58 | 63.58 |
| 23.250 | 63.57 | 63.57 | 63.57 | 63.57 | 63.57 |
| 23.500 | 63.56 | 63.56 | 63.56 | 63.56 | 63.55 |
| 23.750 | 63.55 | 63.55 | 63.55 | 63.55 | 63.54 |
| 24.000 | 63.54 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 11.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 11.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 11.500 | 78.81 | 78.81 | 78.82 | 78.82 | 78.82 |
| 11.750 | 78.83 | 78.84 | 78.86 | 78.88 | 78.90 |
| 12.000 | 78.93 | 78.98 | 79.03 | 79.07 | 79.11 |
| 12.250 | 79.13 | 79.15 | 79.17 | 79.18 | 79.19 |
| 12.500 | 79.19 | 79.20 | 79.20 | 79.20 | 79.20 |
| 12.750 | 79.20 | 79.20 | 79.20 | 79.19 | 79.19 |
| 13.000 | 79.19 | 79.19 | 79.18 | 79.18 | 79.18 |
| 13.250 | 79.17 | 79.17 | 79.17 | 79.16 | 79.16 |
| 13.500 | 79.15 | 79.15 | 79.15 | 79.14 | 79.14 |
| 13.750 | 79.13 | 79.13 | 79.12 | 79.12 | 79.12 |
| 14.000 | 79.11 | 79.11 | 79.10 | 79.10 | 79.09 |
| 14.250 | 79.09 | 79.08 | 79.08 | 79.07 | 79.07 |
| 14.500 | 79.06 | 79.05 | 79.05 | 79.04 | 79.04 |
| 14.750 | 79.03 | 79.03 | 79.02 | 79.02 | 79.01 |
| 15.000 | 79.01 | 79.00 | 78.99 | 78.99 | 78.98 |
| 15.250 | 78.98 | 78.97 | 78.96 | 78.96 | 78.95 |
| 15.500 | 78.95 | 78.94 | 78.93 | 78.93 | 78.92 |
| 15.750 | 78.92 | 78.91 | 78.90 | 78.90 | 78.89 |
| 16.000 | 78.88 | 78.88 | 78.87 | 78.87 | 78.86 |
| 16.250 | 78.85 | 78.85 | 78.84 | 78.83 | 78.83 |
| 16.500 | 78.82 | 78.81 | 78.81 | 78.81 | 78.81 |
| 16.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 17.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 17.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 17.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 17.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 18.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 18.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 18.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 18.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 19.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 19.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 19.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 19.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 20.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 20.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 20.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 20.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 21.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 21.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 21.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 21.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 22.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 22.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 22.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 22.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 24.000 | 78.81 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|-----------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.82 |
| 11.000 | 78.82 | 78.82 | 78.82 | 78.82 | 78.82 |
| 11.250 | 78.82 | 78.83 | 78.83 | 78.84 | 78.84 |
| 11.500 | 78.85 | 78.85 | 78.86 | 78.88 | 78.89 |
| 11.750 | 78.92 | 78.95 | 78.98 | 79.02 | 79.07 |
| 12.000 | 79.14 | 79.24 | 79.33 | 79.42 | 79.50 |
| 12.250 | 79.55 | 79.59 | 79.63 | 79.66 | 79.68 |
| 12.500 | 79.70 | 79.72 | 79.73 | 79.74 | 79.74 |
| 12.750 | 79.75 | 79.75 | 79.76 | 79.76 | 79.76 |
| 13.000 | 79.76 | 79.77 | 79.77 | 79.77 | 79.77 |
| 13.250 | 79.77 | 79.77 | 79.77 | 79.77 | 79.77 |
| 13.500 | 79.77 | 79.77 | 79.77 | 79.77 | 79.77 |
| 13.750 | 79.77 | 79.77 | 79.77 | 79.76 | 79.76 |
| 14.000 | 79.76 | 79.76 | 79.76 | 79.76 | 79.75 |
| 14.250 | 79.75 | 79.75 | 79.75 | 79.74 | 79.74 |
| 14.500 | 79.74 | 79.74 | 79.73 | 79.73 | 79.73 |
| 14.750 | 79.72 | 79.72 | 79.72 | 79.72 | 79.71 |
| 15.000 | 79.71 | 79.71 | 79.70 | 79.70 | 79.69 |
| 15.250 | 79.69 | 79.69 | 79.68 | 79.68 | 79.68 |
| 15.500 | 79.67 | 79.67 | 79.66 | 79.66 | 79.65 |
| 15.750 | 79.65 | 79.65 | 79.64 | 79.64 | 79.63 |
| 16.000 | 79.63 | 79.62 | 79.62 | 79.61 | 79.61 |
| 16.250 | 79.60 | 79.60 | 79.59 | 79.59 | 79.58 |
| 16.500 | 79.58 | 79.57 | 79.57 | 79.56 | 79.55 |
| 16.750 | 79.55 | 79.54 | 79.54 | 79.53 | 79.53 |
| 17.000 | 79.52 | 79.52 | 79.51 | 79.51 | 79.50 |
| 17.250 | 79.49 | 79.49 | 79.48 | 79.48 | 79.47 |
| 17.500 | 79.47 | 79.46 | 79.45 | 79.45 | 79.44 |
| 17.750 | 79.44 | 79.43 | 79.42 | 79.42 | 79.41 |
| 18.000 | 79.40 | 79.40 | 79.39 | 79.39 | 79.38 |
| 18.250 | 79.37 | 79.37 | 79.36 | 79.35 | 79.35 |
| 18.500 | 79.34 | 79.34 | 79.33 | 79.32 | 79.32 |
| 18.750 | 79.31 | 79.30 | 79.30 | 79.29 | 79.28 |
| 19.000 | 79.28 | 79.27 | 79.27 | 79.26 | 79.25 |
| 19.250 | 79.25 | 79.24 | 79.23 | 79.23 | 79.22 |
| 19.500 | 79.21 | 79.21 | 79.20 | 79.19 | 79.19 |
| 19.750 | 79.18 | 79.17 | 79.17 | 79.16 | 79.15 |
| 20.000 | 79.15 | 79.14 | 79.13 | 79.13 | 79.12 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 79.11 | 79.11 | 79.10 | 79.09 | 79.09 |
| 20.500 | 79.08 | 79.07 | 79.07 | 79.06 | 79.05 |
| 20.750 | 79.05 | 79.04 | 79.03 | 79.03 | 79.02 |
| 21.000 | 79.01 | 79.01 | 79.00 | 78.99 | 78.99 |
| 21.250 | 78.98 | 78.97 | 78.97 | 78.96 | 78.95 |
| 21.500 | 78.95 | 78.94 | 78.93 | 78.93 | 78.92 |
| 21.750 | 78.91 | 78.90 | 78.90 | 78.89 | 78.88 |
| 22.000 | 78.88 | 78.87 | 78.86 | 78.86 | 78.85 |
| 22.250 | 78.84 | 78.84 | 78.83 | 78.82 | 78.81 |
| 22.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 22.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 23.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 24.000 | 78.81 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 10.250 | 78.81 | 78.81 | 78.82 | 78.82 | 78.82 |
| 10.500 | 78.82 | 78.82 | 78.82 | 78.82 | 78.82 |
| 10.750 | 78.83 | 78.83 | 78.83 | 78.83 | 78.84 |
| 11.000 | 78.84 | 78.84 | 78.85 | 78.85 | 78.86 |
| 11.250 | 78.86 | 78.87 | 78.88 | 78.88 | 78.89 |
| 11.500 | 78.90 | 78.91 | 78.93 | 78.95 | 78.97 |
| 11.750 | 79.00 | 79.04 | 79.09 | 79.14 | 79.21 |
| 12.000 | 79.30 | 79.42 | 79.55 | 79.67 | 79.76 |
| 12.250 | 79.83 | 79.87 | 79.89 | 79.90 | 79.90 |
| 12.500 | 79.90 | 79.89 | 79.88 | 79.87 | 79.86 |
| 12.750 | 79.85 | 79.85 | 79.84 | 79.84 | 79.83 |
| 13.000 | 79.83 | 79.83 | 79.83 | 79.82 | 79.82 |
| 13.250 | 79.82 | 79.82 | 79.82 | 79.82 | 79.82 |
| 13.500 | 79.82 | 79.82 | 79.82 | 79.82 | 79.82 |
| 13.750 | 79.81 | 79.81 | 79.81 | 79.81 | 79.81 |
| 14.000 | 79.81 | 79.81 | 79.81 | 79.81 | 79.81 |
| 14.250 | 79.81 | 79.81 | 79.81 | 79.81 | 79.81 |
| 14.500 | 79.80 | 79.80 | 79.80 | 79.80 | 79.80 |
| 14.750 | 79.80 | 79.80 | 79.79 | 79.79 | 79.79 |
| 15.000 | 79.79 | 79.79 | 79.78 | 79.78 | 79.78 |
| 15.250 | 79.78 | 79.78 | 79.77 | 79.77 | 79.77 |
| 15.500 | 79.76 | 79.76 | 79.76 | 79.75 | 79.75 |
| 15.750 | 79.75 | 79.74 | 79.74 | 79.74 | 79.73 |
| 16.000 | 79.73 | 79.73 | 79.72 | 79.72 | 79.71 |
| 16.250 | 79.71 | 79.71 | 79.70 | 79.70 | 79.69 |
| 16.500 | 79.69 | 79.68 | 79.68 | 79.67 | 79.67 |
| 16.750 | 79.67 | 79.66 | 79.66 | 79.65 | 79.65 |
| 17.000 | 79.64 | 79.64 | 79.63 | 79.63 | 79.62 |
| 17.250 | 79.62 | 79.61 | 79.61 | 79.60 | 79.60 |
| 17.500 | 79.59 | 79.59 | 79.58 | 79.58 | 79.57 |
| 17.750 | 79.57 | 79.56 | 79.55 | 79.55 | 79.54 |
| 18.000 | 79.54 | 79.53 | 79.53 | 79.52 | 79.51 |
| 18.250 | 79.51 | 79.50 | 79.50 | 79.49 | 79.49 |
| 18.500 | 79.48 | 79.47 | 79.47 | 79.46 | 79.46 |
| 18.750 | 79.45 | 79.45 | 79.44 | 79.43 | 79.43 |
| 19.000 | 79.42 | 79.42 | 79.41 | 79.40 | 79.40 |
| 19.250 | 79.39 | 79.39 | 79.38 | 79.37 | 79.37 |
| 19.500 | 79.36 | 79.36 | 79.35 | 79.34 | 79.34 |
| 19.750 | 79.33 | 79.33 | 79.32 | 79.31 | 79.31 |
| 20.000 | 79.30 | 79.29 | 79.29 | 79.28 | 79.28 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 79.27 | 79.26 | 79.26 | 79.25 | 79.24 |
| 20.500 | 79.24 | 79.23 | 79.23 | 79.22 | 79.21 |
| 20.750 | 79.21 | 79.20 | 79.19 | 79.19 | 79.18 |
| 21.000 | 79.18 | 79.17 | 79.16 | 79.16 | 79.15 |
| 21.250 | 79.14 | 79.14 | 79.13 | 79.12 | 79.12 |
| 21.500 | 79.11 | 79.10 | 79.10 | 79.09 | 79.09 |
| 21.750 | 79.08 | 79.07 | 79.07 | 79.06 | 79.05 |
| 22.000 | 79.05 | 79.04 | 79.03 | 79.03 | 79.02 |
| 22.250 | 79.01 | 79.01 | 79.00 | 78.99 | 78.99 |
| 22.500 | 78.98 | 78.97 | 78.97 | 78.96 | 78.95 |
| 22.750 | 78.95 | 78.94 | 78.93 | 78.93 | 78.92 |
| 23.000 | 78.91 | 78.91 | 78.90 | 78.89 | 78.89 |
| 23.250 | 78.88 | 78.87 | 78.87 | 78.86 | 78.85 |
| 23.500 | 78.85 | 78.84 | 78.83 | 78.83 | 78.82 |
| 23.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 24.000 | 78.81 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 0.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 0.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 1.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 2.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 3.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 4.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 5.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 6.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 7.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.000 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.250 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.500 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 8.750 | 78.81 | 78.81 | 78.81 | 78.81 | 78.81 |
| 9.000 | 78.81 | 78.81 | 78.81 | 78.82 | 78.82 |
| 9.250 | 78.82 | 78.82 | 78.82 | 78.82 | 78.82 |
| 9.500 | 78.82 | 78.82 | 78.83 | 78.83 | 78.83 |
| 9.750 | 78.83 | 78.83 | 78.84 | 78.84 | 78.84 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 10.000 | 78.84 | 78.85 | 78.85 | 78.85 | 78.86 |
| 10.250 | 78.86 | 78.86 | 78.87 | 78.87 | 78.88 |
| 10.500 | 78.88 | 78.89 | 78.90 | 78.90 | 78.91 |
| 10.750 | 78.92 | 78.92 | 78.93 | 78.94 | 78.94 |
| 11.000 | 78.95 | 78.96 | 78.97 | 78.98 | 78.99 |
| 11.250 | 79.00 | 79.02 | 79.03 | 79.04 | 79.06 |
| 11.500 | 79.08 | 79.10 | 79.12 | 79.15 | 79.19 |
| 11.750 | 79.24 | 79.30 | 79.37 | 79.45 | 79.55 |
| 12.000 | 79.69 | 79.86 | 79.99 | 80.05 | 80.06 |
| 12.250 | 80.03 | 80.01 | 79.99 | 79.97 | 79.95 |
| 12.500 | 79.94 | 79.92 | 79.91 | 79.90 | 79.89 |
| 12.750 | 79.88 | 79.87 | 79.86 | 79.86 | 79.85 |
| 13.000 | 79.85 | 79.85 | 79.84 | 79.84 | 79.84 |
| 13.250 | 79.84 | 79.84 | 79.83 | 79.83 | 79.83 |
| 13.500 | 79.83 | 79.83 | 79.83 | 79.83 | 79.83 |
| 13.750 | 79.83 | 79.83 | 79.83 | 79.82 | 79.82 |
| 14.000 | 79.82 | 79.82 | 79.82 | 79.82 | 79.82 |
| 14.250 | 79.82 | 79.82 | 79.82 | 79.82 | 79.82 |
| 14.500 | 79.82 | 79.82 | 79.82 | 79.82 | 79.82 |
| 14.750 | 79.82 | 79.81 | 79.81 | 79.81 | 79.81 |
| 15.000 | 79.81 | 79.81 | 79.81 | 79.81 | 79.81 |
| 15.250 | 79.81 | 79.81 | 79.81 | 79.81 | 79.81 |
| 15.500 | 79.81 | 79.81 | 79.81 | 79.81 | 79.81 |
| 15.750 | 79.80 | 79.80 | 79.80 | 79.80 | 79.80 |
| 16.000 | 79.80 | 79.79 | 79.79 | 79.79 | 79.79 |
| 16.250 | 79.78 | 79.78 | 79.78 | 79.78 | 79.77 |
| 16.500 | 79.77 | 79.77 | 79.77 | 79.76 | 79.76 |
| 16.750 | 79.76 | 79.75 | 79.75 | 79.75 | 79.75 |
| 17.000 | 79.74 | 79.74 | 79.74 | 79.73 | 79.73 |
| 17.250 | 79.72 | 79.72 | 79.72 | 79.71 | 79.71 |
| 17.500 | 79.71 | 79.70 | 79.70 | 79.69 | 79.69 |
| 17.750 | 79.69 | 79.68 | 79.68 | 79.67 | 79.67 |
| 18.000 | 79.66 | 79.66 | 79.66 | 79.65 | 79.65 |
| 18.250 | 79.64 | 79.64 | 79.63 | 79.63 | 79.62 |
| 18.500 | 79.62 | 79.61 | 79.61 | 79.60 | 79.60 |
| 18.750 | 79.59 | 79.59 | 79.58 | 79.58 | 79.58 |
| 19.000 | 79.57 | 79.57 | 79.56 | 79.56 | 79.55 |
| 19.250 | 79.55 | 79.54 | 79.54 | 79.53 | 79.53 |
| 19.500 | 79.52 | 79.52 | 79.51 | 79.51 | 79.50 |
| 19.750 | 79.49 | 79.49 | 79.48 | 79.48 | 79.47 |
| 20.000 | 79.47 | 79.46 | 79.46 | 79.45 | 79.45 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Elevation

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Elevation (ft)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|--------------|----------------|----------------|----------------|----------------|----------------|
| 20.250 | 79.44 | 79.44 | 79.43 | 79.43 | 79.42 |
| 20.500 | 79.42 | 79.41 | 79.41 | 79.40 | 79.39 |
| 20.750 | 79.39 | 79.38 | 79.38 | 79.37 | 79.37 |
| 21.000 | 79.36 | 79.36 | 79.35 | 79.34 | 79.34 |
| 21.250 | 79.33 | 79.33 | 79.32 | 79.32 | 79.31 |
| 21.500 | 79.31 | 79.30 | 79.29 | 79.29 | 79.28 |
| 21.750 | 79.28 | 79.27 | 79.27 | 79.26 | 79.25 |
| 22.000 | 79.25 | 79.24 | 79.24 | 79.23 | 79.23 |
| 22.250 | 79.22 | 79.21 | 79.21 | 79.20 | 79.20 |
| 22.500 | 79.19 | 79.18 | 79.18 | 79.17 | 79.17 |
| 22.750 | 79.16 | 79.15 | 79.15 | 79.14 | 79.14 |
| 23.000 | 79.13 | 79.12 | 79.12 | 79.11 | 79.11 |
| 23.250 | 79.10 | 79.09 | 79.09 | 79.08 | 79.08 |
| 23.500 | 79.07 | 79.06 | 79.06 | 79.05 | 79.05 |
| 23.750 | 79.04 | 79.03 | 79.03 | 79.02 | 79.01 |
| 24.000 | 79.01 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: 24" Depth Green Roof
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: 24" Depth Green Roof
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 0 | 0 | 0 |
| 11.000 | 0 | 0 | 0 | 0 | 0 |
| 11.250 | 9 | 11 | 13 | 17 | 22 |
| 11.500 | 27 | 35 | 46 | 61 | 81 |
| 11.750 | 122 | 164 | 216 | 276 | 355 |
| 12.000 | 467 | 609 | 760 | 903 | 1,016 |
| 12.250 | 1,099 | 1,166 | 1,221 | 1,267 | 1,303 |
| 12.500 | 1,330 | 1,350 | 1,363 | 1,372 | 1,379 |
| 12.750 | 1,384 | 1,389 | 1,393 | 1,396 | 1,397 |
| 13.000 | 1,398 | 1,398 | 1,398 | 1,396 | 1,395 |
| 13.250 | 1,393 | 1,391 | 1,389 | 1,386 | 1,383 |
| 13.500 | 1,380 | 1,377 | 1,373 | 1,369 | 1,365 |
| 13.750 | 1,361 | 1,356 | 1,352 | 1,347 | 1,341 |
| 14.000 | 1,336 | 1,330 | 1,324 | 1,318 | 1,312 |
| 14.250 | 1,305 | 1,299 | 1,292 | 1,285 | 1,278 |
| 14.500 | 1,271 | 1,264 | 1,257 | 1,250 | 1,242 |
| 14.750 | 1,234 | 1,227 | 1,219 | 1,211 | 1,203 |
| 15.000 | 1,195 | 1,186 | 1,178 | 1,169 | 1,161 |
| 15.250 | 1,152 | 1,143 | 1,134 | 1,125 | 1,116 |
| 15.500 | 1,106 | 1,097 | 1,087 | 1,077 | 1,068 |
| 15.750 | 1,058 | 1,047 | 1,037 | 1,027 | 1,016 |
| 16.000 | 1,006 | 995 | 984 | 974 | 963 |
| 16.250 | 952 | 941 | 930 | 918 | 907 |
| 16.500 | 896 | 885 | 873 | 862 | 851 |
| 16.750 | 839 | 828 | 816 | 804 | 793 |
| 17.000 | 781 | 769 | 757 | 745 | 733 |
| 17.250 | 721 | 709 | 697 | 685 | 673 |
| 17.500 | 661 | 648 | 636 | 624 | 611 |
| 17.750 | 599 | 586 | 573 | 561 | 548 |
| 18.000 | 535 | 522 | 510 | 497 | 484 |
| 18.250 | 471 | 458 | 445 | 432 | 419 |
| 18.500 | 406 | 393 | 380 | 367 | 354 |
| 18.750 | 341 | 328 | 314 | 301 | 288 |
| 19.000 | 275 | 262 | 249 | 235 | 222 |
| 19.250 | 209 | 196 | 182 | 169 | 156 |
| 19.500 | 143 | 129 | 116 | 95 | 81 |
| 19.750 | 71 | 60 | 49 | 35 | 22 |
| 20.000 | 8 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: 24" Depth Green Roof
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 20.250 | 0 | 0 | 0 | 0 | 0 |
| 20.500 | 0 | 0 | 0 | 0 | 0 |
| 20.750 | 0 | 0 | 0 | 0 | 0 |
| 21.000 | 0 | 0 | 0 | 0 | 0 |
| 21.250 | 0 | 0 | 0 | 0 | 0 |
| 21.500 | 0 | 0 | 0 | 0 | 0 |
| 21.750 | 0 | 0 | 0 | 0 | 0 |
| 22.000 | 0 | 0 | 0 | 0 | 0 |
| 22.250 | 0 | 0 | 0 | 0 | 0 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: 24" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 8 |
| 9.750 | 9 | 9 | 10 | 11 | 13 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: 24" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 14 | 16 | 18 | 21 | 24 |
| 10.250 | 27 | 31 | 35 | 40 | 45 |
| 10.500 | 51 | 56 | 61 | 67 | 73 |
| 10.750 | 79 | 86 | 97 | 112 | 123 |
| 11.000 | 133 | 144 | 156 | 169 | 184 |
| 11.250 | 201 | 219 | 239 | 260 | 284 |
| 11.500 | 309 | 338 | 375 | 422 | 483 |
| 11.750 | 561 | 656 | 767 | 896 | 1,058 |
| 12.000 | 1,283 | 1,562 | 1,859 | 2,124 | 2,253 |
| 12.250 | 2,233 | 2,228 | 2,222 | 2,217 | 2,212 |
| 12.500 | 2,207 | 2,203 | 2,201 | 2,199 | 2,198 |
| 12.750 | 2,197 | 2,197 | 2,196 | 2,196 | 2,195 |
| 13.000 | 2,195 | 2,194 | 2,194 | 2,194 | 2,194 |
| 13.250 | 2,193 | 2,193 | 2,193 | 2,193 | 2,193 |
| 13.500 | 2,193 | 2,193 | 2,192 | 2,192 | 2,192 |
| 13.750 | 2,192 | 2,192 | 2,192 | 2,192 | 2,192 |
| 14.000 | 2,191 | 2,191 | 2,191 | 2,191 | 2,191 |
| 14.250 | 2,191 | 2,191 | 2,191 | 2,191 | 2,191 |
| 14.500 | 2,191 | 2,191 | 2,191 | 2,191 | 2,190 |
| 14.750 | 2,190 | 2,190 | 2,189 | 2,188 | 2,187 |
| 15.000 | 2,186 | 2,184 | 2,182 | 2,180 | 2,178 |
| 15.250 | 2,176 | 2,173 | 2,170 | 2,165 | 2,160 |
| 15.500 | 2,154 | 2,148 | 2,142 | 2,135 | 2,128 |
| 15.750 | 2,122 | 2,116 | 2,112 | 2,108 | 2,104 |
| 16.000 | 2,099 | 2,094 | 2,089 | 2,084 | 2,079 |
| 16.250 | 2,074 | 2,069 | 2,063 | 2,058 | 2,052 |
| 16.500 | 2,047 | 2,040 | 2,033 | 2,026 | 2,019 |
| 16.750 | 2,011 | 2,004 | 1,996 | 1,988 | 1,980 |
| 17.000 | 1,972 | 1,964 | 1,956 | 1,948 | 1,940 |
| 17.250 | 1,931 | 1,923 | 1,914 | 1,906 | 1,897 |
| 17.500 | 1,888 | 1,879 | 1,870 | 1,861 | 1,851 |
| 17.750 | 1,842 | 1,832 | 1,823 | 1,813 | 1,803 |
| 18.000 | 1,794 | 1,784 | 1,774 | 1,764 | 1,753 |
| 18.250 | 1,743 | 1,733 | 1,723 | 1,713 | 1,702 |
| 18.500 | 1,692 | 1,682 | 1,672 | 1,661 | 1,651 |
| 18.750 | 1,640 | 1,630 | 1,619 | 1,609 | 1,598 |
| 19.000 | 1,588 | 1,577 | 1,567 | 1,556 | 1,545 |
| 19.250 | 1,535 | 1,524 | 1,513 | 1,502 | 1,491 |
| 19.500 | 1,481 | 1,470 | 1,459 | 1,448 | 1,437 |
| 19.750 | 1,426 | 1,415 | 1,404 | 1,393 | 1,381 |
| 20.000 | 1,370 | 1,359 | 1,348 | 1,337 | 1,326 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: 24" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,314 | 1,303 | 1,292 | 1,280 | 1,269 |
| 20.500 | 1,258 | 1,246 | 1,235 | 1,223 | 1,212 |
| 20.750 | 1,200 | 1,189 | 1,177 | 1,166 | 1,154 |
| 21.000 | 1,143 | 1,131 | 1,119 | 1,108 | 1,096 |
| 21.250 | 1,084 | 1,073 | 1,061 | 1,049 | 1,037 |
| 21.500 | 1,026 | 1,014 | 1,002 | 990 | 978 |
| 21.750 | 966 | 954 | 942 | 930 | 918 |
| 22.000 | 906 | 894 | 882 | 870 | 858 |
| 22.250 | 846 | 834 | 821 | 809 | 797 |
| 22.500 | 785 | 773 | 760 | 748 | 736 |
| 22.750 | 723 | 711 | 699 | 686 | 674 |
| 23.000 | 661 | 649 | 636 | 624 | 611 |
| 23.250 | 599 | 586 | 573 | 561 | 548 |
| 23.500 | 535 | 523 | 510 | 497 | 485 |
| 23.750 | 472 | 459 | 446 | 433 | 420 |
| 24.000 | 408 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: 24" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 8 | 8 | 9 |
| 9.000 | 10 | 11 | 12 | 14 | 16 |
| 9.250 | 19 | 21 | 24 | 27 | 31 |
| 9.500 | 34 | 38 | 43 | 47 | 52 |
| 9.750 | 56 | 60 | 65 | 70 | 75 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: 24" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 80 | 86 | 94 | 106 | 118 |
| 10.250 | 126 | 136 | 146 | 157 | 168 |
| 10.500 | 180 | 192 | 205 | 219 | 233 |
| 10.750 | 248 | 263 | 279 | 295 | 313 |
| 11.000 | 330 | 349 | 369 | 390 | 413 |
| 11.250 | 439 | 466 | 496 | 528 | 563 |
| 11.500 | 599 | 641 | 692 | 756 | 839 |
| 11.750 | 943 | 1,068 | 1,214 | 1,382 | 1,592 |
| 12.000 | 1,883 | 2,209 | 2,322 | 2,283 | 2,268 |
| 12.250 | 2,247 | 2,239 | 2,231 | 2,225 | 2,219 |
| 12.500 | 2,213 | 2,208 | 2,205 | 2,202 | 2,201 |
| 12.750 | 2,200 | 2,200 | 2,199 | 2,198 | 2,198 |
| 13.000 | 2,197 | 2,197 | 2,196 | 2,196 | 2,196 |
| 13.250 | 2,195 | 2,195 | 2,195 | 2,195 | 2,195 |
| 13.500 | 2,195 | 2,194 | 2,194 | 2,194 | 2,194 |
| 13.750 | 2,194 | 2,194 | 2,193 | 2,193 | 2,193 |
| 14.000 | 2,193 | 2,193 | 2,193 | 2,193 | 2,192 |
| 14.250 | 2,192 | 2,192 | 2,192 | 2,192 | 2,192 |
| 14.500 | 2,192 | 2,192 | 2,192 | 2,192 | 2,192 |
| 14.750 | 2,192 | 2,192 | 2,191 | 2,191 | 2,191 |
| 15.000 | 2,191 | 2,191 | 2,191 | 2,191 | 2,191 |
| 15.250 | 2,191 | 2,191 | 2,191 | 2,191 | 2,191 |
| 15.500 | 2,190 | 2,190 | 2,189 | 2,188 | 2,187 |
| 15.750 | 2,185 | 2,184 | 2,181 | 2,179 | 2,176 |
| 16.000 | 2,173 | 2,170 | 2,165 | 2,159 | 2,153 |
| 16.250 | 2,147 | 2,140 | 2,134 | 2,127 | 2,121 |
| 16.500 | 2,116 | 2,113 | 2,109 | 2,105 | 2,101 |
| 16.750 | 2,097 | 2,093 | 2,088 | 2,084 | 2,080 |
| 17.000 | 2,075 | 2,070 | 2,065 | 2,061 | 2,056 |
| 17.250 | 2,051 | 2,045 | 2,039 | 2,033 | 2,026 |
| 17.500 | 2,019 | 2,012 | 2,005 | 1,997 | 1,990 |
| 17.750 | 1,982 | 1,975 | 1,967 | 1,959 | 1,951 |
| 18.000 | 1,943 | 1,935 | 1,926 | 1,918 | 1,909 |
| 18.250 | 1,901 | 1,892 | 1,884 | 1,875 | 1,866 |
| 18.500 | 1,858 | 1,849 | 1,840 | 1,831 | 1,823 |
| 18.750 | 1,814 | 1,805 | 1,796 | 1,787 | 1,778 |
| 19.000 | 1,769 | 1,760 | 1,751 | 1,741 | 1,732 |
| 19.250 | 1,723 | 1,714 | 1,704 | 1,695 | 1,686 |
| 19.500 | 1,676 | 1,667 | 1,657 | 1,648 | 1,638 |
| 19.750 | 1,629 | 1,619 | 1,609 | 1,599 | 1,590 |
| 20.000 | 1,580 | 1,570 | 1,560 | 1,550 | 1,540 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: 24" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,531 | 1,521 | 1,511 | 1,501 | 1,490 |
| 20.500 | 1,480 | 1,470 | 1,460 | 1,450 | 1,440 |
| 20.750 | 1,430 | 1,419 | 1,409 | 1,399 | 1,388 |
| 21.000 | 1,378 | 1,368 | 1,357 | 1,347 | 1,336 |
| 21.250 | 1,326 | 1,315 | 1,305 | 1,294 | 1,284 |
| 21.500 | 1,273 | 1,262 | 1,252 | 1,241 | 1,230 |
| 21.750 | 1,219 | 1,209 | 1,198 | 1,187 | 1,176 |
| 22.000 | 1,165 | 1,154 | 1,143 | 1,132 | 1,121 |
| 22.250 | 1,110 | 1,099 | 1,088 | 1,077 | 1,066 |
| 22.500 | 1,055 | 1,043 | 1,032 | 1,021 | 1,010 |
| 22.750 | 998 | 987 | 976 | 964 | 953 |
| 23.000 | 941 | 930 | 918 | 907 | 895 |
| 23.250 | 884 | 872 | 860 | 849 | 837 |
| 23.500 | 825 | 814 | 802 | 790 | 778 |
| 23.750 | 766 | 754 | 742 | 731 | 719 |
| 24.000 | 707 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: 24" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 8 |
| 7.750 | 8 | 9 | 9 | 10 | 11 |
| 8.000 | 12 | 13 | 15 | 17 | 19 |
| 8.250 | 22 | 25 | 28 | 32 | 36 |
| 8.500 | 41 | 46 | 51 | 56 | 61 |
| 8.750 | 66 | 72 | 78 | 84 | 93 |
| 9.000 | 107 | 119 | 128 | 138 | 148 |
| 9.250 | 159 | 170 | 182 | 194 | 206 |
| 9.500 | 219 | 232 | 246 | 259 | 274 |
| 9.750 | 289 | 304 | 319 | 335 | 352 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: 24" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 369 | 386 | 404 | 422 | 442 |
| 10.250 | 462 | 483 | 504 | 527 | 551 |
| 10.500 | 575 | 600 | 626 | 653 | 681 |
| 10.750 | 709 | 738 | 769 | 800 | 832 |
| 11.000 | 864 | 898 | 934 | 972 | 1,013 |
| 11.250 | 1,056 | 1,103 | 1,154 | 1,207 | 1,264 |
| 11.500 | 1,324 | 1,391 | 1,471 | 1,571 | 1,697 |
| 11.750 | 1,854 | 2,041 | 2,215 | 2,273 | 2,278 |
| 12.000 | 2,318 | 2,341 | 2,346 | 2,335 | 2,301 |
| 12.250 | 2,274 | 2,261 | 2,251 | 2,242 | 2,234 |
| 12.500 | 2,225 | 2,218 | 2,213 | 2,209 | 2,208 |
| 12.750 | 2,206 | 2,205 | 2,205 | 2,204 | 2,203 |
| 13.000 | 2,202 | 2,201 | 2,200 | 2,200 | 2,200 |
| 13.250 | 2,199 | 2,199 | 2,199 | 2,199 | 2,199 |
| 13.500 | 2,198 | 2,198 | 2,198 | 2,198 | 2,197 |
| 13.750 | 2,197 | 2,197 | 2,197 | 2,196 | 2,196 |
| 14.000 | 2,196 | 2,196 | 2,196 | 2,195 | 2,195 |
| 14.250 | 2,195 | 2,195 | 2,195 | 2,195 | 2,195 |
| 14.500 | 2,195 | 2,195 | 2,194 | 2,194 | 2,194 |
| 14.750 | 2,194 | 2,194 | 2,194 | 2,194 | 2,194 |
| 15.000 | 2,194 | 2,193 | 2,193 | 2,193 | 2,193 |
| 15.250 | 2,193 | 2,193 | 2,193 | 2,193 | 2,192 |
| 15.500 | 2,192 | 2,192 | 2,192 | 2,192 | 2,192 |
| 15.750 | 2,192 | 2,192 | 2,192 | 2,191 | 2,191 |
| 16.000 | 2,191 | 2,191 | 2,191 | 2,191 | 2,191 |
| 16.250 | 2,191 | 2,191 | 2,191 | 2,191 | 2,191 |
| 16.500 | 2,191 | 2,191 | 2,191 | 2,191 | 2,190 |
| 16.750 | 2,190 | 2,190 | 2,189 | 2,188 | 2,187 |
| 17.000 | 2,186 | 2,185 | 2,183 | 2,182 | 2,180 |
| 17.250 | 2,178 | 2,175 | 2,173 | 2,170 | 2,166 |
| 17.500 | 2,162 | 2,157 | 2,151 | 2,146 | 2,140 |
| 17.750 | 2,134 | 2,128 | 2,122 | 2,117 | 2,114 |
| 18.000 | 2,110 | 2,106 | 2,102 | 2,098 | 2,094 |
| 18.250 | 2,090 | 2,085 | 2,081 | 2,077 | 2,073 |
| 18.500 | 2,068 | 2,064 | 2,059 | 2,055 | 2,050 |
| 18.750 | 2,046 | 2,041 | 2,035 | 2,029 | 2,023 |
| 19.000 | 2,017 | 2,011 | 2,005 | 1,999 | 1,993 |
| 19.250 | 1,987 | 1,980 | 1,974 | 1,968 | 1,961 |
| 19.500 | 1,955 | 1,948 | 1,942 | 1,935 | 1,928 |
| 19.750 | 1,921 | 1,915 | 1,908 | 1,901 | 1,894 |
| 20.000 | 1,887 | 1,880 | 1,873 | 1,866 | 1,858 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: 24" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,851 | 1,844 | 1,837 | 1,829 | 1,822 |
| 20.500 | 1,815 | 1,807 | 1,800 | 1,792 | 1,784 |
| 20.750 | 1,777 | 1,769 | 1,761 | 1,754 | 1,746 |
| 21.000 | 1,738 | 1,730 | 1,722 | 1,714 | 1,706 |
| 21.250 | 1,698 | 1,690 | 1,682 | 1,674 | 1,666 |
| 21.500 | 1,658 | 1,649 | 1,641 | 1,633 | 1,624 |
| 21.750 | 1,616 | 1,608 | 1,599 | 1,591 | 1,582 |
| 22.000 | 1,573 | 1,565 | 1,556 | 1,547 | 1,539 |
| 22.250 | 1,530 | 1,521 | 1,512 | 1,503 | 1,494 |
| 22.500 | 1,485 | 1,476 | 1,467 | 1,458 | 1,449 |
| 22.750 | 1,440 | 1,430 | 1,421 | 1,412 | 1,402 |
| 23.000 | 1,393 | 1,384 | 1,374 | 1,365 | 1,355 |
| 23.250 | 1,345 | 1,336 | 1,326 | 1,316 | 1,307 |
| 23.500 | 1,297 | 1,287 | 1,277 | 1,267 | 1,257 |
| 23.750 | 1,247 | 1,237 | 1,227 | 1,217 | 1,207 |
| 24.000 | 1,197 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: 6" Depth Green Roof
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: 6" Depth Green Roof
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 0 | 0 | 0 |
| 11.000 | 0 | 0 | 0 | 0 | 0 |
| 11.250 | 0 | 0 | 0 | 0 | 0 |
| 11.500 | 0 | 0 | 0 | 0 | 0 |
| 11.750 | 0 | 13 | 19 | 28 | 45 |
| 12.000 | 75 | 109 | 166 | 211 | 242 |
| 12.250 | 261 | 272 | 279 | 282 | 281 |
| 12.500 | 277 | 269 | 258 | 245 | 232 |
| 12.750 | 218 | 204 | 189 | 174 | 159 |
| 13.000 | 135 | 116 | 102 | 89 | 75 |
| 13.250 | 60 | 43 | 25 | 0 | 0 |
| 13.500 | 0 | 0 | 0 | 0 | 0 |
| 13.750 | 0 | 0 | 0 | 0 | 0 |
| 14.000 | 0 | 0 | 0 | 0 | 0 |
| 14.250 | 0 | 0 | 0 | 0 | 0 |
| 14.500 | 0 | 0 | 0 | 0 | 0 |
| 14.750 | 0 | 0 | 0 | 0 | 0 |
| 15.000 | 0 | 0 | 0 | 0 | 0 |
| 15.250 | 0 | 0 | 0 | 0 | 0 |
| 15.500 | 0 | 0 | 0 | 0 | 0 |
| 15.750 | 0 | 0 | 0 | 0 | 0 |
| 16.000 | 0 | 0 | 0 | 0 | 0 |
| 16.250 | 0 | 0 | 0 | 0 | 0 |
| 16.500 | 0 | 0 | 0 | 0 | 0 |
| 16.750 | 0 | 0 | 0 | 0 | 0 |
| 17.000 | 0 | 0 | 0 | 0 | 0 |
| 17.250 | 0 | 0 | 0 | 0 | 0 |
| 17.500 | 0 | 0 | 0 | 0 | 0 |
| 17.750 | 0 | 0 | 0 | 0 | 0 |
| 18.000 | 0 | 0 | 0 | 0 | 0 |
| 18.250 | 0 | 0 | 0 | 0 | 0 |
| 18.500 | 0 | 0 | 0 | 0 | 0 |
| 18.750 | 0 | 0 | 0 | 0 | 0 |
| 19.000 | 0 | 0 | 0 | 0 | 0 |
| 19.250 | 0 | 0 | 0 | 0 | 0 |
| 19.500 | 0 | 0 | 0 | 0 | 0 |
| 19.750 | 0 | 0 | 0 | 0 | 0 |
| 20.000 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: 6" Depth Green Roof
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 20.250 | 0 | 0 | 0 | 0 | 0 |
| 20.500 | 0 | 0 | 0 | 0 | 0 |
| 20.750 | 0 | 0 | 0 | 0 | 0 |
| 21.000 | 0 | 0 | 0 | 0 | 0 |
| 21.250 | 0 | 0 | 0 | 0 | 0 |
| 21.500 | 0 | 0 | 0 | 0 | 0 |
| 21.750 | 0 | 0 | 0 | 0 | 0 |
| 22.000 | 0 | 0 | 0 | 0 | 0 |
| 22.250 | 0 | 0 | 0 | 0 | 0 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: 6" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: 6" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 0 | 0 | 0 |
| 11.000 | 0 | 0 | 0 | 0 | 0 |
| 11.250 | 0 | 0 | 0 | 0 | 0 |
| 11.500 | 0 | 0 | 0 | 15 | 25 |
| 11.750 | 41 | 65 | 91 | 121 | 186 |
| 12.000 | 264 | 365 | 474 | 576 | 655 |
| 12.250 | 710 | 744 | 770 | 791 | 805 |
| 12.500 | 814 | 819 | 819 | 816 | 811 |
| 12.750 | 806 | 801 | 795 | 788 | 781 |
| 13.000 | 773 | 765 | 756 | 747 | 738 |
| 13.250 | 728 | 719 | 708 | 696 | 683 |
| 13.500 | 670 | 657 | 644 | 631 | 617 |
| 13.750 | 603 | 589 | 575 | 561 | 546 |
| 14.000 | 532 | 517 | 502 | 487 | 471 |
| 14.250 | 456 | 440 | 425 | 409 | 393 |
| 14.500 | 378 | 362 | 346 | 329 | 313 |
| 14.750 | 297 | 280 | 264 | 247 | 231 |
| 15.000 | 214 | 197 | 180 | 163 | 139 |
| 15.250 | 117 | 103 | 89 | 75 | 59 |
| 15.500 | 41 | 23 | 0 | 0 | 0 |
| 15.750 | 0 | 0 | 0 | 0 | 0 |
| 16.000 | 0 | 0 | 0 | 0 | 0 |
| 16.250 | 0 | 0 | 0 | 0 | 0 |
| 16.500 | 0 | 0 | 0 | 0 | 0 |
| 16.750 | 0 | 0 | 0 | 0 | 0 |
| 17.000 | 0 | 0 | 0 | 0 | 0 |
| 17.250 | 0 | 0 | 0 | 0 | 0 |
| 17.500 | 0 | 0 | 0 | 0 | 0 |
| 17.750 | 0 | 0 | 0 | 0 | 0 |
| 18.000 | 0 | 0 | 0 | 0 | 0 |
| 18.250 | 0 | 0 | 0 | 0 | 0 |
| 18.500 | 0 | 0 | 0 | 0 | 0 |
| 18.750 | 0 | 0 | 0 | 0 | 0 |
| 19.000 | 0 | 0 | 0 | 0 | 0 |
| 19.250 | 0 | 0 | 0 | 0 | 0 |
| 19.500 | 0 | 0 | 0 | 0 | 0 |
| 19.750 | 0 | 0 | 0 | 0 | 0 |
| 20.000 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: 6" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 0 | 0 | 0 | 0 | 0 |
| 20.500 | 0 | 0 | 0 | 0 | 0 |
| 20.750 | 0 | 0 | 0 | 0 | 0 |
| 21.000 | 0 | 0 | 0 | 0 | 0 |
| 21.250 | 0 | 0 | 0 | 0 | 0 |
| 21.500 | 0 | 0 | 0 | 0 | 0 |
| 21.750 | 0 | 0 | 0 | 0 | 0 |
| 22.000 | 0 | 0 | 0 | 0 | 0 |
| 22.250 | 0 | 0 | 0 | 0 | 0 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: 6" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: 6" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 0 | 0 | 0 |
| 11.000 | 0 | 0 | 0 | 0 | 0 |
| 11.250 | 0 | 0 | 0 | 0 | 0 |
| 11.500 | 0 | 13 | 18 | 29 | 47 |
| 11.750 | 74 | 103 | 157 | 211 | 283 |
| 12.000 | 389 | 524 | 669 | 787 | 911 |
| 12.250 | 950 | 944 | 938 | 934 | 929 |
| 12.500 | 925 | 921 | 918 | 916 | 915 |
| 12.750 | 913 | 911 | 908 | 903 | 898 |
| 13.000 | 892 | 884 | 872 | 859 | 845 |
| 13.250 | 831 | 819 | 810 | 802 | 794 |
| 13.500 | 786 | 778 | 770 | 761 | 752 |
| 13.750 | 743 | 734 | 725 | 715 | 703 |
| 14.000 | 691 | 678 | 665 | 652 | 639 |
| 14.250 | 625 | 612 | 598 | 585 | 571 |
| 14.500 | 557 | 543 | 529 | 514 | 500 |
| 14.750 | 486 | 471 | 456 | 441 | 426 |
| 15.000 | 411 | 396 | 381 | 365 | 350 |
| 15.250 | 334 | 318 | 302 | 286 | 270 |
| 15.500 | 254 | 237 | 221 | 204 | 187 |
| 15.750 | 170 | 152 | 125 | 109 | 95 |
| 16.000 | 81 | 67 | 49 | 31 | 14 |
| 16.250 | 0 | 0 | 0 | 0 | 0 |
| 16.500 | 0 | 0 | 0 | 0 | 0 |
| 16.750 | 0 | 0 | 0 | 0 | 0 |
| 17.000 | 0 | 0 | 0 | 0 | 0 |
| 17.250 | 0 | 0 | 0 | 0 | 0 |
| 17.500 | 0 | 0 | 0 | 0 | 0 |
| 17.750 | 0 | 0 | 0 | 0 | 0 |
| 18.000 | 0 | 0 | 0 | 0 | 0 |
| 18.250 | 0 | 0 | 0 | 0 | 0 |
| 18.500 | 0 | 0 | 0 | 0 | 0 |
| 18.750 | 0 | 0 | 0 | 0 | 0 |
| 19.000 | 0 | 0 | 0 | 0 | 0 |
| 19.250 | 0 | 0 | 0 | 0 | 0 |
| 19.500 | 0 | 0 | 0 | 0 | 0 |
| 19.750 | 0 | 0 | 0 | 0 | 0 |
| 20.000 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: 6" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 20.250 | 0 | 0 | 0 | 0 | 0 |
| 20.500 | 0 | 0 | 0 | 0 | 0 |
| 20.750 | 0 | 0 | 0 | 0 | 0 |
| 21.000 | 0 | 0 | 0 | 0 | 0 |
| 21.250 | 0 | 0 | 0 | 0 | 0 |
| 21.500 | 0 | 0 | 0 | 0 | 0 |
| 21.750 | 0 | 0 | 0 | 0 | 0 |
| 22.000 | 0 | 0 | 0 | 0 | 0 |
| 22.250 | 0 | 0 | 0 | 0 | 0 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: 6" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: 6" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 0 | 0 | 0 |
| 11.000 | 0 | 0 | 0 | 0 | 12 |
| 11.250 | 15 | 18 | 23 | 29 | 37 |
| 11.500 | 46 | 58 | 74 | 95 | 128 |
| 11.750 | 188 | 250 | 326 | 414 | 528 |
| 12.000 | 691 | 894 | 1,013 | 1,017 | 995 |
| 12.250 | 973 | 962 | 954 | 947 | 940 |
| 12.500 | 934 | 928 | 924 | 921 | 920 |
| 12.750 | 919 | 918 | 917 | 917 | 916 |
| 13.000 | 915 | 915 | 914 | 912 | 910 |
| 13.250 | 907 | 904 | 901 | 897 | 893 |
| 13.500 | 889 | 882 | 874 | 866 | 856 |
| 13.750 | 847 | 836 | 826 | 817 | 810 |
| 14.000 | 803 | 797 | 790 | 783 | 776 |
| 14.250 | 768 | 761 | 753 | 746 | 738 |
| 14.500 | 730 | 722 | 713 | 703 | 692 |
| 14.750 | 682 | 671 | 659 | 648 | 637 |
| 15.000 | 625 | 613 | 601 | 589 | 577 |
| 15.250 | 564 | 551 | 539 | 526 | 512 |
| 15.500 | 499 | 486 | 472 | 458 | 444 |
| 15.750 | 430 | 415 | 401 | 386 | 371 |
| 16.000 | 356 | 341 | 326 | 310 | 295 |
| 16.250 | 279 | 263 | 248 | 232 | 216 |
| 16.500 | 200 | 184 | 168 | 149 | 123 |
| 16.750 | 109 | 96 | 83 | 70 | 53 |
| 17.000 | 36 | 19 | 0 | 0 | 0 |
| 17.250 | 0 | 0 | 0 | 0 | 0 |
| 17.500 | 0 | 0 | 0 | 0 | 0 |
| 17.750 | 0 | 0 | 0 | 0 | 0 |
| 18.000 | 0 | 0 | 0 | 0 | 0 |
| 18.250 | 0 | 0 | 0 | 0 | 0 |
| 18.500 | 0 | 0 | 0 | 0 | 0 |
| 18.750 | 0 | 0 | 0 | 0 | 0 |
| 19.000 | 0 | 0 | 0 | 0 | 0 |
| 19.250 | 0 | 0 | 0 | 0 | 0 |
| 19.500 | 0 | 0 | 0 | 0 | 0 |
| 19.750 | 0 | 0 | 0 | 0 | 0 |
| 20.000 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: 6" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 0 | 0 | 0 | 0 | 0 |
| 20.500 | 0 | 0 | 0 | 0 | 0 |
| 20.750 | 0 | 0 | 0 | 0 | 0 |
| 21.000 | 0 | 0 | 0 | 0 | 0 |
| 21.250 | 0 | 0 | 0 | 0 | 0 |
| 21.500 | 0 | 0 | 0 | 0 | 0 |
| 21.750 | 0 | 0 | 0 | 0 | 0 |
| 22.000 | 0 | 0 | 0 | 0 | 0 |
| 22.250 | 0 | 0 | 0 | 0 | 0 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 1 years

Label: MC-3500 - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 16 | 15 | 15 | 14 |
| 0.250 | 14 | 13 | 13 | 12 | 12 |
| 0.500 | 12 | 11 | 11 | 10 | 10 |
| 0.750 | 10 | 9 | 9 | 9 | 8 |
| 1.000 | 8 | 8 | 8 | 7 | 7 |
| 1.250 | 7 | 7 | 6 | 6 | 6 |
| 1.500 | 6 | 6 | 5 | 5 | 5 |
| 1.750 | 5 | 5 | 5 | 6 | 6 |
| 2.000 | 6 | 6 | 7 | 7 | 8 |
| 2.250 | 8 | 9 | 9 | 10 | 11 |
| 2.500 | 11 | 12 | 13 | 14 | 15 |
| 2.750 | 15 | 16 | 17 | 18 | 19 |
| 3.000 | 20 | 21 | 22 | 23 | 25 |
| 3.250 | 26 | 27 | 28 | 29 | 31 |
| 3.500 | 32 | 33 | 34 | 36 | 37 |
| 3.750 | 38 | 40 | 41 | 42 | 44 |
| 4.000 | 45 | 47 | 48 | 50 | 51 |
| 4.250 | 52 | 54 | 55 | 57 | 58 |
| 4.500 | 60 | 61 | 63 | 65 | 66 |
| 4.750 | 68 | 69 | 71 | 72 | 74 |
| 5.000 | 75 | 77 | 79 | 80 | 82 |
| 5.250 | 83 | 85 | 87 | 88 | 90 |
| 5.500 | 91 | 93 | 95 | 96 | 98 |
| 5.750 | 100 | 101 | 103 | 104 | 106 |
| 6.000 | 108 | 109 | 111 | 113 | 114 |
| 6.250 | 116 | 118 | 120 | 122 | 124 |
| 6.500 | 126 | 128 | 130 | 132 | 135 |
| 6.750 | 137 | 139 | 142 | 144 | 147 |
| 7.000 | 149 | 152 | 154 | 157 | 160 |
| 7.250 | 162 | 165 | 168 | 171 | 174 |
| 7.500 | 176 | 179 | 182 | 185 | 188 |
| 7.750 | 191 | 195 | 198 | 201 | 204 |
| 8.000 | 207 | 210 | 214 | 217 | 221 |
| 8.250 | 224 | 228 | 232 | 236 | 240 |
| 8.500 | 245 | 249 | 254 | 258 | 263 |
| 8.750 | 268 | 273 | 279 | 284 | 289 |
| 9.000 | 295 | 301 | 306 | 312 | 318 |
| 9.250 | 324 | 330 | 336 | 343 | 349 |
| 9.500 | 355 | 362 | 368 | 375 | 382 |
| 9.750 | 389 | 395 | 402 | 409 | 416 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 1 years

Label: MC-3500 - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 424 | 431 | 438 | 446 | 453 |
| 10.250 | 461 | 470 | 478 | 487 | 497 |
| 10.500 | 506 | 516 | 526 | 537 | 547 |
| 10.750 | 558 | 569 | 581 | 592 | 604 |
| 11.000 | 616 | 628 | 641 | 655 | 670 |
| 11.250 | 680 | 691 | 703 | 716 | 729 |
| 11.500 | 743 | 759 | 776 | 794 | 814 |
| 11.750 | 837 | 861 | 886 | 911 | 937 |
| 12.000 | 963 | 992 | 1,045 | 1,111 | 1,175 |
| 12.250 | 1,235 | 1,292 | 1,346 | 1,399 | 1,450 |
| 12.500 | 1,499 | 1,546 | 1,592 | 1,636 | 1,679 |
| 12.750 | 1,722 | 1,756 | 1,786 | 1,816 | 1,845 |
| 13.000 | 1,874 | 1,903 | 1,932 | 1,960 | 1,988 |
| 13.250 | 2,015 | 2,043 | 2,070 | 2,095 | 2,112 |
| 13.500 | 2,121 | 2,130 | 2,139 | 2,147 | 2,156 |
| 13.750 | 2,164 | 2,172 | 2,180 | 2,188 | 2,195 |
| 14.000 | 2,203 | 2,210 | 2,217 | 2,224 | 2,230 |
| 14.250 | 2,237 | 2,243 | 2,250 | 2,256 | 2,262 |
| 14.500 | 2,268 | 2,274 | 2,280 | 2,285 | 2,291 |
| 14.750 | 2,296 | 2,302 | 2,307 | 2,312 | 2,317 |
| 15.000 | 2,322 | 2,327 | 2,332 | 2,337 | 2,341 |
| 15.250 | 2,346 | 2,350 | 2,354 | 2,358 | 2,363 |
| 15.500 | 2,366 | 2,370 | 2,374 | 2,378 | 2,382 |
| 15.750 | 2,385 | 2,388 | 2,392 | 2,395 | 2,398 |
| 16.000 | 2,401 | 2,404 | 2,407 | 2,410 | 2,413 |
| 16.250 | 2,416 | 2,418 | 2,421 | 2,424 | 2,426 |
| 16.500 | 2,429 | 2,428 | 2,418 | 2,400 | 2,382 |
| 16.750 | 2,364 | 2,347 | 2,329 | 2,312 | 2,294 |
| 17.000 | 2,276 | 2,259 | 2,242 | 2,224 | 2,207 |
| 17.250 | 2,190 | 2,172 | 2,155 | 2,138 | 2,121 |
| 17.500 | 2,104 | 2,087 | 2,070 | 2,053 | 2,036 |
| 17.750 | 2,019 | 2,002 | 1,986 | 1,969 | 1,952 |
| 18.000 | 1,936 | 1,919 | 1,903 | 1,886 | 1,870 |
| 18.250 | 1,853 | 1,837 | 1,821 | 1,805 | 1,789 |
| 18.500 | 1,773 | 1,758 | 1,742 | 1,722 | 1,701 |
| 18.750 | 1,680 | 1,660 | 1,639 | 1,619 | 1,599 |
| 19.000 | 1,579 | 1,559 | 1,540 | 1,521 | 1,502 |
| 19.250 | 1,483 | 1,464 | 1,446 | 1,428 | 1,410 |
| 19.500 | 1,392 | 1,374 | 1,357 | 1,339 | 1,322 |
| 19.750 | 1,305 | 1,289 | 1,272 | 1,256 | 1,239 |
| 20.000 | 1,223 | 1,198 | 1,165 | 1,131 | 1,097 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 1 years

Label: MC-3500 - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,065 | 1,032 | 1,001 | 986 | 972 |
| 20.500 | 958 | 944 | 930 | 916 | 903 |
| 20.750 | 889 | 876 | 863 | 850 | 837 |
| 21.000 | 824 | 812 | 799 | 787 | 775 |
| 21.250 | 763 | 751 | 739 | 728 | 716 |
| 21.500 | 705 | 693 | 682 | 671 | 656 |
| 21.750 | 639 | 623 | 607 | 592 | 577 |
| 22.000 | 563 | 549 | 536 | 523 | 510 |
| 22.250 | 498 | 487 | 475 | 464 | 454 |
| 22.500 | 443 | 434 | 424 | 415 | 406 |
| 22.750 | 397 | 388 | 380 | 372 | 365 |
| 23.000 | 357 | 350 | 343 | 336 | 329 |
| 23.250 | 323 | 317 | 311 | 305 | 299 |
| 23.500 | 294 | 288 | 283 | 278 | 273 |
| 23.750 | 268 | 264 | 259 | 255 | 251 |
| 24.000 | 247 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: MC-3500 - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 16 | 15 | 15 | 14 |
| 0.250 | 14 | 13 | 13 | 12 | 12 |
| 0.500 | 12 | 11 | 11 | 10 | 10 |
| 0.750 | 10 | 9 | 9 | 9 | 9 |
| 1.000 | 9 | 9 | 9 | 10 | 11 |
| 1.250 | 12 | 13 | 14 | 15 | 17 |
| 1.500 | 18 | 20 | 22 | 23 | 25 |
| 1.750 | 27 | 29 | 31 | 34 | 36 |
| 2.000 | 38 | 40 | 43 | 45 | 47 |
| 2.250 | 50 | 52 | 55 | 57 | 60 |
| 2.500 | 63 | 65 | 68 | 71 | 74 |
| 2.750 | 76 | 79 | 82 | 85 | 88 |
| 3.000 | 91 | 94 | 97 | 100 | 103 |
| 3.250 | 106 | 109 | 112 | 115 | 118 |
| 3.500 | 121 | 124 | 127 | 130 | 133 |
| 3.750 | 137 | 140 | 143 | 146 | 149 |
| 4.000 | 152 | 155 | 159 | 162 | 165 |
| 4.250 | 168 | 171 | 174 | 177 | 180 |
| 4.500 | 184 | 187 | 190 | 193 | 196 |
| 4.750 | 199 | 202 | 205 | 208 | 212 |
| 5.000 | 215 | 218 | 221 | 224 | 227 |
| 5.250 | 230 | 233 | 236 | 239 | 242 |
| 5.500 | 245 | 248 | 251 | 254 | 257 |
| 5.750 | 260 | 263 | 266 | 269 | 272 |
| 6.000 | 275 | 278 | 281 | 284 | 287 |
| 6.250 | 290 | 293 | 297 | 300 | 304 |
| 6.500 | 308 | 312 | 316 | 320 | 324 |
| 6.750 | 328 | 333 | 337 | 342 | 346 |
| 7.000 | 351 | 356 | 361 | 366 | 371 |
| 7.250 | 376 | 381 | 386 | 391 | 397 |
| 7.500 | 402 | 407 | 413 | 419 | 424 |
| 7.750 | 430 | 436 | 441 | 447 | 453 |
| 8.000 | 459 | 465 | 471 | 477 | 484 |
| 8.250 | 490 | 497 | 505 | 512 | 520 |
| 8.500 | 528 | 537 | 545 | 554 | 564 |
| 8.750 | 573 | 583 | 593 | 603 | 613 |
| 9.000 | 623 | 634 | 645 | 656 | 667 |
| 9.250 | 675 | 682 | 690 | 698 | 706 |
| 9.500 | 715 | 724 | 733 | 742 | 751 |
| 9.750 | 761 | 771 | 780 | 790 | 800 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: MC-3500 - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 811 | 821 | 831 | 842 | 853 |
| 10.250 | 864 | 875 | 887 | 899 | 911 |
| 10.500 | 924 | 937 | 950 | 964 | 977 |
| 10.750 | 992 | 1,011 | 1,043 | 1,075 | 1,107 |
| 11.000 | 1,139 | 1,171 | 1,204 | 1,236 | 1,270 |
| 11.250 | 1,304 | 1,338 | 1,374 | 1,411 | 1,448 |
| 11.500 | 1,487 | 1,527 | 1,570 | 1,617 | 1,666 |
| 11.750 | 1,717 | 1,761 | 1,802 | 1,845 | 1,891 |
| 12.000 | 1,944 | 2,006 | 2,074 | 2,142 | 2,319 |
| 12.250 | 2,561 | 2,748 | 2,905 | 3,035 | 3,142 |
| 12.500 | 3,227 | 3,291 | 3,339 | 3,375 | 3,404 |
| 12.750 | 3,429 | 3,451 | 3,470 | 3,487 | 3,500 |
| 13.000 | 3,512 | 3,521 | 3,528 | 3,534 | 3,538 |
| 13.250 | 3,542 | 3,545 | 3,548 | 3,550 | 3,551 |
| 13.500 | 3,552 | 3,552 | 3,552 | 3,551 | 3,550 |
| 13.750 | 3,548 | 3,546 | 3,543 | 3,540 | 3,536 |
| 14.000 | 3,532 | 3,528 | 3,523 | 3,518 | 3,513 |
| 14.250 | 3,508 | 3,503 | 3,497 | 3,492 | 3,486 |
| 14.500 | 3,481 | 3,475 | 3,469 | 3,463 | 3,457 |
| 14.750 | 3,452 | 3,446 | 3,441 | 3,435 | 3,430 |
| 15.000 | 3,425 | 3,420 | 3,415 | 3,410 | 3,406 |
| 15.250 | 3,401 | 3,397 | 3,393 | 3,389 | 3,384 |
| 15.500 | 3,381 | 3,377 | 3,370 | 3,354 | 3,333 |
| 15.750 | 3,313 | 3,293 | 3,273 | 3,254 | 3,236 |
| 16.000 | 3,218 | 3,200 | 3,183 | 3,167 | 3,151 |
| 16.250 | 3,135 | 3,120 | 3,105 | 3,091 | 3,077 |
| 16.500 | 3,063 | 3,050 | 3,037 | 3,024 | 3,012 |
| 16.750 | 3,000 | 2,988 | 2,977 | 2,966 | 2,955 |
| 17.000 | 2,944 | 2,934 | 2,924 | 2,914 | 2,905 |
| 17.250 | 2,895 | 2,886 | 2,877 | 2,869 | 2,860 |
| 17.500 | 2,852 | 2,844 | 2,836 | 2,828 | 2,821 |
| 17.750 | 2,814 | 2,807 | 2,800 | 2,793 | 2,786 |
| 18.000 | 2,779 | 2,773 | 2,767 | 2,761 | 2,755 |
| 18.250 | 2,749 | 2,743 | 2,738 | 2,733 | 2,727 |
| 18.500 | 2,722 | 2,717 | 2,713 | 2,708 | 2,704 |
| 18.750 | 2,699 | 2,695 | 2,691 | 2,687 | 2,683 |
| 19.000 | 2,679 | 2,675 | 2,671 | 2,668 | 2,664 |
| 19.250 | 2,661 | 2,658 | 2,655 | 2,651 | 2,648 |
| 19.500 | 2,645 | 2,643 | 2,640 | 2,637 | 2,634 |
| 19.750 | 2,632 | 2,629 | 2,627 | 2,624 | 2,622 |
| 20.000 | 2,619 | 2,617 | 2,615 | 2,613 | 2,611 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: MC-3500 - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 2,609 | 2,607 | 2,605 | 2,603 | 2,601 |
| 20.500 | 2,599 | 2,597 | 2,595 | 2,594 | 2,592 |
| 20.750 | 2,590 | 2,589 | 2,587 | 2,586 | 2,584 |
| 21.000 | 2,583 | 2,581 | 2,580 | 2,579 | 2,577 |
| 21.250 | 2,576 | 2,575 | 2,573 | 2,572 | 2,571 |
| 21.500 | 2,570 | 2,569 | 2,567 | 2,566 | 2,565 |
| 21.750 | 2,564 | 2,563 | 2,562 | 2,561 | 2,560 |
| 22.000 | 2,559 | 2,558 | 2,557 | 2,556 | 2,555 |
| 22.250 | 2,554 | 2,554 | 2,553 | 2,552 | 2,551 |
| 22.500 | 2,540 | 2,519 | 2,498 | 2,478 | 2,458 |
| 22.750 | 2,438 | 2,419 | 2,400 | 2,381 | 2,361 |
| 23.000 | 2,342 | 2,324 | 2,305 | 2,286 | 2,268 |
| 23.250 | 2,249 | 2,231 | 2,212 | 2,194 | 2,176 |
| 23.500 | 2,158 | 2,140 | 2,123 | 2,105 | 2,087 |
| 23.750 | 2,070 | 2,052 | 2,035 | 2,018 | 2,001 |
| 24.000 | 1,984 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: MC-3500 - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 16 | 15 | 15 | 14 |
| 0.250 | 14 | 13 | 13 | 12 | 12 |
| 0.500 | 12 | 11 | 11 | 10 | 10 |
| 0.750 | 10 | 10 | 10 | 11 | 12 |
| 1.000 | 13 | 14 | 16 | 18 | 20 |
| 1.250 | 22 | 24 | 27 | 30 | 32 |
| 1.500 | 35 | 38 | 41 | 44 | 48 |
| 1.750 | 51 | 54 | 57 | 61 | 64 |
| 2.000 | 68 | 71 | 75 | 78 | 82 |
| 2.250 | 85 | 89 | 92 | 96 | 100 |
| 2.500 | 104 | 107 | 111 | 115 | 119 |
| 2.750 | 123 | 127 | 131 | 135 | 139 |
| 3.000 | 143 | 147 | 151 | 155 | 159 |
| 3.250 | 163 | 167 | 171 | 175 | 179 |
| 3.500 | 183 | 187 | 191 | 195 | 199 |
| 3.750 | 203 | 207 | 211 | 215 | 219 |
| 4.000 | 223 | 227 | 231 | 235 | 239 |
| 4.250 | 243 | 247 | 251 | 255 | 259 |
| 4.500 | 263 | 267 | 271 | 275 | 279 |
| 4.750 | 283 | 287 | 290 | 294 | 298 |
| 5.000 | 302 | 306 | 310 | 313 | 317 |
| 5.250 | 321 | 325 | 328 | 332 | 336 |
| 5.500 | 339 | 343 | 347 | 351 | 354 |
| 5.750 | 358 | 361 | 365 | 369 | 372 |
| 6.000 | 376 | 379 | 383 | 387 | 391 |
| 6.250 | 394 | 399 | 403 | 407 | 412 |
| 6.500 | 417 | 421 | 426 | 431 | 437 |
| 6.750 | 442 | 447 | 453 | 459 | 465 |
| 7.000 | 470 | 476 | 482 | 489 | 495 |
| 7.250 | 501 | 508 | 514 | 521 | 528 |
| 7.500 | 534 | 541 | 548 | 555 | 563 |
| 7.750 | 570 | 577 | 584 | 592 | 599 |
| 8.000 | 607 | 614 | 622 | 630 | 639 |
| 8.250 | 647 | 656 | 666 | 673 | 679 |
| 8.500 | 686 | 693 | 701 | 709 | 717 |
| 8.750 | 726 | 735 | 744 | 754 | 764 |
| 9.000 | 773 | 783 | 794 | 804 | 815 |
| 9.250 | 825 | 836 | 847 | 858 | 869 |
| 9.500 | 881 | 892 | 904 | 916 | 928 |
| 9.750 | 940 | 952 | 964 | 977 | 989 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: MC-3500 - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 1,003 | 1,031 | 1,060 | 1,089 | 1,119 |
| 10.250 | 1,150 | 1,181 | 1,212 | 1,243 | 1,275 |
| 10.500 | 1,306 | 1,337 | 1,369 | 1,400 | 1,432 |
| 10.750 | 1,463 | 1,495 | 1,527 | 1,559 | 1,591 |
| 11.000 | 1,623 | 1,655 | 1,688 | 1,721 | 1,750 |
| 11.250 | 1,776 | 1,803 | 1,831 | 1,860 | 1,890 |
| 11.500 | 1,921 | 1,953 | 1,987 | 2,021 | 2,058 |
| 11.750 | 2,097 | 2,139 | 2,184 | 2,232 | 2,285 |
| 12.000 | 2,348 | 2,456 | 2,802 | 3,272 | 3,626 |
| 12.250 | 3,939 | 4,240 | 4,522 | 4,779 | 5,001 |
| 12.500 | 5,182 | 5,317 | 5,413 | 5,477 | 5,520 |
| 12.750 | 5,549 | 5,567 | 5,577 | 5,580 | 5,577 |
| 13.000 | 5,568 | 5,553 | 5,535 | 5,512 | 5,488 |
| 13.250 | 5,461 | 5,433 | 5,404 | 5,374 | 5,343 |
| 13.500 | 5,311 | 5,279 | 5,245 | 5,210 | 5,175 |
| 13.750 | 5,139 | 5,103 | 5,066 | 5,028 | 4,990 |
| 14.000 | 4,952 | 4,913 | 4,874 | 4,834 | 4,795 |
| 14.250 | 4,756 | 4,717 | 4,679 | 4,641 | 4,604 |
| 14.500 | 4,568 | 4,533 | 4,498 | 4,465 | 4,432 |
| 14.750 | 4,400 | 4,368 | 4,338 | 4,308 | 4,278 |
| 15.000 | 4,250 | 4,222 | 4,194 | 4,167 | 4,141 |
| 15.250 | 4,115 | 4,089 | 4,065 | 4,040 | 4,016 |
| 15.500 | 3,993 | 3,970 | 3,948 | 3,927 | 3,906 |
| 15.750 | 3,886 | 3,866 | 3,847 | 3,829 | 3,810 |
| 16.000 | 3,793 | 3,776 | 3,759 | 3,743 | 3,728 |
| 16.250 | 3,705 | 3,674 | 3,643 | 3,613 | 3,583 |
| 16.500 | 3,555 | 3,528 | 3,501 | 3,475 | 3,450 |
| 16.750 | 3,425 | 3,402 | 3,379 | 3,356 | 3,335 |
| 17.000 | 3,314 | 3,293 | 3,273 | 3,254 | 3,235 |
| 17.250 | 3,217 | 3,199 | 3,182 | 3,166 | 3,150 |
| 17.500 | 3,134 | 3,118 | 3,103 | 3,089 | 3,075 |
| 17.750 | 3,061 | 3,047 | 3,034 | 3,021 | 3,009 |
| 18.000 | 2,997 | 2,985 | 2,973 | 2,962 | 2,951 |
| 18.250 | 2,940 | 2,930 | 2,920 | 2,910 | 2,900 |
| 18.500 | 2,891 | 2,882 | 2,873 | 2,865 | 2,857 |
| 18.750 | 2,849 | 2,841 | 2,833 | 2,826 | 2,819 |
| 19.000 | 2,812 | 2,805 | 2,798 | 2,792 | 2,785 |
| 19.250 | 2,779 | 2,773 | 2,768 | 2,762 | 2,756 |
| 19.500 | 2,751 | 2,746 | 2,741 | 2,736 | 2,731 |
| 19.750 | 2,727 | 2,722 | 2,718 | 2,713 | 2,709 |
| 20.000 | 2,705 | 2,701 | 2,697 | 2,693 | 2,689 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: MC-3500 - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 2,686 | 2,682 | 2,679 | 2,676 | 2,672 |
| 20.500 | 2,669 | 2,666 | 2,663 | 2,660 | 2,657 |
| 20.750 | 2,654 | 2,652 | 2,649 | 2,647 | 2,644 |
| 21.000 | 2,641 | 2,639 | 2,637 | 2,634 | 2,632 |
| 21.250 | 2,630 | 2,628 | 2,626 | 2,624 | 2,622 |
| 21.500 | 2,620 | 2,618 | 2,616 | 2,614 | 2,612 |
| 21.750 | 2,611 | 2,609 | 2,607 | 2,605 | 2,604 |
| 22.000 | 2,602 | 2,601 | 2,599 | 2,598 | 2,596 |
| 22.250 | 2,595 | 2,593 | 2,592 | 2,591 | 2,589 |
| 22.500 | 2,588 | 2,587 | 2,585 | 2,584 | 2,583 |
| 22.750 | 2,582 | 2,581 | 2,579 | 2,578 | 2,577 |
| 23.000 | 2,576 | 2,575 | 2,574 | 2,573 | 2,572 |
| 23.250 | 2,571 | 2,570 | 2,569 | 2,568 | 2,567 |
| 23.500 | 2,566 | 2,565 | 2,564 | 2,563 | 2,562 |
| 23.750 | 2,558 | 2,544 | 2,523 | 2,502 | 2,482 |
| 24.000 | 2,463 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: MC-3500 - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 16 | 15 | 15 | 14 |
| 0.250 | 14 | 13 | 13 | 12 | 12 |
| 0.500 | 12 | 11 | 12 | 12 | 14 |
| 0.750 | 16 | 18 | 21 | 24 | 28 |
| 1.000 | 32 | 36 | 41 | 46 | 51 |
| 1.250 | 56 | 61 | 67 | 72 | 78 |
| 1.500 | 84 | 90 | 95 | 101 | 107 |
| 1.750 | 113 | 119 | 125 | 131 | 137 |
| 2.000 | 143 | 148 | 154 | 160 | 166 |
| 2.250 | 172 | 178 | 183 | 189 | 195 |
| 2.500 | 201 | 207 | 213 | 219 | 225 |
| 2.750 | 231 | 237 | 243 | 249 | 255 |
| 3.000 | 261 | 267 | 273 | 279 | 285 |
| 3.250 | 290 | 296 | 302 | 308 | 314 |
| 3.500 | 320 | 326 | 331 | 337 | 343 |
| 3.750 | 349 | 354 | 360 | 366 | 371 |
| 4.000 | 377 | 383 | 388 | 394 | 399 |
| 4.250 | 405 | 410 | 416 | 421 | 427 |
| 4.500 | 432 | 437 | 443 | 448 | 453 |
| 4.750 | 459 | 464 | 469 | 474 | 480 |
| 5.000 | 485 | 490 | 495 | 500 | 505 |
| 5.250 | 510 | 515 | 520 | 526 | 530 |
| 5.500 | 535 | 540 | 545 | 550 | 555 |
| 5.750 | 560 | 565 | 570 | 575 | 580 |
| 6.000 | 584 | 589 | 594 | 599 | 605 |
| 6.250 | 610 | 616 | 622 | 628 | 634 |
| 6.500 | 641 | 648 | 655 | 662 | 669 |
| 6.750 | 674 | 679 | 684 | 690 | 695 |
| 7.000 | 701 | 707 | 714 | 720 | 727 |
| 7.250 | 734 | 741 | 749 | 756 | 764 |
| 7.500 | 772 | 780 | 789 | 797 | 806 |
| 7.750 | 815 | 824 | 833 | 842 | 851 |
| 8.000 | 860 | 869 | 879 | 888 | 898 |
| 8.250 | 908 | 918 | 929 | 940 | 951 |
| 8.500 | 962 | 974 | 985 | 997 | 1,020 |
| 8.750 | 1,047 | 1,076 | 1,104 | 1,134 | 1,164 |
| 9.000 | 1,194 | 1,224 | 1,255 | 1,285 | 1,315 |
| 9.250 | 1,345 | 1,375 | 1,405 | 1,436 | 1,466 |
| 9.500 | 1,496 | 1,526 | 1,555 | 1,585 | 1,615 |
| 9.750 | 1,645 | 1,675 | 1,705 | 1,735 | 1,757 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: MC-3500 - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 1,779 | 1,801 | 1,823 | 1,845 | 1,867 |
| 10.250 | 1,890 | 1,913 | 1,937 | 1,961 | 1,985 |
| 10.500 | 2,009 | 2,034 | 2,059 | 2,084 | 2,110 |
| 10.750 | 2,136 | 2,163 | 2,189 | 2,216 | 2,244 |
| 11.000 | 2,271 | 2,300 | 2,328 | 2,358 | 2,389 |
| 11.250 | 2,420 | 2,451 | 2,482 | 2,513 | 2,544 |
| 11.500 | 2,574 | 2,604 | 2,636 | 2,668 | 2,704 |
| 11.750 | 2,743 | 2,786 | 2,875 | 3,113 | 3,466 |
| 12.000 | 3,905 | 4,479 | 5,339 | 6,448 | 7,501 |
| 12.250 | 8,338 | 9,011 | 9,521 | 9,960 | 10,266 |
| 12.500 | 10,504 | 10,660 | 10,748 | 10,790 | 10,803 |
| 12.750 | 10,798 | 10,778 | 10,747 | 10,706 | 10,655 |
| 13.000 | 10,596 | 10,529 | 10,457 | 10,381 | 10,302 |
| 13.250 | 10,222 | 10,147 | 10,071 | 9,995 | 9,918 |
| 13.500 | 9,837 | 9,747 | 9,656 | 9,566 | 9,475 |
| 13.750 | 9,392 | 9,311 | 9,230 | 9,149 | 9,067 |
| 14.000 | 8,984 | 8,896 | 8,806 | 8,715 | 8,625 |
| 14.250 | 8,535 | 8,445 | 8,360 | 8,278 | 8,196 |
| 14.500 | 8,114 | 8,033 | 7,952 | 7,872 | 7,790 |
| 14.750 | 7,706 | 7,623 | 7,541 | 7,459 | 7,378 |
| 15.000 | 7,297 | 7,217 | 7,140 | 7,063 | 6,987 |
| 15.250 | 6,912 | 6,837 | 6,762 | 6,688 | 6,615 |
| 15.500 | 6,540 | 6,466 | 6,393 | 6,320 | 6,249 |
| 15.750 | 6,178 | 6,108 | 6,038 | 5,970 | 5,903 |
| 16.000 | 5,838 | 5,774 | 5,710 | 5,648 | 5,587 |
| 16.250 | 5,526 | 5,467 | 5,409 | 5,352 | 5,295 |
| 16.500 | 5,239 | 5,183 | 5,129 | 5,075 | 5,022 |
| 16.750 | 4,970 | 4,920 | 4,870 | 4,821 | 4,773 |
| 17.000 | 4,727 | 4,681 | 4,631 | 4,575 | 4,516 |
| 17.250 | 4,460 | 4,405 | 4,352 | 4,301 | 4,251 |
| 17.500 | 4,203 | 4,156 | 4,110 | 4,066 | 4,023 |
| 17.750 | 3,982 | 3,942 | 3,902 | 3,864 | 3,827 |
| 18.000 | 3,791 | 3,756 | 3,721 | 3,688 | 3,656 |
| 18.250 | 3,625 | 3,595 | 3,566 | 3,538 | 3,511 |
| 18.500 | 3,484 | 3,458 | 3,434 | 3,410 | 3,386 |
| 18.750 | 3,364 | 3,342 | 3,321 | 3,300 | 3,280 |
| 19.000 | 3,261 | 3,242 | 3,224 | 3,206 | 3,189 |
| 19.250 | 3,173 | 3,157 | 3,141 | 3,126 | 3,112 |
| 19.500 | 3,097 | 3,084 | 3,070 | 3,057 | 3,044 |
| 19.750 | 3,032 | 3,020 | 3,008 | 2,997 | 2,986 |
| 20.000 | 2,975 | 2,965 | 2,955 | 2,945 | 2,935 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: MC-3500 - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 2,926 | 2,917 | 2,908 | 2,900 | 2,891 |
| 20.500 | 2,883 | 2,875 | 2,868 | 2,860 | 2,853 |
| 20.750 | 2,846 | 2,839 | 2,832 | 2,826 | 2,819 |
| 21.000 | 2,813 | 2,807 | 2,801 | 2,796 | 2,790 |
| 21.250 | 2,785 | 2,779 | 2,774 | 2,769 | 2,764 |
| 21.500 | 2,760 | 2,755 | 2,751 | 2,746 | 2,742 |
| 21.750 | 2,738 | 2,734 | 2,730 | 2,726 | 2,722 |
| 22.000 | 2,718 | 2,715 | 2,711 | 2,708 | 2,704 |
| 22.250 | 2,701 | 2,698 | 2,695 | 2,692 | 2,689 |
| 22.500 | 2,686 | 2,683 | 2,680 | 2,677 | 2,675 |
| 22.750 | 2,672 | 2,670 | 2,667 | 2,665 | 2,662 |
| 23.000 | 2,660 | 2,658 | 2,655 | 2,653 | 2,651 |
| 23.250 | 2,649 | 2,647 | 2,645 | 2,643 | 2,641 |
| 23.500 | 2,639 | 2,637 | 2,635 | 2,633 | 2,631 |
| 23.750 | 2,629 | 2,628 | 2,626 | 2,624 | 2,623 |
| 24.000 | 2,621 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 1 years

Label: MC-3500 - 3

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 1 | 2 | 2 | 3 |
| 8.250 | 5 | 6 | 8 | 10 | 12 |
| 8.500 | 14 | 16 | 19 | 22 | 25 |
| 8.750 | 29 | 32 | 36 | 40 | 45 |
| 9.000 | 49 | 54 | 59 | 64 | 70 |
| 9.250 | 76 | 82 | 88 | 95 | 101 |
| 9.500 | 109 | 116 | 123 | 131 | 139 |
| 9.750 | 148 | 156 | 165 | 174 | 184 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 1 years

Label: MC-3500 - 3

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 193 | 203 | 214 | 224 | 235 |
| 10.250 | 247 | 259 | 271 | 285 | 298 |
| 10.500 | 312 | 327 | 343 | 359 | 375 |
| 10.750 | 392 | 410 | 429 | 447 | 467 |
| 11.000 | 487 | 508 | 530 | 553 | 579 |
| 11.250 | 607 | 637 | 671 | 707 | 747 |
| 11.500 | 789 | 836 | 893 | 967 | 1,064 |
| 11.750 | 1,194 | 1,358 | 1,533 | 1,685 | 1,873 |
| 12.000 | 2,132 | 2,792 | 3,714 | 4,452 | 5,058 |
| 12.250 | 5,498 | 5,790 | 5,980 | 6,091 | 6,135 |
| 12.500 | 6,118 | 6,047 | 5,934 | 5,791 | 5,633 |
| 12.750 | 5,470 | 5,305 | 5,142 | 4,982 | 4,826 |
| 13.000 | 4,672 | 4,521 | 4,375 | 4,232 | 4,095 |
| 13.250 | 3,964 | 3,829 | 3,666 | 3,510 | 3,362 |
| 13.500 | 3,220 | 3,085 | 2,955 | 2,832 | 2,713 |
| 13.750 | 2,600 | 2,491 | 2,387 | 2,286 | 2,211 |
| 14.000 | 2,169 | 2,128 | 2,089 | 2,052 | 2,016 |
| 14.250 | 1,982 | 1,949 | 1,918 | 1,888 | 1,859 |
| 14.500 | 1,832 | 1,806 | 1,781 | 1,757 | 1,734 |
| 14.750 | 1,711 | 1,690 | 1,670 | 1,650 | 1,631 |
| 15.000 | 1,612 | 1,595 | 1,577 | 1,561 | 1,545 |
| 15.250 | 1,529 | 1,514 | 1,499 | 1,484 | 1,461 |
| 15.500 | 1,439 | 1,416 | 1,395 | 1,373 | 1,352 |
| 15.750 | 1,331 | 1,310 | 1,289 | 1,268 | 1,248 |
| 16.000 | 1,228 | 1,208 | 1,188 | 1,169 | 1,150 |
| 16.250 | 1,131 | 1,113 | 1,096 | 1,079 | 1,062 |
| 16.500 | 1,046 | 1,031 | 1,015 | 1,001 | 986 |
| 16.750 | 972 | 958 | 945 | 931 | 919 |
| 17.000 | 906 | 893 | 881 | 869 | 858 |
| 17.250 | 846 | 835 | 824 | 813 | 802 |
| 17.500 | 792 | 781 | 771 | 761 | 751 |
| 17.750 | 741 | 731 | 721 | 712 | 702 |
| 18.000 | 693 | 684 | 675 | 666 | 657 |
| 18.250 | 648 | 640 | 632 | 625 | 618 |
| 18.500 | 611 | 604 | 597 | 591 | 584 |
| 18.750 | 578 | 573 | 567 | 562 | 556 |
| 19.000 | 551 | 546 | 541 | 536 | 532 |
| 19.250 | 527 | 523 | 519 | 514 | 510 |
| 19.500 | 506 | 502 | 499 | 495 | 491 |
| 19.750 | 487 | 484 | 480 | 477 | 474 |
| 20.000 | 470 | 467 | 464 | 461 | 458 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 1 years

Label: MC-3500 - 3

Storm Event: 1 year

Scenario: Post-Development 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 455 | 452 | 449 | 446 | 443 |
| 20.500 | 441 | 438 | 435 | 433 | 430 |
| 20.750 | 428 | 425 | 423 | 420 | 418 |
| 21.000 | 416 | 413 | 411 | 409 | 407 |
| 21.250 | 405 | 403 | 400 | 398 | 396 |
| 21.500 | 394 | 392 | 390 | 388 | 386 |
| 21.750 | 384 | 382 | 380 | 378 | 376 |
| 22.000 | 374 | 373 | 371 | 369 | 367 |
| 22.250 | 365 | 363 | 361 | 359 | 358 |
| 22.500 | 356 | 354 | 352 | 350 | 349 |
| 22.750 | 347 | 345 | 343 | 341 | 340 |
| 23.000 | 338 | 336 | 334 | 332 | 331 |
| 23.250 | 329 | 327 | 325 | 324 | 322 |
| 23.500 | 320 | 318 | 317 | 315 | 313 |
| 23.750 | 311 | 310 | 308 | 306 | 304 |
| 24.000 | 303 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: MC-3500 - 3

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 1 | 1 | 2 |
| 5.500 | 3 | 4 | 5 | 7 | 8 |
| 5.750 | 10 | 12 | 14 | 17 | 19 |
| 6.000 | 22 | 25 | 28 | 31 | 34 |
| 6.250 | 37 | 41 | 45 | 49 | 53 |
| 6.500 | 57 | 61 | 66 | 71 | 76 |
| 6.750 | 81 | 86 | 92 | 98 | 104 |
| 7.000 | 110 | 116 | 123 | 129 | 136 |
| 7.250 | 143 | 150 | 158 | 165 | 173 |
| 7.500 | 181 | 189 | 198 | 206 | 215 |
| 7.750 | 224 | 233 | 243 | 252 | 262 |
| 8.000 | 272 | 282 | 292 | 303 | 314 |
| 8.250 | 325 | 337 | 349 | 362 | 376 |
| 8.500 | 390 | 404 | 419 | 434 | 450 |
| 8.750 | 467 | 483 | 501 | 519 | 537 |
| 9.000 | 556 | 575 | 595 | 616 | 636 |
| 9.250 | 658 | 680 | 702 | 725 | 748 |
| 9.500 | 772 | 796 | 821 | 846 | 871 |
| 9.750 | 898 | 924 | 951 | 979 | 1,006 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: MC-3500 - 3

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 1,035 | 1,064 | 1,093 | 1,123 | 1,155 |
| 10.250 | 1,188 | 1,222 | 1,257 | 1,294 | 1,332 |
| 10.500 | 1,372 | 1,413 | 1,455 | 1,494 | 1,522 |
| 10.750 | 1,550 | 1,579 | 1,608 | 1,637 | 1,667 |
| 11.000 | 1,698 | 1,729 | 1,762 | 1,796 | 1,834 |
| 11.250 | 1,876 | 1,922 | 1,972 | 2,027 | 2,086 |
| 11.500 | 2,148 | 2,218 | 2,392 | 2,637 | 2,969 |
| 11.750 | 3,409 | 3,939 | 4,436 | 5,024 | 5,744 |
| 12.000 | 6,723 | 8,042 | 9,556 | 11,070 | 12,309 |
| 12.250 | 13,119 | 13,589 | 13,813 | 13,858 | 13,759 |
| 12.500 | 13,538 | 13,218 | 12,833 | 12,403 | 11,959 |
| 12.750 | 11,516 | 11,085 | 10,674 | 10,283 | 9,916 |
| 13.000 | 9,563 | 9,223 | 8,896 | 8,583 | 8,283 |
| 13.250 | 7,999 | 7,732 | 7,480 | 7,243 | 7,020 |
| 13.500 | 6,809 | 6,608 | 6,415 | 6,230 | 6,053 |
| 13.750 | 5,883 | 5,719 | 5,562 | 5,410 | 5,262 |
| 14.000 | 5,120 | 4,982 | 4,850 | 4,723 | 4,601 |
| 14.250 | 4,484 | 4,373 | 4,266 | 4,164 | 4,066 |
| 14.500 | 3,973 | 3,883 | 3,772 | 3,659 | 3,551 |
| 14.750 | 3,447 | 3,346 | 3,250 | 3,157 | 3,067 |
| 15.000 | 2,981 | 2,897 | 2,816 | 2,738 | 2,662 |
| 15.250 | 2,588 | 2,516 | 2,447 | 2,379 | 2,313 |
| 15.500 | 2,249 | 2,209 | 2,181 | 2,154 | 2,128 |
| 15.750 | 2,101 | 2,076 | 2,051 | 2,026 | 2,002 |
| 16.000 | 1,978 | 1,954 | 1,931 | 1,909 | 1,887 |
| 16.250 | 1,866 | 1,846 | 1,826 | 1,808 | 1,789 |
| 16.500 | 1,772 | 1,755 | 1,739 | 1,723 | 1,707 |
| 16.750 | 1,692 | 1,678 | 1,664 | 1,650 | 1,637 |
| 17.000 | 1,624 | 1,611 | 1,599 | 1,587 | 1,575 |
| 17.250 | 1,564 | 1,552 | 1,541 | 1,530 | 1,519 |
| 17.500 | 1,509 | 1,499 | 1,488 | 1,473 | 1,457 |
| 17.750 | 1,441 | 1,425 | 1,409 | 1,393 | 1,377 |
| 18.000 | 1,361 | 1,345 | 1,329 | 1,314 | 1,298 |
| 18.250 | 1,284 | 1,269 | 1,255 | 1,242 | 1,229 |
| 18.500 | 1,216 | 1,204 | 1,192 | 1,181 | 1,170 |
| 18.750 | 1,159 | 1,148 | 1,138 | 1,128 | 1,118 |
| 19.000 | 1,109 | 1,100 | 1,091 | 1,082 | 1,073 |
| 19.250 | 1,065 | 1,057 | 1,048 | 1,041 | 1,033 |
| 19.500 | 1,025 | 1,018 | 1,011 | 1,003 | 996 |
| 19.750 | 989 | 983 | 976 | 969 | 963 |
| 20.000 | 956 | 950 | 944 | 938 | 931 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: MC-3500 - 3

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 926 | 920 | 914 | 909 | 903 |
| 20.500 | 898 | 892 | 887 | 882 | 877 |
| 20.750 | 872 | 867 | 862 | 857 | 853 |
| 21.000 | 848 | 844 | 839 | 835 | 830 |
| 21.250 | 826 | 821 | 817 | 813 | 809 |
| 21.500 | 804 | 800 | 796 | 792 | 788 |
| 21.750 | 784 | 780 | 776 | 772 | 768 |
| 22.000 | 764 | 760 | 756 | 753 | 749 |
| 22.250 | 745 | 741 | 737 | 733 | 730 |
| 22.500 | 726 | 722 | 718 | 715 | 711 |
| 22.750 | 707 | 704 | 700 | 696 | 693 |
| 23.000 | 689 | 685 | 682 | 678 | 674 |
| 23.250 | 671 | 667 | 663 | 660 | 656 |
| 23.500 | 653 | 649 | 645 | 642 | 638 |
| 23.750 | 635 | 631 | 628 | 624 | 620 |
| 24.000 | 617 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: MC-3500 - 3

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 1 |
| 4.500 | 1 | 2 | 3 | 5 | 6 |
| 4.750 | 8 | 10 | 13 | 15 | 18 |
| 5.000 | 21 | 25 | 28 | 32 | 36 |
| 5.250 | 40 | 44 | 48 | 52 | 57 |
| 5.500 | 62 | 67 | 72 | 77 | 82 |
| 5.750 | 87 | 93 | 99 | 104 | 110 |
| 6.000 | 116 | 122 | 128 | 135 | 141 |
| 6.250 | 148 | 155 | 162 | 169 | 177 |
| 6.500 | 185 | 193 | 201 | 210 | 219 |
| 6.750 | 228 | 237 | 246 | 256 | 266 |
| 7.000 | 277 | 287 | 298 | 309 | 320 |
| 7.250 | 331 | 343 | 355 | 367 | 380 |
| 7.500 | 392 | 405 | 418 | 432 | 445 |
| 7.750 | 459 | 473 | 487 | 502 | 516 |
| 8.000 | 531 | 546 | 562 | 578 | 594 |
| 8.250 | 612 | 629 | 648 | 667 | 687 |
| 8.500 | 708 | 730 | 752 | 775 | 798 |
| 8.750 | 823 | 848 | 873 | 900 | 927 |
| 9.000 | 954 | 983 | 1,012 | 1,041 | 1,072 |
| 9.250 | 1,102 | 1,134 | 1,166 | 1,199 | 1,232 |
| 9.500 | 1,266 | 1,301 | 1,336 | 1,371 | 1,408 |
| 9.750 | 1,444 | 1,482 | 1,507 | 1,531 | 1,554 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: MC-3500 - 3

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 1,578 | 1,602 | 1,626 | 1,651 | 1,676 |
| 10.250 | 1,702 | 1,730 | 1,758 | 1,787 | 1,817 |
| 10.500 | 1,848 | 1,880 | 1,912 | 1,946 | 1,980 |
| 10.750 | 2,016 | 2,052 | 2,088 | 2,126 | 2,164 |
| 11.000 | 2,203 | 2,259 | 2,351 | 2,450 | 2,559 |
| 11.250 | 2,681 | 2,815 | 2,962 | 3,123 | 3,296 |
| 11.500 | 3,481 | 3,687 | 3,920 | 4,164 | 4,495 |
| 11.750 | 4,934 | 5,491 | 6,161 | 6,951 | 7,922 |
| 12.000 | 9,227 | 10,950 | 12,909 | 14,841 | 16,347 |
| 12.250 | 17,309 | 17,760 | 17,897 | 17,817 | 17,570 |
| 12.500 | 17,174 | 16,657 | 16,064 | 15,455 | 14,839 |
| 12.750 | 14,229 | 13,647 | 13,104 | 12,600 | 12,122 |
| 13.000 | 11,666 | 11,224 | 10,806 | 10,411 | 10,043 |
| 13.250 | 9,699 | 9,375 | 9,070 | 8,782 | 8,508 |
| 13.500 | 8,247 | 8,001 | 7,768 | 7,548 | 7,339 |
| 13.750 | 7,140 | 6,952 | 6,772 | 6,598 | 6,430 |
| 14.000 | 6,267 | 6,109 | 5,956 | 5,809 | 5,668 |
| 14.250 | 5,533 | 5,402 | 5,277 | 5,156 | 5,041 |
| 14.500 | 4,930 | 4,823 | 4,721 | 4,623 | 4,528 |
| 14.750 | 4,436 | 4,348 | 4,263 | 4,181 | 4,101 |
| 15.000 | 4,024 | 3,949 | 3,876 | 3,784 | 3,690 |
| 15.250 | 3,599 | 3,511 | 3,425 | 3,340 | 3,258 |
| 15.500 | 3,178 | 3,100 | 3,023 | 2,948 | 2,874 |
| 15.750 | 2,802 | 2,731 | 2,661 | 2,592 | 2,525 |
| 16.000 | 2,458 | 2,393 | 2,329 | 2,266 | 2,218 |
| 16.250 | 2,192 | 2,166 | 2,141 | 2,117 | 2,094 |
| 16.500 | 2,071 | 2,050 | 2,029 | 2,009 | 1,989 |
| 16.750 | 1,970 | 1,952 | 1,934 | 1,916 | 1,899 |
| 17.000 | 1,882 | 1,866 | 1,850 | 1,835 | 1,820 |
| 17.250 | 1,805 | 1,790 | 1,776 | 1,762 | 1,748 |
| 17.500 | 1,734 | 1,721 | 1,708 | 1,695 | 1,682 |
| 17.750 | 1,669 | 1,657 | 1,645 | 1,632 | 1,620 |
| 18.000 | 1,608 | 1,596 | 1,585 | 1,573 | 1,562 |
| 18.250 | 1,552 | 1,542 | 1,532 | 1,522 | 1,514 |
| 18.500 | 1,505 | 1,497 | 1,489 | 1,478 | 1,466 |
| 18.750 | 1,454 | 1,443 | 1,432 | 1,421 | 1,410 |
| 19.000 | 1,400 | 1,390 | 1,380 | 1,370 | 1,360 |
| 19.250 | 1,351 | 1,341 | 1,332 | 1,323 | 1,314 |
| 19.500 | 1,306 | 1,297 | 1,289 | 1,280 | 1,272 |
| 19.750 | 1,264 | 1,256 | 1,248 | 1,240 | 1,232 |
| 20.000 | 1,225 | 1,217 | 1,210 | 1,202 | 1,195 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: MC-3500 - 3

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,188 | 1,181 | 1,174 | 1,167 | 1,161 |
| 20.500 | 1,154 | 1,148 | 1,141 | 1,135 | 1,129 |
| 20.750 | 1,122 | 1,116 | 1,110 | 1,104 | 1,099 |
| 21.000 | 1,093 | 1,087 | 1,082 | 1,076 | 1,070 |
| 21.250 | 1,065 | 1,059 | 1,054 | 1,049 | 1,043 |
| 21.500 | 1,038 | 1,033 | 1,027 | 1,022 | 1,017 |
| 21.750 | 1,012 | 1,007 | 1,002 | 997 | 992 |
| 22.000 | 987 | 982 | 977 | 972 | 967 |
| 22.250 | 962 | 957 | 952 | 947 | 943 |
| 22.500 | 938 | 933 | 928 | 923 | 919 |
| 22.750 | 914 | 909 | 904 | 900 | 895 |
| 23.000 | 890 | 886 | 881 | 876 | 871 |
| 23.250 | 867 | 862 | 857 | 853 | 848 |
| 23.500 | 844 | 839 | 834 | 830 | 825 |
| 23.750 | 820 | 816 | 811 | 806 | 802 |
| 24.000 | 797 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: MC-3500 - 3

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 1 | 2 | 4 |
| 3.500 | 6 | 8 | 11 | 14 | 18 |
| 3.750 | 22 | 26 | 31 | 35 | 41 |
| 4.000 | 46 | 52 | 58 | 64 | 71 |
| 4.250 | 78 | 85 | 92 | 100 | 108 |
| 4.500 | 116 | 124 | 132 | 141 | 149 |
| 4.750 | 158 | 167 | 176 | 186 | 195 |
| 5.000 | 205 | 215 | 224 | 234 | 245 |
| 5.250 | 255 | 265 | 276 | 286 | 297 |
| 5.500 | 308 | 319 | 330 | 341 | 352 |
| 5.750 | 364 | 375 | 386 | 398 | 410 |
| 6.000 | 421 | 433 | 445 | 457 | 469 |
| 6.250 | 482 | 495 | 509 | 523 | 538 |
| 6.500 | 552 | 568 | 583 | 599 | 616 |
| 6.750 | 633 | 650 | 668 | 686 | 704 |
| 7.000 | 723 | 742 | 762 | 781 | 802 |
| 7.250 | 822 | 843 | 864 | 886 | 908 |
| 7.500 | 930 | 953 | 976 | 999 | 1,023 |
| 7.750 | 1,047 | 1,071 | 1,095 | 1,120 | 1,145 |
| 8.000 | 1,171 | 1,197 | 1,223 | 1,250 | 1,278 |
| 8.250 | 1,307 | 1,337 | 1,369 | 1,401 | 1,435 |
| 8.500 | 1,471 | 1,499 | 1,522 | 1,546 | 1,570 |
| 8.750 | 1,594 | 1,619 | 1,644 | 1,670 | 1,696 |
| 9.000 | 1,722 | 1,749 | 1,776 | 1,804 | 1,832 |
| 9.250 | 1,860 | 1,889 | 1,918 | 1,947 | 1,977 |
| 9.500 | 2,007 | 2,037 | 2,068 | 2,099 | 2,130 |
| 9.750 | 2,162 | 2,194 | 2,226 | 2,294 | 2,366 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: MC-3500 - 3

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 2,439 | 2,512 | 2,587 | 2,664 | 2,743 |
| 10.250 | 2,827 | 2,913 | 3,004 | 3,098 | 3,195 |
| 10.500 | 3,296 | 3,400 | 3,507 | 3,617 | 3,730 |
| 10.750 | 3,846 | 3,938 | 4,026 | 4,116 | 4,208 |
| 11.000 | 4,302 | 4,398 | 4,500 | 4,609 | 4,730 |
| 11.250 | 4,866 | 5,016 | 5,182 | 5,362 | 5,555 |
| 11.500 | 5,761 | 5,991 | 6,274 | 6,648 | 7,158 |
| 11.750 | 7,836 | 8,685 | 9,689 | 10,868 | 12,282 |
| 12.000 | 14,178 | 16,645 | 19,402 | 21,962 | 23,648 |
| 12.250 | 24,412 | 24,465 | 24,130 | 23,583 | 22,909 |
| 12.500 | 22,187 | 21,322 | 20,447 | 19,559 | 18,655 |
| 12.750 | 17,856 | 17,094 | 16,368 | 15,710 | 15,103 |
| 13.000 | 14,527 | 13,970 | 13,448 | 12,965 | 12,516 |
| 13.250 | 12,097 | 11,704 | 11,331 | 10,982 | 10,656 |
| 13.500 | 10,352 | 10,068 | 9,802 | 9,548 | 9,306 |
| 13.750 | 9,074 | 8,853 | 8,641 | 8,435 | 8,237 |
| 14.000 | 8,046 | 7,863 | 7,687 | 7,518 | 7,357 |
| 14.250 | 7,204 | 7,058 | 6,920 | 6,787 | 6,659 |
| 14.500 | 6,535 | 6,415 | 6,299 | 6,187 | 6,078 |
| 14.750 | 5,972 | 5,870 | 5,770 | 5,673 | 5,578 |
| 15.000 | 5,486 | 5,395 | 5,306 | 5,220 | 5,135 |
| 15.250 | 5,051 | 4,970 | 4,890 | 4,811 | 4,734 |
| 15.500 | 4,658 | 4,584 | 4,510 | 4,438 | 4,366 |
| 15.750 | 4,296 | 4,226 | 4,158 | 4,090 | 4,022 |
| 16.000 | 3,956 | 3,890 | 3,811 | 3,725 | 3,640 |
| 16.250 | 3,559 | 3,480 | 3,404 | 3,330 | 3,259 |
| 16.500 | 3,190 | 3,124 | 3,059 | 2,997 | 2,936 |
| 16.750 | 2,877 | 2,820 | 2,764 | 2,709 | 2,656 |
| 17.000 | 2,604 | 2,553 | 2,503 | 2,455 | 2,407 |
| 17.250 | 2,360 | 2,315 | 2,270 | 2,227 | 2,208 |
| 17.500 | 2,188 | 2,169 | 2,150 | 2,131 | 2,113 |
| 17.750 | 2,094 | 2,076 | 2,059 | 2,041 | 2,023 |
| 18.000 | 2,006 | 1,989 | 1,972 | 1,955 | 1,939 |
| 18.250 | 1,924 | 1,909 | 1,895 | 1,882 | 1,869 |
| 18.500 | 1,856 | 1,844 | 1,833 | 1,821 | 1,811 |
| 18.750 | 1,800 | 1,790 | 1,781 | 1,771 | 1,762 |
| 19.000 | 1,754 | 1,745 | 1,737 | 1,729 | 1,721 |
| 19.250 | 1,713 | 1,706 | 1,699 | 1,692 | 1,685 |
| 19.500 | 1,678 | 1,671 | 1,665 | 1,659 | 1,652 |
| 19.750 | 1,646 | 1,640 | 1,634 | 1,628 | 1,623 |
| 20.000 | 1,617 | 1,611 | 1,606 | 1,600 | 1,595 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: MC-3500 - 3

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,590 | 1,585 | 1,580 | 1,575 | 1,570 |
| 20.500 | 1,565 | 1,561 | 1,556 | 1,552 | 1,547 |
| 20.750 | 1,543 | 1,539 | 1,534 | 1,530 | 1,526 |
| 21.000 | 1,522 | 1,518 | 1,514 | 1,510 | 1,506 |
| 21.250 | 1,502 | 1,499 | 1,495 | 1,491 | 1,487 |
| 21.500 | 1,482 | 1,476 | 1,470 | 1,464 | 1,458 |
| 21.750 | 1,451 | 1,445 | 1,439 | 1,433 | 1,427 |
| 22.000 | 1,421 | 1,414 | 1,408 | 1,402 | 1,396 |
| 22.250 | 1,389 | 1,383 | 1,376 | 1,370 | 1,363 |
| 22.500 | 1,357 | 1,351 | 1,344 | 1,338 | 1,332 |
| 22.750 | 1,325 | 1,319 | 1,312 | 1,306 | 1,299 |
| 23.000 | 1,293 | 1,286 | 1,280 | 1,273 | 1,266 |
| 23.250 | 1,260 | 1,253 | 1,247 | 1,240 | 1,234 |
| 23.500 | 1,227 | 1,221 | 1,214 | 1,207 | 1,201 |
| 23.750 | 1,194 | 1,188 | 1,181 | 1,174 | 1,168 |
| 24.000 | 1,161 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: Stormwater Planters - 2
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: Stormwater Planters - 2
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 0 | 0 | 0 |
| 11.000 | 0 | 0 | 0 | 0 | 0 |
| 11.250 | 0 | 0 | 0 | 0 | 0 |
| 11.500 | 0 | 0 | 16 | 24 | 41 |
| 11.750 | 67 | 101 | 145 | 199 | 270 |
| 12.000 | 377 | 513 | 659 | 797 | 904 |
| 12.250 | 981 | 1,040 | 1,088 | 1,126 | 1,154 |
| 12.500 | 1,173 | 1,184 | 1,189 | 1,189 | 1,188 |
| 12.750 | 1,185 | 1,181 | 1,176 | 1,170 | 1,163 |
| 13.000 | 1,155 | 1,146 | 1,137 | 1,127 | 1,117 |
| 13.250 | 1,106 | 1,095 | 1,084 | 1,073 | 1,061 |
| 13.500 | 1,049 | 1,037 | 1,024 | 1,012 | 999 |
| 13.750 | 986 | 972 | 958 | 945 | 930 |
| 14.000 | 916 | 901 | 886 | 871 | 856 |
| 14.250 | 841 | 825 | 810 | 794 | 778 |
| 14.500 | 762 | 746 | 730 | 714 | 697 |
| 14.750 | 681 | 664 | 647 | 630 | 613 |
| 15.000 | 596 | 579 | 562 | 544 | 526 |
| 15.250 | 509 | 491 | 473 | 455 | 436 |
| 15.500 | 418 | 399 | 381 | 362 | 343 |
| 15.750 | 324 | 305 | 286 | 267 | 247 |
| 16.000 | 228 | 208 | 188 | 168 | 148 |
| 16.250 | 128 | 108 | 88 | 68 | 48 |
| 16.500 | 28 | 0 | 0 | 0 | 0 |
| 16.750 | 0 | 0 | 0 | 0 | 0 |
| 17.000 | 0 | 0 | 0 | 0 | 0 |
| 17.250 | 0 | 0 | 0 | 0 | 0 |
| 17.500 | 0 | 0 | 0 | 0 | 0 |
| 17.750 | 0 | 0 | 0 | 0 | 0 |
| 18.000 | 0 | 0 | 0 | 0 | 0 |
| 18.250 | 0 | 0 | 0 | 0 | 0 |
| 18.500 | 0 | 0 | 0 | 0 | 0 |
| 18.750 | 0 | 0 | 0 | 0 | 0 |
| 19.000 | 0 | 0 | 0 | 0 | 0 |
| 19.250 | 0 | 0 | 0 | 0 | 0 |
| 19.500 | 0 | 0 | 0 | 0 | 0 |
| 19.750 | 0 | 0 | 0 | 0 | 0 |
| 20.000 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume
 Label: Stormwater Planters - 2
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours
Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 20.250 | 0 | 0 | 0 | 0 | 0 |
| 20.500 | 0 | 0 | 0 | 0 | 0 |
| 20.750 | 0 | 0 | 0 | 0 | 0 |
| 21.000 | 0 | 0 | 0 | 0 | 0 |
| 21.250 | 0 | 0 | 0 | 0 | 0 |
| 21.500 | 0 | 0 | 0 | 0 | 0 |
| 21.750 | 0 | 0 | 0 | 0 | 0 |
| 22.000 | 0 | 0 | 0 | 0 | 0 |
| 22.250 | 0 | 0 | 0 | 0 | 0 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: Stormwater Planters - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|-----------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: Stormwater Planters - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 0 | 0 | 0 | 0 | 0 |
| 10.500 | 0 | 0 | 0 | 0 | 0 |
| 10.750 | 0 | 0 | 13 | 14 | 15 |
| 11.000 | 17 | 20 | 23 | 28 | 34 |
| 11.250 | 42 | 52 | 64 | 77 | 93 |
| 11.500 | 110 | 131 | 159 | 199 | 253 |
| 11.750 | 324 | 412 | 518 | 641 | 798 |
| 12.000 | 1,020 | 1,297 | 1,592 | 1,872 | 2,094 |
| 12.250 | 2,258 | 2,390 | 2,501 | 2,594 | 2,668 |
| 12.500 | 2,726 | 2,768 | 2,799 | 2,821 | 2,840 |
| 12.750 | 2,857 | 2,871 | 2,883 | 2,894 | 2,903 |
| 13.000 | 2,910 | 2,916 | 2,920 | 2,923 | 2,926 |
| 13.250 | 2,928 | 2,929 | 2,930 | 2,931 | 2,931 |
| 13.500 | 2,930 | 2,929 | 2,928 | 2,926 | 2,924 |
| 13.750 | 2,921 | 2,918 | 2,914 | 2,910 | 2,906 |
| 14.000 | 2,901 | 2,895 | 2,889 | 2,883 | 2,876 |
| 14.250 | 2,870 | 2,863 | 2,855 | 2,848 | 2,840 |
| 14.500 | 2,832 | 2,824 | 2,816 | 2,807 | 2,799 |
| 14.750 | 2,790 | 2,780 | 2,771 | 2,761 | 2,751 |
| 15.000 | 2,741 | 2,731 | 2,720 | 2,710 | 2,699 |
| 15.250 | 2,687 | 2,676 | 2,664 | 2,652 | 2,640 |
| 15.500 | 2,628 | 2,615 | 2,602 | 2,589 | 2,576 |
| 15.750 | 2,562 | 2,548 | 2,534 | 2,520 | 2,506 |
| 16.000 | 2,491 | 2,476 | 2,461 | 2,446 | 2,431 |
| 16.250 | 2,415 | 2,400 | 2,384 | 2,369 | 2,353 |
| 16.500 | 2,337 | 2,321 | 2,305 | 2,289 | 2,272 |
| 16.750 | 2,256 | 2,239 | 2,223 | 2,206 | 2,189 |
| 17.000 | 2,172 | 2,155 | 2,138 | 2,121 | 2,104 |
| 17.250 | 2,086 | 2,069 | 2,051 | 2,034 | 2,016 |
| 17.500 | 1,998 | 1,980 | 1,962 | 1,944 | 1,926 |
| 17.750 | 1,907 | 1,889 | 1,870 | 1,852 | 1,833 |
| 18.000 | 1,814 | 1,795 | 1,776 | 1,757 | 1,738 |
| 18.250 | 1,719 | 1,699 | 1,680 | 1,661 | 1,642 |
| 18.500 | 1,622 | 1,603 | 1,584 | 1,564 | 1,545 |
| 18.750 | 1,526 | 1,506 | 1,487 | 1,467 | 1,447 |
| 19.000 | 1,428 | 1,408 | 1,389 | 1,369 | 1,349 |
| 19.250 | 1,330 | 1,310 | 1,290 | 1,270 | 1,250 |
| 19.500 | 1,230 | 1,210 | 1,191 | 1,171 | 1,151 |
| 19.750 | 1,131 | 1,110 | 1,090 | 1,070 | 1,050 |
| 20.000 | 1,030 | 1,010 | 990 | 969 | 949 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 10 years

Label: Stormwater Planters - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 929 | 908 | 888 | 868 | 847 |
| 20.500 | 827 | 806 | 786 | 765 | 745 |
| 20.750 | 724 | 704 | 683 | 663 | 642 |
| 21.000 | 621 | 601 | 580 | 559 | 539 |
| 21.250 | 518 | 497 | 476 | 456 | 435 |
| 21.500 | 414 | 393 | 372 | 351 | 330 |
| 21.750 | 309 | 288 | 267 | 246 | 225 |
| 22.000 | 204 | 183 | 162 | 141 | 120 |
| 22.250 | 98 | 77 | 56 | 35 | 13 |
| 22.500 | 0 | 0 | 0 | 0 | 0 |
| 22.750 | 0 | 0 | 0 | 0 | 0 |
| 23.000 | 0 | 0 | 0 | 0 | 0 |
| 23.250 | 0 | 0 | 0 | 0 | 0 |
| 23.500 | 0 | 0 | 0 | 0 | 0 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: Stormwater Planters - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 0 | 0 | 0 | 0 | 0 |
| 9.250 | 0 | 0 | 0 | 0 | 0 |
| 9.500 | 0 | 0 | 0 | 0 | 0 |
| 9.750 | 0 | 0 | 0 | 0 | 0 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: Stormwater Planters - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 0 | 0 | 0 | 0 | 0 |
| 10.250 | 13 | 14 | 16 | 18 | 20 |
| 10.500 | 24 | 28 | 32 | 37 | 43 |
| 10.750 | 50 | 56 | 64 | 72 | 81 |
| 11.000 | 90 | 101 | 112 | 125 | 140 |
| 11.250 | 157 | 177 | 199 | 223 | 250 |
| 11.500 | 278 | 312 | 355 | 412 | 489 |
| 11.750 | 586 | 706 | 847 | 1,010 | 1,217 |
| 12.000 | 1,506 | 1,864 | 2,247 | 2,609 | 2,898 |
| 12.250 | 3,103 | 3,236 | 3,306 | 3,335 | 3,336 |
| 12.500 | 3,319 | 3,290 | 3,257 | 3,226 | 3,199 |
| 12.750 | 3,178 | 3,161 | 3,147 | 3,136 | 3,125 |
| 13.000 | 3,116 | 3,108 | 3,101 | 3,095 | 3,090 |
| 13.250 | 3,086 | 3,083 | 3,080 | 3,077 | 3,075 |
| 13.500 | 3,073 | 3,071 | 3,069 | 3,067 | 3,065 |
| 13.750 | 3,064 | 3,062 | 3,060 | 3,058 | 3,057 |
| 14.000 | 3,055 | 3,053 | 3,052 | 3,050 | 3,049 |
| 14.250 | 3,047 | 3,045 | 3,043 | 3,040 | 3,037 |
| 14.500 | 3,034 | 3,031 | 3,027 | 3,023 | 3,018 |
| 14.750 | 3,014 | 3,009 | 3,004 | 2,998 | 2,993 |
| 15.000 | 2,987 | 2,980 | 2,974 | 2,967 | 2,959 |
| 15.250 | 2,952 | 2,944 | 2,936 | 2,928 | 2,919 |
| 15.500 | 2,910 | 2,901 | 2,892 | 2,882 | 2,872 |
| 15.750 | 2,861 | 2,851 | 2,840 | 2,829 | 2,817 |
| 16.000 | 2,805 | 2,793 | 2,781 | 2,769 | 2,756 |
| 16.250 | 2,743 | 2,730 | 2,717 | 2,704 | 2,691 |
| 16.500 | 2,678 | 2,664 | 2,651 | 2,637 | 2,623 |
| 16.750 | 2,609 | 2,595 | 2,581 | 2,566 | 2,552 |
| 17.000 | 2,537 | 2,522 | 2,508 | 2,493 | 2,477 |
| 17.250 | 2,462 | 2,447 | 2,431 | 2,416 | 2,400 |
| 17.500 | 2,384 | 2,368 | 2,352 | 2,336 | 2,319 |
| 17.750 | 2,303 | 2,286 | 2,270 | 2,253 | 2,236 |
| 18.000 | 2,219 | 2,201 | 2,184 | 2,167 | 2,149 |
| 18.250 | 2,132 | 2,114 | 2,097 | 2,079 | 2,062 |
| 18.500 | 2,044 | 2,026 | 2,008 | 1,991 | 1,973 |
| 18.750 | 1,955 | 1,937 | 1,919 | 1,901 | 1,883 |
| 19.000 | 1,865 | 1,847 | 1,829 | 1,811 | 1,793 |
| 19.250 | 1,774 | 1,756 | 1,738 | 1,720 | 1,701 |
| 19.500 | 1,683 | 1,664 | 1,646 | 1,627 | 1,609 |
| 19.750 | 1,590 | 1,571 | 1,553 | 1,534 | 1,515 |
| 20.000 | 1,497 | 1,478 | 1,459 | 1,440 | 1,421 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 25 years

Label: Stormwater Planters - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,402 | 1,383 | 1,364 | 1,345 | 1,326 |
| 20.500 | 1,307 | 1,288 | 1,269 | 1,250 | 1,230 |
| 20.750 | 1,211 | 1,192 | 1,173 | 1,153 | 1,134 |
| 21.000 | 1,114 | 1,095 | 1,076 | 1,056 | 1,037 |
| 21.250 | 1,017 | 998 | 978 | 959 | 939 |
| 21.500 | 919 | 900 | 880 | 860 | 840 |
| 21.750 | 821 | 801 | 781 | 761 | 741 |
| 22.000 | 721 | 701 | 681 | 661 | 641 |
| 22.250 | 621 | 601 | 581 | 561 | 541 |
| 22.500 | 520 | 500 | 480 | 460 | 439 |
| 22.750 | 419 | 399 | 378 | 358 | 337 |
| 23.000 | 317 | 296 | 276 | 255 | 234 |
| 23.250 | 214 | 193 | 172 | 152 | 131 |
| 23.500 | 110 | 89 | 69 | 48 | 27 |
| 23.750 | 0 | 0 | 0 | 0 | 0 |
| 24.000 | 0 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: Stormwater Planters - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 0.000 | 0 | 0 | 0 | 0 | 0 |
| 0.250 | 0 | 0 | 0 | 0 | 0 |
| 0.500 | 0 | 0 | 0 | 0 | 0 |
| 0.750 | 0 | 0 | 0 | 0 | 0 |
| 1.000 | 0 | 0 | 0 | 0 | 0 |
| 1.250 | 0 | 0 | 0 | 0 | 0 |
| 1.500 | 0 | 0 | 0 | 0 | 0 |
| 1.750 | 0 | 0 | 0 | 0 | 0 |
| 2.000 | 0 | 0 | 0 | 0 | 0 |
| 2.250 | 0 | 0 | 0 | 0 | 0 |
| 2.500 | 0 | 0 | 0 | 0 | 0 |
| 2.750 | 0 | 0 | 0 | 0 | 0 |
| 3.000 | 0 | 0 | 0 | 0 | 0 |
| 3.250 | 0 | 0 | 0 | 0 | 0 |
| 3.500 | 0 | 0 | 0 | 0 | 0 |
| 3.750 | 0 | 0 | 0 | 0 | 0 |
| 4.000 | 0 | 0 | 0 | 0 | 0 |
| 4.250 | 0 | 0 | 0 | 0 | 0 |
| 4.500 | 0 | 0 | 0 | 0 | 0 |
| 4.750 | 0 | 0 | 0 | 0 | 0 |
| 5.000 | 0 | 0 | 0 | 0 | 0 |
| 5.250 | 0 | 0 | 0 | 0 | 0 |
| 5.500 | 0 | 0 | 0 | 0 | 0 |
| 5.750 | 0 | 0 | 0 | 0 | 0 |
| 6.000 | 0 | 0 | 0 | 0 | 0 |
| 6.250 | 0 | 0 | 0 | 0 | 0 |
| 6.500 | 0 | 0 | 0 | 0 | 0 |
| 6.750 | 0 | 0 | 0 | 0 | 0 |
| 7.000 | 0 | 0 | 0 | 0 | 0 |
| 7.250 | 0 | 0 | 0 | 0 | 0 |
| 7.500 | 0 | 0 | 0 | 0 | 0 |
| 7.750 | 0 | 0 | 0 | 0 | 0 |
| 8.000 | 0 | 0 | 0 | 0 | 0 |
| 8.250 | 0 | 0 | 0 | 0 | 0 |
| 8.500 | 0 | 0 | 0 | 0 | 0 |
| 8.750 | 0 | 0 | 0 | 0 | 0 |
| 9.000 | 13 | 13 | 14 | 16 | 18 |
| 9.250 | 20 | 22 | 25 | 29 | 33 |
| 9.500 | 37 | 42 | 47 | 53 | 58 |
| 9.750 | 65 | 72 | 79 | 87 | 95 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: Stormwater Planters - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 10.000 | 103 | 112 | 121 | 132 | 143 |
| 10.250 | 155 | 167 | 181 | 195 | 211 |
| 10.500 | 227 | 244 | 262 | 280 | 300 |
| 10.750 | 320 | 342 | 364 | 387 | 411 |
| 11.000 | 436 | 462 | 489 | 519 | 552 |
| 11.250 | 588 | 628 | 671 | 717 | 766 |
| 11.500 | 819 | 878 | 952 | 1,045 | 1,166 |
| 11.750 | 1,318 | 1,500 | 1,714 | 1,960 | 2,268 |
| 12.000 | 2,695 | 3,195 | 3,598 | 3,792 | 3,800 |
| 12.250 | 3,729 | 3,659 | 3,599 | 3,542 | 3,489 |
| 12.500 | 3,438 | 3,390 | 3,349 | 3,313 | 3,281 |
| 12.750 | 3,255 | 3,234 | 3,216 | 3,201 | 3,187 |
| 13.000 | 3,175 | 3,164 | 3,154 | 3,145 | 3,139 |
| 13.250 | 3,133 | 3,128 | 3,124 | 3,120 | 3,117 |
| 13.500 | 3,114 | 3,111 | 3,109 | 3,106 | 3,103 |
| 13.750 | 3,101 | 3,098 | 3,096 | 3,093 | 3,091 |
| 14.000 | 3,089 | 3,086 | 3,084 | 3,082 | 3,080 |
| 14.250 | 3,078 | 3,077 | 3,075 | 3,074 | 3,073 |
| 14.500 | 3,071 | 3,070 | 3,069 | 3,068 | 3,066 |
| 14.750 | 3,065 | 3,064 | 3,063 | 3,062 | 3,061 |
| 15.000 | 3,059 | 3,058 | 3,057 | 3,056 | 3,055 |
| 15.250 | 3,054 | 3,052 | 3,051 | 3,050 | 3,049 |
| 15.500 | 3,047 | 3,045 | 3,042 | 3,039 | 3,036 |
| 15.750 | 3,032 | 3,028 | 3,023 | 3,018 | 3,012 |
| 16.000 | 3,007 | 3,000 | 2,994 | 2,987 | 2,980 |
| 16.250 | 2,973 | 2,965 | 2,957 | 2,950 | 2,942 |
| 16.500 | 2,933 | 2,925 | 2,917 | 2,908 | 2,899 |
| 16.750 | 2,890 | 2,881 | 2,871 | 2,862 | 2,852 |
| 17.000 | 2,842 | 2,832 | 2,822 | 2,811 | 2,800 |
| 17.250 | 2,790 | 2,779 | 2,767 | 2,756 | 2,744 |
| 17.500 | 2,733 | 2,721 | 2,709 | 2,696 | 2,684 |
| 17.750 | 2,671 | 2,658 | 2,645 | 2,632 | 2,619 |
| 18.000 | 2,605 | 2,592 | 2,578 | 2,564 | 2,550 |
| 18.250 | 2,536 | 2,522 | 2,508 | 2,493 | 2,479 |
| 18.500 | 2,465 | 2,450 | 2,436 | 2,421 | 2,407 |
| 18.750 | 2,392 | 2,378 | 2,363 | 2,348 | 2,333 |
| 19.000 | 2,319 | 2,304 | 2,289 | 2,274 | 2,259 |
| 19.250 | 2,243 | 2,228 | 2,213 | 2,198 | 2,182 |
| 19.500 | 2,167 | 2,151 | 2,136 | 2,120 | 2,105 |
| 19.750 | 2,089 | 2,073 | 2,058 | 2,042 | 2,026 |
| 20.000 | 2,010 | 1,994 | 1,978 | 1,962 | 1,946 |

Existing and Proposed Hydrologic Calculations

Subsection: Time vs. Volume

Return Event: 100 years

Label: Stormwater Planters - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

Time vs. Volume (ft³)

Output Time increment = 0.050 hours

Time on left represents time for first value in each row.

| Time (hours) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) | Volume (ft ³) |
|--------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 20.250 | 1,930 | 1,913 | 1,897 | 1,881 | 1,865 |
| 20.500 | 1,848 | 1,832 | 1,815 | 1,799 | 1,782 |
| 20.750 | 1,766 | 1,749 | 1,732 | 1,716 | 1,699 |
| 21.000 | 1,682 | 1,665 | 1,649 | 1,632 | 1,615 |
| 21.250 | 1,598 | 1,581 | 1,564 | 1,547 | 1,530 |
| 21.500 | 1,512 | 1,495 | 1,478 | 1,461 | 1,443 |
| 21.750 | 1,426 | 1,408 | 1,391 | 1,374 | 1,356 |
| 22.000 | 1,338 | 1,321 | 1,303 | 1,285 | 1,268 |
| 22.250 | 1,250 | 1,232 | 1,214 | 1,196 | 1,178 |
| 22.500 | 1,160 | 1,142 | 1,124 | 1,106 | 1,088 |
| 22.750 | 1,070 | 1,052 | 1,033 | 1,015 | 997 |
| 23.000 | 978 | 960 | 942 | 923 | 904 |
| 23.250 | 886 | 867 | 849 | 830 | 811 |
| 23.500 | 792 | 774 | 755 | 736 | 717 |
| 23.750 | 698 | 679 | 660 | 641 | 621 |
| 24.000 | 602 | (N/A) | (N/A) | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 1 years

Label: 24" Depth Green Roof

Storm Event: 1 year

Scenario: Post-Development 1 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 508 | 0 | 0 | 0 |
| 93.17 | 0.0 | 508 | 1,523 | 86 | 86 |
| 93.18 | 0.0 | 1,016 | 2,241 | 7 | 94 |
| 95.17 | 0.0 | 1,016 | 3,047 | 2,021 | 2,115 |
| 95.18 | 0.0 | 2,031 | 4,483 | 15 | 2,130 |
| 95.30 | 0.0 | 2,031 | 6,093 | 244 | 2,373 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 10 years

Label: 24" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 508 | 0 | 0 | 0 |
| 93.17 | 0.0 | 508 | 1,523 | 86 | 86 |
| 93.18 | 0.0 | 1,016 | 2,241 | 7 | 94 |
| 95.17 | 0.0 | 1,016 | 3,047 | 2,021 | 2,115 |
| 95.18 | 0.0 | 2,031 | 4,483 | 15 | 2,130 |
| 95.30 | 0.0 | 2,031 | 6,093 | 244 | 2,373 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 25 years

Label: 24" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 508 | 0 | 0 | 0 |
| 93.17 | 0.0 | 508 | 1,523 | 86 | 86 |
| 93.18 | 0.0 | 1,016 | 2,241 | 7 | 94 |
| 95.17 | 0.0 | 1,016 | 3,047 | 2,021 | 2,115 |
| 95.18 | 0.0 | 2,031 | 4,483 | 15 | 2,130 |
| 95.30 | 0.0 | 2,031 | 6,093 | 244 | 2,373 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 100 years

Label: 24" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 508 | 0 | 0 | 0 |
| 93.17 | 0.0 | 508 | 1,523 | 86 | 86 |
| 93.18 | 0.0 | 1,016 | 2,241 | 7 | 94 |
| 95.17 | 0.0 | 1,016 | 3,047 | 2,021 | 2,115 |
| 95.18 | 0.0 | 2,031 | 4,483 | 15 | 2,130 |
| 95.30 | 0.0 | 2,031 | 6,093 | 244 | 2,373 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 1 years

Label: 6" Depth Green Roof

Storm Event: 1 year

Scenario: Post-Development 1 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 696 | 0 | 0 | 0 |
| 93.17 | 0.0 | 696 | 2,088 | 118 | 118 |
| 93.18 | 0.0 | 1,392 | 3,072 | 10 | 129 |
| 93.67 | 0.0 | 1,392 | 4,176 | 682 | 811 |
| 93.68 | 0.0 | 2,784 | 6,145 | 20 | 831 |
| 93.75 | 0.0 | 2,784 | 8,352 | 195 | 1,026 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 10 years

Label: 6" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sqr (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|--|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 696 | 0 | 0 | 0 |
| 93.17 | 0.0 | 696 | 2,088 | 118 | 118 |
| 93.18 | 0.0 | 1,392 | 3,072 | 10 | 129 |
| 93.67 | 0.0 | 1,392 | 4,176 | 682 | 811 |
| 93.68 | 0.0 | 2,784 | 6,145 | 20 | 831 |
| 93.75 | 0.0 | 2,784 | 8,352 | 195 | 1,026 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 25 years

Label: 6" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 696 | 0 | 0 | 0 |
| 93.17 | 0.0 | 696 | 2,088 | 118 | 118 |
| 93.18 | 0.0 | 1,392 | 3,072 | 10 | 129 |
| 93.67 | 0.0 | 1,392 | 4,176 | 682 | 811 |
| 93.68 | 0.0 | 2,784 | 6,145 | 20 | 831 |
| 93.75 | 0.0 | 2,784 | 8,352 | 195 | 1,026 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 100 years

Label: 6" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sq (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|---|------------------------------|--------------------------------------|
| 93.00 | 0.0 | 696 | 0 | 0 | 0 |
| 93.17 | 0.0 | 696 | 2,088 | 118 | 118 |
| 93.18 | 0.0 | 1,392 | 3,072 | 10 | 129 |
| 93.67 | 0.0 | 1,392 | 4,176 | 682 | 811 |
| 93.68 | 0.0 | 2,784 | 6,145 | 20 | 831 |
| 93.75 | 0.0 | 2,784 | 8,352 | 195 | 1,026 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Return Event: 1 years

Label: MC-3500 - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 71.50 | 0 |
| 72.25 | 1,002 |
| 72.50 | 1,737 |
| 72.75 | 2,464 |
| 73.00 | 3,184 |
| 73.25 | 3,893 |
| 73.50 | 4,592 |
| 73.75 | 5,277 |
| 74.00 | 5,947 |
| 74.25 | 6,599 |
| 74.50 | 7,230 |
| 74.75 | 7,837 |
| 75.00 | 8,415 |
| 75.25 | 8,957 |
| 75.50 | 9,452 |
| 75.75 | 9,866 |
| 76.00 | 10,221 |
| 77.00 | 11,556 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Label: MC-3500 - 2

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 71.50 | 0 |
| 72.25 | 1,002 |
| 72.50 | 1,737 |
| 72.75 | 2,464 |
| 73.00 | 3,184 |
| 73.25 | 3,893 |
| 73.50 | 4,592 |
| 73.75 | 5,277 |
| 74.00 | 5,947 |
| 74.25 | 6,599 |
| 74.50 | 7,230 |
| 74.75 | 7,837 |
| 75.00 | 8,415 |
| 75.25 | 8,957 |
| 75.50 | 9,452 |
| 75.75 | 9,866 |
| 76.00 | 10,221 |
| 77.00 | 11,556 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Label: MC-3500 - 2

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 71.50 | 0 |
| 72.25 | 1,002 |
| 72.50 | 1,737 |
| 72.75 | 2,464 |
| 73.00 | 3,184 |
| 73.25 | 3,893 |
| 73.50 | 4,592 |
| 73.75 | 5,277 |
| 74.00 | 5,947 |
| 74.25 | 6,599 |
| 74.50 | 7,230 |
| 74.75 | 7,837 |
| 75.00 | 8,415 |
| 75.25 | 8,957 |
| 75.50 | 9,452 |
| 75.75 | 9,866 |
| 76.00 | 10,221 |
| 77.00 | 11,556 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Label: MC-3500 - 2

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 71.50 | 0 |
| 72.25 | 1,002 |
| 72.50 | 1,737 |
| 72.75 | 2,464 |
| 73.00 | 3,184 |
| 73.25 | 3,893 |
| 73.50 | 4,592 |
| 73.75 | 5,277 |
| 74.00 | 5,947 |
| 74.25 | 6,599 |
| 74.50 | 7,230 |
| 74.75 | 7,837 |
| 75.00 | 8,415 |
| 75.25 | 8,957 |
| 75.50 | 9,452 |
| 75.75 | 9,866 |
| 76.00 | 10,221 |
| 77.00 | 11,556 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Return Event: 1 years

Label: MC-3500 - 3

Storm Event: 1 year

Scenario: Post-Development 1 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 63.15 | 0 |
| 63.90 | 2,229 |
| 64.15 | 3,865 |
| 64.40 | 5,483 |
| 64.65 | 7,084 |
| 64.90 | 8,662 |
| 65.15 | 10,217 |
| 65.40 | 11,741 |
| 65.65 | 13,232 |
| 65.90 | 14,682 |
| 66.15 | 16,086 |
| 66.40 | 17,436 |
| 66.65 | 18,721 |
| 66.90 | 19,927 |
| 67.15 | 21,030 |
| 67.40 | 21,951 |
| 67.65 | 22,741 |
| 68.65 | 25,712 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Label: MC-3500 - 3

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 63.15 | 0 |
| 63.90 | 2,229 |
| 64.15 | 3,865 |
| 64.40 | 5,483 |
| 64.65 | 7,084 |
| 64.90 | 8,662 |
| 65.15 | 10,217 |
| 65.40 | 11,741 |
| 65.65 | 13,232 |
| 65.90 | 14,682 |
| 66.15 | 16,086 |
| 66.40 | 17,436 |
| 66.65 | 18,721 |
| 66.90 | 19,927 |
| 67.15 | 21,030 |
| 67.40 | 21,951 |
| 67.65 | 22,741 |
| 68.65 | 25,712 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Label: MC-3500 - 3

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 63.15 | 0 |
| 63.90 | 2,229 |
| 64.15 | 3,865 |
| 64.40 | 5,483 |
| 64.65 | 7,084 |
| 64.90 | 8,662 |
| 65.15 | 10,217 |
| 65.40 | 11,741 |
| 65.65 | 13,232 |
| 65.90 | 14,682 |
| 66.15 | 16,086 |
| 66.40 | 17,436 |
| 66.65 | 18,721 |
| 66.90 | 19,927 |
| 67.15 | 21,030 |
| 67.40 | 21,951 |
| 67.65 | 22,741 |
| 68.65 | 25,712 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation vs. Volume Curve

Label: MC-3500 - 3

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Elevation-Volume

| Pond Elevation (ft) | Pond Volume (ft ³) |
|------------------------|-----------------------------------|
| 63.15 | 0 |
| 63.90 | 2,229 |
| 64.15 | 3,865 |
| 64.40 | 5,483 |
| 64.65 | 7,084 |
| 64.90 | 8,662 |
| 65.15 | 10,217 |
| 65.40 | 11,741 |
| 65.65 | 13,232 |
| 65.90 | 14,682 |
| 66.15 | 16,086 |
| 66.40 | 17,436 |
| 66.65 | 18,721 |
| 66.90 | 19,927 |
| 67.15 | 21,030 |
| 67.40 | 21,951 |
| 67.65 | 22,741 |
| 68.65 | 25,712 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 1 years

Label: Stormwater Planters - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sqr (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|--|------------------------------|--------------------------------------|
| 78.81 | 0.0 | 3,050 | 0 | 0 | 0 |
| 80.31 | 0.0 | 3,050 | 9,150 | 4,575 | 4,575 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 10 years

Label: Stormwater Planters - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sqr (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|--|------------------------------|--------------------------------------|
| 78.81 | 0.0 | 3,050 | 0 | 0 | 0 |
| 80.31 | 0.0 | 3,050 | 9,150 | 4,575 | 4,575 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 25 years

Label: Stormwater Planters - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sqr (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|--|------------------------------|--------------------------------------|
| 78.81 | 0.0 | 3,050 | 0 | 0 | 0 |
| 80.31 | 0.0 | 3,050 | 9,150 | 4,575 | 4,575 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Area Volume Curve

Return Event: 100 years

Label: Stormwater Planters - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

| Elevation (ft) | Planimeter (ft ²) | Area (ft ²) | A1+A2+sqr (A1*A2) (ft ²) | Volume (ft ³) | Volume (Total) (ft ³) |
|-------------------|----------------------------------|----------------------------|--|------------------------------|--------------------------------------|
| 78.81 | 0.0 | 3,050 | 0 | 0 | 0 |
| 80.31 | 0.0 | 3,050 | 9,150 | 4,575 | 4,575 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: 24-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| Requested Pond Water Surface Elevations | |
|---|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 95.30 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 95.30 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 95.21 (N/A) | 95.30 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: 24-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Structure ID: User Defined Rating Table - 1
 Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.09 |
| 2.00 | 0.09 |
| 2.30 | 0.09 |

Structure ID: Weir - 1
 Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 95.21 ft |
| Weir Length | 45.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
 Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 0.09 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: 24-GR OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Computation Messages

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.80 | 0.00 | (N/A) | 0.00 |
| 93.90 | 0.00 | (N/A) | 0.00 |
| 94.00 | 0.00 | (N/A) | 0.00 |
| 94.10 | 0.00 | (N/A) | 0.00 |
| 94.20 | 0.00 | (N/A) | 0.00 |
| 94.30 | 0.00 | (N/A) | 0.00 |
| 94.40 | 0.00 | (N/A) | 0.00 |
| 94.50 | 0.00 | (N/A) | 0.00 |
| 94.60 | 0.00 | (N/A) | 0.00 |
| 94.70 | 0.00 | (N/A) | 0.00 |
| 94.80 | 0.00 | (N/A) | 0.00 |
| 94.90 | 0.00 | (N/A) | 0.00 |
| 95.00 | 0.00 | (N/A) | 0.00 |
| 95.10 | 0.00 | (N/A) | 0.00 |
| 95.20 | 0.00 | (N/A) | 0.00 |
| 95.21 | 0.00 | (N/A) | 0.00 |
| 95.30 | 3.65 | (N/A) | 0.00 |

Computation Messages

HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: 24-GR OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

Computation Messages

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

HW & TW below

Inv.El.=95.210

H=.00; Htw=.00;

Qfree=.00;

H=.09; Htw=.00;

Qfree=3.65;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 24-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 3.74 | (N/A) | 0.00 |

Contributing Structures

- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1
- User Defined Rating Table
- 1

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve

Label: 24-GR OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Composite Outflow Summary

| Contributing Structures |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: 24-GR OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 95.30 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 95.30 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 95.21 (N/A) | 95.30 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: 24-GR OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.09 |
| 2.00 | 0.09 |
| 2.30 | 0.09 |

Structure ID: Weir - 1
Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 95.21 ft |
| Weir Length | 45.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 0.09 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: 24-GR OUT
Scenario: Post-Development 10 year

Return Event: 10 years
Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
Downstream ID = Tailwater (Pond Outfall)

Computation Messages

Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
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Interpolated from input table
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Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.80 | 0.00 | (N/A) | 0.00 |
| 93.90 | 0.00 | (N/A) | 0.00 |
| 94.00 | 0.00 | (N/A) | 0.00 |
| 94.10 | 0.00 | (N/A) | 0.00 |
| 94.20 | 0.00 | (N/A) | 0.00 |
| 94.30 | 0.00 | (N/A) | 0.00 |
| 94.40 | 0.00 | (N/A) | 0.00 |
| 94.50 | 0.00 | (N/A) | 0.00 |
| 94.60 | 0.00 | (N/A) | 0.00 |
| 94.70 | 0.00 | (N/A) | 0.00 |
| 94.80 | 0.00 | (N/A) | 0.00 |
| 94.90 | 0.00 | (N/A) | 0.00 |
| 95.00 | 0.00 | (N/A) | 0.00 |
| 95.10 | 0.00 | (N/A) | 0.00 |
| 95.20 | 0.00 | (N/A) | 0.00 |
| 95.21 | 0.00 | (N/A) | 0.00 |
| 95.30 | 3.65 | (N/A) | 0.00 |

Computation Messages

| |
|---------------------------------|
| HW & TW below Inv.El.=95.210 |
| HW & TW below Inv.El.=95.210 |
| HW & TW below Inv.El.=95.210 |
| HW & TW below Inv.El.=95.210 |
| HW & TW below Inv.El.=95.210 |
| HW & TW below Inv.El.=95.210 |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: 24-GR OUT
Scenario: Post-Development 10 year

Return Event: 10 years
Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
Downstream ID = Tailwater (Pond Outfall)

Computation Messages

| |
|---|
| HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 H=.00; Htw=.00; Qfree=.00; H=.09; Htw=.00; Qfree=3.65; |
|---|

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 24-GR OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 3.74 | (N/A) | 0.00 |

Contributing Structures

- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
Label: 24-GR OUT
Scenario: Post-Development 10 year

Return Event: 10 years
Storm Event: 10 year

Composite Outflow Summary

| Contributing Structures |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
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| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: 24-GR OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 95.30 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 95.30 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 95.21 (N/A) | 95.30 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: 24-GR OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Structure ID: User Defined Rating Table - 1
 Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.09 |
| 2.00 | 0.09 |
| 2.30 | 0.09 |

Structure ID: Weir - 1
 Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 95.21 ft |
| Weir Length | 45.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
 Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 0.09 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: 24-GR OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
Downstream ID = Tailwater (Pond Outfall)

Computation Messages

Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
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Interpolated from input table
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Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.80 | 0.00 | (N/A) | 0.00 |
| 93.90 | 0.00 | (N/A) | 0.00 |
| 94.00 | 0.00 | (N/A) | 0.00 |
| 94.10 | 0.00 | (N/A) | 0.00 |
| 94.20 | 0.00 | (N/A) | 0.00 |
| 94.30 | 0.00 | (N/A) | 0.00 |
| 94.40 | 0.00 | (N/A) | 0.00 |
| 94.50 | 0.00 | (N/A) | 0.00 |
| 94.60 | 0.00 | (N/A) | 0.00 |
| 94.70 | 0.00 | (N/A) | 0.00 |
| 94.80 | 0.00 | (N/A) | 0.00 |
| 94.90 | 0.00 | (N/A) | 0.00 |
| 95.00 | 0.00 | (N/A) | 0.00 |
| 95.10 | 0.00 | (N/A) | 0.00 |
| 95.20 | 0.00 | (N/A) | 0.00 |
| 95.21 | 0.00 | (N/A) | 0.00 |
| 95.30 | 3.65 | (N/A) | 0.00 |

Computation Messages

| |
|---|
| HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 |
|---|

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: 24-GR OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
Downstream ID = Tailwater (Pond Outfall)

Computation Messages

| |
|---|
| HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 H=.00; Htw=.00; Qfree=.00; H=.09; Htw=.00; Qfree=3.65; |
|---|

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 24-GR OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 3.74 | (N/A) | 0.00 |

Contributing Structures

- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1
- User Defined Rating Table - 1

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
Label: 24-GR OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

Composite Outflow Summary

| Contributing Structures |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: 24-GR OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 95.30 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 95.30 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 95.21 (N/A) | 95.30 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: 24-GR OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.09 |
| 2.00 | 0.09 |
| 2.30 | 0.09 |

Structure ID: Weir - 1
Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 95.21 ft |
| Weir Length | 45.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = User Defined Rating Table - 1 (User Defined Table)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 0.09 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: 24-GR OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
Downstream ID = Tailwater (Pond Outfall)

Computation Messages

Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
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Interpolated from input table
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Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table
Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 24-GR OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.80 | 0.00 | (N/A) | 0.00 |
| 93.90 | 0.00 | (N/A) | 0.00 |
| 94.00 | 0.00 | (N/A) | 0.00 |
| 94.10 | 0.00 | (N/A) | 0.00 |
| 94.20 | 0.00 | (N/A) | 0.00 |
| 94.30 | 0.00 | (N/A) | 0.00 |
| 94.40 | 0.00 | (N/A) | 0.00 |
| 94.50 | 0.00 | (N/A) | 0.00 |
| 94.60 | 0.00 | (N/A) | 0.00 |
| 94.70 | 0.00 | (N/A) | 0.00 |
| 94.80 | 0.00 | (N/A) | 0.00 |
| 94.90 | 0.00 | (N/A) | 0.00 |
| 95.00 | 0.00 | (N/A) | 0.00 |
| 95.10 | 0.00 | (N/A) | 0.00 |
| 95.20 | 0.00 | (N/A) | 0.00 |
| 95.21 | 0.00 | (N/A) | 0.00 |
| 95.30 | 3.65 | (N/A) | 0.00 |

Computation Messages

HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210
 HW & TW below
 Inv.El.=95.210

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: 24-GR OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
Downstream ID = Tailwater (Pond Outfall)

Computation Messages

| |
|---|
| HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 HW & TW below Inv.El.=95.210 H=.00; Htw=.00; Qfree=.00; H=.09; Htw=.00; Qfree=3.65; |
|---|

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 24-GR OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.09 | (N/A) | 0.00 |
| 93.10 | 0.09 | (N/A) | 0.00 |
| 93.20 | 0.09 | (N/A) | 0.00 |
| 93.30 | 0.09 | (N/A) | 0.00 |
| 93.40 | 0.09 | (N/A) | 0.00 |
| 93.50 | 0.09 | (N/A) | 0.00 |
| 93.60 | 0.09 | (N/A) | 0.00 |
| 93.70 | 0.09 | (N/A) | 0.00 |
| 93.80 | 0.09 | (N/A) | 0.00 |
| 93.90 | 0.09 | (N/A) | 0.00 |
| 94.00 | 0.09 | (N/A) | 0.00 |
| 94.10 | 0.09 | (N/A) | 0.00 |
| 94.20 | 0.09 | (N/A) | 0.00 |
| 94.30 | 0.09 | (N/A) | 0.00 |
| 94.40 | 0.09 | (N/A) | 0.00 |
| 94.50 | 0.09 | (N/A) | 0.00 |
| 94.60 | 0.09 | (N/A) | 0.00 |
| 94.70 | 0.09 | (N/A) | 0.00 |
| 94.80 | 0.09 | (N/A) | 0.00 |
| 94.90 | 0.09 | (N/A) | 0.00 |
| 95.00 | 0.09 | (N/A) | 0.00 |
| 95.10 | 0.09 | (N/A) | 0.00 |
| 95.20 | 0.09 | (N/A) | 0.00 |
| 95.21 | 0.09 | (N/A) | 0.00 |
| 95.30 | 3.74 | (N/A) | 0.00 |

Contributing Structures

| |
|----------------------------------|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
Label: 24-GR OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

Composite Outflow Summary

| Contributing Structures |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: 6-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| Requested Pond Water Surface Elevations | |
|---|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 93.75 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 93.75 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 93.71 (N/A) | 93.75 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: 6-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Structure ID: User Defined Rating Table - 1
 Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.13 |
| 0.50 | 0.13 |
| 0.75 | 0.13 |

Structure ID: Weir - 1
 Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 93.71 ft |
| Weir Length | 52.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
 Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Return Event: 1 years

Label: 6-GR OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 0.13 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.71 | 0.00 | (N/A) | 0.00 |
| 93.75 | 1.25 | (N/A) | 0.00 |

Computation Messages

HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 H=.00; Htw=.00;
 Qfree=.00;
 H=.04; Htw=.00;
 Qfree=1.25;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve

Return Event: 1 years

Label: 6-GR OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------|---------------------------|--------------------------|------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 1.38 | (N/A) | 0.00 |

Contributing Structures

| |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: 6-GR OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 93.75 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 93.75 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 93.71 (N/A) | 93.75 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: 6-GR OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Structure ID: User Defined Rating Table - 1
 Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.13 |
| 0.50 | 0.13 |
| 0.75 | 0.13 |

Structure ID: Weir - 1
 Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 93.71 ft |
| Weir Length | 52.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
 Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 0.13 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.71 | 0.00 | (N/A) | 0.00 |
| 93.75 | 1.25 | (N/A) | 0.00 |

Computation Messages

HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 H=.00; Htw=.00;
 Qfree=.00;
 H=.04; Htw=.00;
 Qfree=1.25;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 6-GR OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 1.38 | (N/A) | 0.00 |

Contributing Structures

| |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: 6-GR OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 93.75 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 93.75 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 93.71 (N/A) | 93.75 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: 6-GR OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.13 |
| 0.50 | 0.13 |
| 0.75 | 0.13 |

Structure ID: Weir - 1
Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 93.71 ft |
| Weir Length | 52.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 0.13 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.71 | 0.00 | (N/A) | 0.00 |
| 93.75 | 1.25 | (N/A) | 0.00 |

Computation Messages

HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 H=.00; Htw=.00;
 Qfree=.00;
 H=.04; Htw=.00;
 Qfree=1.25;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 6-GR OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 1.38 | (N/A) | 0.00 |

Contributing Structures

| |
|---|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: 6-GR OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 93.00 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 93.75 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|-------------------------------------|-------------------------------|-----------|---------|----------------|----------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | TW | 0.00 | 93.75 |
| Rectangular Weir Tailwater Settings | Weir - 1 Tailwater | Forward | TW | 93.71 (N/A) | 93.75 (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: 6-GR OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.13 |
| 0.50 | 0.13 |
| 0.75 | 0.13 |

Structure ID: Weir - 1
Structure Type: Rectangular Weir

| | |
|--------------------|-----------------------------|
| Number of Openings | 1 |
| Elevation | 93.71 ft |
| Weir Length | 52.00 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |

Structure ID: TW
Structure Type: TW Setup, DS Channel

| | |
|----------------|--------------|
| Tailwater Type | Free Outfall |
|----------------|--------------|

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = User Defined Rating Table - 1 (User Defined Table)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 0.13 | (N/A) | 0.00 |

Computation Messages

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: 6-GR OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 93.00 | 0.00 | (N/A) | 0.00 |
| 93.10 | 0.00 | (N/A) | 0.00 |
| 93.20 | 0.00 | (N/A) | 0.00 |
| 93.30 | 0.00 | (N/A) | 0.00 |
| 93.40 | 0.00 | (N/A) | 0.00 |
| 93.50 | 0.00 | (N/A) | 0.00 |
| 93.60 | 0.00 | (N/A) | 0.00 |
| 93.70 | 0.00 | (N/A) | 0.00 |
| 93.71 | 0.00 | (N/A) | 0.00 |
| 93.75 | 1.25 | (N/A) | 0.00 |

Computation Messages

HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 HW & TW below
 Inv.El.=93.710
 H=.00; Htw=.00;
 Qfree=.00;
 H=.04; Htw=.00;
 Qfree=1.25;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: 6-GR OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------|---------------------------|--------------------------|------------------------|
| 93.00 | 0.13 | (N/A) | 0.00 |
| 93.10 | 0.13 | (N/A) | 0.00 |
| 93.20 | 0.13 | (N/A) | 0.00 |
| 93.30 | 0.13 | (N/A) | 0.00 |
| 93.40 | 0.13 | (N/A) | 0.00 |
| 93.50 | 0.13 | (N/A) | 0.00 |
| 93.60 | 0.13 | (N/A) | 0.00 |
| 93.70 | 0.13 | (N/A) | 0.00 |
| 93.71 | 0.13 | (N/A) | 0.00 |
| 93.75 | 1.38 | (N/A) | 0.00 |

Contributing Structures

| |
|--|
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 |
| User Defined Rating Table - 1 + Weir - 1 |
| User Defined Rating Table - 1 + Weir - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| Requested Pond Water Surface Elevations | |
|---|----------|
| Minimum (Headwater) | 71.50 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 77.00 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Orifice-Circular | Orifice - 1 | Forward | Culvert - 1 | 71.50 | 77.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 72.75 | 77.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 71.50 | 77.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 33.36 ft |
| Length (Computed Barrel) | 33.36 ft |
| Slope (Computed) | 0.015 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.074 |
| T2 ratio (HW/D) | 1.211 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 72.84 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 73.01 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 1 years

Label: MC-3500 - 2 OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|----------------------------------|----------|
| Structure ID: Orifice - 1 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 71.50 ft |
| Orifice Diameter | 3.0 in |
| Orifice Coefficient | 0.600 |

| | |
|----------------------------------|----------|
| Structure ID: Orifice - 2 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 72.75 ft |
| Orifice Diameter | 4.0 in |
| Orifice Coefficient | 0.600 |

| | |
|--------------------------------------|--------------|
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |

| | |
|-------------------------------|---------------------------|
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 8.51 ft³/s
 Upstream ID = Orifice - 1, Orifice - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 71.70 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.20 | 71.75 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 71.77 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.36 | 71.83 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.62 | 71.94 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.77 | 71.99 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.90 | 72.03 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 1.01 | 72.07 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 1.11 | 72.10 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 1.20 | 72.12 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 1.29 | 72.15 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 1.38 | 72.17 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .048ft Dcr= .139ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .060ft Dcr= .174ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .064ft Dcr= .187ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE
 CRIT.DEPTH CONTROL
 Vh= .108ft Dcr= .306ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: MC-3500 - 2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 8.51 ft³/s

Upstream ID = Orifice - 1, Orifice - 2

Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .134ft Dcr= .372ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .143ft Dcr= .395ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 72.00 | 71.70 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.21 | 72.50 | 71.75 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 72.75 | 71.76 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.26 | 73.00 | 71.83 | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.30 | 73.50 | 71.94 | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.33 | 74.00 | 71.99 | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.37 | 74.50 | 72.03 | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.40 | 75.00 | 72.07 | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.44 | 75.50 | 72.10 | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.47 | 76.00 | 72.12 | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.49 | 76.50 | 72.15 | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.52 | 77.00 | 72.17 | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H =.30
 H =.75
 H =.99
 H =1.17
 H =1.56
 H =2.01
 H =2.47
 H =2.93
 H =3.40
 H =3.88
 H =4.35
 H =4.83

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.00 | 0.00 | 0.00 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.00 | 0.00 | 0.00 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.00 | 0.00 | 0.00 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.10 | 73.00 | Free Outfall | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.32 | 73.50 | Free Outfall | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.44 | 74.00 | Free Outfall | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.53 | 74.50 | Free Outfall | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.61 | 75.00 | Free Outfall | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.68 | 75.50 | Free Outfall | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.74 | 76.00 | Free Outfall | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.80 | 76.50 | Free Outfall | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.85 | 77.00 | Free Outfall | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .071ft Dcr= .178ft
 CRIT.DEPTH Hev= .00ft
 H =.58
 H =1.08
 H =1.58
 H =2.08
 H =2.58
 H =3.08
 H =3.58
 H =4.08

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 71.50 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | (N/A) | 0.00 |
| 72.50 | 0.20 | (N/A) | 0.00 |
| 72.75 | 0.23 | (N/A) | 0.00 |
| 73.00 | 0.36 | (N/A) | 0.00 |
| 73.50 | 0.62 | (N/A) | 0.00 |
| 74.00 | 0.77 | (N/A) | 0.00 |
| 74.50 | 0.90 | (N/A) | 0.00 |
| 75.00 | 1.01 | (N/A) | 0.00 |
| 75.50 | 1.11 | (N/A) | 0.00 |
| 76.00 | 1.20 | (N/A) | 0.00 |
| 76.50 | 1.29 | (N/A) | 0.00 |
| 77.00 | 1.37 | (N/A) | 0.00 |

Contributing Structures

| |
|---|
| (no Q: Orifice - 1, Orifice - 2, Culvert - 1) |
| Orifice - 1, Culvert - 1 |
| (no Q: Orifice - 2) |
| Orifice - 1, Culvert - 1 |
| (no Q: Orifice - 2) |
| Orifice - 1, Culvert - 1 |
| (no Q: Orifice - 2) |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: MC-3500 - 2 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 71.50 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 77.00 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Orifice-Circular | Orifice - 1 | Forward | Culvert - 1 | 71.50 | 77.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 72.75 | 77.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 71.50 | 77.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: MC-3500 - 2 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 33.36 ft |
| Length (Computed Barrel) | 33.36 ft |
| Slope (Computed) | 0.015 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.074 |
| T2 ratio (HW/D) | 1.211 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 72.84 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 73.01 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: MC-3500 - 2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

| | |
|----------------------------------|----------|
| Structure ID: Orifice - 1 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 71.50 ft |
| Orifice Diameter | 3.0 in |
| Orifice Coefficient | 0.600 |

| | |
|----------------------------------|----------|
| Structure ID: Orifice - 2 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 72.75 ft |
| Orifice Diameter | 4.0 in |
| Orifice Coefficient | 0.600 |

| | |
|--------------------------------------|--------------|
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |

| | |
|-------------------------------|---------------------------|
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 8.51 ft³/s
 Upstream ID = Orifice - 1, Orifice - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 71.70 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.20 | 71.75 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 71.77 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.36 | 71.83 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.62 | 71.94 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.77 | 71.99 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.90 | 72.03 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 1.01 | 72.07 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 1.11 | 72.10 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 1.20 | 72.12 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 1.29 | 72.15 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 1.38 | 72.17 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .048ft Dcr= .139ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .060ft Dcr= .174ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .064ft Dcr= .187ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE
 CRIT.DEPTH CONTROL
 Vh= .108ft Dcr= .306ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 2 OUT
Scenario: Post-Development 10 year

Return Event: 10 years
Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 8.51 ft³/s
Upstream ID = Orifice - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .134ft Dcr= .372ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .143ft Dcr= .395ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 72.00 | 71.70 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.21 | 72.50 | 71.75 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 72.75 | 71.76 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.26 | 73.00 | 71.83 | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.30 | 73.50 | 71.94 | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.33 | 74.00 | 71.99 | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.37 | 74.50 | 72.03 | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.40 | 75.00 | 72.07 | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.44 | 75.50 | 72.10 | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.47 | 76.00 | 72.12 | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.49 | 76.50 | 72.15 | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.52 | 77.00 | 72.17 | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H =.30
 H =.75
 H =.99
 H =1.17
 H =1.56
 H =2.01
 H =2.47
 H =2.93
 H =3.40
 H =3.88
 H =4.35
 H =4.83

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.00 | 0.00 | 0.00 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.00 | 0.00 | 0.00 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.00 | 0.00 | 0.00 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.10 | 73.00 | Free Outfall | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.32 | 73.50 | Free Outfall | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.44 | 74.00 | Free Outfall | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.53 | 74.50 | Free Outfall | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.61 | 75.00 | Free Outfall | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.68 | 75.50 | Free Outfall | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.74 | 76.00 | Free Outfall | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.80 | 76.50 | Free Outfall | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.85 | 77.00 | Free Outfall | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .071ft Dcr= .178ft
 CRIT.DEPTH Hev= .00ft
 H =.58
 H =1.08
 H =1.58
 H =2.08
 H =2.58
 H =3.08
 H =3.58
 H =4.08

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: MC-3500 - 2 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 71.50 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 77.00 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Orifice-Circular | Orifice - 1 | Forward | Culvert - 1 | 71.50 | 77.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 72.75 | 77.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 71.50 | 77.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: MC-3500 - 2 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 33.36 ft |
| Length (Computed Barrel) | 33.36 ft |
| Slope (Computed) | 0.015 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.074 |
| T2 ratio (HW/D) | 1.211 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 72.84 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 73.01 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: MC-3500 - 2 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

| | |
|--------------------------------------|---------------------------|
| Structure ID: Orifice - 1 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 71.50 ft |
| Orifice Diameter | 3.0 in |
| Orifice Coefficient | 0.600 |
| Structure ID: Orifice - 2 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 72.75 ft |
| Orifice Diameter | 4.0 in |
| Orifice Coefficient | 0.600 |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 8.51 ft³/s
 Upstream ID = Orifice - 1, Orifice - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 71.70 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.20 | 71.75 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 71.77 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.36 | 71.83 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.62 | 71.94 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.77 | 71.99 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.90 | 72.03 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 1.01 | 72.07 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 1.11 | 72.10 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 1.20 | 72.12 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 1.29 | 72.15 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 1.38 | 72.17 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .048ft Dcr= .139ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .060ft Dcr= .174ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .064ft Dcr= .187ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE
 CRIT.DEPTH CONTROL
 Vh= .108ft Dcr= .306ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 2 OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 8.51 ft³/s
Upstream ID = Orifice - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .134ft Dcr= .372ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .143ft Dcr= .395ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 72.00 | 71.70 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.21 | 72.50 | 71.75 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 72.75 | 71.76 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.26 | 73.00 | 71.83 | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.30 | 73.50 | 71.94 | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.33 | 74.00 | 71.99 | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.37 | 74.50 | 72.03 | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.40 | 75.00 | 72.07 | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.44 | 75.50 | 72.10 | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.47 | 76.00 | 72.12 | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.49 | 76.50 | 72.15 | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.52 | 77.00 | 72.17 | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H =.30
 H =.75
 H =.99
 H =1.17
 H =1.56
 H =2.01
 H =2.47
 H =2.93
 H =3.40
 H =3.88
 H =4.35
 H =4.83

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.00 | 0.00 | 0.00 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.00 | 0.00 | 0.00 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.00 | 0.00 | 0.00 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.10 | 73.00 | Free Outfall | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.32 | 73.50 | Free Outfall | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.44 | 74.00 | Free Outfall | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.53 | 74.50 | Free Outfall | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.61 | 75.00 | Free Outfall | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.68 | 75.50 | Free Outfall | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.74 | 76.00 | Free Outfall | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.80 | 76.50 | Free Outfall | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.85 | 77.00 | Free Outfall | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .071ft Dcr= .178ft
 CRIT.DEPTH Hev= .00ft
 H =.58
 H =1.08
 H =1.58
 H =2.08
 H =2.58
 H =3.08
 H =3.58
 H =4.08

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 71.50 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | (N/A) | 0.00 |
| 72.50 | 0.20 | (N/A) | 0.00 |
| 72.75 | 0.23 | (N/A) | 0.00 |
| 73.00 | 0.36 | (N/A) | 0.00 |
| 73.50 | 0.62 | (N/A) | 0.00 |
| 74.00 | 0.77 | (N/A) | 0.00 |
| 74.50 | 0.90 | (N/A) | 0.00 |
| 75.00 | 1.01 | (N/A) | 0.00 |
| 75.50 | 1.11 | (N/A) | 0.00 |
| 76.00 | 1.20 | (N/A) | 0.00 |
| 76.50 | 1.29 | (N/A) | 0.00 |
| 77.00 | 1.37 | (N/A) | 0.00 |

Contributing Structures

| |
|--|
| (no Q: Orifice - 1,Orifice - 2,Culvert - 1) Orifice - 1,Culvert - 1 (no Q: Orifice - 2) Orifice - 1,Culvert - 1 (no Q: Orifice - 2) Orifice - 1,Culvert - 1 (no Q: Orifice - 2) Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 Orifice - 1,Orifice - 2,Culvert - 1 |
|--|

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: MC-3500 - 2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 71.50 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 77.00 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Orifice-Circular | Orifice - 1 | Forward | Culvert - 1 | 71.50 | 77.00 |
| Orifice-Circular | Orifice - 2 | Forward | Culvert - 1 | 72.75 | 77.00 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 71.50 | 77.00 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: MC-3500 - 2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 33.36 ft |
| Length (Computed Barrel) | 33.36 ft |
| Slope (Computed) | 0.015 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.074 |
| T2 ratio (HW/D) | 1.211 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 72.84 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 73.01 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: MC-3500 - 2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|---------------------------|
| Structure ID: Orifice - 1 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 71.50 ft |
| Orifice Diameter | 3.0 in |
| Orifice Coefficient | 0.600 |
| Structure ID: Orifice - 2 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 1 |
| Elevation | 72.75 ft |
| Orifice Diameter | 4.0 in |
| Orifice Coefficient | 0.600 |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 8.51 ft³/s
 Upstream ID = Orifice - 1, Orifice - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 71.70 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.20 | 71.75 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 71.77 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.36 | 71.83 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.62 | 71.94 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.77 | 71.99 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.90 | 72.03 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 1.01 | 72.07 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 1.11 | 72.10 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 1.20 | 72.12 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 1.29 | 72.15 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 1.38 | 72.17 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .048ft Dcr= .139ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .060ft Dcr= .174ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .064ft Dcr= .187ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE
 CRIT.DEPTH CONTROL
 Vh= .108ft Dcr= .306ft
 CRIT.DEPTH Hev= .00ft
 FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 2 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 8.51 ft³/s
Upstream ID = Orifice - 1, Orifice - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .134ft Dcr= .372ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .143ft Dcr= .395ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Return Event: 100 years

Label: MC-3500 - 2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | 72.00 | 71.70 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.21 | 72.50 | 71.75 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.23 | 72.75 | 71.76 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.26 | 73.00 | 71.83 | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.30 | 73.50 | 71.94 | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.33 | 74.00 | 71.99 | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.37 | 74.50 | 72.03 | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.40 | 75.00 | 72.07 | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.44 | 75.50 | 72.10 | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.47 | 76.00 | 72.12 | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.49 | 76.50 | 72.15 | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.52 | 77.00 | 72.17 | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.

H =.30

H =.75

H =.99

H =1.17

H =1.56

H =2.01

H =2.47

H =2.93

H =3.40

H =3.88

H =4.35

H =4.83

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Return Event: 100 years

Label: MC-3500 - 2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Orifice - 2 (Orifice-Circular)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 71.50 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.00 | 0.00 | 0.00 | 71.70 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.50 | 0.00 | 0.00 | 0.00 | 71.75 | 0.00 | 0.00 | (N/A) | 0.00 |
| 72.75 | 0.00 | 0.00 | 0.00 | 71.77 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.00 | 0.10 | 73.00 | Free Outfall | 71.83 | 0.00 | 0.00 | (N/A) | 0.00 |
| 73.50 | 0.32 | 73.50 | Free Outfall | 71.94 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.00 | 0.44 | 74.00 | Free Outfall | 71.99 | 0.00 | 0.00 | (N/A) | 0.00 |
| 74.50 | 0.53 | 74.50 | Free Outfall | 72.03 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.00 | 0.61 | 75.00 | Free Outfall | 72.07 | 0.00 | 0.00 | (N/A) | 0.00 |
| 75.50 | 0.68 | 75.50 | Free Outfall | 72.10 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.00 | 0.74 | 76.00 | Free Outfall | 72.12 | 0.00 | 0.00 | (N/A) | 0.00 |
| 76.50 | 0.80 | 76.50 | Free Outfall | 72.15 | 0.00 | 0.00 | (N/A) | 0.00 |
| 77.00 | 0.85 | 77.00 | Free Outfall | 72.17 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .071ft Dcr= .178ft
 CRIT.DEPTH Hev= .00ft
 H =.58
 H =1.08
 H =1.58
 H =2.08
 H =2.58
 H =3.08
 H =3.58
 H =4.08

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: MC-3500 - 2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 71.50 | 0.00 | (N/A) | 0.00 |
| 72.00 | 0.13 | (N/A) | 0.00 |
| 72.50 | 0.20 | (N/A) | 0.00 |
| 72.75 | 0.23 | (N/A) | 0.00 |
| 73.00 | 0.36 | (N/A) | 0.00 |
| 73.50 | 0.62 | (N/A) | 0.00 |
| 74.00 | 0.77 | (N/A) | 0.00 |
| 74.50 | 0.90 | (N/A) | 0.00 |
| 75.00 | 1.01 | (N/A) | 0.00 |
| 75.50 | 1.11 | (N/A) | 0.00 |
| 76.00 | 1.20 | (N/A) | 0.00 |
| 76.50 | 1.29 | (N/A) | 0.00 |
| 77.00 | 1.37 | (N/A) | 0.00 |

Contributing Structures

| |
|---|
| (no Q: Orifice - 1, Orifice - 2, Culvert - 1) |
| Orifice - 1, Culvert - 1 |
| (no Q: Orifice - 2) |
| Orifice - 1, Culvert - 1 |
| (no Q: Orifice - 2) |
| Orifice - 1, Culvert - 1 |
| (no Q: Orifice - 2) |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |
| Orifice - 1, Orifice - 2, Culvert - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| Requested Pond Water Surface Elevations | |
|---|----------|
| Minimum (Headwater) | 63.15 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 68.65 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 63.15 | 68.65 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 63.15 | 68.65 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 24.0 in |
| Length | 109.67 ft |
| Length (Computed Barrel) | 109.67 ft |
| Slope (Computed) | 0.005 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.012 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.079 |
| T2 ratio (HW/D) | 1.216 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|--------------------------|
| T1 Elevation | 65.31 ft | T1 Flow | 15.55 ft ³ /s |
| T2 Elevation | 65.58 ft | T2 Flow | 17.77 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

| | |
|--------------------------------------|-----------------------------|
| Structure ID: Weir - 1 | |
| Structure Type: Rectangular Weir | |
| Number of Openings | 1 |
| Elevation | 63.15 ft |
| Weir Length | 0.50 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 17.23 ft³/s
 Upstream ID = Weir - 1 (Rectangular Weir)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.46 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 63.69 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 63.91 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 64.11 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.12 | 64.31 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.78 | 64.50 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 64.69 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.15 | 10.55 | 64.89 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.65 | 12.61 | 65.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 65.29 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.00 | 65.52 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .075ft Dcr= .219ft
 H.JUMP IN PIPE
 Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .133ft Dcr= .383ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .189ft Dcr= .530ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .243ft Dcr= .667ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .298ft Dcr= .798ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .356ft Dcr= .924ft
 CRIT.DEPTH Hev= .00ft

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: MC-3500 - 3 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 17.23 ft³/s

Upstream ID = Weir - 1 (Rectangular Weir)

Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .416ft Dcr= 1.045ft CRIT.DEPTH Hev= .00ft |
| BACKWATER CONTROL.. Vh= .456ft hwDi= 1.190ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .499ft hwDi= 1.335ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .523ft hwDi= 1.513ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .545ft hwDi= 1.717ft Lbw= 109.7ft Hev= .00ft |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.65 | 63.46 | 63.46 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 64.15 | 63.69 | 63.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 64.65 | 63.91 | 63.91 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 65.15 | 64.11 | 64.11 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.13 | 65.65 | 64.31 | 64.31 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.79 | 66.15 | 64.50 | 64.50 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 66.65 | 64.69 | 64.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.15 | 10.54 | 67.15 | 64.89 | 64.89 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.65 | 12.61 | 67.65 | 65.08 | 65.08 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 68.15 | 65.29 | 65.29 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.02 | 68.65 | 65.52 | 65.52 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H=.50; Htw=.31;
 Qfree=.53;
 H=1.00; Htw=.54;
 Qfree=1.50;
 H=1.50; Htw=.76;
 Qfree=2.76;
 H=2.00; Htw=.96;
 Qfree=4.24;
 H=2.50; Htw=1.16;
 Qfree=5.93;
 H=3.00; Htw=1.35;
 Qfree=7.79;
 H=3.50; Htw=1.54;
 Qfree=9.82;
 H=4.00; Htw=1.74;
 Qfree=12.00;
 H=4.50; Htw=1.93;
 Qfree=14.32;
 H=5.00; Htw=2.14;
 Qfree=16.77;

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: MC-3500 - 3 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

H=5.50; Htw=2.37;
Qfree=19.35;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve

Return Event: 1 years

Label: MC-3500 - 3 OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------|---------------------------|--------------------------|------------------------|
| 63.15 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | (N/A) | 0.00 |
| 64.15 | 1.23 | (N/A) | 0.00 |
| 64.65 | 2.32 | (N/A) | 0.00 |
| 65.15 | 3.63 | (N/A) | 0.00 |
| 65.65 | 5.12 | (N/A) | 0.00 |
| 66.15 | 6.78 | (N/A) | 0.00 |
| 66.65 | 8.59 | (N/A) | 0.00 |
| 67.15 | 10.55 | (N/A) | 0.00 |
| 67.65 | 12.61 | (N/A) | 0.00 |
| 68.15 | 14.78 | (N/A) | 0.00 |
| 68.65 | 17.00 | (N/A) | 0.00 |

Contributing Structures

(no Q: Weir - 1,Culvert - 1)
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: MC-3500 - 3 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 63.15 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 68.65 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 63.15 | 68.65 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 63.15 | 68.65 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: MC-3500 - 3 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 24.0 in |
| Length | 109.67 ft |
| Length (Computed Barrel) | 109.67 ft |
| Slope (Computed) | 0.005 ft/ft |

| | |
|-----------------------|---------|
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.012 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| | |
|-------------------------|--------|
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.079 |
| T2 ratio (HW/D) | 1.216 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|--------------------------|
| T1 Elevation | 65.31 ft | T1 Flow | 15.55 ft ³ /s |
| T2 Elevation | 65.58 ft | T2 Flow | 17.77 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: MC-3500 - 3 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

| | |
|--------------------------------------|-----------------------------|
| Structure ID: Weir - 1 | |
| Structure Type: Rectangular Weir | |
| Number of Openings | 1 |
| Elevation | 63.15 ft |
| Weir Length | 0.50 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 17.23 ft³/s
 Upstream ID = Weir - 1 (Rectangular Weir)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.46 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 63.69 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 63.91 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 64.11 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.12 | 64.31 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.78 | 64.50 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 64.69 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.15 | 10.55 | 64.89 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.65 | 12.61 | 65.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 65.29 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.00 | 65.52 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .075ft Dcr= .219ft
 H.JUMP IN PIPE
 Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .133ft Dcr= .383ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .189ft Dcr= .530ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .243ft Dcr= .667ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .298ft Dcr= .798ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .356ft Dcr= .924ft
 CRIT.DEPTH Hev= .00ft

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 3 OUT
Scenario: Post-Development 10 year

Return Event: 10 years
Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 17.23 ft³/s
Upstream ID = Weir - 1 (Rectangular Weir)
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .416ft Dcr= 1.045ft CRIT.DEPTH Hev= .00ft |
| BACKWATER CONTROL.. Vh= .456ft hwDi= 1.190ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .499ft hwDi= 1.335ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .523ft hwDi= 1.513ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .545ft hwDi= 1.717ft Lbw= 109.7ft Hev= .00ft |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.65 | 63.46 | 63.46 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 64.15 | 63.69 | 63.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 64.65 | 63.91 | 63.91 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 65.15 | 64.11 | 64.11 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.13 | 65.65 | 64.31 | 64.31 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.79 | 66.15 | 64.50 | 64.50 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 66.65 | 64.69 | 64.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.15 | 10.54 | 67.15 | 64.89 | 64.89 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.65 | 12.61 | 67.65 | 65.08 | 65.08 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 68.15 | 65.29 | 65.29 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.02 | 68.65 | 65.52 | 65.52 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H=.50; Htw=.31;
 Qfree=.53;
 H=1.00; Htw=.54;
 Qfree=1.50;
 H=1.50; Htw=.76;
 Qfree=2.76;
 H=2.00; Htw=.96;
 Qfree=4.24;
 H=2.50; Htw=1.16;
 Qfree=5.93;
 H=3.00; Htw=1.35;
 Qfree=7.79;
 H=3.50; Htw=1.54;
 Qfree=9.82;
 H=4.00; Htw=1.74;
 Qfree=12.00;
 H=4.50; Htw=1.93;
 Qfree=14.32;
 H=5.00; Htw=2.14;
 Qfree=16.77;

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: MC-3500 - 3 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

H=5.50; Htw=2.37;
Qfree=19.35;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 63.15 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | (N/A) | 0.00 |
| 64.15 | 1.23 | (N/A) | 0.00 |
| 64.65 | 2.32 | (N/A) | 0.00 |
| 65.15 | 3.63 | (N/A) | 0.00 |
| 65.65 | 5.12 | (N/A) | 0.00 |
| 66.15 | 6.78 | (N/A) | 0.00 |
| 66.65 | 8.59 | (N/A) | 0.00 |
| 67.15 | 10.55 | (N/A) | 0.00 |
| 67.65 | 12.61 | (N/A) | 0.00 |
| 68.15 | 14.78 | (N/A) | 0.00 |
| 68.65 | 17.00 | (N/A) | 0.00 |

Contributing Structures

(no Q: Weir - 1,Culvert - 1)
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: MC-3500 - 3 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 63.15 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 68.65 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 63.15 | 68.65 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 63.15 | 68.65 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: MC-3500 - 3 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 24.0 in |
| Length | 109.67 ft |
| Length (Computed Barrel) | 109.67 ft |
| Slope (Computed) | 0.005 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.012 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.079 |
| T2 ratio (HW/D) | 1.216 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|--------------------------|
| T1 Elevation | 65.31 ft | T1 Flow | 15.55 ft ³ /s |
| T2 Elevation | 65.58 ft | T2 Flow | 17.77 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: MC-3500 - 3 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

| | |
|--------------------------------------|-----------------------------|
| Structure ID: Weir - 1 | |
| Structure Type: Rectangular Weir | |
| Number of Openings | 1 |
| Elevation | 63.15 ft |
| Weir Length | 0.50 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 17.23 ft³/s
 Upstream ID = Weir - 1 (Rectangular Weir)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.46 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 63.69 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 63.91 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 64.11 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.12 | 64.31 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.78 | 64.50 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 64.69 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.15 | 10.55 | 64.89 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.65 | 12.61 | 65.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 65.29 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.00 | 65.52 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .075ft Dcr= .219ft
 H.JUMP IN PIPE
 Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .133ft Dcr= .383ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .189ft Dcr= .530ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .243ft Dcr= .667ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .298ft Dcr= .798ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .356ft Dcr= .924ft
 CRIT.DEPTH Hev= .00ft

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 3 OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 17.23 ft³/s
Upstream ID = Weir - 1 (Rectangular Weir)
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .416ft Dcr= 1.045ft CRIT.DEPTH Hev= .00ft |
| BACKWATER CONTROL.. Vh= .456ft hwDi= 1.190ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .499ft hwDi= 1.335ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .523ft hwDi= 1.513ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .545ft hwDi= 1.717ft Lbw= 109.7ft Hev= .00ft |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.65 | 63.46 | 63.46 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 64.15 | 63.69 | 63.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 64.65 | 63.91 | 63.91 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 65.15 | 64.11 | 64.11 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.13 | 65.65 | 64.31 | 64.31 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.79 | 66.15 | 64.50 | 64.50 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 66.65 | 64.69 | 64.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.15 | 10.54 | 67.15 | 64.89 | 64.89 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.65 | 12.61 | 67.65 | 65.08 | 65.08 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 68.15 | 65.29 | 65.29 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.02 | 68.65 | 65.52 | 65.52 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H=.50; Htw=.31;
 Qfree=.53;
 H=1.00; Htw=.54;
 Qfree=1.50;
 H=1.50; Htw=.76;
 Qfree=2.76;
 H=2.00; Htw=.96;
 Qfree=4.24;
 H=2.50; Htw=1.16;
 Qfree=5.93;
 H=3.00; Htw=1.35;
 Qfree=7.79;
 H=3.50; Htw=1.54;
 Qfree=9.82;
 H=4.00; Htw=1.74;
 Qfree=12.00;
 H=4.50; Htw=1.93;
 Qfree=14.32;
 H=5.00; Htw=2.14;
 Qfree=16.77;

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: MC-3500 - 3 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

H=5.50; Htw=2.37;
Qfree=19.35;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 63.15 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | (N/A) | 0.00 |
| 64.15 | 1.23 | (N/A) | 0.00 |
| 64.65 | 2.32 | (N/A) | 0.00 |
| 65.15 | 3.63 | (N/A) | 0.00 |
| 65.65 | 5.12 | (N/A) | 0.00 |
| 66.15 | 6.78 | (N/A) | 0.00 |
| 66.65 | 8.59 | (N/A) | 0.00 |
| 67.15 | 10.55 | (N/A) | 0.00 |
| 67.65 | 12.61 | (N/A) | 0.00 |
| 68.15 | 14.78 | (N/A) | 0.00 |
| 68.65 | 17.00 | (N/A) | 0.00 |

Contributing Structures

(no Q: Weir - 1,Culvert - 1)
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: MC-3500 - 3 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 63.15 ft |
| Increment (Headwater) | 0.50 ft |
| Maximum (Headwater) | 68.65 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------|-----------|-------------|------------|------------|
| Rectangular Weir | Weir - 1 | Forward | Culvert - 1 | 63.15 | 68.65 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 63.15 | 68.65 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: MC-3500 - 3 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 24.0 in |
| Length | 109.67 ft |
| Length (Computed Barrel) | 109.67 ft |
| Slope (Computed) | 0.005 ft/ft |

| | |
|-----------------------|---------|
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.012 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |

| | |
|-------------------------|--------|
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.079 |
| T2 ratio (HW/D) | 1.216 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|--------------------------|
| T1 Elevation | 65.31 ft | T1 Flow | 15.55 ft ³ /s |
| T2 Elevation | 65.58 ft | T2 Flow | 17.77 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: MC-3500 - 3 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|--------------------------------------|-----------------------------|
| Structure ID: Weir - 1 | |
| Structure Type: Rectangular Weir | |
| Number of Openings | 1 |
| Elevation | 63.15 ft |
| Weir Length | 0.50 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 17.23 ft³/s
 Upstream ID = Weir - 1 (Rectangular Weir)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.46 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 63.69 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 63.91 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 64.11 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.12 | 64.31 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.78 | 64.50 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 64.69 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.15 | 10.55 | 64.89 | Free Outfall | Free Outfall | 0.00 | 0.01 | (N/A) | 0.00 |
| 67.65 | 12.61 | 65.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 65.29 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.00 | 65.52 | Free Outfall | Free Outfall | 0.00 | 0.02 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 CRIT.DEPTH CONTROL
 Vh= .075ft Dcr= .219ft
 H.JUMP IN PIPE
 Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .133ft Dcr= .383ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .189ft Dcr= .530ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .243ft Dcr= .667ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .298ft Dcr= .798ft
 CRIT.DEPTH Hev= .00ft
 CRIT.DEPTH CONTROL
 Vh= .356ft Dcr= .924ft
 CRIT.DEPTH Hev= .00ft

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 3 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 17.23 ft³/s
Upstream ID = Weir - 1 (Rectangular Weir)
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .416ft Dcr= 1.045ft CRIT.DEPTH Hev= .00ft |
| BACKWATER CONTROL.. Vh= .456ft hwDi= 1.190ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .499ft hwDi= 1.335ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .523ft hwDi= 1.513ft Lbw= 109.7ft Hev= .00ft |
| BACKWATER CONTROL.. Vh= .545ft hwDi= 1.717ft Lbw= 109.7ft Hev= .00ft |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 63.15 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | 63.65 | 63.46 | 63.46 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.15 | 1.23 | 64.15 | 63.69 | 63.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 64.65 | 2.32 | 64.65 | 63.91 | 63.91 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.15 | 3.63 | 65.15 | 64.11 | 64.11 | 0.00 | 0.00 | (N/A) | 0.00 |
| 65.65 | 5.13 | 65.65 | 64.31 | 64.31 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.15 | 6.79 | 66.15 | 64.50 | 64.50 | 0.00 | 0.00 | (N/A) | 0.00 |
| 66.65 | 8.59 | 66.65 | 64.69 | 64.69 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.15 | 10.54 | 67.15 | 64.89 | 64.89 | 0.00 | 0.00 | (N/A) | 0.00 |
| 67.65 | 12.61 | 67.65 | 65.08 | 65.08 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.15 | 14.78 | 68.15 | 65.29 | 65.29 | 0.00 | 0.00 | (N/A) | 0.00 |
| 68.65 | 17.02 | 68.65 | 65.52 | 65.52 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 H=.50; Htw=.31;
 Qfree=.53;
 H=1.00; Htw=.54;
 Qfree=1.50;
 H=1.50; Htw=.76;
 Qfree=2.76;
 H=2.00; Htw=.96;
 Qfree=4.24;
 H=2.50; Htw=1.16;
 Qfree=5.93;
 H=3.00; Htw=1.35;
 Qfree=7.79;
 H=3.50; Htw=1.54;
 Qfree=9.82;
 H=4.00; Htw=1.74;
 Qfree=12.00;
 H=4.50; Htw=1.93;
 Qfree=14.32;
 H=5.00; Htw=2.14;
 Qfree=16.77;

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: MC-3500 - 3 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Weir - 1 (Rectangular Weir)

Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

Message

H=5.50; Htw=2.37;
Qfree=19.35;

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: MC-3500 - 3 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 63.15 | 0.00 | (N/A) | 0.00 |
| 63.65 | 0.41 | (N/A) | 0.00 |
| 64.15 | 1.23 | (N/A) | 0.00 |
| 64.65 | 2.32 | (N/A) | 0.00 |
| 65.15 | 3.63 | (N/A) | 0.00 |
| 65.65 | 5.12 | (N/A) | 0.00 |
| 66.15 | 6.78 | (N/A) | 0.00 |
| 66.65 | 8.59 | (N/A) | 0.00 |
| 67.15 | 10.55 | (N/A) | 0.00 |
| 67.65 | 12.61 | (N/A) | 0.00 |
| 68.15 | 14.78 | (N/A) | 0.00 |
| 68.65 | 17.00 | (N/A) | 0.00 |

Contributing Structures

(no Q: Weir - 1,Culvert - 1)
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1
 Weir - 1,Culvert - 1

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 1 years

Label: SP-2 OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 78.81 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 80.31 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------------------------|-----------|-------------|------------|------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | Culvert - 1 | 0.00 | 80.31 |
| Stand Pipe | Riser - 1 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Stand Pipe | Riser - 2 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 74.56 | 80.31 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.14 |
| 1.00 | 0.14 |
| 1.50 | 0.14 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 1 years

Label: SP-2 OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 9.69 ft |
| Length (Computed Barrel) | 9.69 ft |
| Slope (Computed) | 0.010 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.076 |
| T2 ratio (HW/D) | 1.214 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 75.91 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 76.08 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 1 years

Label: SP-2 OUT

Storm Event: 1 year

Scenario: Post-Development 1 year

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 1 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 2 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|--------------------------------------|--------------|
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| <hr/> | |
| Tailwater Type | Free Outfall |

| | |
|-------------------------------|---------|
| Convergence Tolerances | |
| <hr/> | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

| Convergence Tolerances | |
|-------------------------------|---------------------------|
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 78.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 78.91 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 79.01 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 79.11 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 79.21 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 79.31 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 79.41 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 79.51 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 79.61 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 79.71 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 79.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.14 | 79.91 | 75.04 | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.14 | 80.01 | 75.34 | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 0.14 | 80.11 | 75.64 | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 0.14 | 80.21 | 75.96 | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 0.14 | 80.31 | 76.08 | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|-------------------------------|
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 7.06 ft³/s
 Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.74 | 75.04 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 1.83 | 75.34 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 3.24 | 75.64 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 4.91 | 75.96 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 5.49 | 76.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

```

CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
    
```

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 7.06 ft³/s

Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2

Downstream ID = Tailwater (Pond Outfall)

| Message |
|------------------------|
| CRIT.DEPTH CONTROL |
| Vh= .049ft Dcr= .145ft |
| CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL |
| Vh= .049ft Dcr= .145ft |
| CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL |
| Vh= .049ft Dcr= .145ft |
| CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL |
| Vh= .049ft Dcr= .145ft |
| CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL |
| Vh= .049ft Dcr= .145ft |
| CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET |
| TO UPSTREAM |
| CONTROLLING |
| STRUCTURE |
| CRIT.DEPTH CONTROL |
| Vh= .204ft Dcr= .537ft |
| CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL |
| Vh= .299ft Dcr= .725ft |
| CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL |
| Vh= .420ft Dcr= .899ft |
| CRIT.DEPTH Hev= .00ft |
| INLET CONTROL... |
| Transition: HW =1.52 |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 1 (Stand Pipe)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

Weir: H =0.1ft

Weir: H =0.2ft

Weir: H =0.3ft

Weir: H =0.4ft

Orifice: H = .50; Riser orifice equation controlling.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 2 (Stand Pipe)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|---|
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| Weir: H =0.1ft |
| Weir: H =0.2ft |
| Weir: H =0.3ft |
| Weir: H =0.4ft |
| Orifice: H = .50; Riser orifice equation controlling. |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: SP-2 OUT
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 78.81 | 0.14 | (N/A) | 0.00 |
| 78.91 | 0.14 | (N/A) | 0.00 |
| 79.01 | 0.14 | (N/A) | 0.00 |
| 79.11 | 0.14 | (N/A) | 0.00 |
| 79.21 | 0.14 | (N/A) | 0.00 |
| 79.31 | 0.14 | (N/A) | 0.00 |
| 79.41 | 0.14 | (N/A) | 0.00 |
| 79.51 | 0.14 | (N/A) | 0.00 |
| 79.61 | 0.14 | (N/A) | 0.00 |
| 79.71 | 0.14 | (N/A) | 0.00 |
| 79.81 | 0.14 | (N/A) | 0.00 |
| 79.91 | 0.74 | (N/A) | 0.00 |
| 80.01 | 1.83 | (N/A) | 0.00 |
| 80.11 | 3.24 | (N/A) | 0.00 |
| 80.21 | 4.91 | (N/A) | 0.00 |
| 80.31 | 5.49 | (N/A) | 0.00 |

Contributing Structures

| |
|---------------------------|
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve

Label: SP-2 OUT

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Composite Outflow Summary

Contributing Structures

| |
|---|
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: SP-2 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 78.81 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 80.31 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------------------------|-----------|-------------|------------|------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | Culvert - 1 | 0.00 | 80.31 |
| Stand Pipe | Riser - 1 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Stand Pipe | Riser - 2 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 74.56 | 80.31 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.14 |
| 1.00 | 0.14 |
| 1.50 | 0.14 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: SP-2 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 9.69 ft |
| Length (Computed Barrel) | 9.69 ft |
| Slope (Computed) | 0.010 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.076 |
| T2 ratio (HW/D) | 1.214 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 75.91 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 76.08 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 10 years

Label: SP-2 OUT

Storm Event: 10 year

Scenario: Post-Development 10 year

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 1 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 2 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|--------------------------------------|--------------|
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| <hr/> | |
| Tailwater Type | Free Outfall |

| | |
|-------------------------------|---------|
| Convergence Tolerances | |
| <hr/> | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

| Convergence Tolerances | |
|-------------------------------|---------------------------|
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 78.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 78.91 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 79.01 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 79.11 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 79.21 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 79.31 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 79.41 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 79.51 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 79.61 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 79.71 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 79.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.14 | 79.91 | 75.04 | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.14 | 80.01 | 75.34 | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 0.14 | 80.11 | 75.64 | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 0.14 | 80.21 | 75.96 | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 0.14 | 80.31 | 76.08 | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|-------------------------------|
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 7.06 ft³/s
 Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.74 | 75.04 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 1.83 | 75.34 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 3.24 | 75.64 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 4.91 | 75.96 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 5.49 | 76.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

```

CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
    
```


Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: SP-2 OUT
Scenario: Post-Development 10 year

Return Event: 10 years
Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 7.06 ft³/s
Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| CRIT.DEPTH CONTROL Vh= .204ft Dcr= .537ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .299ft Dcr= .725ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .420ft Dcr= .899ft CRIT.DEPTH Hev= .00ft |
| INLET CONTROL... Transition: HW =1.52 |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 1 (Stand Pipe)

 Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

Weir: H =0.1ft

Weir: H =0.2ft

Weir: H =0.3ft

Weir: H =0.4ft

Orifice: H = .50; Riser orifice equation controlling.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

Weir: H =0.1ft

Weir: H =0.2ft

Weir: H =0.3ft

Weir: H =0.4ft

Orifice: H = .50; Riser orifice equation controlling.

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: SP-2 OUT
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 78.81 | 0.14 | (N/A) | 0.00 |
| 78.91 | 0.14 | (N/A) | 0.00 |
| 79.01 | 0.14 | (N/A) | 0.00 |
| 79.11 | 0.14 | (N/A) | 0.00 |
| 79.21 | 0.14 | (N/A) | 0.00 |
| 79.31 | 0.14 | (N/A) | 0.00 |
| 79.41 | 0.14 | (N/A) | 0.00 |
| 79.51 | 0.14 | (N/A) | 0.00 |
| 79.61 | 0.14 | (N/A) | 0.00 |
| 79.71 | 0.14 | (N/A) | 0.00 |
| 79.81 | 0.14 | (N/A) | 0.00 |
| 79.91 | 0.74 | (N/A) | 0.00 |
| 80.01 | 1.83 | (N/A) | 0.00 |
| 80.11 | 3.24 | (N/A) | 0.00 |
| 80.21 | 4.91 | (N/A) | 0.00 |
| 80.31 | 5.49 | (N/A) | 0.00 |

Contributing Structures

| |
|---------------------------|
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve

Label: SP-2 OUT

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Composite Outflow Summary

Contributing Structures

User Defined Rating
Table - 1,Culvert - 1 (no
Q: Riser - 1,Riser - 2)

User Defined Rating
Table - 1,Culvert - 1 (no
Q: Riser - 1,Riser - 2)

User Defined Rating
Table - 1,Riser - 1,Riser -
2,Culvert - 1

User Defined Rating
Table - 1,Riser - 1,Riser -
2,Culvert - 1

User Defined Rating
Table - 1,Riser - 1,Riser -
2,Culvert - 1

User Defined Rating
Table - 1,Riser - 1,Riser -
2,Culvert - 1

User Defined Rating
Table - 1,Riser - 1,Riser -
2,Culvert - 1

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: SP-2 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 78.81 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 80.31 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------------------------|-----------|-------------|------------|------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | Culvert - 1 | 0.00 | 80.31 |
| Stand Pipe | Riser - 1 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Stand Pipe | Riser - 2 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 74.56 | 80.31 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.14 |
| 1.00 | 0.14 |
| 1.50 | 0.14 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: SP-2 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 9.69 ft |
| Length (Computed Barrel) | 9.69 ft |
| Slope (Computed) | 0.010 ft/ft |
| <hr/> | |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| <hr/> | |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.076 |
| T2 ratio (HW/D) | 1.214 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 75.91 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 76.08 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 25 years

Label: SP-2 OUT

Storm Event: 25 year

Scenario: Post-Development 25 year

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 1 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 2 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|--------------------------------------|--------------|
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| <hr/> | |
| Tailwater Type | Free Outfall |

| | |
|-------------------------------|---------|
| Convergence Tolerances | |
| <hr/> | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

| Convergence Tolerances | |
|-------------------------------|---------------------------|
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 78.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 78.91 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 79.01 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 79.11 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 79.21 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 79.31 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 79.41 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 79.51 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 79.61 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 79.71 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 79.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.14 | 79.91 | 75.04 | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.14 | 80.01 | 75.34 | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 0.14 | 80.11 | 75.64 | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 0.14 | 80.21 | 75.96 | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 0.14 | 80.31 | 76.08 | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table
 Interpolated from input table

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|-------------------------------|
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 7.06 ft³/s
 Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.74 | 75.04 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 1.83 | 75.34 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 3.24 | 75.64 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 4.91 | 75.96 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 5.49 | 76.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

```

CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
    
```

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: SP-2 OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 7.06 ft³/s
Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .204ft Dcr= .537ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .299ft Dcr= .725ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .420ft Dcr= .899ft CRIT.DEPTH Hev= .00ft |
| INLET CONTROL... Transition: HW =1.52 |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

Weir: H =0.1ft

Weir: H =0.2ft

Weir: H =0.3ft

Weir: H =0.4ft

Orifice: H = .50; Riser orifice equation controlling.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves

Label: SP-2 OUT

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

Message

WS below an invert; no flow.

WS below an invert; no flow.

Weir: H =0.1ft

Weir: H =0.2ft

Weir: H =0.3ft

Weir: H =0.4ft

Orifice: H = .50; Riser orifice equation controlling.

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: SP-2 OUT
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 78.81 | 0.14 | (N/A) | 0.00 |
| 78.91 | 0.14 | (N/A) | 0.00 |
| 79.01 | 0.14 | (N/A) | 0.00 |
| 79.11 | 0.14 | (N/A) | 0.00 |
| 79.21 | 0.14 | (N/A) | 0.00 |
| 79.31 | 0.14 | (N/A) | 0.00 |
| 79.41 | 0.14 | (N/A) | 0.00 |
| 79.51 | 0.14 | (N/A) | 0.00 |
| 79.61 | 0.14 | (N/A) | 0.00 |
| 79.71 | 0.14 | (N/A) | 0.00 |
| 79.81 | 0.14 | (N/A) | 0.00 |
| 79.91 | 0.74 | (N/A) | 0.00 |
| 80.01 | 1.83 | (N/A) | 0.00 |
| 80.11 | 3.24 | (N/A) | 0.00 |
| 80.21 | 4.91 | (N/A) | 0.00 |
| 80.31 | 5.49 | (N/A) | 0.00 |

Contributing Structures

| |
|---|
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
Label: SP-2 OUT
Scenario: Post-Development 25 year

Return Event: 25 years
Storm Event: 25 year

Composite Outflow Summary

Contributing Structures

| |
|---|
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: SP-2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

Requested Pond Water Surface Elevations

| | |
|-----------------------|----------|
| Minimum (Headwater) | 78.81 ft |
| Increment (Headwater) | 0.10 ft |
| Maximum (Headwater) | 80.31 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--------------------|-------------------------------|-----------|-------------|------------|------------|
| User Defined Table | User Defined Rating Table - 1 | Forward | Culvert - 1 | 0.00 | 80.31 |
| Stand Pipe | Riser - 1 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Stand Pipe | Riser - 2 | Forward | Culvert - 1 | 79.81 | 80.31 |
| Culvert-Circular | Culvert - 1 | Forward | TW | 74.56 | 80.31 |
| Tailwater Settings | Tailwater | | | (N/A) | (N/A) |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Structure ID: User Defined Rating Table - 1
Structure Type: User Defined Table

| Elevation (ft) | Flow (ft ³ /s) |
|-------------------|------------------------------|
| 0.00 | 0.14 |
| 1.00 | 0.14 |
| 1.50 | 0.14 |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: SP-2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|----------------------------------|-------------|
| Structure ID: Culvert - 1 | |
| Structure Type: Culvert-Circular | |
| Number of Barrels | 1 |
| Diameter | 15.0 in |
| Length | 9.69 ft |
| Length (Computed Barrel) | 9.69 ft |
| Slope (Computed) | 0.010 ft/ft |
| Outlet Control Data | |
| Manning's n | 0.013 |
| Ke | 0.200 |
| Kb | 0.023 |
| Kr | 0.200 |
| Convergence Tolerance | 0.00 ft |
| Inlet Control Data | |
| Equation Form | Form 1 |
| K | 0.0018 |
| M | 2.5000 |
| C | 0.0243 |
| Y | 0.8300 |
| T1 ratio (HW/D) | 1.076 |
| T2 ratio (HW/D) | 1.214 |
| Slope Correction Factor | -0.500 |

Use unsubmerged inlet control 0 equation below T1 elevation.

Use submerged inlet control 0 equation above T2 elevation

In transition zone between unsubmerged and submerged inlet control, interpolate between flows at T1 & T2...

| | | | |
|--------------|----------|---------|-------------------------|
| T1 Elevation | 75.91 ft | T1 Flow | 4.80 ft ³ /s |
| T2 Elevation | 76.08 ft | T2 Flow | 5.49 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Return Event: 100 years

Label: SP-2 OUT

Storm Event: 100 year

Scenario: Post-Development 100 year

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 1 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|----------------------------|-----------------------------|
| Structure ID: Riser - 2 | |
| Structure Type: Stand Pipe | |
| <hr/> | |
| Number of Openings | 1 |
| Elevation | 79.81 ft |
| Diameter | 12.0 in |
| Orifice Area | 0.8 ft ² |
| Orifice Coefficient | 0.600 |
| Weir Length | 3.14 ft |
| Weir Coefficient | 3.00 (ft ^{0.5})/s |
| K Reverse | 1.000 |
| Manning's n | 0.000 |
| Kev, Charged Riser | 0.000 |
| Weir Submergence | False |
| Orifice H to crest | False |

| | |
|--------------------------------------|--------------|
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| <hr/> | |
| Tailwater Type | Free Outfall |

| | |
|-------------------------------|---------|
| Convergence Tolerances | |
| <hr/> | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |

Existing and Proposed Hydrologic Calculations

Subsection: Outlet Input Data

Label: SP-2 OUT

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Convergence Tolerances

| | |
|----------------------------------|---------------------------|
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 78.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 78.91 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 79.01 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 79.11 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 79.21 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 79.31 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 79.41 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 79.51 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 79.61 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 79.71 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 79.81 | 74.76 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.14 | 79.91 | 75.04 | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.14 | 80.01 | 75.34 | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 0.14 | 80.11 | 75.64 | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 0.14 | 80.21 | 75.96 | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 0.14 | 80.31 | 76.08 | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

| Message |
|-------------------------------|
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: SP-2 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE

Structure ID = User Defined Rating Table - 1 (User Defined Table)

Upstream ID = (Pond Water Surface)

Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|-------------------------------|
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |
| Interpolated from input table |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Culvert - 1 (Culvert-Circular)

 Mannings open channel maximum capacity: 7.06 ft³/s
 Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.14 | 74.76 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.74 | 75.04 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 1.83 | 75.34 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 3.24 | 75.64 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 4.91 | 75.96 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 5.49 | 76.08 | Free Outfall | Free Outfall | 0.00 | 0.00 | (N/A) | 0.00 |

Message

```

CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
CRIT.DEPTH CONTROL
Vh= .049ft Dcr= .145ft
CRIT.DEPTH Hev= .00ft
    
```

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: SP-2 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Culvert - 1 (Culvert-Circular)

Mannings open channel maximum capacity: 7.06 ft³/s
Upstream ID = User Defined Rating Table - 1, Riser - 1, Riser - 2
Downstream ID = Tailwater (Pond Outfall)

| Message |
|---|
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .049ft Dcr= .145ft CRIT.DEPTH Hev= .00ft |
| FLOW PRECEDENCE SET TO UPSTREAM CONTROLLING STRUCTURE |
| CRIT.DEPTH CONTROL Vh= .204ft Dcr= .537ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .299ft Dcr= .725ft CRIT.DEPTH Hev= .00ft |
| CRIT.DEPTH CONTROL Vh= .420ft Dcr= .899ft CRIT.DEPTH Hev= .00ft |
| INLET CONTROL... Transition: HW =1.52 |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: SP-2 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 1 (Stand Pipe)

Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|--|
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| Weir: H =0.1ft |
| Weir: H =0.2ft |
| Weir: H =0.3ft |
| Weir: H =0.4ft |
| Orifice: H =.50; Riser orifice equation controlling. |

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
 Label: SP-2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)
 Downstream ID = Culvert - 1 (Culvert-Circular)

| Water Surface Elevation (ft) | Device Flow (ft ³ /s) | (into) Headwater Hydraulic Grade Line (ft) | Converge Downstream Hydraulic Grade Line (ft) | Next Downstream Hydraulic Grade Line (ft) | Downstream Hydraulic Grade Line Error (ft) | Convergence Error (ft ³ /s) | Downstream Channel Tailwater (ft) | Tailwater Error (ft) |
|------------------------------|----------------------------------|--|---|---|--|--|-----------------------------------|----------------------|
| 78.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 78.91 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.01 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.11 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.21 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.31 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.41 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.51 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.61 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.71 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.81 | 0.00 | 0.00 | 0.00 | 74.76 | 0.00 | 0.00 | (N/A) | 0.00 |
| 79.91 | 0.30 | 79.91 | Free Outfall | 75.04 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.01 | 0.84 | 80.01 | Free Outfall | 75.34 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.11 | 1.55 | 80.11 | Free Outfall | 75.64 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.21 | 2.38 | 80.21 | Free Outfall | 75.96 | 0.00 | 0.00 | (N/A) | 0.00 |
| 80.31 | 2.67 | 80.31 | Free Outfall | 76.08 | 0.00 | 0.00 | (N/A) | 0.00 |

Message

WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.
 WS below an invert; no flow.

Existing and Proposed Hydrologic Calculations

Subsection: Individual Outlet Curves
Label: SP-2 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

RATING TABLE FOR ONE OUTLET TYPE
Structure ID = Riser - 2 (Stand Pipe)

Upstream ID = (Pond Water Surface)
Downstream ID = Culvert - 1 (Culvert-Circular)

| Message |
|--|
| WS below an invert; no flow. |
| WS below an invert; no flow. |
| Weir: H =0.1ft |
| Weir: H =0.2ft |
| Weir: H =0.3ft |
| Weir: H =0.4ft |
| Orifice: H =.50; Riser orifice equation controlling. |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
 Label: SP-2 OUT
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 78.81 | 0.14 | (N/A) | 0.00 |
| 78.91 | 0.14 | (N/A) | 0.00 |
| 79.01 | 0.14 | (N/A) | 0.00 |
| 79.11 | 0.14 | (N/A) | 0.00 |
| 79.21 | 0.14 | (N/A) | 0.00 |
| 79.31 | 0.14 | (N/A) | 0.00 |
| 79.41 | 0.14 | (N/A) | 0.00 |
| 79.51 | 0.14 | (N/A) | 0.00 |
| 79.61 | 0.14 | (N/A) | 0.00 |
| 79.71 | 0.14 | (N/A) | 0.00 |
| 79.81 | 0.14 | (N/A) | 0.00 |
| 79.91 | 0.74 | (N/A) | 0.00 |
| 80.01 | 1.83 | (N/A) | 0.00 |
| 80.11 | 3.24 | (N/A) | 0.00 |
| 80.21 | 4.91 | (N/A) | 0.00 |
| 80.31 | 5.49 | (N/A) | 0.00 |

Contributing Structures

| |
|---------------------------|
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |
| User Defined Rating |
| Table - 1,Culvert - 1 (no |
| Q: Riser - 1,Riser - 2) |

Existing and Proposed Hydrologic Calculations

Subsection: Composite Rating Curve
Label: SP-2 OUT
Scenario: Post-Development 100 year

Return Event: 100 years
Storm Event: 100 year

Composite Outflow Summary

Contributing Structures

| |
|---|
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Culvert - 1 (no Q: Riser - 1,Riser - 2) |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |
| User Defined Rating Table - 1,Riser - 1,Riser - 2,Culvert - 1 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 1 years

Label: 24" Depth Green Roof

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.09 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.09 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.09 | 0 | 508 | 0.00 | 0.09 | 0.09 |
| 93.10 | 0.09 | 51 | 508 | 0.00 | 0.09 | 0.65 |
| 93.20 | 0.09 | 114 | 1,016 | 0.00 | 0.09 | 1.36 |
| 93.30 | 0.09 | 216 | 1,016 | 0.00 | 0.09 | 2.49 |
| 93.40 | 0.09 | 317 | 1,016 | 0.00 | 0.09 | 3.61 |
| 93.50 | 0.09 | 419 | 1,016 | 0.00 | 0.09 | 4.74 |
| 93.60 | 0.09 | 520 | 1,016 | 0.00 | 0.09 | 5.87 |
| 93.70 | 0.09 | 622 | 1,016 | 0.00 | 0.09 | 7.00 |
| 93.80 | 0.09 | 723 | 1,016 | 0.00 | 0.09 | 8.13 |
| 93.90 | 0.09 | 825 | 1,016 | 0.00 | 0.09 | 9.26 |
| 94.00 | 0.09 | 926 | 1,016 | 0.00 | 0.09 | 10.38 |
| 94.10 | 0.09 | 1,028 | 1,016 | 0.00 | 0.09 | 11.51 |
| 94.20 | 0.09 | 1,130 | 1,016 | 0.00 | 0.09 | 12.64 |
| 94.30 | 0.09 | 1,231 | 1,016 | 0.00 | 0.09 | 13.77 |
| 94.40 | 0.09 | 1,333 | 1,016 | 0.00 | 0.09 | 14.90 |
| 94.50 | 0.09 | 1,434 | 1,016 | 0.00 | 0.09 | 16.03 |
| 94.60 | 0.09 | 1,536 | 1,016 | 0.00 | 0.09 | 17.15 |
| 94.70 | 0.09 | 1,637 | 1,016 | 0.00 | 0.09 | 18.28 |
| 94.80 | 0.09 | 1,739 | 1,016 | 0.00 | 0.09 | 19.41 |
| 94.90 | 0.09 | 1,840 | 1,016 | 0.00 | 0.09 | 20.54 |
| 95.00 | 0.09 | 1,942 | 1,016 | 0.00 | 0.09 | 21.67 |
| 95.10 | 0.09 | 2,044 | 1,016 | 0.00 | 0.09 | 22.80 |
| 95.20 | 0.09 | 2,170 | 2,031 | 0.00 | 0.09 | 24.20 |
| 95.21 | 0.09 | 2,191 | 2,031 | 0.00 | 0.09 | 24.43 |
| 95.30 | 3.74 | 2,373 | 2,031 | 0.00 | 3.74 | 30.10 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 10 years

Label: 24" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.09 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.09 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.09 | 0 | 508 | 0.00 | 0.09 | 0.09 |
| 93.10 | 0.09 | 51 | 508 | 0.00 | 0.09 | 0.65 |
| 93.20 | 0.09 | 114 | 1,016 | 0.00 | 0.09 | 1.36 |
| 93.30 | 0.09 | 216 | 1,016 | 0.00 | 0.09 | 2.49 |
| 93.40 | 0.09 | 317 | 1,016 | 0.00 | 0.09 | 3.61 |
| 93.50 | 0.09 | 419 | 1,016 | 0.00 | 0.09 | 4.74 |
| 93.60 | 0.09 | 520 | 1,016 | 0.00 | 0.09 | 5.87 |
| 93.70 | 0.09 | 622 | 1,016 | 0.00 | 0.09 | 7.00 |
| 93.80 | 0.09 | 723 | 1,016 | 0.00 | 0.09 | 8.13 |
| 93.90 | 0.09 | 825 | 1,016 | 0.00 | 0.09 | 9.26 |
| 94.00 | 0.09 | 926 | 1,016 | 0.00 | 0.09 | 10.38 |
| 94.10 | 0.09 | 1,028 | 1,016 | 0.00 | 0.09 | 11.51 |
| 94.20 | 0.09 | 1,130 | 1,016 | 0.00 | 0.09 | 12.64 |
| 94.30 | 0.09 | 1,231 | 1,016 | 0.00 | 0.09 | 13.77 |
| 94.40 | 0.09 | 1,333 | 1,016 | 0.00 | 0.09 | 14.90 |
| 94.50 | 0.09 | 1,434 | 1,016 | 0.00 | 0.09 | 16.03 |
| 94.60 | 0.09 | 1,536 | 1,016 | 0.00 | 0.09 | 17.15 |
| 94.70 | 0.09 | 1,637 | 1,016 | 0.00 | 0.09 | 18.28 |
| 94.80 | 0.09 | 1,739 | 1,016 | 0.00 | 0.09 | 19.41 |
| 94.90 | 0.09 | 1,840 | 1,016 | 0.00 | 0.09 | 20.54 |
| 95.00 | 0.09 | 1,942 | 1,016 | 0.00 | 0.09 | 21.67 |
| 95.10 | 0.09 | 2,044 | 1,016 | 0.00 | 0.09 | 22.80 |
| 95.20 | 0.09 | 2,170 | 2,031 | 0.00 | 0.09 | 24.20 |
| 95.21 | 0.09 | 2,191 | 2,031 | 0.00 | 0.09 | 24.43 |
| 95.30 | 3.74 | 2,373 | 2,031 | 0.00 | 3.74 | 30.10 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 25 years

Label: 24" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.09 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.09 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.09 | 0 | 508 | 0.00 | 0.09 | 0.09 |
| 93.10 | 0.09 | 51 | 508 | 0.00 | 0.09 | 0.65 |
| 93.20 | 0.09 | 114 | 1,016 | 0.00 | 0.09 | 1.36 |
| 93.30 | 0.09 | 216 | 1,016 | 0.00 | 0.09 | 2.49 |
| 93.40 | 0.09 | 317 | 1,016 | 0.00 | 0.09 | 3.61 |
| 93.50 | 0.09 | 419 | 1,016 | 0.00 | 0.09 | 4.74 |
| 93.60 | 0.09 | 520 | 1,016 | 0.00 | 0.09 | 5.87 |
| 93.70 | 0.09 | 622 | 1,016 | 0.00 | 0.09 | 7.00 |
| 93.80 | 0.09 | 723 | 1,016 | 0.00 | 0.09 | 8.13 |
| 93.90 | 0.09 | 825 | 1,016 | 0.00 | 0.09 | 9.26 |
| 94.00 | 0.09 | 926 | 1,016 | 0.00 | 0.09 | 10.38 |
| 94.10 | 0.09 | 1,028 | 1,016 | 0.00 | 0.09 | 11.51 |
| 94.20 | 0.09 | 1,130 | 1,016 | 0.00 | 0.09 | 12.64 |
| 94.30 | 0.09 | 1,231 | 1,016 | 0.00 | 0.09 | 13.77 |
| 94.40 | 0.09 | 1,333 | 1,016 | 0.00 | 0.09 | 14.90 |
| 94.50 | 0.09 | 1,434 | 1,016 | 0.00 | 0.09 | 16.03 |
| 94.60 | 0.09 | 1,536 | 1,016 | 0.00 | 0.09 | 17.15 |
| 94.70 | 0.09 | 1,637 | 1,016 | 0.00 | 0.09 | 18.28 |
| 94.80 | 0.09 | 1,739 | 1,016 | 0.00 | 0.09 | 19.41 |
| 94.90 | 0.09 | 1,840 | 1,016 | 0.00 | 0.09 | 20.54 |
| 95.00 | 0.09 | 1,942 | 1,016 | 0.00 | 0.09 | 21.67 |
| 95.10 | 0.09 | 2,044 | 1,016 | 0.00 | 0.09 | 22.80 |
| 95.20 | 0.09 | 2,170 | 2,031 | 0.00 | 0.09 | 24.20 |
| 95.21 | 0.09 | 2,191 | 2,031 | 0.00 | 0.09 | 24.43 |
| 95.30 | 3.74 | 2,373 | 2,031 | 0.00 | 3.74 | 30.10 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 100 years

Label: 24" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.09 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.09 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.09 | 0 | 508 | 0.00 | 0.09 | 0.09 |
| 93.10 | 0.09 | 51 | 508 | 0.00 | 0.09 | 0.65 |
| 93.20 | 0.09 | 114 | 1,016 | 0.00 | 0.09 | 1.36 |
| 93.30 | 0.09 | 216 | 1,016 | 0.00 | 0.09 | 2.49 |
| 93.40 | 0.09 | 317 | 1,016 | 0.00 | 0.09 | 3.61 |
| 93.50 | 0.09 | 419 | 1,016 | 0.00 | 0.09 | 4.74 |
| 93.60 | 0.09 | 520 | 1,016 | 0.00 | 0.09 | 5.87 |
| 93.70 | 0.09 | 622 | 1,016 | 0.00 | 0.09 | 7.00 |
| 93.80 | 0.09 | 723 | 1,016 | 0.00 | 0.09 | 8.13 |
| 93.90 | 0.09 | 825 | 1,016 | 0.00 | 0.09 | 9.26 |
| 94.00 | 0.09 | 926 | 1,016 | 0.00 | 0.09 | 10.38 |
| 94.10 | 0.09 | 1,028 | 1,016 | 0.00 | 0.09 | 11.51 |
| 94.20 | 0.09 | 1,130 | 1,016 | 0.00 | 0.09 | 12.64 |
| 94.30 | 0.09 | 1,231 | 1,016 | 0.00 | 0.09 | 13.77 |
| 94.40 | 0.09 | 1,333 | 1,016 | 0.00 | 0.09 | 14.90 |
| 94.50 | 0.09 | 1,434 | 1,016 | 0.00 | 0.09 | 16.03 |
| 94.60 | 0.09 | 1,536 | 1,016 | 0.00 | 0.09 | 17.15 |
| 94.70 | 0.09 | 1,637 | 1,016 | 0.00 | 0.09 | 18.28 |
| 94.80 | 0.09 | 1,739 | 1,016 | 0.00 | 0.09 | 19.41 |
| 94.90 | 0.09 | 1,840 | 1,016 | 0.00 | 0.09 | 20.54 |
| 95.00 | 0.09 | 1,942 | 1,016 | 0.00 | 0.09 | 21.67 |
| 95.10 | 0.09 | 2,044 | 1,016 | 0.00 | 0.09 | 22.80 |
| 95.20 | 0.09 | 2,170 | 2,031 | 0.00 | 0.09 | 24.20 |
| 95.21 | 0.09 | 2,191 | 2,031 | 0.00 | 0.09 | 24.43 |
| 95.30 | 3.74 | 2,373 | 2,031 | 0.00 | 3.74 | 30.10 |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 1 years

Label: 24" Depth Green Roof (IN)

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.09 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.09 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 0.94 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.09 ft ³ /s | Time to Peak (Flow, Outlet) | 11.250 hours |
| Peak Values | | | |
| Elevation (Water Surface, Peak) | 94.46 ft | | |
| Volume (Peak) | 1,398 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 3,814 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 3,817 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 3 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 10 years

Label: 24" Depth Green Roof (IN)

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.09 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.09 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 1.76 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 1.34 ft ³ /s | Time to Peak (Flow, Outlet) | 12.200 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 95.24 ft | | |
| Volume (Peak) | 2,253 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 7,332 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 6,928 ft ³ | | |
| Volume (Retained) | 391 ft ³ | | |
| Volume (Unrouted) | -12 ft ³ | | |
| Error (Mass Balance) | 0.2 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 25 years

Label: 24" Depth Green Roof (IN)

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.09 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.09 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 2.24 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 2.71 ft ³ /s | Time to Peak (Flow, Outlet) | 12.100 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 95.27 ft | | |
| Volume (Peak) | 2,322 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 9,388 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 8,686 ft ³ | | |
| Volume (Retained) | 690 ft ³ | | |
| Volume (Unrouted) | -12 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 100 years

Label: 24" Depth Green Roof (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.09 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.09 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 3.22 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 3.20 ft ³ /s | Time to Peak (Flow, Outlet) | 12.100 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 95.29 ft | | |
| Volume (Peak) | 2,346 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 13,610 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 12,417 ft ³ | | |
| Volume (Retained) | 1,181 ft ³ | | |
| Volume (Unrouted) | -12 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.100 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.150 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 4.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 4.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 4.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 4.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 4.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.300 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.750 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.800 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.850 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.900 | 0.04 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.950 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.000 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.050 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.350 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.400 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.450 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.500 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.550 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.600 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.650 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.700 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.750 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.800 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.100 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.200 | 0.06 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.250 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 10.300 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 10.350 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.400 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.450 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 10.550 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 10.600 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 10.650 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 10.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.750 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.800 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.850 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.900 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 10.950 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 11.000 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 11.050 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.100 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.150 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 11.200 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 11.250 | 0.10 | 0.01 | 0.19 | 0.00 | 0.09 | 9 | 93.02 |
| 11.300 | 0.10 | 0.03 | 0.21 | 0.00 | 0.09 | 11 | 93.02 |
| 11.350 | 0.11 | 0.06 | 0.24 | 0.00 | 0.09 | 13 | 93.03 |
| 11.400 | 0.11 | 0.10 | 0.28 | 0.00 | 0.09 | 17 | 93.03 |
| 11.450 | 0.12 | 0.15 | 0.33 | 0.00 | 0.09 | 22 | 93.04 |
| 11.500 | 0.12 | 0.21 | 0.39 | 0.00 | 0.09 | 27 | 93.05 |
| 11.550 | 0.14 | 0.30 | 0.48 | 0.00 | 0.09 | 35 | 93.07 |
| 11.600 | 0.17 | 0.42 | 0.60 | 0.00 | 0.09 | 46 | 93.09 |
| 11.650 | 0.20 | 0.61 | 0.79 | 0.00 | 0.09 | 61 | 93.12 |
| 11.700 | 0.25 | 0.89 | 1.07 | 0.00 | 0.09 | 81 | 93.16 |
| 11.750 | 0.30 | 1.26 | 1.44 | 0.00 | 0.09 | 122 | 93.21 |
| 11.800 | 0.35 | 1.73 | 1.91 | 0.00 | 0.09 | 164 | 93.25 |
| 11.850 | 0.40 | 2.31 | 2.49 | 0.00 | 0.09 | 216 | 93.30 |
| 11.900 | 0.45 | 2.98 | 3.16 | 0.00 | 0.09 | 276 | 93.36 |
| 11.950 | 0.60 | 3.85 | 4.03 | 0.00 | 0.09 | 355 | 93.44 |
| 12.000 | 0.83 | 5.10 | 5.28 | 0.00 | 0.09 | 467 | 93.55 |
| 12.050 | 0.92 | 6.67 | 6.85 | 0.00 | 0.09 | 609 | 93.69 |
| 12.100 | 0.94 | 8.35 | 8.53 | 0.00 | 0.09 | 760 | 93.84 |
| 12.150 | 0.83 | 9.95 | 10.13 | 0.00 | 0.09 | 903 | 93.98 |
| 12.200 | 0.61 | 11.20 | 11.38 | 0.00 | 0.09 | 1,016 | 94.09 |
| 12.250 | 0.50 | 12.13 | 12.31 | 0.00 | 0.09 | 1,099 | 94.17 |
| 12.300 | 0.42 | 12.86 | 13.04 | 0.00 | 0.09 | 1,166 | 94.24 |
| 12.350 | 0.37 | 13.48 | 13.66 | 0.00 | 0.09 | 1,221 | 94.29 |
| 12.400 | 0.32 | 13.98 | 14.16 | 0.00 | 0.09 | 1,267 | 94.33 |
| 12.450 | 0.27 | 14.39 | 14.57 | 0.00 | 0.09 | 1,303 | 94.37 |
| 12.500 | 0.21 | 14.69 | 14.87 | 0.00 | 0.09 | 1,330 | 94.40 |
| 12.550 | 0.18 | 14.90 | 15.08 | 0.00 | 0.09 | 1,350 | 94.42 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.15 | 15.05 | 15.23 | 0.00 | 0.09 | 1,363 | 94.43 |
| 12.650 | 0.13 | 15.15 | 15.33 | 0.00 | 0.09 | 1,372 | 94.44 |
| 12.700 | 0.12 | 15.23 | 15.41 | 0.00 | 0.09 | 1,379 | 94.45 |
| 12.750 | 0.12 | 15.29 | 15.47 | 0.00 | 0.09 | 1,384 | 94.45 |
| 12.800 | 0.11 | 15.35 | 15.53 | 0.00 | 0.09 | 1,389 | 94.46 |
| 12.850 | 0.11 | 15.39 | 15.57 | 0.00 | 0.09 | 1,393 | 94.46 |
| 12.900 | 0.10 | 15.42 | 15.60 | 0.00 | 0.09 | 1,396 | 94.46 |
| 12.950 | 0.10 | 15.44 | 15.62 | 0.00 | 0.09 | 1,397 | 94.46 |
| 13.000 | 0.09 | 15.45 | 15.63 | 0.00 | 0.09 | 1,398 | 94.46 |
| 13.050 | 0.09 | 15.45 | 15.63 | 0.00 | 0.09 | 1,398 | 94.46 |
| 13.100 | 0.08 | 15.44 | 15.62 | 0.00 | 0.09 | 1,398 | 94.46 |
| 13.150 | 0.08 | 15.43 | 15.61 | 0.00 | 0.09 | 1,396 | 94.46 |
| 13.200 | 0.08 | 15.41 | 15.59 | 0.00 | 0.09 | 1,395 | 94.46 |
| 13.250 | 0.08 | 15.39 | 15.57 | 0.00 | 0.09 | 1,393 | 94.46 |
| 13.300 | 0.08 | 15.36 | 15.54 | 0.00 | 0.09 | 1,391 | 94.46 |
| 13.350 | 0.08 | 15.34 | 15.52 | 0.00 | 0.09 | 1,389 | 94.46 |
| 13.400 | 0.07 | 15.31 | 15.49 | 0.00 | 0.09 | 1,386 | 94.45 |
| 13.450 | 0.07 | 15.28 | 15.46 | 0.00 | 0.09 | 1,383 | 94.45 |
| 13.500 | 0.07 | 15.24 | 15.42 | 0.00 | 0.09 | 1,380 | 94.45 |
| 13.550 | 0.07 | 15.21 | 15.39 | 0.00 | 0.09 | 1,377 | 94.44 |
| 13.600 | 0.07 | 15.17 | 15.35 | 0.00 | 0.09 | 1,373 | 94.44 |
| 13.650 | 0.07 | 15.13 | 15.31 | 0.00 | 0.09 | 1,369 | 94.44 |
| 13.700 | 0.07 | 15.08 | 15.26 | 0.00 | 0.09 | 1,365 | 94.43 |
| 13.750 | 0.07 | 15.03 | 15.21 | 0.00 | 0.09 | 1,361 | 94.43 |
| 13.800 | 0.06 | 14.98 | 15.16 | 0.00 | 0.09 | 1,356 | 94.42 |
| 13.850 | 0.06 | 14.93 | 15.11 | 0.00 | 0.09 | 1,352 | 94.42 |
| 13.900 | 0.06 | 14.87 | 15.05 | 0.00 | 0.09 | 1,347 | 94.41 |
| 13.950 | 0.06 | 14.81 | 14.99 | 0.00 | 0.09 | 1,341 | 94.41 |
| 14.000 | 0.06 | 14.75 | 14.93 | 0.00 | 0.09 | 1,336 | 94.40 |
| 14.050 | 0.06 | 14.69 | 14.87 | 0.00 | 0.09 | 1,330 | 94.40 |
| 14.100 | 0.06 | 14.62 | 14.80 | 0.00 | 0.09 | 1,324 | 94.39 |
| 14.150 | 0.06 | 14.55 | 14.73 | 0.00 | 0.09 | 1,318 | 94.39 |
| 14.200 | 0.05 | 14.48 | 14.66 | 0.00 | 0.09 | 1,312 | 94.38 |
| 14.250 | 0.05 | 14.41 | 14.59 | 0.00 | 0.09 | 1,305 | 94.37 |
| 14.300 | 0.05 | 14.34 | 14.52 | 0.00 | 0.09 | 1,299 | 94.37 |
| 14.350 | 0.05 | 14.26 | 14.44 | 0.00 | 0.09 | 1,292 | 94.36 |
| 14.400 | 0.05 | 14.19 | 14.37 | 0.00 | 0.09 | 1,285 | 94.35 |
| 14.450 | 0.05 | 14.11 | 14.29 | 0.00 | 0.09 | 1,278 | 94.35 |
| 14.500 | 0.05 | 14.04 | 14.22 | 0.00 | 0.09 | 1,271 | 94.34 |
| 14.550 | 0.05 | 13.96 | 14.14 | 0.00 | 0.09 | 1,264 | 94.33 |
| 14.600 | 0.05 | 13.88 | 14.06 | 0.00 | 0.09 | 1,257 | 94.33 |
| 14.650 | 0.05 | 13.79 | 13.97 | 0.00 | 0.09 | 1,250 | 94.32 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.05 | 13.71 | 13.89 | 0.00 | 0.09 | 1,242 | 94.31 |
| 14.750 | 0.05 | 13.63 | 13.81 | 0.00 | 0.09 | 1,234 | 94.30 |
| 14.800 | 0.05 | 13.54 | 13.72 | 0.00 | 0.09 | 1,227 | 94.30 |
| 14.850 | 0.05 | 13.45 | 13.63 | 0.00 | 0.09 | 1,219 | 94.29 |
| 14.900 | 0.05 | 13.36 | 13.54 | 0.00 | 0.09 | 1,211 | 94.28 |
| 14.950 | 0.04 | 13.28 | 13.46 | 0.00 | 0.09 | 1,203 | 94.27 |
| 15.000 | 0.04 | 13.18 | 13.36 | 0.00 | 0.09 | 1,195 | 94.26 |
| 15.050 | 0.04 | 13.09 | 13.27 | 0.00 | 0.09 | 1,186 | 94.26 |
| 15.100 | 0.04 | 13.00 | 13.18 | 0.00 | 0.09 | 1,178 | 94.25 |
| 15.150 | 0.04 | 12.90 | 13.08 | 0.00 | 0.09 | 1,169 | 94.24 |
| 15.200 | 0.04 | 12.81 | 12.99 | 0.00 | 0.09 | 1,161 | 94.23 |
| 15.250 | 0.04 | 12.71 | 12.89 | 0.00 | 0.09 | 1,152 | 94.22 |
| 15.300 | 0.04 | 12.61 | 12.79 | 0.00 | 0.09 | 1,143 | 94.21 |
| 15.350 | 0.04 | 12.51 | 12.69 | 0.00 | 0.09 | 1,134 | 94.20 |
| 15.400 | 0.04 | 12.41 | 12.59 | 0.00 | 0.09 | 1,125 | 94.20 |
| 15.450 | 0.04 | 12.31 | 12.49 | 0.00 | 0.09 | 1,116 | 94.19 |
| 15.500 | 0.04 | 12.20 | 12.38 | 0.00 | 0.09 | 1,106 | 94.18 |
| 15.550 | 0.04 | 12.10 | 12.28 | 0.00 | 0.09 | 1,097 | 94.17 |
| 15.600 | 0.04 | 11.99 | 12.17 | 0.00 | 0.09 | 1,087 | 94.16 |
| 15.650 | 0.04 | 11.88 | 12.06 | 0.00 | 0.09 | 1,077 | 94.15 |
| 15.700 | 0.03 | 11.77 | 11.95 | 0.00 | 0.09 | 1,068 | 94.14 |
| 15.750 | 0.03 | 11.66 | 11.84 | 0.00 | 0.09 | 1,058 | 94.13 |
| 15.800 | 0.03 | 11.55 | 11.73 | 0.00 | 0.09 | 1,047 | 94.12 |
| 15.850 | 0.03 | 11.43 | 11.61 | 0.00 | 0.09 | 1,037 | 94.11 |
| 15.900 | 0.03 | 11.32 | 11.50 | 0.00 | 0.09 | 1,027 | 94.10 |
| 15.950 | 0.03 | 11.20 | 11.38 | 0.00 | 0.09 | 1,016 | 94.09 |
| 16.000 | 0.03 | 11.09 | 11.27 | 0.00 | 0.09 | 1,006 | 94.08 |
| 16.050 | 0.03 | 10.97 | 11.15 | 0.00 | 0.09 | 995 | 94.07 |
| 16.100 | 0.03 | 10.85 | 11.03 | 0.00 | 0.09 | 984 | 94.06 |
| 16.150 | 0.03 | 10.73 | 10.91 | 0.00 | 0.09 | 974 | 94.05 |
| 16.200 | 0.03 | 10.61 | 10.79 | 0.00 | 0.09 | 963 | 94.04 |
| 16.250 | 0.03 | 10.48 | 10.66 | 0.00 | 0.09 | 952 | 94.02 |
| 16.300 | 0.03 | 10.36 | 10.54 | 0.00 | 0.09 | 941 | 94.01 |
| 16.350 | 0.03 | 10.24 | 10.42 | 0.00 | 0.09 | 930 | 94.00 |
| 16.400 | 0.03 | 10.12 | 10.30 | 0.00 | 0.09 | 918 | 93.99 |
| 16.450 | 0.03 | 9.99 | 10.17 | 0.00 | 0.09 | 907 | 93.98 |
| 16.500 | 0.03 | 9.87 | 10.05 | 0.00 | 0.09 | 896 | 93.97 |
| 16.550 | 0.03 | 9.74 | 9.92 | 0.00 | 0.09 | 885 | 93.96 |
| 16.600 | 0.03 | 9.62 | 9.80 | 0.00 | 0.09 | 873 | 93.95 |
| 16.650 | 0.03 | 9.49 | 9.67 | 0.00 | 0.09 | 862 | 93.94 |
| 16.700 | 0.03 | 9.36 | 9.54 | 0.00 | 0.09 | 851 | 93.93 |
| 16.750 | 0.03 | 9.23 | 9.41 | 0.00 | 0.09 | 839 | 93.91 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.03 | 9.11 | 9.29 | 0.00 | 0.09 | 828 | 93.90 |
| 16.850 | 0.03 | 8.98 | 9.16 | 0.00 | 0.09 | 816 | 93.89 |
| 16.900 | 0.03 | 8.85 | 9.03 | 0.00 | 0.09 | 804 | 93.88 |
| 16.950 | 0.02 | 8.72 | 8.90 | 0.00 | 0.09 | 793 | 93.87 |
| 17.000 | 0.02 | 8.59 | 8.77 | 0.00 | 0.09 | 781 | 93.86 |
| 17.050 | 0.02 | 8.46 | 8.64 | 0.00 | 0.09 | 769 | 93.85 |
| 17.100 | 0.02 | 8.32 | 8.50 | 0.00 | 0.09 | 757 | 93.83 |
| 17.150 | 0.02 | 8.19 | 8.37 | 0.00 | 0.09 | 745 | 93.82 |
| 17.200 | 0.02 | 8.06 | 8.24 | 0.00 | 0.09 | 733 | 93.81 |
| 17.250 | 0.02 | 7.93 | 8.11 | 0.00 | 0.09 | 721 | 93.80 |
| 17.300 | 0.02 | 7.79 | 7.97 | 0.00 | 0.09 | 709 | 93.79 |
| 17.350 | 0.02 | 7.66 | 7.84 | 0.00 | 0.09 | 697 | 93.77 |
| 17.400 | 0.02 | 7.52 | 7.70 | 0.00 | 0.09 | 685 | 93.76 |
| 17.450 | 0.02 | 7.39 | 7.57 | 0.00 | 0.09 | 673 | 93.75 |
| 17.500 | 0.02 | 7.25 | 7.43 | 0.00 | 0.09 | 661 | 93.74 |
| 17.550 | 0.02 | 7.11 | 7.29 | 0.00 | 0.09 | 648 | 93.73 |
| 17.600 | 0.02 | 6.98 | 7.16 | 0.00 | 0.09 | 636 | 93.71 |
| 17.650 | 0.02 | 6.84 | 7.02 | 0.00 | 0.09 | 624 | 93.70 |
| 17.700 | 0.02 | 6.70 | 6.88 | 0.00 | 0.09 | 611 | 93.69 |
| 17.750 | 0.02 | 6.56 | 6.74 | 0.00 | 0.09 | 599 | 93.68 |
| 17.800 | 0.02 | 6.42 | 6.60 | 0.00 | 0.09 | 586 | 93.66 |
| 17.850 | 0.02 | 6.28 | 6.46 | 0.00 | 0.09 | 573 | 93.65 |
| 17.900 | 0.02 | 6.14 | 6.32 | 0.00 | 0.09 | 561 | 93.64 |
| 17.950 | 0.02 | 6.00 | 6.18 | 0.00 | 0.09 | 548 | 93.63 |
| 18.000 | 0.02 | 5.86 | 6.04 | 0.00 | 0.09 | 535 | 93.61 |
| 18.050 | 0.02 | 5.71 | 5.89 | 0.00 | 0.09 | 522 | 93.60 |
| 18.100 | 0.02 | 5.57 | 5.75 | 0.00 | 0.09 | 510 | 93.59 |
| 18.150 | 0.02 | 5.43 | 5.61 | 0.00 | 0.09 | 497 | 93.58 |
| 18.200 | 0.02 | 5.28 | 5.46 | 0.00 | 0.09 | 484 | 93.56 |
| 18.250 | 0.02 | 5.14 | 5.32 | 0.00 | 0.09 | 471 | 93.55 |
| 18.300 | 0.02 | 5.00 | 5.18 | 0.00 | 0.09 | 458 | 93.54 |
| 18.350 | 0.02 | 4.85 | 5.03 | 0.00 | 0.09 | 445 | 93.53 |
| 18.400 | 0.02 | 4.71 | 4.89 | 0.00 | 0.09 | 432 | 93.51 |
| 18.450 | 0.02 | 4.56 | 4.74 | 0.00 | 0.09 | 419 | 93.50 |
| 18.500 | 0.02 | 4.42 | 4.60 | 0.00 | 0.09 | 406 | 93.49 |
| 18.550 | 0.02 | 4.28 | 4.46 | 0.00 | 0.09 | 393 | 93.47 |
| 18.600 | 0.02 | 4.13 | 4.31 | 0.00 | 0.09 | 380 | 93.46 |
| 18.650 | 0.02 | 3.99 | 4.17 | 0.00 | 0.09 | 367 | 93.45 |
| 18.700 | 0.02 | 3.84 | 4.02 | 0.00 | 0.09 | 354 | 93.44 |
| 18.750 | 0.02 | 3.70 | 3.88 | 0.00 | 0.09 | 341 | 93.42 |
| 18.800 | 0.02 | 3.55 | 3.73 | 0.00 | 0.09 | 328 | 93.41 |
| 18.850 | 0.02 | 3.40 | 3.58 | 0.00 | 0.09 | 314 | 93.40 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.02 | 3.26 | 3.44 | 0.00 | 0.09 | 301 | 93.38 |
| 18.950 | 0.02 | 3.11 | 3.29 | 0.00 | 0.09 | 288 | 93.37 |
| 19.000 | 0.02 | 2.97 | 3.15 | 0.00 | 0.09 | 275 | 93.36 |
| 19.050 | 0.02 | 2.82 | 3.00 | 0.00 | 0.09 | 262 | 93.35 |
| 19.100 | 0.02 | 2.67 | 2.85 | 0.00 | 0.09 | 249 | 93.33 |
| 19.150 | 0.02 | 2.53 | 2.71 | 0.00 | 0.09 | 235 | 93.32 |
| 19.200 | 0.02 | 2.38 | 2.56 | 0.00 | 0.09 | 222 | 93.31 |
| 19.250 | 0.02 | 2.23 | 2.41 | 0.00 | 0.09 | 209 | 93.29 |
| 19.300 | 0.02 | 2.08 | 2.26 | 0.00 | 0.09 | 196 | 93.28 |
| 19.350 | 0.02 | 1.94 | 2.12 | 0.00 | 0.09 | 182 | 93.27 |
| 19.400 | 0.02 | 1.79 | 1.97 | 0.00 | 0.09 | 169 | 93.25 |
| 19.450 | 0.02 | 1.64 | 1.82 | 0.00 | 0.09 | 156 | 93.24 |
| 19.500 | 0.02 | 1.49 | 1.67 | 0.00 | 0.09 | 143 | 93.23 |
| 19.550 | 0.02 | 1.35 | 1.53 | 0.00 | 0.09 | 129 | 93.21 |
| 19.600 | 0.02 | 1.20 | 1.38 | 0.00 | 0.09 | 116 | 93.20 |
| 19.650 | 0.02 | 1.05 | 1.23 | 0.00 | 0.09 | 95 | 93.18 |
| 19.700 | 0.02 | 0.90 | 1.08 | 0.00 | 0.09 | 81 | 93.16 |
| 19.750 | 0.02 | 0.75 | 0.93 | 0.00 | 0.09 | 71 | 93.14 |
| 19.800 | 0.02 | 0.60 | 0.78 | 0.00 | 0.09 | 60 | 93.12 |
| 19.850 | 0.02 | 0.45 | 0.63 | 0.00 | 0.09 | 49 | 93.10 |
| 19.900 | 0.02 | 0.30 | 0.48 | 0.00 | 0.09 | 35 | 93.07 |
| 19.950 | 0.02 | 0.15 | 0.33 | 0.00 | 0.09 | 22 | 93.04 |
| 20.000 | 0.02 | 0.00 | 0.18 | 0.00 | 0.09 | 8 | 93.02 |
| 20.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 20.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 22.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 22.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 24.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.450 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.650 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 4.700 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 4.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 4.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 4.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 4.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 4.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.300 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.350 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.400 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.450 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.500 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.550 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.600 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.650 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.700 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 5.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 5.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 5.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 5.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 5.950 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.000 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.050 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.100 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.150 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.200 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.250 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.450 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 6.500 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 6.550 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 6.600 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 6.650 | 0.04 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 6.700 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 6.750 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 6.800 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 6.850 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 6.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.350 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 7.400 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 7.450 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 7.500 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 7.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 7.600 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 7.650 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 7.700 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 7.750 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 7.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 7.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 7.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 7.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.100 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 8.200 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 8.250 | 0.06 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 8.300 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 8.350 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 8.450 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 8.500 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 8.550 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 8.600 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 8.650 | 0.07 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 8.700 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 8.750 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 8.800 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 8.850 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 8.900 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 8.950 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.000 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 9.050 | 0.08 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 9.100 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 9.150 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 9.200 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 9.250 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 9.300 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 9.350 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 9.400 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 9.450 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 9.500 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 9.550 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 9.600 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 9.650 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 9.700 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 8 | 93.02 |
| 9.750 | 0.09 | 0.01 | 0.19 | 0.00 | 0.09 | 9 | 93.02 |
| 9.800 | 0.09 | 0.01 | 0.19 | 0.00 | 0.09 | 9 | 93.02 |
| 9.850 | 0.10 | 0.02 | 0.20 | 0.00 | 0.09 | 10 | 93.02 |
| 9.900 | 0.10 | 0.04 | 0.22 | 0.00 | 0.09 | 11 | 93.02 |
| 9.950 | 0.10 | 0.05 | 0.23 | 0.00 | 0.09 | 13 | 93.02 |
| 10.000 | 0.10 | 0.07 | 0.25 | 0.00 | 0.09 | 14 | 93.03 |
| 10.050 | 0.10 | 0.09 | 0.27 | 0.00 | 0.09 | 16 | 93.03 |
| 10.100 | 0.10 | 0.11 | 0.29 | 0.00 | 0.09 | 18 | 93.04 |
| 10.150 | 0.10 | 0.14 | 0.32 | 0.00 | 0.09 | 21 | 93.04 |
| 10.200 | 0.11 | 0.17 | 0.35 | 0.00 | 0.09 | 24 | 93.05 |
| 10.250 | 0.11 | 0.21 | 0.39 | 0.00 | 0.09 | 27 | 93.05 |
| 10.300 | 0.11 | 0.25 | 0.43 | 0.00 | 0.09 | 31 | 93.06 |
| 10.350 | 0.12 | 0.30 | 0.48 | 0.00 | 0.09 | 35 | 93.07 |
| 10.400 | 0.12 | 0.35 | 0.53 | 0.00 | 0.09 | 40 | 93.08 |
| 10.450 | 0.12 | 0.41 | 0.59 | 0.00 | 0.09 | 45 | 93.09 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.12 | 0.47 | 0.65 | 0.00 | 0.09 | 51 | 93.10 |
| 10.550 | 0.13 | 0.54 | 0.72 | 0.00 | 0.09 | 56 | 93.11 |
| 10.600 | 0.13 | 0.62 | 0.80 | 0.00 | 0.09 | 61 | 93.12 |
| 10.650 | 0.13 | 0.70 | 0.88 | 0.00 | 0.09 | 67 | 93.13 |
| 10.700 | 0.13 | 0.78 | 0.96 | 0.00 | 0.09 | 73 | 93.14 |
| 10.750 | 0.14 | 0.87 | 1.05 | 0.00 | 0.09 | 79 | 93.16 |
| 10.800 | 0.14 | 0.96 | 1.14 | 0.00 | 0.09 | 86 | 93.17 |
| 10.850 | 0.14 | 1.06 | 1.24 | 0.00 | 0.09 | 97 | 93.18 |
| 10.900 | 0.14 | 1.17 | 1.35 | 0.00 | 0.09 | 112 | 93.20 |
| 10.950 | 0.15 | 1.28 | 1.46 | 0.00 | 0.09 | 123 | 93.21 |
| 11.000 | 0.15 | 1.39 | 1.57 | 0.00 | 0.09 | 133 | 93.22 |
| 11.050 | 0.15 | 1.51 | 1.69 | 0.00 | 0.09 | 144 | 93.23 |
| 11.100 | 0.16 | 1.65 | 1.83 | 0.00 | 0.09 | 156 | 93.24 |
| 11.150 | 0.17 | 1.79 | 1.97 | 0.00 | 0.09 | 169 | 93.25 |
| 11.200 | 0.18 | 1.96 | 2.14 | 0.00 | 0.09 | 184 | 93.27 |
| 11.250 | 0.19 | 2.14 | 2.32 | 0.00 | 0.09 | 201 | 93.29 |
| 11.300 | 0.20 | 2.34 | 2.52 | 0.00 | 0.09 | 219 | 93.30 |
| 11.350 | 0.21 | 2.56 | 2.74 | 0.00 | 0.09 | 239 | 93.32 |
| 11.400 | 0.22 | 2.80 | 2.98 | 0.00 | 0.09 | 260 | 93.34 |
| 11.450 | 0.22 | 3.06 | 3.24 | 0.00 | 0.09 | 284 | 93.37 |
| 11.500 | 0.24 | 3.35 | 3.53 | 0.00 | 0.09 | 309 | 93.39 |
| 11.550 | 0.27 | 3.67 | 3.85 | 0.00 | 0.09 | 338 | 93.42 |
| 11.600 | 0.32 | 4.07 | 4.25 | 0.00 | 0.09 | 375 | 93.46 |
| 11.650 | 0.39 | 4.59 | 4.77 | 0.00 | 0.09 | 422 | 93.50 |
| 11.700 | 0.48 | 5.28 | 5.46 | 0.00 | 0.09 | 483 | 93.56 |
| 11.750 | 0.57 | 6.15 | 6.33 | 0.00 | 0.09 | 561 | 93.64 |
| 11.800 | 0.67 | 7.20 | 7.38 | 0.00 | 0.09 | 656 | 93.73 |
| 11.850 | 0.75 | 8.44 | 8.62 | 0.00 | 0.09 | 767 | 93.84 |
| 11.900 | 0.86 | 9.87 | 10.05 | 0.00 | 0.09 | 896 | 93.97 |
| 11.950 | 1.12 | 11.67 | 11.85 | 0.00 | 0.09 | 1,058 | 94.13 |
| 12.000 | 1.56 | 14.17 | 14.35 | 0.00 | 0.09 | 1,283 | 94.35 |
| 12.050 | 1.72 | 17.27 | 17.45 | 0.00 | 0.09 | 1,562 | 94.63 |
| 12.100 | 1.76 | 20.57 | 20.75 | 0.00 | 0.09 | 1,859 | 94.92 |
| 12.150 | 1.55 | 23.70 | 23.88 | 0.00 | 0.09 | 2,124 | 95.18 |
| 12.200 | 1.13 | 23.69 | 26.38 | 0.00 | 1.34 | 2,253 | 95.24 |
| 12.250 | 0.92 | 23.87 | 25.75 | 0.00 | 0.94 | 2,233 | 95.23 |
| 12.300 | 0.79 | 23.92 | 25.59 | 0.00 | 0.83 | 2,228 | 95.23 |
| 12.350 | 0.69 | 23.97 | 25.40 | 0.00 | 0.71 | 2,222 | 95.23 |
| 12.400 | 0.59 | 24.02 | 25.25 | 0.00 | 0.62 | 2,217 | 95.22 |
| 12.450 | 0.50 | 24.06 | 25.10 | 0.00 | 0.52 | 2,212 | 95.22 |
| 12.500 | 0.40 | 24.10 | 24.96 | 0.00 | 0.43 | 2,207 | 95.22 |
| 12.550 | 0.33 | 24.13 | 24.83 | 0.00 | 0.35 | 2,203 | 95.22 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.27 | 24.16 | 24.74 | 0.00 | 0.29 | 2,201 | 95.21 |
| 12.650 | 0.25 | 24.18 | 24.68 | 0.00 | 0.25 | 2,199 | 95.21 |
| 12.700 | 0.23 | 24.18 | 24.66 | 0.00 | 0.24 | 2,198 | 95.21 |
| 12.750 | 0.22 | 24.19 | 24.64 | 0.00 | 0.22 | 2,197 | 95.21 |
| 12.800 | 0.21 | 24.19 | 24.62 | 0.00 | 0.21 | 2,197 | 95.21 |
| 12.850 | 0.20 | 24.20 | 24.61 | 0.00 | 0.20 | 2,196 | 95.21 |
| 12.900 | 0.19 | 24.20 | 24.59 | 0.00 | 0.19 | 2,196 | 95.21 |
| 12.950 | 0.18 | 24.21 | 24.57 | 0.00 | 0.18 | 2,195 | 95.21 |
| 13.000 | 0.17 | 24.21 | 24.56 | 0.00 | 0.17 | 2,195 | 95.21 |
| 13.050 | 0.16 | 24.22 | 24.55 | 0.00 | 0.17 | 2,194 | 95.21 |
| 13.100 | 0.16 | 24.22 | 24.54 | 0.00 | 0.16 | 2,194 | 95.21 |
| 13.150 | 0.15 | 24.22 | 24.53 | 0.00 | 0.15 | 2,194 | 95.21 |
| 13.200 | 0.15 | 24.22 | 24.52 | 0.00 | 0.15 | 2,194 | 95.21 |
| 13.250 | 0.15 | 24.22 | 24.52 | 0.00 | 0.15 | 2,193 | 95.21 |
| 13.300 | 0.14 | 24.22 | 24.51 | 0.00 | 0.15 | 2,193 | 95.21 |
| 13.350 | 0.14 | 24.23 | 24.51 | 0.00 | 0.14 | 2,193 | 95.21 |
| 13.400 | 0.14 | 24.23 | 24.51 | 0.00 | 0.14 | 2,193 | 95.21 |
| 13.450 | 0.14 | 24.23 | 24.50 | 0.00 | 0.14 | 2,193 | 95.21 |
| 13.500 | 0.13 | 24.23 | 24.50 | 0.00 | 0.13 | 2,193 | 95.21 |
| 13.550 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,193 | 95.21 |
| 13.600 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 13.650 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 13.700 | 0.12 | 24.23 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 13.750 | 0.12 | 24.23 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 13.800 | 0.12 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |
| 13.850 | 0.12 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |
| 13.900 | 0.11 | 24.24 | 24.47 | 0.00 | 0.11 | 2,192 | 95.21 |
| 13.950 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,192 | 95.21 |
| 14.000 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,191 | 95.21 |
| 14.050 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,191 | 95.21 |
| 14.100 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.150 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.200 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.250 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.300 | 0.10 | 24.24 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.350 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.400 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.450 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 14.500 | 0.09 | 24.25 | 24.44 | 0.00 | 0.09 | 2,191 | 95.21 |
| 14.550 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 14.600 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 14.650 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,190 | 95.21 |
| 14.750 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,190 | 95.21 |
| 14.800 | 0.09 | 24.24 | 24.42 | 0.00 | 0.09 | 2,190 | 95.21 |
| 14.850 | 0.09 | 24.23 | 24.41 | 0.00 | 0.09 | 2,189 | 95.21 |
| 14.900 | 0.08 | 24.22 | 24.40 | 0.00 | 0.09 | 2,188 | 95.21 |
| 14.950 | 0.08 | 24.21 | 24.39 | 0.00 | 0.09 | 2,187 | 95.21 |
| 15.000 | 0.08 | 24.20 | 24.38 | 0.00 | 0.09 | 2,186 | 95.21 |
| 15.050 | 0.08 | 24.18 | 24.36 | 0.00 | 0.09 | 2,184 | 95.21 |
| 15.100 | 0.08 | 24.16 | 24.34 | 0.00 | 0.09 | 2,182 | 95.21 |
| 15.150 | 0.08 | 24.14 | 24.32 | 0.00 | 0.09 | 2,180 | 95.21 |
| 15.200 | 0.08 | 24.11 | 24.29 | 0.00 | 0.09 | 2,178 | 95.20 |
| 15.250 | 0.08 | 24.08 | 24.26 | 0.00 | 0.09 | 2,176 | 95.20 |
| 15.300 | 0.07 | 24.06 | 24.24 | 0.00 | 0.09 | 2,173 | 95.20 |
| 15.350 | 0.07 | 24.02 | 24.20 | 0.00 | 0.09 | 2,170 | 95.20 |
| 15.400 | 0.07 | 23.99 | 24.17 | 0.00 | 0.09 | 2,165 | 95.20 |
| 15.450 | 0.07 | 23.95 | 24.13 | 0.00 | 0.09 | 2,160 | 95.19 |
| 15.500 | 0.07 | 23.91 | 24.09 | 0.00 | 0.09 | 2,154 | 95.19 |
| 15.550 | 0.07 | 23.87 | 24.05 | 0.00 | 0.09 | 2,148 | 95.19 |
| 15.600 | 0.07 | 23.83 | 24.01 | 0.00 | 0.09 | 2,142 | 95.19 |
| 15.650 | 0.07 | 23.78 | 23.96 | 0.00 | 0.09 | 2,135 | 95.18 |
| 15.700 | 0.06 | 23.73 | 23.91 | 0.00 | 0.09 | 2,128 | 95.18 |
| 15.750 | 0.06 | 23.68 | 23.86 | 0.00 | 0.09 | 2,122 | 95.18 |
| 15.800 | 0.06 | 23.62 | 23.80 | 0.00 | 0.09 | 2,116 | 95.17 |
| 15.850 | 0.06 | 23.57 | 23.75 | 0.00 | 0.09 | 2,112 | 95.17 |
| 15.900 | 0.06 | 23.51 | 23.69 | 0.00 | 0.09 | 2,108 | 95.16 |
| 15.950 | 0.06 | 23.45 | 23.63 | 0.00 | 0.09 | 2,104 | 95.16 |
| 16.000 | 0.06 | 23.38 | 23.56 | 0.00 | 0.09 | 2,099 | 95.15 |
| 16.050 | 0.06 | 23.32 | 23.50 | 0.00 | 0.09 | 2,094 | 95.15 |
| 16.100 | 0.06 | 23.25 | 23.43 | 0.00 | 0.09 | 2,089 | 95.14 |
| 16.150 | 0.05 | 23.18 | 23.36 | 0.00 | 0.09 | 2,084 | 95.14 |
| 16.200 | 0.05 | 23.11 | 23.29 | 0.00 | 0.09 | 2,079 | 95.13 |
| 16.250 | 0.05 | 23.04 | 23.22 | 0.00 | 0.09 | 2,074 | 95.13 |
| 16.300 | 0.05 | 22.96 | 23.14 | 0.00 | 0.09 | 2,069 | 95.12 |
| 16.350 | 0.05 | 22.89 | 23.07 | 0.00 | 0.09 | 2,063 | 95.12 |
| 16.400 | 0.05 | 22.81 | 22.99 | 0.00 | 0.09 | 2,058 | 95.11 |
| 16.450 | 0.05 | 22.74 | 22.92 | 0.00 | 0.09 | 2,052 | 95.11 |
| 16.500 | 0.05 | 22.66 | 22.84 | 0.00 | 0.09 | 2,047 | 95.10 |
| 16.550 | 0.05 | 22.58 | 22.76 | 0.00 | 0.09 | 2,040 | 95.10 |
| 16.600 | 0.05 | 22.50 | 22.68 | 0.00 | 0.09 | 2,033 | 95.09 |
| 16.650 | 0.05 | 22.42 | 22.60 | 0.00 | 0.09 | 2,026 | 95.08 |
| 16.700 | 0.05 | 22.34 | 22.52 | 0.00 | 0.09 | 2,019 | 95.08 |
| 16.750 | 0.05 | 22.26 | 22.44 | 0.00 | 0.09 | 2,011 | 95.07 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.05 | 22.17 | 22.35 | 0.00 | 0.09 | 2,004 | 95.06 |
| 16.850 | 0.05 | 22.09 | 22.27 | 0.00 | 0.09 | 1,996 | 95.05 |
| 16.900 | 0.05 | 22.00 | 22.18 | 0.00 | 0.09 | 1,988 | 95.05 |
| 16.950 | 0.05 | 21.91 | 22.09 | 0.00 | 0.09 | 1,980 | 95.04 |
| 17.000 | 0.05 | 21.83 | 22.01 | 0.00 | 0.09 | 1,972 | 95.03 |
| 17.050 | 0.05 | 21.74 | 21.92 | 0.00 | 0.09 | 1,964 | 95.02 |
| 17.100 | 0.04 | 21.65 | 21.83 | 0.00 | 0.09 | 1,956 | 95.01 |
| 17.150 | 0.04 | 21.56 | 21.74 | 0.00 | 0.09 | 1,948 | 95.01 |
| 17.200 | 0.04 | 21.46 | 21.64 | 0.00 | 0.09 | 1,940 | 95.00 |
| 17.250 | 0.04 | 21.37 | 21.55 | 0.00 | 0.09 | 1,931 | 94.99 |
| 17.300 | 0.04 | 21.27 | 21.45 | 0.00 | 0.09 | 1,923 | 94.98 |
| 17.350 | 0.04 | 21.18 | 21.36 | 0.00 | 0.09 | 1,914 | 94.97 |
| 17.400 | 0.04 | 21.08 | 21.26 | 0.00 | 0.09 | 1,906 | 94.96 |
| 17.450 | 0.04 | 20.98 | 21.16 | 0.00 | 0.09 | 1,897 | 94.96 |
| 17.500 | 0.04 | 20.89 | 21.07 | 0.00 | 0.09 | 1,888 | 94.95 |
| 17.550 | 0.04 | 20.79 | 20.97 | 0.00 | 0.09 | 1,879 | 94.94 |
| 17.600 | 0.04 | 20.69 | 20.87 | 0.00 | 0.09 | 1,870 | 94.93 |
| 17.650 | 0.04 | 20.58 | 20.76 | 0.00 | 0.09 | 1,861 | 94.92 |
| 17.700 | 0.04 | 20.48 | 20.66 | 0.00 | 0.09 | 1,851 | 94.91 |
| 17.750 | 0.04 | 20.38 | 20.56 | 0.00 | 0.09 | 1,842 | 94.90 |
| 17.800 | 0.04 | 20.27 | 20.45 | 0.00 | 0.09 | 1,832 | 94.89 |
| 17.850 | 0.04 | 20.16 | 20.34 | 0.00 | 0.09 | 1,823 | 94.88 |
| 17.900 | 0.04 | 20.06 | 20.24 | 0.00 | 0.09 | 1,813 | 94.87 |
| 17.950 | 0.04 | 19.95 | 20.13 | 0.00 | 0.09 | 1,803 | 94.86 |
| 18.000 | 0.03 | 19.84 | 20.02 | 0.00 | 0.09 | 1,794 | 94.85 |
| 18.050 | 0.03 | 19.73 | 19.91 | 0.00 | 0.09 | 1,784 | 94.84 |
| 18.100 | 0.03 | 19.62 | 19.80 | 0.00 | 0.09 | 1,774 | 94.83 |
| 18.150 | 0.03 | 19.51 | 19.69 | 0.00 | 0.09 | 1,764 | 94.82 |
| 18.200 | 0.03 | 19.39 | 19.57 | 0.00 | 0.09 | 1,753 | 94.81 |
| 18.250 | 0.03 | 19.28 | 19.46 | 0.00 | 0.09 | 1,743 | 94.80 |
| 18.300 | 0.03 | 19.17 | 19.35 | 0.00 | 0.09 | 1,733 | 94.79 |
| 18.350 | 0.03 | 19.05 | 19.23 | 0.00 | 0.09 | 1,723 | 94.78 |
| 18.400 | 0.03 | 18.94 | 19.12 | 0.00 | 0.09 | 1,713 | 94.77 |
| 18.450 | 0.03 | 18.83 | 19.01 | 0.00 | 0.09 | 1,702 | 94.76 |
| 18.500 | 0.03 | 18.71 | 18.89 | 0.00 | 0.09 | 1,692 | 94.75 |
| 18.550 | 0.03 | 18.60 | 18.78 | 0.00 | 0.09 | 1,682 | 94.74 |
| 18.600 | 0.03 | 18.48 | 18.66 | 0.00 | 0.09 | 1,672 | 94.73 |
| 18.650 | 0.03 | 18.37 | 18.55 | 0.00 | 0.09 | 1,661 | 94.72 |
| 18.700 | 0.03 | 18.25 | 18.43 | 0.00 | 0.09 | 1,651 | 94.71 |
| 18.750 | 0.03 | 18.14 | 18.32 | 0.00 | 0.09 | 1,640 | 94.70 |
| 18.800 | 0.03 | 18.02 | 18.20 | 0.00 | 0.09 | 1,630 | 94.69 |
| 18.850 | 0.03 | 17.90 | 18.08 | 0.00 | 0.09 | 1,619 | 94.68 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.03 | 17.79 | 17.97 | 0.00 | 0.09 | 1,609 | 94.67 |
| 18.950 | 0.03 | 17.67 | 17.85 | 0.00 | 0.09 | 1,598 | 94.66 |
| 19.000 | 0.03 | 17.55 | 17.73 | 0.00 | 0.09 | 1,588 | 94.65 |
| 19.050 | 0.03 | 17.43 | 17.61 | 0.00 | 0.09 | 1,577 | 94.64 |
| 19.100 | 0.03 | 17.32 | 17.50 | 0.00 | 0.09 | 1,567 | 94.63 |
| 19.150 | 0.03 | 17.20 | 17.38 | 0.00 | 0.09 | 1,556 | 94.62 |
| 19.200 | 0.03 | 17.08 | 17.26 | 0.00 | 0.09 | 1,545 | 94.61 |
| 19.250 | 0.03 | 16.96 | 17.14 | 0.00 | 0.09 | 1,535 | 94.60 |
| 19.300 | 0.03 | 16.84 | 17.02 | 0.00 | 0.09 | 1,524 | 94.59 |
| 19.350 | 0.03 | 16.72 | 16.90 | 0.00 | 0.09 | 1,513 | 94.58 |
| 19.400 | 0.03 | 16.60 | 16.78 | 0.00 | 0.09 | 1,502 | 94.57 |
| 19.450 | 0.03 | 16.48 | 16.66 | 0.00 | 0.09 | 1,491 | 94.56 |
| 19.500 | 0.03 | 16.36 | 16.54 | 0.00 | 0.09 | 1,481 | 94.55 |
| 19.550 | 0.03 | 16.24 | 16.42 | 0.00 | 0.09 | 1,470 | 94.53 |
| 19.600 | 0.03 | 16.12 | 16.30 | 0.00 | 0.09 | 1,459 | 94.52 |
| 19.650 | 0.03 | 16.00 | 16.18 | 0.00 | 0.09 | 1,448 | 94.51 |
| 19.700 | 0.03 | 15.87 | 16.05 | 0.00 | 0.09 | 1,437 | 94.50 |
| 19.750 | 0.03 | 15.75 | 15.93 | 0.00 | 0.09 | 1,426 | 94.49 |
| 19.800 | 0.03 | 15.63 | 15.81 | 0.00 | 0.09 | 1,415 | 94.48 |
| 19.850 | 0.03 | 15.51 | 15.69 | 0.00 | 0.09 | 1,404 | 94.47 |
| 19.900 | 0.03 | 15.38 | 15.56 | 0.00 | 0.09 | 1,393 | 94.46 |
| 19.950 | 0.03 | 15.26 | 15.44 | 0.00 | 0.09 | 1,381 | 94.45 |
| 20.000 | 0.03 | 15.14 | 15.32 | 0.00 | 0.09 | 1,370 | 94.44 |
| 20.050 | 0.03 | 15.01 | 15.19 | 0.00 | 0.09 | 1,359 | 94.43 |
| 20.100 | 0.03 | 14.89 | 15.07 | 0.00 | 0.09 | 1,348 | 94.42 |
| 20.150 | 0.03 | 14.76 | 14.94 | 0.00 | 0.09 | 1,337 | 94.40 |
| 20.200 | 0.03 | 14.64 | 14.82 | 0.00 | 0.09 | 1,326 | 94.39 |
| 20.250 | 0.03 | 14.51 | 14.69 | 0.00 | 0.09 | 1,314 | 94.38 |
| 20.300 | 0.03 | 14.39 | 14.57 | 0.00 | 0.09 | 1,303 | 94.37 |
| 20.350 | 0.03 | 14.26 | 14.44 | 0.00 | 0.09 | 1,292 | 94.36 |
| 20.400 | 0.03 | 14.14 | 14.32 | 0.00 | 0.09 | 1,280 | 94.35 |
| 20.450 | 0.03 | 14.01 | 14.19 | 0.00 | 0.09 | 1,269 | 94.34 |
| 20.500 | 0.03 | 13.88 | 14.06 | 0.00 | 0.09 | 1,258 | 94.33 |
| 20.550 | 0.03 | 13.76 | 13.94 | 0.00 | 0.09 | 1,246 | 94.31 |
| 20.600 | 0.03 | 13.63 | 13.81 | 0.00 | 0.09 | 1,235 | 94.30 |
| 20.650 | 0.03 | 13.50 | 13.68 | 0.00 | 0.09 | 1,223 | 94.29 |
| 20.700 | 0.03 | 13.38 | 13.56 | 0.00 | 0.09 | 1,212 | 94.28 |
| 20.750 | 0.03 | 13.25 | 13.43 | 0.00 | 0.09 | 1,200 | 94.27 |
| 20.800 | 0.03 | 13.12 | 13.30 | 0.00 | 0.09 | 1,189 | 94.26 |
| 20.850 | 0.03 | 12.99 | 13.17 | 0.00 | 0.09 | 1,177 | 94.25 |
| 20.900 | 0.03 | 12.86 | 13.04 | 0.00 | 0.09 | 1,166 | 94.24 |
| 20.950 | 0.03 | 12.73 | 12.91 | 0.00 | 0.09 | 1,154 | 94.22 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.03 | 12.61 | 12.79 | 0.00 | 0.09 | 1,143 | 94.21 |
| 21.050 | 0.03 | 12.48 | 12.66 | 0.00 | 0.09 | 1,131 | 94.20 |
| 21.100 | 0.03 | 12.35 | 12.53 | 0.00 | 0.09 | 1,119 | 94.19 |
| 21.150 | 0.03 | 12.22 | 12.40 | 0.00 | 0.09 | 1,108 | 94.18 |
| 21.200 | 0.03 | 12.09 | 12.27 | 0.00 | 0.09 | 1,096 | 94.17 |
| 21.250 | 0.02 | 11.96 | 12.14 | 0.00 | 0.09 | 1,084 | 94.16 |
| 21.300 | 0.02 | 11.83 | 12.01 | 0.00 | 0.09 | 1,073 | 94.14 |
| 21.350 | 0.02 | 11.70 | 11.88 | 0.00 | 0.09 | 1,061 | 94.13 |
| 21.400 | 0.02 | 11.57 | 11.75 | 0.00 | 0.09 | 1,049 | 94.12 |
| 21.450 | 0.02 | 11.44 | 11.62 | 0.00 | 0.09 | 1,037 | 94.11 |
| 21.500 | 0.02 | 11.30 | 11.48 | 0.00 | 0.09 | 1,026 | 94.10 |
| 21.550 | 0.02 | 11.17 | 11.35 | 0.00 | 0.09 | 1,014 | 94.09 |
| 21.600 | 0.02 | 11.04 | 11.22 | 0.00 | 0.09 | 1,002 | 94.07 |
| 21.650 | 0.02 | 10.91 | 11.09 | 0.00 | 0.09 | 990 | 94.06 |
| 21.700 | 0.02 | 10.78 | 10.96 | 0.00 | 0.09 | 978 | 94.05 |
| 21.750 | 0.02 | 10.64 | 10.82 | 0.00 | 0.09 | 966 | 94.04 |
| 21.800 | 0.02 | 10.51 | 10.69 | 0.00 | 0.09 | 954 | 94.03 |
| 21.850 | 0.02 | 10.38 | 10.56 | 0.00 | 0.09 | 942 | 94.02 |
| 21.900 | 0.02 | 10.25 | 10.43 | 0.00 | 0.09 | 930 | 94.00 |
| 21.950 | 0.02 | 10.11 | 10.29 | 0.00 | 0.09 | 918 | 93.99 |
| 22.000 | 0.02 | 9.98 | 10.16 | 0.00 | 0.09 | 906 | 93.98 |
| 22.050 | 0.02 | 9.85 | 10.03 | 0.00 | 0.09 | 894 | 93.97 |
| 22.100 | 0.02 | 9.71 | 9.89 | 0.00 | 0.09 | 882 | 93.96 |
| 22.150 | 0.02 | 9.58 | 9.76 | 0.00 | 0.09 | 870 | 93.94 |
| 22.200 | 0.02 | 9.44 | 9.62 | 0.00 | 0.09 | 858 | 93.93 |
| 22.250 | 0.02 | 9.31 | 9.49 | 0.00 | 0.09 | 846 | 93.92 |
| 22.300 | 0.02 | 9.17 | 9.35 | 0.00 | 0.09 | 834 | 93.91 |
| 22.350 | 0.02 | 9.04 | 9.22 | 0.00 | 0.09 | 821 | 93.90 |
| 22.400 | 0.02 | 8.90 | 9.08 | 0.00 | 0.09 | 809 | 93.88 |
| 22.450 | 0.02 | 8.77 | 8.95 | 0.00 | 0.09 | 797 | 93.87 |
| 22.500 | 0.02 | 8.63 | 8.81 | 0.00 | 0.09 | 785 | 93.86 |
| 22.550 | 0.02 | 8.49 | 8.67 | 0.00 | 0.09 | 773 | 93.85 |
| 22.600 | 0.02 | 8.36 | 8.54 | 0.00 | 0.09 | 760 | 93.84 |
| 22.650 | 0.02 | 8.22 | 8.40 | 0.00 | 0.09 | 748 | 93.82 |
| 22.700 | 0.02 | 8.08 | 8.26 | 0.00 | 0.09 | 736 | 93.81 |
| 22.750 | 0.02 | 7.95 | 8.13 | 0.00 | 0.09 | 723 | 93.80 |
| 22.800 | 0.02 | 7.81 | 7.99 | 0.00 | 0.09 | 711 | 93.79 |
| 22.850 | 0.02 | 7.67 | 7.85 | 0.00 | 0.09 | 699 | 93.78 |
| 22.900 | 0.02 | 7.53 | 7.71 | 0.00 | 0.09 | 686 | 93.76 |
| 22.950 | 0.02 | 7.40 | 7.58 | 0.00 | 0.09 | 674 | 93.75 |
| 23.000 | 0.02 | 7.26 | 7.44 | 0.00 | 0.09 | 661 | 93.74 |
| 23.050 | 0.02 | 7.12 | 7.30 | 0.00 | 0.09 | 649 | 93.73 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.02 | 6.98 | 7.16 | 0.00 | 0.09 | 636 | 93.71 |
| 23.150 | 0.02 | 6.84 | 7.02 | 0.00 | 0.09 | 624 | 93.70 |
| 23.200 | 0.02 | 6.70 | 6.88 | 0.00 | 0.09 | 611 | 93.69 |
| 23.250 | 0.02 | 6.56 | 6.74 | 0.00 | 0.09 | 599 | 93.68 |
| 23.300 | 0.02 | 6.42 | 6.60 | 0.00 | 0.09 | 586 | 93.66 |
| 23.350 | 0.02 | 6.28 | 6.46 | 0.00 | 0.09 | 573 | 93.65 |
| 23.400 | 0.02 | 6.14 | 6.32 | 0.00 | 0.09 | 561 | 93.64 |
| 23.450 | 0.02 | 6.00 | 6.18 | 0.00 | 0.09 | 548 | 93.63 |
| 23.500 | 0.02 | 5.86 | 6.04 | 0.00 | 0.09 | 535 | 93.61 |
| 23.550 | 0.02 | 5.72 | 5.90 | 0.00 | 0.09 | 523 | 93.60 |
| 23.600 | 0.02 | 5.58 | 5.76 | 0.00 | 0.09 | 510 | 93.59 |
| 23.650 | 0.02 | 5.44 | 5.62 | 0.00 | 0.09 | 497 | 93.58 |
| 23.700 | 0.02 | 5.29 | 5.47 | 0.00 | 0.09 | 485 | 93.56 |
| 23.750 | 0.02 | 5.15 | 5.33 | 0.00 | 0.09 | 472 | 93.55 |
| 23.800 | 0.02 | 5.01 | 5.19 | 0.00 | 0.09 | 459 | 93.54 |
| 23.850 | 0.02 | 4.87 | 5.05 | 0.00 | 0.09 | 446 | 93.53 |
| 23.900 | 0.02 | 4.72 | 4.90 | 0.00 | 0.09 | 433 | 93.51 |
| 23.950 | 0.02 | 4.58 | 4.76 | 0.00 | 0.09 | 420 | 93.50 |
| 24.000 | 0.02 | 4.44 | 4.62 | 0.00 | 0.09 | 408 | 93.49 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 1.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 2.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 2.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 2.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 2.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 2.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 2.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 2.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.400 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.450 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.500 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.600 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.650 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 3.700 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 3.750 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 3.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 3.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 3.900 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 3.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 4.000 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 4.050 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 4.100 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.150 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.250 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 4.950 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.000 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.050 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.100 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.150 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.200 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.250 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.300 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.350 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 5.400 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.450 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.500 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.550 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.600 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.650 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.700 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.750 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.800 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.850 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 5.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 5.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.350 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 6.400 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 6.450 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 6.500 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 6.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 6.600 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 6.650 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 6.700 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 6.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 6.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 6.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 6.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 6.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 7.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 7.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 7.100 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 7.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 7.200 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 7.250 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 7.300 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 7.350 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 7.400 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 7.450 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 7.500 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.550 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.600 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.650 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.700 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.750 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.800 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 7.850 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 7.900 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 7.950 | 0.07 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 8.000 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 8.050 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 8.100 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 8.150 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 8.200 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 8.250 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 8.300 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 8.350 | 0.08 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 8.450 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 8.500 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 8.550 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 8.600 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 8.650 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 8.700 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 8.750 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 8.800 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 8.850 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 8 | 93.02 |
| 8.900 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 8 | 93.02 |
| 8.950 | 0.09 | 0.01 | 0.19 | 0.00 | 0.09 | 9 | 93.02 |
| 9.000 | 0.10 | 0.02 | 0.20 | 0.00 | 0.09 | 10 | 93.02 |
| 9.050 | 0.10 | 0.03 | 0.21 | 0.00 | 0.09 | 11 | 93.02 |
| 9.100 | 0.10 | 0.05 | 0.23 | 0.00 | 0.09 | 12 | 93.02 |
| 9.150 | 0.10 | 0.07 | 0.25 | 0.00 | 0.09 | 14 | 93.03 |
| 9.200 | 0.10 | 0.09 | 0.27 | 0.00 | 0.09 | 16 | 93.03 |
| 9.250 | 0.10 | 0.12 | 0.30 | 0.00 | 0.09 | 19 | 93.04 |
| 9.300 | 0.11 | 0.14 | 0.32 | 0.00 | 0.09 | 21 | 93.04 |
| 9.350 | 0.11 | 0.18 | 0.36 | 0.00 | 0.09 | 24 | 93.05 |
| 9.400 | 0.11 | 0.21 | 0.39 | 0.00 | 0.09 | 27 | 93.05 |
| 9.450 | 0.11 | 0.25 | 0.43 | 0.00 | 0.09 | 31 | 93.06 |
| 9.500 | 0.11 | 0.29 | 0.47 | 0.00 | 0.09 | 34 | 93.07 |
| 9.550 | 0.11 | 0.34 | 0.52 | 0.00 | 0.09 | 38 | 93.08 |
| 9.600 | 0.11 | 0.38 | 0.56 | 0.00 | 0.09 | 43 | 93.08 |
| 9.650 | 0.12 | 0.43 | 0.61 | 0.00 | 0.09 | 47 | 93.09 |
| 9.700 | 0.12 | 0.49 | 0.67 | 0.00 | 0.09 | 52 | 93.10 |
| 9.750 | 0.12 | 0.55 | 0.73 | 0.00 | 0.09 | 56 | 93.11 |
| 9.800 | 0.12 | 0.61 | 0.79 | 0.00 | 0.09 | 60 | 93.12 |
| 9.850 | 0.12 | 0.67 | 0.85 | 0.00 | 0.09 | 65 | 93.13 |
| 9.900 | 0.12 | 0.74 | 0.92 | 0.00 | 0.09 | 70 | 93.14 |
| 9.950 | 0.13 | 0.81 | 0.99 | 0.00 | 0.09 | 75 | 93.15 |
| 10.000 | 0.13 | 0.88 | 1.06 | 0.00 | 0.09 | 80 | 93.16 |
| 10.050 | 0.13 | 0.96 | 1.14 | 0.00 | 0.09 | 86 | 93.17 |
| 10.100 | 0.13 | 1.04 | 1.22 | 0.00 | 0.09 | 94 | 93.18 |
| 10.150 | 0.13 | 1.12 | 1.30 | 0.00 | 0.09 | 106 | 93.19 |
| 10.200 | 0.14 | 1.22 | 1.40 | 0.00 | 0.09 | 118 | 93.20 |
| 10.250 | 0.14 | 1.31 | 1.49 | 0.00 | 0.09 | 126 | 93.21 |
| 10.300 | 0.14 | 1.42 | 1.60 | 0.00 | 0.09 | 136 | 93.22 |
| 10.350 | 0.15 | 1.53 | 1.71 | 0.00 | 0.09 | 146 | 93.23 |
| 10.400 | 0.15 | 1.65 | 1.83 | 0.00 | 0.09 | 157 | 93.24 |
| 10.450 | 0.15 | 1.78 | 1.96 | 0.00 | 0.09 | 168 | 93.25 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.16 | 1.91 | 2.09 | 0.00 | 0.09 | 180 | 93.26 |
| 10.550 | 0.16 | 2.04 | 2.22 | 0.00 | 0.09 | 192 | 93.28 |
| 10.600 | 0.16 | 2.19 | 2.37 | 0.00 | 0.09 | 205 | 93.29 |
| 10.650 | 0.17 | 2.34 | 2.52 | 0.00 | 0.09 | 219 | 93.30 |
| 10.700 | 0.17 | 2.50 | 2.68 | 0.00 | 0.09 | 233 | 93.32 |
| 10.750 | 0.17 | 2.66 | 2.84 | 0.00 | 0.09 | 248 | 93.33 |
| 10.800 | 0.18 | 2.83 | 3.01 | 0.00 | 0.09 | 263 | 93.35 |
| 10.850 | 0.18 | 3.01 | 3.19 | 0.00 | 0.09 | 279 | 93.36 |
| 10.900 | 0.18 | 3.19 | 3.37 | 0.00 | 0.09 | 295 | 93.38 |
| 10.950 | 0.19 | 3.38 | 3.56 | 0.00 | 0.09 | 313 | 93.40 |
| 11.000 | 0.19 | 3.58 | 3.76 | 0.00 | 0.09 | 330 | 93.41 |
| 11.050 | 0.20 | 3.79 | 3.97 | 0.00 | 0.09 | 349 | 93.43 |
| 11.100 | 0.20 | 4.00 | 4.18 | 0.00 | 0.09 | 369 | 93.45 |
| 11.150 | 0.21 | 4.24 | 4.42 | 0.00 | 0.09 | 390 | 93.47 |
| 11.200 | 0.23 | 4.50 | 4.68 | 0.00 | 0.09 | 413 | 93.49 |
| 11.250 | 0.24 | 4.78 | 4.96 | 0.00 | 0.09 | 439 | 93.52 |
| 11.300 | 0.25 | 5.09 | 5.27 | 0.00 | 0.09 | 466 | 93.55 |
| 11.350 | 0.26 | 5.42 | 5.60 | 0.00 | 0.09 | 496 | 93.58 |
| 11.400 | 0.28 | 5.78 | 5.96 | 0.00 | 0.09 | 528 | 93.61 |
| 11.450 | 0.29 | 6.16 | 6.34 | 0.00 | 0.09 | 563 | 93.64 |
| 11.500 | 0.30 | 6.57 | 6.75 | 0.00 | 0.09 | 599 | 93.68 |
| 11.550 | 0.34 | 7.03 | 7.21 | 0.00 | 0.09 | 641 | 93.72 |
| 11.600 | 0.40 | 7.59 | 7.77 | 0.00 | 0.09 | 692 | 93.77 |
| 11.650 | 0.49 | 8.31 | 8.49 | 0.00 | 0.09 | 756 | 93.83 |
| 11.700 | 0.61 | 9.23 | 9.41 | 0.00 | 0.09 | 839 | 93.91 |
| 11.750 | 0.72 | 10.39 | 10.57 | 0.00 | 0.09 | 943 | 94.02 |
| 11.800 | 0.85 | 11.77 | 11.95 | 0.00 | 0.09 | 1,068 | 94.14 |
| 11.850 | 0.96 | 13.40 | 13.58 | 0.00 | 0.09 | 1,214 | 94.28 |
| 11.900 | 1.09 | 15.26 | 15.44 | 0.00 | 0.09 | 1,382 | 94.45 |
| 11.950 | 1.43 | 17.60 | 17.78 | 0.00 | 0.09 | 1,592 | 94.66 |
| 12.000 | 1.98 | 20.83 | 21.01 | 0.00 | 0.09 | 1,883 | 94.94 |
| 12.050 | 2.18 | 24.09 | 25.00 | 0.00 | 0.46 | 2,209 | 95.22 |
| 12.100 | 2.24 | 23.09 | 28.51 | 0.00 | 2.71 | 2,322 | 95.27 |
| 12.150 | 1.97 | 23.43 | 27.30 | 0.00 | 1.93 | 2,283 | 95.26 |
| 12.200 | 1.43 | 23.56 | 26.83 | 0.00 | 1.63 | 2,268 | 95.25 |
| 12.250 | 1.17 | 23.75 | 26.17 | 0.00 | 1.21 | 2,247 | 95.24 |
| 12.300 | 1.00 | 23.82 | 25.93 | 0.00 | 1.05 | 2,239 | 95.23 |
| 12.350 | 0.88 | 23.89 | 25.70 | 0.00 | 0.91 | 2,231 | 95.23 |
| 12.400 | 0.74 | 23.94 | 25.51 | 0.00 | 0.78 | 2,225 | 95.23 |
| 12.450 | 0.63 | 24.00 | 25.32 | 0.00 | 0.66 | 2,219 | 95.22 |
| 12.500 | 0.51 | 24.05 | 25.14 | 0.00 | 0.54 | 2,213 | 95.22 |
| 12.550 | 0.42 | 24.09 | 24.98 | 0.00 | 0.44 | 2,208 | 95.22 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.35 | 24.13 | 24.86 | 0.00 | 0.37 | 2,205 | 95.22 |
| 12.650 | 0.31 | 24.15 | 24.79 | 0.00 | 0.32 | 2,202 | 95.22 |
| 12.700 | 0.29 | 24.16 | 24.75 | 0.00 | 0.30 | 2,201 | 95.22 |
| 12.750 | 0.28 | 24.16 | 24.73 | 0.00 | 0.28 | 2,200 | 95.21 |
| 12.800 | 0.27 | 24.17 | 24.71 | 0.00 | 0.27 | 2,200 | 95.21 |
| 12.850 | 0.26 | 24.17 | 24.69 | 0.00 | 0.26 | 2,199 | 95.21 |
| 12.900 | 0.24 | 24.18 | 24.67 | 0.00 | 0.25 | 2,198 | 95.21 |
| 12.950 | 0.23 | 24.19 | 24.65 | 0.00 | 0.23 | 2,198 | 95.21 |
| 13.000 | 0.22 | 24.19 | 24.63 | 0.00 | 0.22 | 2,197 | 95.21 |
| 13.050 | 0.21 | 24.20 | 24.62 | 0.00 | 0.21 | 2,197 | 95.21 |
| 13.100 | 0.20 | 24.20 | 24.60 | 0.00 | 0.20 | 2,196 | 95.21 |
| 13.150 | 0.19 | 24.20 | 24.59 | 0.00 | 0.19 | 2,196 | 95.21 |
| 13.200 | 0.19 | 24.20 | 24.59 | 0.00 | 0.19 | 2,196 | 95.21 |
| 13.250 | 0.19 | 24.21 | 24.58 | 0.00 | 0.19 | 2,195 | 95.21 |
| 13.300 | 0.18 | 24.21 | 24.58 | 0.00 | 0.18 | 2,195 | 95.21 |
| 13.350 | 0.18 | 24.21 | 24.57 | 0.00 | 0.18 | 2,195 | 95.21 |
| 13.400 | 0.18 | 24.21 | 24.57 | 0.00 | 0.18 | 2,195 | 95.21 |
| 13.450 | 0.17 | 24.21 | 24.56 | 0.00 | 0.17 | 2,195 | 95.21 |
| 13.500 | 0.17 | 24.21 | 24.56 | 0.00 | 0.17 | 2,195 | 95.21 |
| 13.550 | 0.17 | 24.21 | 24.55 | 0.00 | 0.17 | 2,194 | 95.21 |
| 13.600 | 0.16 | 24.22 | 24.55 | 0.00 | 0.16 | 2,194 | 95.21 |
| 13.650 | 0.16 | 24.22 | 24.54 | 0.00 | 0.16 | 2,194 | 95.21 |
| 13.700 | 0.16 | 24.22 | 24.54 | 0.00 | 0.16 | 2,194 | 95.21 |
| 13.750 | 0.15 | 24.22 | 24.53 | 0.00 | 0.15 | 2,194 | 95.21 |
| 13.800 | 0.15 | 24.22 | 24.52 | 0.00 | 0.15 | 2,194 | 95.21 |
| 13.850 | 0.15 | 24.22 | 24.52 | 0.00 | 0.15 | 2,193 | 95.21 |
| 13.900 | 0.14 | 24.22 | 24.51 | 0.00 | 0.15 | 2,193 | 95.21 |
| 13.950 | 0.14 | 24.23 | 24.51 | 0.00 | 0.14 | 2,193 | 95.21 |
| 14.000 | 0.14 | 24.23 | 24.50 | 0.00 | 0.14 | 2,193 | 95.21 |
| 14.050 | 0.14 | 24.23 | 24.50 | 0.00 | 0.14 | 2,193 | 95.21 |
| 14.100 | 0.13 | 24.23 | 24.50 | 0.00 | 0.13 | 2,193 | 95.21 |
| 14.150 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,193 | 95.21 |
| 14.200 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 14.250 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 14.300 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 14.350 | 0.12 | 24.23 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 14.400 | 0.12 | 24.23 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 14.450 | 0.12 | 24.23 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 14.500 | 0.12 | 24.24 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 14.550 | 0.12 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |
| 14.600 | 0.12 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |
| 14.650 | 0.11 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.11 | 24.24 | 24.47 | 0.00 | 0.11 | 2,192 | 95.21 |
| 14.750 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,192 | 95.21 |
| 14.800 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,192 | 95.21 |
| 14.850 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,191 | 95.21 |
| 14.900 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,191 | 95.21 |
| 14.950 | 0.11 | 24.24 | 24.45 | 0.00 | 0.11 | 2,191 | 95.21 |
| 15.000 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.050 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.100 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.150 | 0.10 | 24.24 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.200 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.250 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.300 | 0.09 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 15.350 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 15.400 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 15.450 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 15.500 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,190 | 95.21 |
| 15.550 | 0.09 | 24.24 | 24.42 | 0.00 | 0.09 | 2,190 | 95.21 |
| 15.600 | 0.09 | 24.23 | 24.41 | 0.00 | 0.09 | 2,189 | 95.21 |
| 15.650 | 0.08 | 24.22 | 24.40 | 0.00 | 0.09 | 2,188 | 95.21 |
| 15.700 | 0.08 | 24.21 | 24.39 | 0.00 | 0.09 | 2,187 | 95.21 |
| 15.750 | 0.08 | 24.19 | 24.37 | 0.00 | 0.09 | 2,185 | 95.21 |
| 15.800 | 0.08 | 24.17 | 24.35 | 0.00 | 0.09 | 2,184 | 95.21 |
| 15.850 | 0.08 | 24.15 | 24.33 | 0.00 | 0.09 | 2,181 | 95.21 |
| 15.900 | 0.08 | 24.12 | 24.30 | 0.00 | 0.09 | 2,179 | 95.20 |
| 15.950 | 0.07 | 24.09 | 24.27 | 0.00 | 0.09 | 2,176 | 95.20 |
| 16.000 | 0.07 | 24.06 | 24.24 | 0.00 | 0.09 | 2,173 | 95.20 |
| 16.050 | 0.07 | 24.02 | 24.20 | 0.00 | 0.09 | 2,170 | 95.20 |
| 16.100 | 0.07 | 23.99 | 24.17 | 0.00 | 0.09 | 2,165 | 95.20 |
| 16.150 | 0.07 | 23.95 | 24.13 | 0.00 | 0.09 | 2,159 | 95.19 |
| 16.200 | 0.07 | 23.90 | 24.08 | 0.00 | 0.09 | 2,153 | 95.19 |
| 16.250 | 0.07 | 23.86 | 24.04 | 0.00 | 0.09 | 2,147 | 95.19 |
| 16.300 | 0.07 | 23.82 | 24.00 | 0.00 | 0.09 | 2,140 | 95.19 |
| 16.350 | 0.07 | 23.77 | 23.95 | 0.00 | 0.09 | 2,134 | 95.18 |
| 16.400 | 0.07 | 23.72 | 23.90 | 0.00 | 0.09 | 2,127 | 95.18 |
| 16.450 | 0.07 | 23.67 | 23.85 | 0.00 | 0.09 | 2,121 | 95.18 |
| 16.500 | 0.06 | 23.62 | 23.80 | 0.00 | 0.09 | 2,116 | 95.17 |
| 16.550 | 0.06 | 23.57 | 23.75 | 0.00 | 0.09 | 2,113 | 95.17 |
| 16.600 | 0.06 | 23.52 | 23.70 | 0.00 | 0.09 | 2,109 | 95.16 |
| 16.650 | 0.06 | 23.47 | 23.65 | 0.00 | 0.09 | 2,105 | 95.16 |
| 16.700 | 0.06 | 23.41 | 23.59 | 0.00 | 0.09 | 2,101 | 95.16 |
| 16.750 | 0.06 | 23.36 | 23.54 | 0.00 | 0.09 | 2,097 | 95.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.06 | 23.30 | 23.48 | 0.00 | 0.09 | 2,093 | 95.15 |
| 16.850 | 0.06 | 23.24 | 23.42 | 0.00 | 0.09 | 2,088 | 95.14 |
| 16.900 | 0.06 | 23.18 | 23.36 | 0.00 | 0.09 | 2,084 | 95.14 |
| 16.950 | 0.06 | 23.11 | 23.29 | 0.00 | 0.09 | 2,080 | 95.14 |
| 17.000 | 0.06 | 23.05 | 23.23 | 0.00 | 0.09 | 2,075 | 95.13 |
| 17.050 | 0.06 | 22.99 | 23.17 | 0.00 | 0.09 | 2,070 | 95.13 |
| 17.100 | 0.06 | 22.92 | 23.10 | 0.00 | 0.09 | 2,065 | 95.12 |
| 17.150 | 0.06 | 22.85 | 23.03 | 0.00 | 0.09 | 2,061 | 95.12 |
| 17.200 | 0.06 | 22.78 | 22.96 | 0.00 | 0.09 | 2,056 | 95.11 |
| 17.250 | 0.05 | 22.71 | 22.89 | 0.00 | 0.09 | 2,051 | 95.11 |
| 17.300 | 0.05 | 22.64 | 22.82 | 0.00 | 0.09 | 2,045 | 95.10 |
| 17.350 | 0.05 | 22.57 | 22.75 | 0.00 | 0.09 | 2,039 | 95.10 |
| 17.400 | 0.05 | 22.49 | 22.67 | 0.00 | 0.09 | 2,033 | 95.09 |
| 17.450 | 0.05 | 22.42 | 22.60 | 0.00 | 0.09 | 2,026 | 95.08 |
| 17.500 | 0.05 | 22.34 | 22.52 | 0.00 | 0.09 | 2,019 | 95.08 |
| 17.550 | 0.05 | 22.26 | 22.44 | 0.00 | 0.09 | 2,012 | 95.07 |
| 17.600 | 0.05 | 22.18 | 22.36 | 0.00 | 0.09 | 2,005 | 95.06 |
| 17.650 | 0.05 | 22.10 | 22.28 | 0.00 | 0.09 | 1,997 | 95.05 |
| 17.700 | 0.05 | 22.02 | 22.20 | 0.00 | 0.09 | 1,990 | 95.05 |
| 17.750 | 0.05 | 21.94 | 22.12 | 0.00 | 0.09 | 1,982 | 95.04 |
| 17.800 | 0.05 | 21.85 | 22.03 | 0.00 | 0.09 | 1,975 | 95.03 |
| 17.850 | 0.05 | 21.76 | 21.94 | 0.00 | 0.09 | 1,967 | 95.02 |
| 17.900 | 0.05 | 21.68 | 21.86 | 0.00 | 0.09 | 1,959 | 95.02 |
| 17.950 | 0.05 | 21.59 | 21.77 | 0.00 | 0.09 | 1,951 | 95.01 |
| 18.000 | 0.04 | 21.50 | 21.68 | 0.00 | 0.09 | 1,943 | 95.00 |
| 18.050 | 0.04 | 21.41 | 21.59 | 0.00 | 0.09 | 1,935 | 94.99 |
| 18.100 | 0.04 | 21.31 | 21.49 | 0.00 | 0.09 | 1,926 | 94.98 |
| 18.150 | 0.04 | 21.22 | 21.40 | 0.00 | 0.09 | 1,918 | 94.98 |
| 18.200 | 0.04 | 21.12 | 21.30 | 0.00 | 0.09 | 1,909 | 94.97 |
| 18.250 | 0.04 | 21.03 | 21.21 | 0.00 | 0.09 | 1,901 | 94.96 |
| 18.300 | 0.04 | 20.94 | 21.12 | 0.00 | 0.09 | 1,892 | 94.95 |
| 18.350 | 0.04 | 20.84 | 21.02 | 0.00 | 0.09 | 1,884 | 94.94 |
| 18.400 | 0.04 | 20.74 | 20.92 | 0.00 | 0.09 | 1,875 | 94.93 |
| 18.450 | 0.04 | 20.65 | 20.83 | 0.00 | 0.09 | 1,866 | 94.93 |
| 18.500 | 0.04 | 20.55 | 20.73 | 0.00 | 0.09 | 1,858 | 94.92 |
| 18.550 | 0.04 | 20.45 | 20.63 | 0.00 | 0.09 | 1,849 | 94.91 |
| 18.600 | 0.04 | 20.36 | 20.54 | 0.00 | 0.09 | 1,840 | 94.90 |
| 18.650 | 0.04 | 20.26 | 20.44 | 0.00 | 0.09 | 1,831 | 94.89 |
| 18.700 | 0.04 | 20.16 | 20.34 | 0.00 | 0.09 | 1,823 | 94.88 |
| 18.750 | 0.04 | 20.06 | 20.24 | 0.00 | 0.09 | 1,814 | 94.87 |
| 18.800 | 0.04 | 19.96 | 20.14 | 0.00 | 0.09 | 1,805 | 94.86 |
| 18.850 | 0.04 | 19.86 | 20.04 | 0.00 | 0.09 | 1,796 | 94.86 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.04 | 19.76 | 19.94 | 0.00 | 0.09 | 1,787 | 94.85 |
| 18.950 | 0.04 | 19.66 | 19.84 | 0.00 | 0.09 | 1,778 | 94.84 |
| 19.000 | 0.04 | 19.56 | 19.74 | 0.00 | 0.09 | 1,769 | 94.83 |
| 19.050 | 0.04 | 19.46 | 19.64 | 0.00 | 0.09 | 1,760 | 94.82 |
| 19.100 | 0.04 | 19.36 | 19.54 | 0.00 | 0.09 | 1,751 | 94.81 |
| 19.150 | 0.04 | 19.26 | 19.44 | 0.00 | 0.09 | 1,741 | 94.80 |
| 19.200 | 0.04 | 19.16 | 19.34 | 0.00 | 0.09 | 1,732 | 94.79 |
| 19.250 | 0.04 | 19.05 | 19.23 | 0.00 | 0.09 | 1,723 | 94.78 |
| 19.300 | 0.04 | 18.95 | 19.13 | 0.00 | 0.09 | 1,714 | 94.78 |
| 19.350 | 0.04 | 18.85 | 19.03 | 0.00 | 0.09 | 1,704 | 94.77 |
| 19.400 | 0.04 | 18.74 | 18.92 | 0.00 | 0.09 | 1,695 | 94.76 |
| 19.450 | 0.04 | 18.64 | 18.82 | 0.00 | 0.09 | 1,686 | 94.75 |
| 19.500 | 0.04 | 18.53 | 18.71 | 0.00 | 0.09 | 1,676 | 94.74 |
| 19.550 | 0.04 | 18.43 | 18.61 | 0.00 | 0.09 | 1,667 | 94.73 |
| 19.600 | 0.04 | 18.32 | 18.50 | 0.00 | 0.09 | 1,657 | 94.72 |
| 19.650 | 0.04 | 18.22 | 18.40 | 0.00 | 0.09 | 1,648 | 94.71 |
| 19.700 | 0.04 | 18.11 | 18.29 | 0.00 | 0.09 | 1,638 | 94.70 |
| 19.750 | 0.04 | 18.00 | 18.18 | 0.00 | 0.09 | 1,629 | 94.69 |
| 19.800 | 0.04 | 17.90 | 18.08 | 0.00 | 0.09 | 1,619 | 94.68 |
| 19.850 | 0.04 | 17.79 | 17.97 | 0.00 | 0.09 | 1,609 | 94.67 |
| 19.900 | 0.04 | 17.68 | 17.86 | 0.00 | 0.09 | 1,599 | 94.66 |
| 19.950 | 0.04 | 17.57 | 17.75 | 0.00 | 0.09 | 1,590 | 94.65 |
| 20.000 | 0.04 | 17.46 | 17.64 | 0.00 | 0.09 | 1,580 | 94.64 |
| 20.050 | 0.04 | 17.36 | 17.54 | 0.00 | 0.09 | 1,570 | 94.63 |
| 20.100 | 0.04 | 17.25 | 17.43 | 0.00 | 0.09 | 1,560 | 94.62 |
| 20.150 | 0.03 | 17.14 | 17.32 | 0.00 | 0.09 | 1,550 | 94.61 |
| 20.200 | 0.03 | 17.03 | 17.21 | 0.00 | 0.09 | 1,540 | 94.60 |
| 20.250 | 0.03 | 16.92 | 17.10 | 0.00 | 0.09 | 1,531 | 94.59 |
| 20.300 | 0.03 | 16.81 | 16.99 | 0.00 | 0.09 | 1,521 | 94.58 |
| 20.350 | 0.03 | 16.69 | 16.87 | 0.00 | 0.09 | 1,511 | 94.58 |
| 20.400 | 0.03 | 16.58 | 16.76 | 0.00 | 0.09 | 1,501 | 94.57 |
| 20.450 | 0.03 | 16.47 | 16.65 | 0.00 | 0.09 | 1,490 | 94.56 |
| 20.500 | 0.03 | 16.36 | 16.54 | 0.00 | 0.09 | 1,480 | 94.55 |
| 20.550 | 0.03 | 16.25 | 16.43 | 0.00 | 0.09 | 1,470 | 94.54 |
| 20.600 | 0.03 | 16.13 | 16.31 | 0.00 | 0.09 | 1,460 | 94.53 |
| 20.650 | 0.03 | 16.02 | 16.20 | 0.00 | 0.09 | 1,450 | 94.52 |
| 20.700 | 0.03 | 15.91 | 16.09 | 0.00 | 0.09 | 1,440 | 94.51 |
| 20.750 | 0.03 | 15.79 | 15.97 | 0.00 | 0.09 | 1,430 | 94.50 |
| 20.800 | 0.03 | 15.68 | 15.86 | 0.00 | 0.09 | 1,419 | 94.49 |
| 20.850 | 0.03 | 15.57 | 15.75 | 0.00 | 0.09 | 1,409 | 94.48 |
| 20.900 | 0.03 | 15.45 | 15.63 | 0.00 | 0.09 | 1,399 | 94.47 |
| 20.950 | 0.03 | 15.34 | 15.52 | 0.00 | 0.09 | 1,388 | 94.45 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.03 | 15.22 | 15.40 | 0.00 | 0.09 | 1,378 | 94.44 |
| 21.050 | 0.03 | 15.11 | 15.29 | 0.00 | 0.09 | 1,368 | 94.43 |
| 21.100 | 0.03 | 14.99 | 15.17 | 0.00 | 0.09 | 1,357 | 94.42 |
| 21.150 | 0.03 | 14.87 | 15.05 | 0.00 | 0.09 | 1,347 | 94.41 |
| 21.200 | 0.03 | 14.76 | 14.94 | 0.00 | 0.09 | 1,336 | 94.40 |
| 21.250 | 0.03 | 14.64 | 14.82 | 0.00 | 0.09 | 1,326 | 94.39 |
| 21.300 | 0.03 | 14.53 | 14.71 | 0.00 | 0.09 | 1,315 | 94.38 |
| 21.350 | 0.03 | 14.41 | 14.59 | 0.00 | 0.09 | 1,305 | 94.37 |
| 21.400 | 0.03 | 14.29 | 14.47 | 0.00 | 0.09 | 1,294 | 94.36 |
| 21.450 | 0.03 | 14.17 | 14.35 | 0.00 | 0.09 | 1,284 | 94.35 |
| 21.500 | 0.03 | 14.05 | 14.23 | 0.00 | 0.09 | 1,273 | 94.34 |
| 21.550 | 0.03 | 13.94 | 14.12 | 0.00 | 0.09 | 1,262 | 94.33 |
| 21.600 | 0.03 | 13.82 | 14.00 | 0.00 | 0.09 | 1,252 | 94.32 |
| 21.650 | 0.03 | 13.70 | 13.88 | 0.00 | 0.09 | 1,241 | 94.31 |
| 21.700 | 0.03 | 13.58 | 13.76 | 0.00 | 0.09 | 1,230 | 94.30 |
| 21.750 | 0.03 | 13.46 | 13.64 | 0.00 | 0.09 | 1,219 | 94.29 |
| 21.800 | 0.03 | 13.34 | 13.52 | 0.00 | 0.09 | 1,209 | 94.28 |
| 21.850 | 0.03 | 13.22 | 13.40 | 0.00 | 0.09 | 1,198 | 94.27 |
| 21.900 | 0.03 | 13.10 | 13.28 | 0.00 | 0.09 | 1,187 | 94.26 |
| 21.950 | 0.03 | 12.98 | 13.16 | 0.00 | 0.09 | 1,176 | 94.25 |
| 22.000 | 0.03 | 12.86 | 13.04 | 0.00 | 0.09 | 1,165 | 94.24 |
| 22.050 | 0.03 | 12.74 | 12.92 | 0.00 | 0.09 | 1,154 | 94.22 |
| 22.100 | 0.03 | 12.61 | 12.79 | 0.00 | 0.09 | 1,143 | 94.21 |
| 22.150 | 0.03 | 12.49 | 12.67 | 0.00 | 0.09 | 1,132 | 94.20 |
| 22.200 | 0.03 | 12.37 | 12.55 | 0.00 | 0.09 | 1,121 | 94.19 |
| 22.250 | 0.03 | 12.25 | 12.43 | 0.00 | 0.09 | 1,110 | 94.18 |
| 22.300 | 0.03 | 12.12 | 12.30 | 0.00 | 0.09 | 1,099 | 94.17 |
| 22.350 | 0.03 | 12.00 | 12.18 | 0.00 | 0.09 | 1,088 | 94.16 |
| 22.400 | 0.03 | 11.88 | 12.06 | 0.00 | 0.09 | 1,077 | 94.15 |
| 22.450 | 0.03 | 11.75 | 11.93 | 0.00 | 0.09 | 1,066 | 94.14 |
| 22.500 | 0.03 | 11.63 | 11.81 | 0.00 | 0.09 | 1,055 | 94.13 |
| 22.550 | 0.03 | 11.50 | 11.68 | 0.00 | 0.09 | 1,043 | 94.12 |
| 22.600 | 0.03 | 11.38 | 11.56 | 0.00 | 0.09 | 1,032 | 94.10 |
| 22.650 | 0.03 | 11.25 | 11.43 | 0.00 | 0.09 | 1,021 | 94.09 |
| 22.700 | 0.03 | 11.13 | 11.31 | 0.00 | 0.09 | 1,010 | 94.08 |
| 22.750 | 0.03 | 11.00 | 11.18 | 0.00 | 0.09 | 998 | 94.07 |
| 22.800 | 0.03 | 10.88 | 11.06 | 0.00 | 0.09 | 987 | 94.06 |
| 22.850 | 0.03 | 10.75 | 10.93 | 0.00 | 0.09 | 976 | 94.05 |
| 22.900 | 0.03 | 10.62 | 10.80 | 0.00 | 0.09 | 964 | 94.04 |
| 22.950 | 0.03 | 10.50 | 10.68 | 0.00 | 0.09 | 953 | 94.03 |
| 23.000 | 0.03 | 10.37 | 10.55 | 0.00 | 0.09 | 941 | 94.01 |
| 23.050 | 0.03 | 10.24 | 10.42 | 0.00 | 0.09 | 930 | 94.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.03 | 10.11 | 10.29 | 0.00 | 0.09 | 918 | 93.99 |
| 23.150 | 0.03 | 9.99 | 10.17 | 0.00 | 0.09 | 907 | 93.98 |
| 23.200 | 0.03 | 9.86 | 10.04 | 0.00 | 0.09 | 895 | 93.97 |
| 23.250 | 0.03 | 9.73 | 9.91 | 0.00 | 0.09 | 884 | 93.96 |
| 23.300 | 0.03 | 9.60 | 9.78 | 0.00 | 0.09 | 872 | 93.95 |
| 23.350 | 0.03 | 9.47 | 9.65 | 0.00 | 0.09 | 860 | 93.93 |
| 23.400 | 0.03 | 9.34 | 9.52 | 0.00 | 0.09 | 849 | 93.92 |
| 23.450 | 0.03 | 9.21 | 9.39 | 0.00 | 0.09 | 837 | 93.91 |
| 23.500 | 0.02 | 9.08 | 9.26 | 0.00 | 0.09 | 825 | 93.90 |
| 23.550 | 0.02 | 8.95 | 9.13 | 0.00 | 0.09 | 814 | 93.89 |
| 23.600 | 0.02 | 8.82 | 9.00 | 0.00 | 0.09 | 802 | 93.88 |
| 23.650 | 0.02 | 8.69 | 8.87 | 0.00 | 0.09 | 790 | 93.87 |
| 23.700 | 0.02 | 8.56 | 8.74 | 0.00 | 0.09 | 778 | 93.85 |
| 23.750 | 0.02 | 8.42 | 8.60 | 0.00 | 0.09 | 766 | 93.84 |
| 23.800 | 0.02 | 8.29 | 8.47 | 0.00 | 0.09 | 754 | 93.83 |
| 23.850 | 0.02 | 8.16 | 8.34 | 0.00 | 0.09 | 742 | 93.82 |
| 23.900 | 0.02 | 8.03 | 8.21 | 0.00 | 0.09 | 731 | 93.81 |
| 23.950 | 0.02 | 7.89 | 8.07 | 0.00 | 0.09 | 719 | 93.80 |
| 24.000 | 0.02 | 7.76 | 7.94 | 0.00 | 0.09 | 707 | 93.78 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 0.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 0.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 0.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 0.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 1.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 1.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 1.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 1.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 1.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 1.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 1.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 1.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 1.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 1.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 1.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 2.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 2.050 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 2.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 2.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 2.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 2.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 2.800 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 2.850 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 2.900 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 2.950 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 3.000 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 3.050 | 0.04 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 3.100 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 3.150 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 3.200 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 3.250 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 3.300 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 3.350 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.400 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.450 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.500 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.550 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.600 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.650 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.700 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.750 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.800 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.850 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 3.950 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 4.000 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 4.050 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 4.100 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 4.150 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 4.250 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 4.300 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 4.350 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 4.400 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 4.450 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 4.500 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 4.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 4.600 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.650 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.700 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 4.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.100 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.150 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.200 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.250 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 5.300 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.350 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.400 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.450 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.500 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.550 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.600 | 0.06 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 5.650 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 5.700 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 5.750 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 5.800 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 5.850 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 5.900 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 5.950 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 6.000 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 6.050 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 6.100 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 6.150 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 6.200 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 6.250 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 6.350 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 6.400 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 6.450 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 6.500 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 6.550 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 6.600 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 6.650 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 6.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 6.750 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 6.800 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 6.850 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 6.900 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 6.950 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 7.000 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 7.050 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 7.100 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 7.150 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 7.200 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 7.250 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 7.300 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 7.350 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 7.400 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 7.450 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 7.500 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 7.550 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 7.600 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 7.650 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 7.700 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 8 | 93.02 |
| 7.750 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 8 | 93.02 |
| 7.800 | 0.09 | 0.01 | 0.19 | 0.00 | 0.09 | 9 | 93.02 |
| 7.850 | 0.09 | 0.01 | 0.19 | 0.00 | 0.09 | 9 | 93.02 |
| 7.900 | 0.09 | 0.02 | 0.20 | 0.00 | 0.09 | 10 | 93.02 |
| 7.950 | 0.10 | 0.03 | 0.21 | 0.00 | 0.09 | 11 | 93.02 |
| 8.000 | 0.10 | 0.04 | 0.22 | 0.00 | 0.09 | 12 | 93.02 |
| 8.050 | 0.10 | 0.06 | 0.24 | 0.00 | 0.09 | 13 | 93.03 |
| 8.100 | 0.10 | 0.07 | 0.25 | 0.00 | 0.09 | 15 | 93.03 |
| 8.150 | 0.10 | 0.10 | 0.28 | 0.00 | 0.09 | 17 | 93.03 |
| 8.200 | 0.10 | 0.12 | 0.30 | 0.00 | 0.09 | 19 | 93.04 |
| 8.250 | 0.11 | 0.15 | 0.33 | 0.00 | 0.09 | 22 | 93.04 |
| 8.300 | 0.11 | 0.18 | 0.36 | 0.00 | 0.09 | 25 | 93.05 |
| 8.350 | 0.11 | 0.22 | 0.40 | 0.00 | 0.09 | 28 | 93.06 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.11 | 0.26 | 0.44 | 0.00 | 0.09 | 32 | 93.06 |
| 8.450 | 0.11 | 0.31 | 0.49 | 0.00 | 0.09 | 36 | 93.07 |
| 8.500 | 0.12 | 0.36 | 0.54 | 0.00 | 0.09 | 41 | 93.08 |
| 8.550 | 0.12 | 0.42 | 0.60 | 0.00 | 0.09 | 46 | 93.09 |
| 8.600 | 0.12 | 0.48 | 0.66 | 0.00 | 0.09 | 51 | 93.10 |
| 8.650 | 0.12 | 0.55 | 0.73 | 0.00 | 0.09 | 56 | 93.11 |
| 8.700 | 0.13 | 0.61 | 0.79 | 0.00 | 0.09 | 61 | 93.12 |
| 8.750 | 0.13 | 0.69 | 0.87 | 0.00 | 0.09 | 66 | 93.13 |
| 8.800 | 0.13 | 0.77 | 0.95 | 0.00 | 0.09 | 72 | 93.14 |
| 8.850 | 0.13 | 0.85 | 1.03 | 0.00 | 0.09 | 78 | 93.15 |
| 8.900 | 0.14 | 0.94 | 1.12 | 0.00 | 0.09 | 84 | 93.17 |
| 8.950 | 0.14 | 1.03 | 1.21 | 0.00 | 0.09 | 93 | 93.18 |
| 9.000 | 0.14 | 1.13 | 1.31 | 0.00 | 0.09 | 107 | 93.19 |
| 9.050 | 0.14 | 1.23 | 1.41 | 0.00 | 0.09 | 119 | 93.20 |
| 9.100 | 0.14 | 1.33 | 1.51 | 0.00 | 0.09 | 128 | 93.21 |
| 9.150 | 0.15 | 1.44 | 1.62 | 0.00 | 0.09 | 138 | 93.22 |
| 9.200 | 0.15 | 1.56 | 1.74 | 0.00 | 0.09 | 148 | 93.23 |
| 9.250 | 0.15 | 1.68 | 1.86 | 0.00 | 0.09 | 159 | 93.24 |
| 9.300 | 0.15 | 1.80 | 1.98 | 0.00 | 0.09 | 170 | 93.26 |
| 9.350 | 0.16 | 1.93 | 2.11 | 0.00 | 0.09 | 182 | 93.27 |
| 9.400 | 0.16 | 2.06 | 2.24 | 0.00 | 0.09 | 194 | 93.28 |
| 9.450 | 0.16 | 2.20 | 2.38 | 0.00 | 0.09 | 206 | 93.29 |
| 9.500 | 0.16 | 2.34 | 2.52 | 0.00 | 0.09 | 219 | 93.30 |
| 9.550 | 0.16 | 2.49 | 2.67 | 0.00 | 0.09 | 232 | 93.32 |
| 9.600 | 0.17 | 2.64 | 2.82 | 0.00 | 0.09 | 246 | 93.33 |
| 9.650 | 0.17 | 2.79 | 2.97 | 0.00 | 0.09 | 259 | 93.34 |
| 9.700 | 0.17 | 2.95 | 3.13 | 0.00 | 0.09 | 274 | 93.36 |
| 9.750 | 0.17 | 3.12 | 3.30 | 0.00 | 0.09 | 289 | 93.37 |
| 9.800 | 0.18 | 3.29 | 3.47 | 0.00 | 0.09 | 304 | 93.39 |
| 9.850 | 0.18 | 3.46 | 3.64 | 0.00 | 0.09 | 319 | 93.40 |
| 9.900 | 0.18 | 3.64 | 3.82 | 0.00 | 0.09 | 335 | 93.42 |
| 9.950 | 0.18 | 3.82 | 4.00 | 0.00 | 0.09 | 352 | 93.43 |
| 10.000 | 0.18 | 4.01 | 4.19 | 0.00 | 0.09 | 369 | 93.45 |
| 10.050 | 0.19 | 4.20 | 4.38 | 0.00 | 0.09 | 386 | 93.47 |
| 10.100 | 0.19 | 4.40 | 4.58 | 0.00 | 0.09 | 404 | 93.49 |
| 10.150 | 0.19 | 4.60 | 4.78 | 0.00 | 0.09 | 422 | 93.50 |
| 10.200 | 0.20 | 4.82 | 5.00 | 0.00 | 0.09 | 442 | 93.52 |
| 10.250 | 0.20 | 5.04 | 5.22 | 0.00 | 0.09 | 462 | 93.54 |
| 10.300 | 0.21 | 5.27 | 5.45 | 0.00 | 0.09 | 483 | 93.56 |
| 10.350 | 0.21 | 5.52 | 5.70 | 0.00 | 0.09 | 504 | 93.58 |
| 10.400 | 0.22 | 5.77 | 5.95 | 0.00 | 0.09 | 527 | 93.61 |
| 10.450 | 0.22 | 6.03 | 6.21 | 0.00 | 0.09 | 551 | 93.63 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.23 | 6.30 | 6.48 | 0.00 | 0.09 | 575 | 93.65 |
| 10.550 | 0.23 | 6.58 | 6.76 | 0.00 | 0.09 | 600 | 93.68 |
| 10.600 | 0.24 | 6.87 | 7.05 | 0.00 | 0.09 | 626 | 93.70 |
| 10.650 | 0.24 | 7.16 | 7.34 | 0.00 | 0.09 | 653 | 93.73 |
| 10.700 | 0.25 | 7.47 | 7.65 | 0.00 | 0.09 | 681 | 93.76 |
| 10.750 | 0.25 | 7.79 | 7.97 | 0.00 | 0.09 | 709 | 93.79 |
| 10.800 | 0.26 | 8.12 | 8.30 | 0.00 | 0.09 | 738 | 93.81 |
| 10.850 | 0.26 | 8.45 | 8.63 | 0.00 | 0.09 | 769 | 93.84 |
| 10.900 | 0.27 | 8.80 | 8.98 | 0.00 | 0.09 | 800 | 93.88 |
| 10.950 | 0.27 | 9.15 | 9.33 | 0.00 | 0.09 | 832 | 93.91 |
| 11.000 | 0.27 | 9.51 | 9.69 | 0.00 | 0.09 | 864 | 93.94 |
| 11.050 | 0.28 | 9.89 | 10.07 | 0.00 | 0.09 | 898 | 93.97 |
| 11.100 | 0.29 | 10.29 | 10.47 | 0.00 | 0.09 | 934 | 94.01 |
| 11.150 | 0.31 | 10.71 | 10.89 | 0.00 | 0.09 | 972 | 94.04 |
| 11.200 | 0.33 | 11.16 | 11.34 | 0.00 | 0.09 | 1,013 | 94.08 |
| 11.250 | 0.34 | 11.65 | 11.83 | 0.00 | 0.09 | 1,056 | 94.13 |
| 11.300 | 0.36 | 12.17 | 12.35 | 0.00 | 0.09 | 1,103 | 94.17 |
| 11.350 | 0.38 | 12.73 | 12.91 | 0.00 | 0.09 | 1,154 | 94.22 |
| 11.400 | 0.40 | 13.32 | 13.50 | 0.00 | 0.09 | 1,207 | 94.28 |
| 11.450 | 0.41 | 13.95 | 14.13 | 0.00 | 0.09 | 1,264 | 94.33 |
| 11.500 | 0.43 | 14.62 | 14.80 | 0.00 | 0.09 | 1,324 | 94.39 |
| 11.550 | 0.49 | 15.36 | 15.54 | 0.00 | 0.09 | 1,391 | 94.46 |
| 11.600 | 0.58 | 16.25 | 16.43 | 0.00 | 0.09 | 1,471 | 94.54 |
| 11.650 | 0.71 | 17.36 | 17.54 | 0.00 | 0.09 | 1,571 | 94.63 |
| 11.700 | 0.88 | 18.77 | 18.95 | 0.00 | 0.09 | 1,697 | 94.76 |
| 11.750 | 1.04 | 20.51 | 20.69 | 0.00 | 0.09 | 1,854 | 94.91 |
| 11.800 | 1.22 | 22.58 | 22.76 | 0.00 | 0.09 | 2,041 | 95.10 |
| 11.850 | 1.38 | 24.04 | 25.18 | 0.00 | 0.57 | 2,215 | 95.22 |
| 11.900 | 1.57 | 23.52 | 26.98 | 0.00 | 1.73 | 2,273 | 95.25 |
| 11.950 | 2.05 | 23.48 | 27.14 | 0.00 | 1.83 | 2,278 | 95.25 |
| 12.000 | 2.85 | 23.13 | 28.38 | 0.00 | 2.62 | 2,318 | 95.27 |
| 12.050 | 3.14 | 22.92 | 29.11 | 0.00 | 3.09 | 2,341 | 95.28 |
| 12.100 | 3.22 | 22.87 | 29.27 | 0.00 | 3.20 | 2,346 | 95.29 |
| 12.150 | 2.82 | 22.97 | 28.91 | 0.00 | 2.97 | 2,335 | 95.28 |
| 12.200 | 2.06 | 23.27 | 27.86 | 0.00 | 2.29 | 2,301 | 95.26 |
| 12.250 | 1.68 | 23.51 | 27.02 | 0.00 | 1.75 | 2,274 | 95.25 |
| 12.300 | 1.43 | 23.62 | 26.63 | 0.00 | 1.50 | 2,261 | 95.24 |
| 12.350 | 1.26 | 23.71 | 26.31 | 0.00 | 1.30 | 2,251 | 95.24 |
| 12.400 | 1.07 | 23.79 | 26.04 | 0.00 | 1.12 | 2,242 | 95.24 |
| 12.450 | 0.91 | 23.87 | 25.77 | 0.00 | 0.95 | 2,234 | 95.23 |
| 12.500 | 0.73 | 23.94 | 25.50 | 0.00 | 0.78 | 2,225 | 95.23 |
| 12.550 | 0.61 | 24.01 | 25.28 | 0.00 | 0.63 | 2,218 | 95.22 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.50 | 24.05 | 25.12 | 0.00 | 0.53 | 2,213 | 95.22 |
| 12.650 | 0.45 | 24.09 | 25.00 | 0.00 | 0.46 | 2,209 | 95.22 |
| 12.700 | 0.42 | 24.10 | 24.96 | 0.00 | 0.43 | 2,208 | 95.22 |
| 12.750 | 0.40 | 24.11 | 24.92 | 0.00 | 0.41 | 2,206 | 95.22 |
| 12.800 | 0.38 | 24.12 | 24.89 | 0.00 | 0.39 | 2,205 | 95.22 |
| 12.850 | 0.37 | 24.12 | 24.87 | 0.00 | 0.37 | 2,205 | 95.22 |
| 12.900 | 0.35 | 24.13 | 24.84 | 0.00 | 0.35 | 2,204 | 95.22 |
| 12.950 | 0.33 | 24.14 | 24.81 | 0.00 | 0.33 | 2,203 | 95.22 |
| 13.000 | 0.31 | 24.15 | 24.78 | 0.00 | 0.32 | 2,202 | 95.22 |
| 13.050 | 0.30 | 24.16 | 24.76 | 0.00 | 0.30 | 2,201 | 95.22 |
| 13.100 | 0.29 | 24.16 | 24.74 | 0.00 | 0.29 | 2,200 | 95.21 |
| 13.150 | 0.28 | 24.17 | 24.72 | 0.00 | 0.28 | 2,200 | 95.21 |
| 13.200 | 0.27 | 24.17 | 24.72 | 0.00 | 0.27 | 2,200 | 95.21 |
| 13.250 | 0.27 | 24.17 | 24.71 | 0.00 | 0.27 | 2,199 | 95.21 |
| 13.300 | 0.26 | 24.17 | 24.70 | 0.00 | 0.26 | 2,199 | 95.21 |
| 13.350 | 0.26 | 24.17 | 24.69 | 0.00 | 0.26 | 2,199 | 95.21 |
| 13.400 | 0.25 | 24.18 | 24.69 | 0.00 | 0.25 | 2,199 | 95.21 |
| 13.450 | 0.25 | 24.18 | 24.68 | 0.00 | 0.25 | 2,199 | 95.21 |
| 13.500 | 0.24 | 24.18 | 24.67 | 0.00 | 0.25 | 2,198 | 95.21 |
| 13.550 | 0.24 | 24.18 | 24.66 | 0.00 | 0.24 | 2,198 | 95.21 |
| 13.600 | 0.23 | 24.18 | 24.66 | 0.00 | 0.24 | 2,198 | 95.21 |
| 13.650 | 0.23 | 24.19 | 24.65 | 0.00 | 0.23 | 2,198 | 95.21 |
| 13.700 | 0.23 | 24.19 | 24.64 | 0.00 | 0.23 | 2,197 | 95.21 |
| 13.750 | 0.22 | 24.19 | 24.63 | 0.00 | 0.22 | 2,197 | 95.21 |
| 13.800 | 0.22 | 24.19 | 24.63 | 0.00 | 0.22 | 2,197 | 95.21 |
| 13.850 | 0.21 | 24.19 | 24.62 | 0.00 | 0.21 | 2,197 | 95.21 |
| 13.900 | 0.21 | 24.20 | 24.61 | 0.00 | 0.21 | 2,196 | 95.21 |
| 13.950 | 0.20 | 24.20 | 24.61 | 0.00 | 0.20 | 2,196 | 95.21 |
| 14.000 | 0.20 | 24.20 | 24.60 | 0.00 | 0.20 | 2,196 | 95.21 |
| 14.050 | 0.19 | 24.20 | 24.59 | 0.00 | 0.19 | 2,196 | 95.21 |
| 14.100 | 0.19 | 24.20 | 24.59 | 0.00 | 0.19 | 2,196 | 95.21 |
| 14.150 | 0.19 | 24.21 | 24.58 | 0.00 | 0.19 | 2,195 | 95.21 |
| 14.200 | 0.18 | 24.21 | 24.58 | 0.00 | 0.19 | 2,195 | 95.21 |
| 14.250 | 0.18 | 24.21 | 24.57 | 0.00 | 0.18 | 2,195 | 95.21 |
| 14.300 | 0.18 | 24.21 | 24.57 | 0.00 | 0.18 | 2,195 | 95.21 |
| 14.350 | 0.18 | 24.21 | 24.57 | 0.00 | 0.18 | 2,195 | 95.21 |
| 14.400 | 0.18 | 24.21 | 24.56 | 0.00 | 0.18 | 2,195 | 95.21 |
| 14.450 | 0.17 | 24.21 | 24.56 | 0.00 | 0.17 | 2,195 | 95.21 |
| 14.500 | 0.17 | 24.21 | 24.56 | 0.00 | 0.17 | 2,195 | 95.21 |
| 14.550 | 0.17 | 24.21 | 24.55 | 0.00 | 0.17 | 2,195 | 95.21 |
| 14.600 | 0.17 | 24.21 | 24.55 | 0.00 | 0.17 | 2,194 | 95.21 |
| 14.650 | 0.16 | 24.22 | 24.55 | 0.00 | 0.17 | 2,194 | 95.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.16 | 24.22 | 24.54 | 0.00 | 0.16 | 2,194 | 95.21 |
| 14.750 | 0.16 | 24.22 | 24.54 | 0.00 | 0.16 | 2,194 | 95.21 |
| 14.800 | 0.16 | 24.22 | 24.54 | 0.00 | 0.16 | 2,194 | 95.21 |
| 14.850 | 0.16 | 24.22 | 24.53 | 0.00 | 0.16 | 2,194 | 95.21 |
| 14.900 | 0.15 | 24.22 | 24.53 | 0.00 | 0.15 | 2,194 | 95.21 |
| 14.950 | 0.15 | 24.22 | 24.53 | 0.00 | 0.15 | 2,194 | 95.21 |
| 15.000 | 0.15 | 24.22 | 24.52 | 0.00 | 0.15 | 2,194 | 95.21 |
| 15.050 | 0.15 | 24.22 | 24.52 | 0.00 | 0.15 | 2,193 | 95.21 |
| 15.100 | 0.14 | 24.22 | 24.51 | 0.00 | 0.15 | 2,193 | 95.21 |
| 15.150 | 0.14 | 24.23 | 24.51 | 0.00 | 0.14 | 2,193 | 95.21 |
| 15.200 | 0.14 | 24.23 | 24.51 | 0.00 | 0.14 | 2,193 | 95.21 |
| 15.250 | 0.14 | 24.23 | 24.50 | 0.00 | 0.14 | 2,193 | 95.21 |
| 15.300 | 0.14 | 24.23 | 24.50 | 0.00 | 0.14 | 2,193 | 95.21 |
| 15.350 | 0.13 | 24.23 | 24.50 | 0.00 | 0.13 | 2,193 | 95.21 |
| 15.400 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,193 | 95.21 |
| 15.450 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 15.500 | 0.13 | 24.23 | 24.49 | 0.00 | 0.13 | 2,192 | 95.21 |
| 15.550 | 0.12 | 24.23 | 24.48 | 0.00 | 0.13 | 2,192 | 95.21 |
| 15.600 | 0.12 | 24.23 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 15.650 | 0.12 | 24.24 | 24.48 | 0.00 | 0.12 | 2,192 | 95.21 |
| 15.700 | 0.12 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |
| 15.750 | 0.12 | 24.24 | 24.47 | 0.00 | 0.12 | 2,192 | 95.21 |
| 15.800 | 0.11 | 24.24 | 24.47 | 0.00 | 0.11 | 2,192 | 95.21 |
| 15.850 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,192 | 95.21 |
| 15.900 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,191 | 95.21 |
| 15.950 | 0.11 | 24.24 | 24.46 | 0.00 | 0.11 | 2,191 | 95.21 |
| 16.000 | 0.10 | 24.24 | 24.45 | 0.00 | 0.11 | 2,191 | 95.21 |
| 16.050 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.100 | 0.10 | 24.24 | 24.45 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.150 | 0.10 | 24.24 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.200 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.250 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.300 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.350 | 0.10 | 24.25 | 24.44 | 0.00 | 0.10 | 2,191 | 95.21 |
| 16.400 | 0.09 | 24.25 | 24.44 | 0.00 | 0.09 | 2,191 | 95.21 |
| 16.450 | 0.09 | 24.25 | 24.44 | 0.00 | 0.09 | 2,191 | 95.21 |
| 16.500 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 16.550 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 16.600 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 16.650 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,191 | 95.21 |
| 16.700 | 0.09 | 24.25 | 24.43 | 0.00 | 0.09 | 2,190 | 95.21 |
| 16.750 | 0.09 | 24.24 | 24.42 | 0.00 | 0.09 | 2,190 | 95.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.09 | 24.24 | 24.42 | 0.00 | 0.09 | 2,190 | 95.21 |
| 16.850 | 0.09 | 24.23 | 24.41 | 0.00 | 0.09 | 2,189 | 95.21 |
| 16.900 | 0.09 | 24.22 | 24.40 | 0.00 | 0.09 | 2,188 | 95.21 |
| 16.950 | 0.08 | 24.21 | 24.39 | 0.00 | 0.09 | 2,187 | 95.21 |
| 17.000 | 0.08 | 24.20 | 24.38 | 0.00 | 0.09 | 2,186 | 95.21 |
| 17.050 | 0.08 | 24.18 | 24.36 | 0.00 | 0.09 | 2,185 | 95.21 |
| 17.100 | 0.08 | 24.17 | 24.35 | 0.00 | 0.09 | 2,183 | 95.21 |
| 17.150 | 0.08 | 24.15 | 24.33 | 0.00 | 0.09 | 2,182 | 95.21 |
| 17.200 | 0.08 | 24.13 | 24.31 | 0.00 | 0.09 | 2,180 | 95.20 |
| 17.250 | 0.08 | 24.11 | 24.29 | 0.00 | 0.09 | 2,178 | 95.20 |
| 17.300 | 0.08 | 24.08 | 24.26 | 0.00 | 0.09 | 2,175 | 95.20 |
| 17.350 | 0.08 | 24.05 | 24.23 | 0.00 | 0.09 | 2,173 | 95.20 |
| 17.400 | 0.08 | 24.03 | 24.21 | 0.00 | 0.09 | 2,170 | 95.20 |
| 17.450 | 0.07 | 24.00 | 24.18 | 0.00 | 0.09 | 2,166 | 95.20 |
| 17.500 | 0.07 | 23.96 | 24.14 | 0.00 | 0.09 | 2,162 | 95.20 |
| 17.550 | 0.07 | 23.93 | 24.11 | 0.00 | 0.09 | 2,157 | 95.19 |
| 17.600 | 0.07 | 23.89 | 24.07 | 0.00 | 0.09 | 2,151 | 95.19 |
| 17.650 | 0.07 | 23.85 | 24.03 | 0.00 | 0.09 | 2,146 | 95.19 |
| 17.700 | 0.07 | 23.81 | 23.99 | 0.00 | 0.09 | 2,140 | 95.19 |
| 17.750 | 0.07 | 23.77 | 23.95 | 0.00 | 0.09 | 2,134 | 95.18 |
| 17.800 | 0.07 | 23.73 | 23.91 | 0.00 | 0.09 | 2,128 | 95.18 |
| 17.850 | 0.07 | 23.68 | 23.86 | 0.00 | 0.09 | 2,122 | 95.18 |
| 17.900 | 0.07 | 23.64 | 23.82 | 0.00 | 0.09 | 2,117 | 95.17 |
| 17.950 | 0.06 | 23.59 | 23.77 | 0.00 | 0.09 | 2,114 | 95.17 |
| 18.000 | 0.06 | 23.53 | 23.71 | 0.00 | 0.09 | 2,110 | 95.17 |
| 18.050 | 0.06 | 23.48 | 23.66 | 0.00 | 0.09 | 2,106 | 95.16 |
| 18.100 | 0.06 | 23.42 | 23.60 | 0.00 | 0.09 | 2,102 | 95.16 |
| 18.150 | 0.06 | 23.37 | 23.55 | 0.00 | 0.09 | 2,098 | 95.15 |
| 18.200 | 0.06 | 23.31 | 23.49 | 0.00 | 0.09 | 2,094 | 95.15 |
| 18.250 | 0.06 | 23.25 | 23.43 | 0.00 | 0.09 | 2,090 | 95.15 |
| 18.300 | 0.06 | 23.20 | 23.38 | 0.00 | 0.09 | 2,085 | 95.14 |
| 18.350 | 0.06 | 23.14 | 23.32 | 0.00 | 0.09 | 2,081 | 95.14 |
| 18.400 | 0.06 | 23.08 | 23.26 | 0.00 | 0.09 | 2,077 | 95.13 |
| 18.450 | 0.06 | 23.02 | 23.20 | 0.00 | 0.09 | 2,073 | 95.13 |
| 18.500 | 0.06 | 22.96 | 23.14 | 0.00 | 0.09 | 2,068 | 95.12 |
| 18.550 | 0.06 | 22.90 | 23.08 | 0.00 | 0.09 | 2,064 | 95.12 |
| 18.600 | 0.06 | 22.84 | 23.02 | 0.00 | 0.09 | 2,059 | 95.12 |
| 18.650 | 0.06 | 22.77 | 22.95 | 0.00 | 0.09 | 2,055 | 95.11 |
| 18.700 | 0.06 | 22.71 | 22.89 | 0.00 | 0.09 | 2,050 | 95.11 |
| 18.750 | 0.06 | 22.65 | 22.83 | 0.00 | 0.09 | 2,046 | 95.10 |
| 18.800 | 0.06 | 22.58 | 22.76 | 0.00 | 0.09 | 2,041 | 95.10 |
| 18.850 | 0.06 | 22.52 | 22.70 | 0.00 | 0.09 | 2,035 | 95.09 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.06 | 22.45 | 22.63 | 0.00 | 0.09 | 2,029 | 95.09 |
| 18.950 | 0.06 | 22.39 | 22.57 | 0.00 | 0.09 | 2,023 | 95.08 |
| 19.000 | 0.06 | 22.32 | 22.50 | 0.00 | 0.09 | 2,017 | 95.07 |
| 19.050 | 0.06 | 22.26 | 22.44 | 0.00 | 0.09 | 2,011 | 95.07 |
| 19.100 | 0.06 | 22.19 | 22.37 | 0.00 | 0.09 | 2,005 | 95.06 |
| 19.150 | 0.06 | 22.12 | 22.30 | 0.00 | 0.09 | 1,999 | 95.06 |
| 19.200 | 0.06 | 22.05 | 22.23 | 0.00 | 0.09 | 1,993 | 95.05 |
| 19.250 | 0.06 | 21.98 | 22.16 | 0.00 | 0.09 | 1,987 | 95.04 |
| 19.300 | 0.05 | 21.91 | 22.09 | 0.00 | 0.09 | 1,980 | 95.04 |
| 19.350 | 0.05 | 21.84 | 22.02 | 0.00 | 0.09 | 1,974 | 95.03 |
| 19.400 | 0.05 | 21.77 | 21.95 | 0.00 | 0.09 | 1,968 | 95.03 |
| 19.450 | 0.05 | 21.70 | 21.88 | 0.00 | 0.09 | 1,961 | 95.02 |
| 19.500 | 0.05 | 21.63 | 21.81 | 0.00 | 0.09 | 1,955 | 95.01 |
| 19.550 | 0.05 | 21.56 | 21.74 | 0.00 | 0.09 | 1,948 | 95.01 |
| 19.600 | 0.05 | 21.48 | 21.66 | 0.00 | 0.09 | 1,942 | 95.00 |
| 19.650 | 0.05 | 21.41 | 21.59 | 0.00 | 0.09 | 1,935 | 94.99 |
| 19.700 | 0.05 | 21.33 | 21.51 | 0.00 | 0.09 | 1,928 | 94.99 |
| 19.750 | 0.05 | 21.26 | 21.44 | 0.00 | 0.09 | 1,921 | 94.98 |
| 19.800 | 0.05 | 21.18 | 21.36 | 0.00 | 0.09 | 1,915 | 94.97 |
| 19.850 | 0.05 | 21.11 | 21.29 | 0.00 | 0.09 | 1,908 | 94.97 |
| 19.900 | 0.05 | 21.03 | 21.21 | 0.00 | 0.09 | 1,901 | 94.96 |
| 19.950 | 0.05 | 20.95 | 21.13 | 0.00 | 0.09 | 1,894 | 94.95 |
| 20.000 | 0.05 | 20.88 | 21.06 | 0.00 | 0.09 | 1,887 | 94.95 |
| 20.050 | 0.05 | 20.80 | 20.98 | 0.00 | 0.09 | 1,880 | 94.94 |
| 20.100 | 0.05 | 20.72 | 20.90 | 0.00 | 0.09 | 1,873 | 94.93 |
| 20.150 | 0.05 | 20.64 | 20.82 | 0.00 | 0.09 | 1,866 | 94.92 |
| 20.200 | 0.05 | 20.56 | 20.74 | 0.00 | 0.09 | 1,858 | 94.92 |
| 20.250 | 0.05 | 20.48 | 20.66 | 0.00 | 0.09 | 1,851 | 94.91 |
| 20.300 | 0.05 | 20.40 | 20.58 | 0.00 | 0.09 | 1,844 | 94.90 |
| 20.350 | 0.05 | 20.32 | 20.50 | 0.00 | 0.09 | 1,837 | 94.90 |
| 20.400 | 0.05 | 20.24 | 20.42 | 0.00 | 0.09 | 1,829 | 94.89 |
| 20.450 | 0.05 | 20.15 | 20.33 | 0.00 | 0.09 | 1,822 | 94.88 |
| 20.500 | 0.05 | 20.07 | 20.25 | 0.00 | 0.09 | 1,815 | 94.87 |
| 20.550 | 0.05 | 19.99 | 20.17 | 0.00 | 0.09 | 1,807 | 94.87 |
| 20.600 | 0.05 | 19.91 | 20.09 | 0.00 | 0.09 | 1,800 | 94.86 |
| 20.650 | 0.05 | 19.82 | 20.00 | 0.00 | 0.09 | 1,792 | 94.85 |
| 20.700 | 0.05 | 19.74 | 19.92 | 0.00 | 0.09 | 1,784 | 94.84 |
| 20.750 | 0.05 | 19.65 | 19.83 | 0.00 | 0.09 | 1,777 | 94.84 |
| 20.800 | 0.05 | 19.57 | 19.75 | 0.00 | 0.09 | 1,769 | 94.83 |
| 20.850 | 0.05 | 19.48 | 19.66 | 0.00 | 0.09 | 1,761 | 94.82 |
| 20.900 | 0.05 | 19.40 | 19.58 | 0.00 | 0.09 | 1,754 | 94.81 |
| 20.950 | 0.05 | 19.31 | 19.49 | 0.00 | 0.09 | 1,746 | 94.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.05 | 19.22 | 19.40 | 0.00 | 0.09 | 1,738 | 94.80 |
| 21.050 | 0.05 | 19.13 | 19.31 | 0.00 | 0.09 | 1,730 | 94.79 |
| 21.100 | 0.05 | 19.05 | 19.23 | 0.00 | 0.09 | 1,722 | 94.78 |
| 21.150 | 0.05 | 18.96 | 19.14 | 0.00 | 0.09 | 1,714 | 94.78 |
| 21.200 | 0.05 | 18.87 | 19.05 | 0.00 | 0.09 | 1,706 | 94.77 |
| 21.250 | 0.05 | 18.78 | 18.96 | 0.00 | 0.09 | 1,698 | 94.76 |
| 21.300 | 0.05 | 18.69 | 18.87 | 0.00 | 0.09 | 1,690 | 94.75 |
| 21.350 | 0.04 | 18.60 | 18.78 | 0.00 | 0.09 | 1,682 | 94.74 |
| 21.400 | 0.04 | 18.51 | 18.69 | 0.00 | 0.09 | 1,674 | 94.74 |
| 21.450 | 0.04 | 18.42 | 18.60 | 0.00 | 0.09 | 1,666 | 94.73 |
| 21.500 | 0.04 | 18.33 | 18.51 | 0.00 | 0.09 | 1,658 | 94.72 |
| 21.550 | 0.04 | 18.24 | 18.42 | 0.00 | 0.09 | 1,649 | 94.71 |
| 21.600 | 0.04 | 18.14 | 18.32 | 0.00 | 0.09 | 1,641 | 94.70 |
| 21.650 | 0.04 | 18.05 | 18.23 | 0.00 | 0.09 | 1,633 | 94.70 |
| 21.700 | 0.04 | 17.96 | 18.14 | 0.00 | 0.09 | 1,624 | 94.69 |
| 21.750 | 0.04 | 17.87 | 18.05 | 0.00 | 0.09 | 1,616 | 94.68 |
| 21.800 | 0.04 | 17.77 | 17.95 | 0.00 | 0.09 | 1,608 | 94.67 |
| 21.850 | 0.04 | 17.68 | 17.86 | 0.00 | 0.09 | 1,599 | 94.66 |
| 21.900 | 0.04 | 17.58 | 17.76 | 0.00 | 0.09 | 1,591 | 94.65 |
| 21.950 | 0.04 | 17.49 | 17.67 | 0.00 | 0.09 | 1,582 | 94.65 |
| 22.000 | 0.04 | 17.39 | 17.57 | 0.00 | 0.09 | 1,573 | 94.64 |
| 22.050 | 0.04 | 17.30 | 17.48 | 0.00 | 0.09 | 1,565 | 94.63 |
| 22.100 | 0.04 | 17.20 | 17.38 | 0.00 | 0.09 | 1,556 | 94.62 |
| 22.150 | 0.04 | 17.10 | 17.28 | 0.00 | 0.09 | 1,547 | 94.61 |
| 22.200 | 0.04 | 17.01 | 17.19 | 0.00 | 0.09 | 1,539 | 94.60 |
| 22.250 | 0.04 | 16.91 | 17.09 | 0.00 | 0.09 | 1,530 | 94.59 |
| 22.300 | 0.04 | 16.81 | 16.99 | 0.00 | 0.09 | 1,521 | 94.59 |
| 22.350 | 0.04 | 16.71 | 16.89 | 0.00 | 0.09 | 1,512 | 94.58 |
| 22.400 | 0.04 | 16.61 | 16.79 | 0.00 | 0.09 | 1,503 | 94.57 |
| 22.450 | 0.04 | 16.51 | 16.69 | 0.00 | 0.09 | 1,494 | 94.56 |
| 22.500 | 0.04 | 16.41 | 16.59 | 0.00 | 0.09 | 1,485 | 94.55 |
| 22.550 | 0.04 | 16.31 | 16.49 | 0.00 | 0.09 | 1,476 | 94.54 |
| 22.600 | 0.04 | 16.21 | 16.39 | 0.00 | 0.09 | 1,467 | 94.53 |
| 22.650 | 0.04 | 16.11 | 16.29 | 0.00 | 0.09 | 1,458 | 94.52 |
| 22.700 | 0.04 | 16.01 | 16.19 | 0.00 | 0.09 | 1,449 | 94.51 |
| 22.750 | 0.04 | 15.91 | 16.09 | 0.00 | 0.09 | 1,440 | 94.51 |
| 22.800 | 0.04 | 15.80 | 15.98 | 0.00 | 0.09 | 1,430 | 94.50 |
| 22.850 | 0.04 | 15.70 | 15.88 | 0.00 | 0.09 | 1,421 | 94.49 |
| 22.900 | 0.04 | 15.60 | 15.78 | 0.00 | 0.09 | 1,412 | 94.48 |
| 22.950 | 0.04 | 15.49 | 15.67 | 0.00 | 0.09 | 1,402 | 94.47 |
| 23.000 | 0.04 | 15.39 | 15.57 | 0.00 | 0.09 | 1,393 | 94.46 |
| 23.050 | 0.04 | 15.28 | 15.46 | 0.00 | 0.09 | 1,384 | 94.45 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 24" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.04 | 15.18 | 15.36 | 0.00 | 0.09 | 1,374 | 94.44 |
| 23.150 | 0.04 | 15.07 | 15.25 | 0.00 | 0.09 | 1,365 | 94.43 |
| 23.200 | 0.04 | 14.97 | 15.15 | 0.00 | 0.09 | 1,355 | 94.42 |
| 23.250 | 0.04 | 14.86 | 15.04 | 0.00 | 0.09 | 1,345 | 94.41 |
| 23.300 | 0.04 | 14.75 | 14.93 | 0.00 | 0.09 | 1,336 | 94.40 |
| 23.350 | 0.04 | 14.65 | 14.83 | 0.00 | 0.09 | 1,326 | 94.39 |
| 23.400 | 0.04 | 14.54 | 14.72 | 0.00 | 0.09 | 1,316 | 94.38 |
| 23.450 | 0.04 | 14.43 | 14.61 | 0.00 | 0.09 | 1,307 | 94.37 |
| 23.500 | 0.04 | 14.32 | 14.50 | 0.00 | 0.09 | 1,297 | 94.36 |
| 23.550 | 0.04 | 14.21 | 14.39 | 0.00 | 0.09 | 1,287 | 94.36 |
| 23.600 | 0.04 | 14.10 | 14.28 | 0.00 | 0.09 | 1,277 | 94.35 |
| 23.650 | 0.03 | 13.99 | 14.17 | 0.00 | 0.09 | 1,267 | 94.34 |
| 23.700 | 0.03 | 13.88 | 14.06 | 0.00 | 0.09 | 1,257 | 94.33 |
| 23.750 | 0.03 | 13.77 | 13.95 | 0.00 | 0.09 | 1,247 | 94.32 |
| 23.800 | 0.03 | 13.66 | 13.84 | 0.00 | 0.09 | 1,237 | 94.31 |
| 23.850 | 0.03 | 13.55 | 13.73 | 0.00 | 0.09 | 1,227 | 94.30 |
| 23.900 | 0.03 | 13.44 | 13.62 | 0.00 | 0.09 | 1,217 | 94.29 |
| 23.950 | 0.03 | 13.32 | 13.50 | 0.00 | 0.09 | 1,207 | 94.28 |
| 24.000 | 0.03 | 13.21 | 13.39 | 0.00 | 0.09 | 1,197 | 94.27 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: 24" Depth Green Roof (IN)
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Summary for Hydrograph Addition at '24" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2C |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|----------------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-2C | 3,814 | 12.100 | 0.94 |
| Flow (In) | 24" Depth Green Roof | 3,814 | 12.100 | 0.94 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: 24" Depth Green Roof (IN)

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at '24" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2C |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2C | 7,332 | 12.100 | 1.76 |
| Flow (In) | 24" Depth Green Roof | 7,332 | 12.100 | 1.76 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: 24" Depth Green Roof (IN)

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at '24" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2C |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|----------------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-2C | 9,388 | 12.100 | 2.24 |
| Flow (In) | 24" Depth Green Roof | 9,388 | 12.100 | 2.24 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: 24" Depth Green Roof (IN)

Scenario: Post-Development 100 year

Return Event: 100 years

Storm Event: 100 year

Summary for Hydrograph Addition at '24" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2C |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|----------------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-2C | 13,610 | 12.100 | 3.22 |
| Flow (In) | 24" Depth Green Roof | 13,610 | 12.100 | 3.22 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 1 years

Label: 6" Depth Green Roof

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.13 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.13 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.13 | 0 | 696 | 0.00 | 0.13 | 0.13 |
| 93.10 | 0.13 | 70 | 696 | 0.00 | 0.13 | 0.90 |
| 93.20 | 0.13 | 156 | 1,392 | 0.00 | 0.13 | 1.87 |
| 93.30 | 0.13 | 296 | 1,392 | 0.00 | 0.13 | 3.41 |
| 93.40 | 0.13 | 435 | 1,392 | 0.00 | 0.13 | 4.96 |
| 93.50 | 0.13 | 574 | 1,392 | 0.00 | 0.13 | 6.51 |
| 93.60 | 0.13 | 713 | 1,392 | 0.00 | 0.13 | 8.05 |
| 93.70 | 0.13 | 887 | 2,784 | 0.00 | 0.13 | 9.98 |
| 93.71 | 0.13 | 915 | 2,784 | 0.00 | 0.13 | 10.29 |
| 93.75 | 1.38 | 1,026 | 2,784 | 0.00 | 1.38 | 12.78 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 10 years

Label: 6" Depth Green Roof

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.13 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.13 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.13 | 0 | 696 | 0.00 | 0.13 | 0.13 |
| 93.10 | 0.13 | 70 | 696 | 0.00 | 0.13 | 0.90 |
| 93.20 | 0.13 | 156 | 1,392 | 0.00 | 0.13 | 1.87 |
| 93.30 | 0.13 | 296 | 1,392 | 0.00 | 0.13 | 3.41 |
| 93.40 | 0.13 | 435 | 1,392 | 0.00 | 0.13 | 4.96 |
| 93.50 | 0.13 | 574 | 1,392 | 0.00 | 0.13 | 6.51 |
| 93.60 | 0.13 | 713 | 1,392 | 0.00 | 0.13 | 8.05 |
| 93.70 | 0.13 | 887 | 2,784 | 0.00 | 0.13 | 9.98 |
| 93.71 | 0.13 | 915 | 2,784 | 0.00 | 0.13 | 10.29 |
| 93.75 | 1.38 | 1,026 | 2,784 | 0.00 | 1.38 | 12.78 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 25 years

Label: 6" Depth Green Roof

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.13 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.13 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.13 | 0 | 696 | 0.00 | 0.13 | 0.13 |
| 93.10 | 0.13 | 70 | 696 | 0.00 | 0.13 | 0.90 |
| 93.20 | 0.13 | 156 | 1,392 | 0.00 | 0.13 | 1.87 |
| 93.30 | 0.13 | 296 | 1,392 | 0.00 | 0.13 | 3.41 |
| 93.40 | 0.13 | 435 | 1,392 | 0.00 | 0.13 | 4.96 |
| 93.50 | 0.13 | 574 | 1,392 | 0.00 | 0.13 | 6.51 |
| 93.60 | 0.13 | 713 | 1,392 | 0.00 | 0.13 | 8.05 |
| 93.70 | 0.13 | 887 | 2,784 | 0.00 | 0.13 | 9.98 |
| 93.71 | 0.13 | 915 | 2,784 | 0.00 | 0.13 | 10.29 |
| 93.75 | 1.38 | 1,026 | 2,784 | 0.00 | 1.38 | 12.78 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 100 years

Label: 6" Depth Green Roof

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 93.00 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.13 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.13 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 93.00 | 0.13 | 0 | 696 | 0.00 | 0.13 | 0.13 |
| 93.10 | 0.13 | 70 | 696 | 0.00 | 0.13 | 0.90 |
| 93.20 | 0.13 | 156 | 1,392 | 0.00 | 0.13 | 1.87 |
| 93.30 | 0.13 | 296 | 1,392 | 0.00 | 0.13 | 3.41 |
| 93.40 | 0.13 | 435 | 1,392 | 0.00 | 0.13 | 4.96 |
| 93.50 | 0.13 | 574 | 1,392 | 0.00 | 0.13 | 6.51 |
| 93.60 | 0.13 | 713 | 1,392 | 0.00 | 0.13 | 8.05 |
| 93.70 | 0.13 | 887 | 2,784 | 0.00 | 0.13 | 9.98 |
| 93.71 | 0.13 | 915 | 2,784 | 0.00 | 0.13 | 10.29 |
| 93.75 | 1.38 | 1,026 | 2,784 | 0.00 | 1.38 | 12.78 |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 1 years

Label: 6" Depth Green Roof (IN)

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.13 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.13 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 0.40 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.13 ft ³ /s | Time to Peak (Flow, Outlet) | 11.800 hours |
| Peak Values | | | |
| Elevation (Water Surface, Peak) | 93.29 ft | | |
| Volume (Peak) | 282 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 1,605 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 1,610 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 5 ft ³ | | |
| Error (Mass Balance) | 0.3 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 10 years

Label: 6" Depth Green Roof (IN)

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.13 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.13 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 0.74 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.13 ft ³ /s | Time to Peak (Flow, Outlet) | 11.650 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 93.68 ft | | |
| Volume (Peak) | 819 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 3,085 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 3,090 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 5 ft ³ | | |
| Error (Mass Balance) | 0.2 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 25 years

Label: 6" Depth Green Roof (IN)

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.13 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.13 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 0.94 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.53 ft ³ /s | Time to Peak (Flow, Outlet) | 12.250 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 93.72 ft | | |
| Volume (Peak) | 950 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 3,951 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 3,955 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 5 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 100 years

Label: 6" Depth Green Roof (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 93.00 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.13 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.13 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 1.35 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 1.27 ft ³ /s | Time to Peak (Flow, Outlet) | 12.150 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 93.75 ft | | |
| Volume (Peak) | 1,017 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 5,727 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 5,731 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 4 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 2.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 3.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 3.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.100 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.150 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.450 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 4.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.100 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.150 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.450 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 5.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 5.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 5.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 6.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 7.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 7.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 7.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 8.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 8.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 9.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 9.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 9.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 10.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 10.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 10.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 10.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 10.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 10.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 10.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 10.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 10.400 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 10.450 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 10.550 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 10.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 10.950 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 11.000 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 11.050 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 11.100 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 11.150 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 11.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 11.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 11.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 11.350 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 11.400 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 11.450 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 11.500 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 11.550 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 11.600 | 0.07 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 11.650 | 0.09 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.700 | 0.11 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 93.00 |
| 11.750 | 0.13 | 0.00 | 0.23 | 0.00 | 0.12 | 0 | 93.00 |
| 11.800 | 0.15 | 0.02 | 0.27 | 0.00 | 0.13 | 13 | 93.02 |
| 11.850 | 0.17 | 0.08 | 0.33 | 0.00 | 0.13 | 19 | 93.03 |
| 11.900 | 0.19 | 0.18 | 0.44 | 0.00 | 0.13 | 28 | 93.04 |
| 11.950 | 0.25 | 0.37 | 0.62 | 0.00 | 0.13 | 45 | 93.06 |
| 12.000 | 0.35 | 0.71 | 0.97 | 0.00 | 0.13 | 75 | 93.11 |
| 12.050 | 0.39 | 1.19 | 1.45 | 0.00 | 0.13 | 109 | 93.16 |
| 12.100 | 0.40 | 1.72 | 1.98 | 0.00 | 0.13 | 166 | 93.21 |
| 12.150 | 0.35 | 2.21 | 2.47 | 0.00 | 0.13 | 211 | 93.24 |
| 12.200 | 0.25 | 2.56 | 2.82 | 0.00 | 0.13 | 242 | 93.26 |
| 12.250 | 0.21 | 2.77 | 3.02 | 0.00 | 0.13 | 261 | 93.27 |
| 12.300 | 0.18 | 2.90 | 3.15 | 0.00 | 0.13 | 272 | 93.28 |
| 12.350 | 0.16 | 2.98 | 3.23 | 0.00 | 0.13 | 279 | 93.29 |
| 12.400 | 0.13 | 3.01 | 3.27 | 0.00 | 0.13 | 282 | 93.29 |
| 12.450 | 0.11 | 3.00 | 3.26 | 0.00 | 0.13 | 281 | 93.29 |
| 12.500 | 0.09 | 2.95 | 3.20 | 0.00 | 0.13 | 277 | 93.29 |
| 12.550 | 0.08 | 2.86 | 3.11 | 0.00 | 0.13 | 269 | 93.28 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.06 | 2.74 | 2.99 | 0.00 | 0.13 | 258 | 93.27 |
| 12.650 | 0.06 | 2.60 | 2.86 | 0.00 | 0.13 | 245 | 93.26 |
| 12.700 | 0.05 | 2.45 | 2.71 | 0.00 | 0.13 | 232 | 93.25 |
| 12.750 | 0.05 | 2.30 | 2.55 | 0.00 | 0.13 | 218 | 93.24 |
| 12.800 | 0.05 | 2.14 | 2.40 | 0.00 | 0.13 | 204 | 93.23 |
| 12.850 | 0.05 | 1.98 | 2.23 | 0.00 | 0.13 | 189 | 93.22 |
| 12.900 | 0.04 | 1.81 | 2.07 | 0.00 | 0.13 | 174 | 93.21 |
| 12.950 | 0.04 | 1.64 | 1.89 | 0.00 | 0.13 | 159 | 93.20 |
| 13.000 | 0.04 | 1.46 | 1.72 | 0.00 | 0.13 | 135 | 93.18 |
| 13.050 | 0.04 | 1.28 | 1.54 | 0.00 | 0.13 | 116 | 93.17 |
| 13.100 | 0.04 | 1.10 | 1.35 | 0.00 | 0.13 | 102 | 93.15 |
| 13.150 | 0.03 | 0.91 | 1.17 | 0.00 | 0.13 | 89 | 93.13 |
| 13.200 | 0.03 | 0.72 | 0.98 | 0.00 | 0.13 | 75 | 93.11 |
| 13.250 | 0.03 | 0.54 | 0.79 | 0.00 | 0.13 | 60 | 93.09 |
| 13.300 | 0.03 | 0.35 | 0.60 | 0.00 | 0.13 | 43 | 93.06 |
| 13.350 | 0.03 | 0.15 | 0.41 | 0.00 | 0.13 | 25 | 93.04 |
| 13.400 | 0.03 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 93.00 |
| 13.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 13.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 13.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 13.900 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 13.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 14.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.150 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 14.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 14.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 15.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 15.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 15.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 15.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 15.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 15.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 15.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 15.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 15.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 15.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 15.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 15.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 16.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 16.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 16.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 16.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 16.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 16.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 17.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 18.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 18.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 19.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 20.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 21.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 22.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 22.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.150 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.450 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 23.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 24.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.150 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.450 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 2.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 3.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 5.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 6.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 6.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 7.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 8.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 8.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 8.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 8.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 8.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 8.450 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.500 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.550 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.600 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.650 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.950 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 9.000 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 9.050 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 9.100 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 9.150 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 9.200 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 9.250 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 9.300 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 9.350 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 9.400 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.450 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.500 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.550 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.600 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 9.650 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.700 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.750 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.800 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.850 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 10.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 10.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 10.100 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 10.150 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 10.200 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 10.250 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 10.300 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 10.350 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.400 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.450 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.550 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 10.600 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.650 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.700 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 10.750 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 10.800 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.850 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.900 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.950 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 11.000 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 11.050 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 11.100 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 11.150 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 11.200 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 11.250 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 11.300 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.350 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 11.400 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 11.450 | 0.09 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 93.00 |
| 11.500 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 93.00 |
| 11.550 | 0.11 | 0.00 | 0.21 | 0.00 | 0.11 | 0 | 93.00 |
| 11.600 | 0.13 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 93.00 |
| 11.650 | 0.16 | 0.04 | 0.30 | 0.00 | 0.13 | 15 | 93.02 |
| 11.700 | 0.20 | 0.15 | 0.40 | 0.00 | 0.13 | 25 | 93.04 |
| 11.750 | 0.24 | 0.33 | 0.59 | 0.00 | 0.13 | 41 | 93.06 |
| 11.800 | 0.28 | 0.60 | 0.85 | 0.00 | 0.13 | 65 | 93.09 |
| 11.850 | 0.32 | 0.94 | 1.19 | 0.00 | 0.13 | 91 | 93.13 |
| 11.900 | 0.36 | 1.36 | 1.61 | 0.00 | 0.13 | 121 | 93.17 |
| 11.950 | 0.47 | 1.93 | 2.19 | 0.00 | 0.13 | 186 | 93.22 |
| 12.000 | 0.66 | 2.81 | 3.06 | 0.00 | 0.13 | 264 | 93.28 |
| 12.050 | 0.72 | 3.93 | 4.19 | 0.00 | 0.13 | 365 | 93.35 |
| 12.100 | 0.74 | 5.14 | 5.40 | 0.00 | 0.13 | 474 | 93.43 |
| 12.150 | 0.65 | 6.28 | 6.53 | 0.00 | 0.13 | 576 | 93.50 |
| 12.200 | 0.48 | 7.15 | 7.40 | 0.00 | 0.13 | 655 | 93.56 |
| 12.250 | 0.39 | 7.76 | 8.01 | 0.00 | 0.13 | 710 | 93.60 |
| 12.300 | 0.33 | 8.22 | 8.48 | 0.00 | 0.13 | 744 | 93.62 |
| 12.350 | 0.29 | 8.59 | 8.84 | 0.00 | 0.13 | 770 | 93.64 |
| 12.400 | 0.25 | 8.87 | 9.12 | 0.00 | 0.13 | 791 | 93.66 |
| 12.450 | 0.21 | 9.07 | 9.32 | 0.00 | 0.13 | 805 | 93.67 |
| 12.500 | 0.17 | 9.19 | 9.45 | 0.00 | 0.13 | 814 | 93.67 |
| 12.550 | 0.14 | 9.24 | 9.50 | 0.00 | 0.13 | 819 | 93.68 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.12 | 9.24 | 9.50 | 0.00 | 0.13 | 819 | 93.68 |
| 12.650 | 0.10 | 9.21 | 9.46 | 0.00 | 0.13 | 816 | 93.67 |
| 12.700 | 0.10 | 9.15 | 9.41 | 0.00 | 0.13 | 811 | 93.67 |
| 12.750 | 0.09 | 9.09 | 9.34 | 0.00 | 0.13 | 806 | 93.67 |
| 12.800 | 0.09 | 9.01 | 9.27 | 0.00 | 0.13 | 801 | 93.66 |
| 12.850 | 0.08 | 8.93 | 9.18 | 0.00 | 0.13 | 795 | 93.66 |
| 12.900 | 0.08 | 8.84 | 9.09 | 0.00 | 0.13 | 788 | 93.65 |
| 12.950 | 0.08 | 8.74 | 8.99 | 0.00 | 0.13 | 781 | 93.65 |
| 13.000 | 0.07 | 8.63 | 8.89 | 0.00 | 0.13 | 773 | 93.64 |
| 13.050 | 0.07 | 8.51 | 8.77 | 0.00 | 0.13 | 765 | 93.64 |
| 13.100 | 0.07 | 8.39 | 8.65 | 0.00 | 0.13 | 756 | 93.63 |
| 13.150 | 0.06 | 8.27 | 8.52 | 0.00 | 0.13 | 747 | 93.62 |
| 13.200 | 0.06 | 8.14 | 8.39 | 0.00 | 0.13 | 738 | 93.62 |
| 13.250 | 0.06 | 8.01 | 8.26 | 0.00 | 0.13 | 728 | 93.61 |
| 13.300 | 0.06 | 7.87 | 8.13 | 0.00 | 0.13 | 719 | 93.60 |
| 13.350 | 0.06 | 7.74 | 7.99 | 0.00 | 0.13 | 708 | 93.60 |
| 13.400 | 0.06 | 7.60 | 7.86 | 0.00 | 0.13 | 696 | 93.59 |
| 13.450 | 0.06 | 7.46 | 7.72 | 0.00 | 0.13 | 683 | 93.58 |
| 13.500 | 0.06 | 7.32 | 7.58 | 0.00 | 0.13 | 670 | 93.57 |
| 13.550 | 0.06 | 7.17 | 7.43 | 0.00 | 0.13 | 657 | 93.56 |
| 13.600 | 0.05 | 7.03 | 7.28 | 0.00 | 0.13 | 644 | 93.55 |
| 13.650 | 0.05 | 6.88 | 7.14 | 0.00 | 0.13 | 631 | 93.54 |
| 13.700 | 0.05 | 6.73 | 6.99 | 0.00 | 0.13 | 617 | 93.53 |
| 13.750 | 0.05 | 6.58 | 6.83 | 0.00 | 0.13 | 603 | 93.52 |
| 13.800 | 0.05 | 6.42 | 6.68 | 0.00 | 0.13 | 589 | 93.51 |
| 13.850 | 0.05 | 6.26 | 6.52 | 0.00 | 0.13 | 575 | 93.50 |
| 13.900 | 0.05 | 6.11 | 6.36 | 0.00 | 0.13 | 561 | 93.49 |
| 13.950 | 0.05 | 5.94 | 6.20 | 0.00 | 0.13 | 546 | 93.48 |
| 14.000 | 0.05 | 5.78 | 6.04 | 0.00 | 0.13 | 532 | 93.47 |
| 14.050 | 0.04 | 5.61 | 5.87 | 0.00 | 0.13 | 517 | 93.46 |
| 14.100 | 0.04 | 5.45 | 5.70 | 0.00 | 0.13 | 502 | 93.45 |
| 14.150 | 0.04 | 5.28 | 5.53 | 0.00 | 0.13 | 487 | 93.44 |
| 14.200 | 0.04 | 5.11 | 5.36 | 0.00 | 0.13 | 471 | 93.43 |
| 14.250 | 0.04 | 4.94 | 5.19 | 0.00 | 0.13 | 456 | 93.42 |
| 14.300 | 0.04 | 4.77 | 5.02 | 0.00 | 0.13 | 440 | 93.40 |
| 14.350 | 0.04 | 4.59 | 4.85 | 0.00 | 0.13 | 425 | 93.39 |
| 14.400 | 0.04 | 4.42 | 4.67 | 0.00 | 0.13 | 409 | 93.38 |
| 14.450 | 0.04 | 4.24 | 4.50 | 0.00 | 0.13 | 393 | 93.37 |
| 14.500 | 0.04 | 4.07 | 4.32 | 0.00 | 0.13 | 378 | 93.36 |
| 14.550 | 0.04 | 3.89 | 4.15 | 0.00 | 0.13 | 362 | 93.35 |
| 14.600 | 0.04 | 3.71 | 3.97 | 0.00 | 0.13 | 346 | 93.34 |
| 14.650 | 0.04 | 3.53 | 3.79 | 0.00 | 0.13 | 329 | 93.32 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.04 | 3.35 | 3.61 | 0.00 | 0.13 | 313 | 93.31 |
| 14.750 | 0.04 | 3.17 | 3.43 | 0.00 | 0.13 | 297 | 93.30 |
| 14.800 | 0.04 | 2.99 | 3.24 | 0.00 | 0.13 | 280 | 93.29 |
| 14.850 | 0.04 | 2.80 | 3.06 | 0.00 | 0.13 | 264 | 93.28 |
| 14.900 | 0.04 | 2.62 | 2.88 | 0.00 | 0.13 | 247 | 93.27 |
| 14.950 | 0.04 | 2.43 | 2.69 | 0.00 | 0.13 | 231 | 93.25 |
| 15.000 | 0.03 | 2.25 | 2.50 | 0.00 | 0.13 | 214 | 93.24 |
| 15.050 | 0.03 | 2.06 | 2.32 | 0.00 | 0.13 | 197 | 93.23 |
| 15.100 | 0.03 | 1.87 | 2.13 | 0.00 | 0.13 | 180 | 93.22 |
| 15.150 | 0.03 | 1.68 | 1.94 | 0.00 | 0.13 | 163 | 93.20 |
| 15.200 | 0.03 | 1.49 | 1.75 | 0.00 | 0.13 | 139 | 93.19 |
| 15.250 | 0.03 | 1.30 | 1.56 | 0.00 | 0.13 | 117 | 93.17 |
| 15.300 | 0.03 | 1.11 | 1.36 | 0.00 | 0.13 | 103 | 93.15 |
| 15.350 | 0.03 | 0.91 | 1.17 | 0.00 | 0.13 | 89 | 93.13 |
| 15.400 | 0.03 | 0.72 | 0.97 | 0.00 | 0.13 | 75 | 93.11 |
| 15.450 | 0.03 | 0.52 | 0.78 | 0.00 | 0.13 | 59 | 93.08 |
| 15.500 | 0.03 | 0.33 | 0.58 | 0.00 | 0.13 | 41 | 93.06 |
| 15.550 | 0.03 | 0.13 | 0.38 | 0.00 | 0.13 | 23 | 93.03 |
| 15.600 | 0.03 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 93.00 |
| 15.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 15.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 15.750 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 15.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 15.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 15.900 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 15.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.150 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 16.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 16.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 17.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 18.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 19.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 19.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 20.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 21.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 24.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 1.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.450 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 2.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 3.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 4.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 4.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 5.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 5.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 6.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 6.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 7.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.400 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.450 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.500 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 7.600 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.650 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.700 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.750 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.900 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 7.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.000 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 8.050 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.100 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.150 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.200 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.250 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 8.450 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.500 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.550 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.600 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 8.650 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 8.700 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 8.750 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 8.800 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 8.850 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 9.200 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.250 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.300 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.350 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 9.400 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.450 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.500 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 9.600 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.650 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.700 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 9.950 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.000 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.050 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.100 | 0.06 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 10.150 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 10.200 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 10.250 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.300 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.350 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 10.400 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 10.450 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 10.550 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 10.600 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.650 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.750 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 10.800 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 10.850 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 10.900 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 10.950 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.000 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.050 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 11.100 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 11.150 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 11.200 | 0.10 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 11.250 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 93.00 |
| 11.300 | 0.11 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 93.00 |
| 11.350 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 93.00 |
| 11.400 | 0.12 | 0.00 | 0.23 | 0.00 | 0.11 | 0 | 93.00 |
| 11.450 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 93.00 |
| 11.500 | 0.13 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 93.00 |
| 11.550 | 0.14 | 0.01 | 0.27 | 0.00 | 0.13 | 13 | 93.02 |
| 11.600 | 0.17 | 0.07 | 0.33 | 0.00 | 0.13 | 18 | 93.03 |
| 11.650 | 0.21 | 0.19 | 0.45 | 0.00 | 0.13 | 29 | 93.04 |
| 11.700 | 0.26 | 0.40 | 0.66 | 0.00 | 0.13 | 47 | 93.07 |
| 11.750 | 0.30 | 0.70 | 0.96 | 0.00 | 0.13 | 74 | 93.11 |
| 11.800 | 0.36 | 1.11 | 1.36 | 0.00 | 0.13 | 103 | 93.15 |
| 11.850 | 0.40 | 1.61 | 1.87 | 0.00 | 0.13 | 157 | 93.20 |
| 11.900 | 0.46 | 2.22 | 2.47 | 0.00 | 0.13 | 211 | 93.24 |
| 11.950 | 0.60 | 3.02 | 3.28 | 0.00 | 0.13 | 283 | 93.29 |
| 12.000 | 0.83 | 4.20 | 4.46 | 0.00 | 0.13 | 389 | 93.37 |
| 12.050 | 0.92 | 5.70 | 5.95 | 0.00 | 0.13 | 524 | 93.46 |
| 12.100 | 0.94 | 7.30 | 7.56 | 0.00 | 0.13 | 669 | 93.57 |
| 12.150 | 0.83 | 8.82 | 9.07 | 0.00 | 0.13 | 787 | 93.65 |
| 12.200 | 0.60 | 9.99 | 10.25 | 0.00 | 0.13 | 911 | 93.71 |
| 12.250 | 0.49 | 10.03 | 11.09 | 0.00 | 0.53 | 950 | 93.72 |
| 12.300 | 0.42 | 10.03 | 10.95 | 0.00 | 0.46 | 944 | 93.72 |
| 12.350 | 0.37 | 10.03 | 10.82 | 0.00 | 0.39 | 938 | 93.72 |
| 12.400 | 0.31 | 10.03 | 10.71 | 0.00 | 0.34 | 934 | 93.72 |
| 12.450 | 0.27 | 10.03 | 10.61 | 0.00 | 0.29 | 929 | 93.72 |
| 12.500 | 0.21 | 10.03 | 10.51 | 0.00 | 0.24 | 925 | 93.71 |
| 12.550 | 0.18 | 10.03 | 10.43 | 0.00 | 0.20 | 921 | 93.71 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.15 | 10.03 | 10.36 | 0.00 | 0.16 | 918 | 93.71 |
| 12.650 | 0.13 | 10.03 | 10.31 | 0.00 | 0.14 | 916 | 93.71 |
| 12.700 | 0.12 | 10.03 | 10.29 | 0.00 | 0.13 | 915 | 93.71 |
| 12.750 | 0.12 | 10.02 | 10.28 | 0.00 | 0.13 | 913 | 93.71 |
| 12.800 | 0.11 | 9.99 | 10.25 | 0.00 | 0.13 | 911 | 93.71 |
| 12.850 | 0.11 | 9.96 | 10.21 | 0.00 | 0.13 | 908 | 93.71 |
| 12.900 | 0.10 | 9.91 | 10.17 | 0.00 | 0.13 | 903 | 93.71 |
| 12.950 | 0.10 | 9.85 | 10.11 | 0.00 | 0.13 | 898 | 93.70 |
| 13.000 | 0.09 | 9.79 | 10.04 | 0.00 | 0.13 | 892 | 93.70 |
| 13.050 | 0.09 | 9.71 | 9.96 | 0.00 | 0.13 | 884 | 93.70 |
| 13.100 | 0.08 | 9.62 | 9.88 | 0.00 | 0.13 | 872 | 93.69 |
| 13.150 | 0.08 | 9.53 | 9.79 | 0.00 | 0.13 | 859 | 93.69 |
| 13.200 | 0.08 | 9.44 | 9.69 | 0.00 | 0.13 | 845 | 93.69 |
| 13.250 | 0.08 | 9.34 | 9.60 | 0.00 | 0.13 | 831 | 93.68 |
| 13.300 | 0.08 | 9.24 | 9.50 | 0.00 | 0.13 | 819 | 93.67 |
| 13.350 | 0.08 | 9.14 | 9.39 | 0.00 | 0.13 | 810 | 93.67 |
| 13.400 | 0.07 | 9.03 | 9.29 | 0.00 | 0.13 | 802 | 93.66 |
| 13.450 | 0.07 | 8.92 | 9.18 | 0.00 | 0.13 | 794 | 93.66 |
| 13.500 | 0.07 | 8.81 | 9.07 | 0.00 | 0.13 | 786 | 93.65 |
| 13.550 | 0.07 | 8.70 | 8.95 | 0.00 | 0.13 | 778 | 93.65 |
| 13.600 | 0.07 | 8.58 | 8.84 | 0.00 | 0.13 | 770 | 93.64 |
| 13.650 | 0.07 | 8.46 | 8.72 | 0.00 | 0.13 | 761 | 93.63 |
| 13.700 | 0.07 | 8.34 | 8.59 | 0.00 | 0.13 | 752 | 93.63 |
| 13.750 | 0.06 | 8.21 | 8.47 | 0.00 | 0.13 | 743 | 93.62 |
| 13.800 | 0.06 | 8.08 | 8.34 | 0.00 | 0.13 | 734 | 93.61 |
| 13.850 | 0.06 | 7.95 | 8.21 | 0.00 | 0.13 | 725 | 93.61 |
| 13.900 | 0.06 | 7.82 | 8.08 | 0.00 | 0.13 | 715 | 93.60 |
| 13.950 | 0.06 | 7.68 | 7.94 | 0.00 | 0.13 | 703 | 93.59 |
| 14.000 | 0.06 | 7.55 | 7.80 | 0.00 | 0.13 | 691 | 93.58 |
| 14.050 | 0.06 | 7.40 | 7.66 | 0.00 | 0.13 | 678 | 93.57 |
| 14.100 | 0.06 | 7.26 | 7.52 | 0.00 | 0.13 | 665 | 93.57 |
| 14.150 | 0.05 | 7.12 | 7.37 | 0.00 | 0.13 | 652 | 93.56 |
| 14.200 | 0.05 | 6.97 | 7.22 | 0.00 | 0.13 | 639 | 93.55 |
| 14.250 | 0.05 | 6.82 | 7.08 | 0.00 | 0.13 | 625 | 93.54 |
| 14.300 | 0.05 | 6.67 | 6.93 | 0.00 | 0.13 | 612 | 93.53 |
| 14.350 | 0.05 | 6.52 | 6.78 | 0.00 | 0.13 | 598 | 93.52 |
| 14.400 | 0.05 | 6.37 | 6.62 | 0.00 | 0.13 | 585 | 93.51 |
| 14.450 | 0.05 | 6.21 | 6.47 | 0.00 | 0.13 | 571 | 93.50 |
| 14.500 | 0.05 | 6.06 | 6.32 | 0.00 | 0.13 | 557 | 93.49 |
| 14.550 | 0.05 | 5.90 | 6.16 | 0.00 | 0.13 | 543 | 93.48 |
| 14.600 | 0.05 | 5.75 | 6.00 | 0.00 | 0.13 | 529 | 93.47 |
| 14.650 | 0.05 | 5.59 | 5.84 | 0.00 | 0.13 | 514 | 93.46 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.05 | 5.43 | 5.68 | 0.00 | 0.13 | 500 | 93.45 |
| 14.750 | 0.05 | 5.27 | 5.52 | 0.00 | 0.13 | 486 | 93.44 |
| 14.800 | 0.05 | 5.10 | 5.36 | 0.00 | 0.13 | 471 | 93.43 |
| 14.850 | 0.05 | 4.94 | 5.20 | 0.00 | 0.13 | 456 | 93.42 |
| 14.900 | 0.05 | 4.77 | 5.03 | 0.00 | 0.13 | 441 | 93.40 |
| 14.950 | 0.04 | 4.61 | 4.86 | 0.00 | 0.13 | 426 | 93.39 |
| 15.000 | 0.04 | 4.44 | 4.70 | 0.00 | 0.13 | 411 | 93.38 |
| 15.050 | 0.04 | 4.27 | 4.53 | 0.00 | 0.13 | 396 | 93.37 |
| 15.100 | 0.04 | 4.10 | 4.36 | 0.00 | 0.13 | 381 | 93.36 |
| 15.150 | 0.04 | 3.93 | 4.19 | 0.00 | 0.13 | 365 | 93.35 |
| 15.200 | 0.04 | 3.76 | 4.01 | 0.00 | 0.13 | 350 | 93.34 |
| 15.250 | 0.04 | 3.58 | 3.84 | 0.00 | 0.13 | 334 | 93.33 |
| 15.300 | 0.04 | 3.41 | 3.66 | 0.00 | 0.13 | 318 | 93.32 |
| 15.350 | 0.04 | 3.23 | 3.48 | 0.00 | 0.13 | 302 | 93.30 |
| 15.400 | 0.04 | 3.05 | 3.31 | 0.00 | 0.13 | 286 | 93.29 |
| 15.450 | 0.04 | 2.87 | 3.13 | 0.00 | 0.13 | 270 | 93.28 |
| 15.500 | 0.04 | 2.69 | 2.95 | 0.00 | 0.13 | 254 | 93.27 |
| 15.550 | 0.04 | 2.51 | 2.76 | 0.00 | 0.13 | 237 | 93.26 |
| 15.600 | 0.04 | 2.32 | 2.58 | 0.00 | 0.13 | 221 | 93.25 |
| 15.650 | 0.04 | 2.14 | 2.40 | 0.00 | 0.13 | 204 | 93.23 |
| 15.700 | 0.03 | 1.95 | 2.21 | 0.00 | 0.13 | 187 | 93.22 |
| 15.750 | 0.03 | 1.77 | 2.02 | 0.00 | 0.13 | 170 | 93.21 |
| 15.800 | 0.03 | 1.58 | 1.83 | 0.00 | 0.13 | 152 | 93.20 |
| 15.850 | 0.03 | 1.39 | 1.64 | 0.00 | 0.13 | 125 | 93.18 |
| 15.900 | 0.03 | 1.20 | 1.45 | 0.00 | 0.13 | 109 | 93.16 |
| 15.950 | 0.03 | 1.00 | 1.26 | 0.00 | 0.13 | 95 | 93.14 |
| 16.000 | 0.03 | 0.81 | 1.06 | 0.00 | 0.13 | 81 | 93.12 |
| 16.050 | 0.03 | 0.61 | 0.87 | 0.00 | 0.13 | 67 | 93.10 |
| 16.100 | 0.03 | 0.42 | 0.67 | 0.00 | 0.13 | 49 | 93.07 |
| 16.150 | 0.03 | 0.22 | 0.48 | 0.00 | 0.13 | 31 | 93.04 |
| 16.200 | 0.03 | 0.02 | 0.28 | 0.00 | 0.13 | 14 | 93.02 |
| 16.250 | 0.03 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 16.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 16.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 16.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 16.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 16.500 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.550 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.600 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.650 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.700 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.750 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 16.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.150 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 17.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 17.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 18.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 18.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 19.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 20.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 20.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 21.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 22.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 23.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 24.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 93.00 |
| 0.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 0.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 93.00 |
| 1.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 93.00 |
| 1.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 1.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 93.00 |
| 2.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 2.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 3.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 3.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 3.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 4.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 5.450 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.500 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.600 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.650 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.700 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 5.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 6.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 6.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 6.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 6.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 6.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 6.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 6.350 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 6.400 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 6.450 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 6.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 6.950 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 7.000 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 7.050 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 7.100 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 7.150 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 7.200 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 7.250 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 7.300 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 7.350 | 0.04 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 7.400 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 7.450 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 7.500 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 7.550 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 7.600 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 7.650 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 93.00 |
| 7.700 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.750 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.800 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.850 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 7.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 93.00 |
| 8.200 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 8.250 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 8.300 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 93.00 |
| 8.350 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 93.00 |
| 8.450 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.500 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.550 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.600 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.650 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 93.00 |
| 8.700 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 8.750 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 8.800 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 93.00 |
| 8.850 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 8.900 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 8.950 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 93.00 |
| 9.000 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 9.050 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 9.100 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 9.150 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 9.200 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 93.00 |
| 9.250 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 9.300 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 9.350 | 0.07 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 93.00 |
| 9.400 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 9.450 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 93.00 |
| 9.500 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.550 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.600 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.650 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.750 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 93.00 |
| 9.800 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 9.850 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 93.00 |
| 9.900 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 9.950 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 10.000 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 93.00 |
| 10.050 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 10.100 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 10.150 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 10.200 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 10.250 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 93.00 |
| 10.300 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 93.00 |
| 10.350 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 10.400 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 93.00 |
| 10.450 | 0.09 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.10 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 93.00 |
| 10.550 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 93.00 |
| 10.600 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 93.00 |
| 10.650 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 93.00 |
| 10.700 | 0.10 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 93.00 |
| 10.750 | 0.11 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 93.00 |
| 10.800 | 0.11 | 0.00 | 0.21 | 0.00 | 0.11 | 0 | 93.00 |
| 10.850 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 93.00 |
| 10.900 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 93.00 |
| 10.950 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 93.00 |
| 11.000 | 0.12 | 0.00 | 0.23 | 0.00 | 0.11 | 0 | 93.00 |
| 11.050 | 0.12 | 0.00 | 0.23 | 0.00 | 0.12 | 0 | 93.00 |
| 11.100 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 93.00 |
| 11.150 | 0.13 | 0.00 | 0.25 | 0.00 | 0.13 | 0 | 93.00 |
| 11.200 | 0.14 | 0.01 | 0.27 | 0.00 | 0.13 | 12 | 93.02 |
| 11.250 | 0.14 | 0.04 | 0.29 | 0.00 | 0.13 | 15 | 93.02 |
| 11.300 | 0.15 | 0.07 | 0.33 | 0.00 | 0.13 | 18 | 93.03 |
| 11.350 | 0.16 | 0.13 | 0.39 | 0.00 | 0.13 | 23 | 93.03 |
| 11.400 | 0.17 | 0.20 | 0.46 | 0.00 | 0.13 | 29 | 93.04 |
| 11.450 | 0.17 | 0.28 | 0.54 | 0.00 | 0.13 | 37 | 93.05 |
| 11.500 | 0.18 | 0.38 | 0.64 | 0.00 | 0.13 | 46 | 93.07 |
| 11.550 | 0.21 | 0.52 | 0.77 | 0.00 | 0.13 | 58 | 93.08 |
| 11.600 | 0.24 | 0.71 | 0.97 | 0.00 | 0.13 | 74 | 93.11 |
| 11.650 | 0.30 | 1.00 | 1.25 | 0.00 | 0.13 | 95 | 93.14 |
| 11.700 | 0.37 | 1.41 | 1.67 | 0.00 | 0.13 | 128 | 93.18 |
| 11.750 | 0.44 | 1.96 | 2.22 | 0.00 | 0.13 | 188 | 93.22 |
| 11.800 | 0.51 | 2.65 | 2.91 | 0.00 | 0.13 | 250 | 93.27 |
| 11.850 | 0.58 | 3.49 | 3.75 | 0.00 | 0.13 | 326 | 93.32 |
| 11.900 | 0.66 | 4.47 | 4.73 | 0.00 | 0.13 | 414 | 93.39 |
| 11.950 | 0.86 | 5.74 | 6.00 | 0.00 | 0.13 | 528 | 93.47 |
| 12.000 | 1.20 | 7.54 | 7.80 | 0.00 | 0.13 | 691 | 93.58 |
| 12.050 | 1.32 | 9.81 | 10.06 | 0.00 | 0.13 | 894 | 93.70 |
| 12.100 | 1.35 | 10.03 | 12.48 | 0.00 | 1.23 | 1,013 | 93.75 |
| 12.150 | 1.19 | 10.02 | 12.57 | 0.00 | 1.27 | 1,017 | 93.75 |
| 12.200 | 0.87 | 10.03 | 12.08 | 0.00 | 1.03 | 995 | 93.74 |
| 12.250 | 0.71 | 10.03 | 11.60 | 0.00 | 0.79 | 973 | 93.73 |
| 12.300 | 0.60 | 10.03 | 11.34 | 0.00 | 0.66 | 962 | 93.73 |
| 12.350 | 0.53 | 10.03 | 11.16 | 0.00 | 0.57 | 954 | 93.72 |
| 12.400 | 0.45 | 10.03 | 11.01 | 0.00 | 0.49 | 947 | 93.72 |
| 12.450 | 0.38 | 10.03 | 10.86 | 0.00 | 0.42 | 940 | 93.72 |
| 12.500 | 0.31 | 10.03 | 10.72 | 0.00 | 0.34 | 934 | 93.72 |
| 12.550 | 0.26 | 10.03 | 10.59 | 0.00 | 0.28 | 928 | 93.71 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.21 | 10.03 | 10.50 | 0.00 | 0.23 | 924 | 93.71 |
| 12.650 | 0.19 | 10.03 | 10.43 | 0.00 | 0.20 | 921 | 93.71 |
| 12.700 | 0.18 | 10.03 | 10.40 | 0.00 | 0.18 | 920 | 93.71 |
| 12.750 | 0.17 | 10.03 | 10.38 | 0.00 | 0.17 | 919 | 93.71 |
| 12.800 | 0.16 | 10.03 | 10.36 | 0.00 | 0.17 | 918 | 93.71 |
| 12.850 | 0.15 | 10.03 | 10.35 | 0.00 | 0.16 | 917 | 93.71 |
| 12.900 | 0.15 | 10.03 | 10.33 | 0.00 | 0.15 | 917 | 93.71 |
| 12.950 | 0.14 | 10.03 | 10.32 | 0.00 | 0.14 | 916 | 93.71 |
| 13.000 | 0.13 | 10.03 | 10.30 | 0.00 | 0.13 | 915 | 93.71 |
| 13.050 | 0.13 | 10.03 | 10.29 | 0.00 | 0.13 | 915 | 93.71 |
| 13.100 | 0.12 | 10.02 | 10.28 | 0.00 | 0.13 | 914 | 93.71 |
| 13.150 | 0.12 | 10.00 | 10.26 | 0.00 | 0.13 | 912 | 93.71 |
| 13.200 | 0.11 | 9.98 | 10.24 | 0.00 | 0.13 | 910 | 93.71 |
| 13.250 | 0.11 | 9.95 | 10.21 | 0.00 | 0.13 | 907 | 93.71 |
| 13.300 | 0.11 | 9.92 | 10.17 | 0.00 | 0.13 | 904 | 93.71 |
| 13.350 | 0.11 | 9.88 | 10.14 | 0.00 | 0.13 | 901 | 93.71 |
| 13.400 | 0.11 | 9.84 | 10.10 | 0.00 | 0.13 | 897 | 93.70 |
| 13.450 | 0.10 | 9.80 | 10.05 | 0.00 | 0.13 | 893 | 93.70 |
| 13.500 | 0.10 | 9.75 | 10.00 | 0.00 | 0.13 | 889 | 93.70 |
| 13.550 | 0.10 | 9.70 | 9.95 | 0.00 | 0.13 | 882 | 93.70 |
| 13.600 | 0.10 | 9.64 | 9.90 | 0.00 | 0.13 | 874 | 93.70 |
| 13.650 | 0.10 | 9.58 | 9.83 | 0.00 | 0.13 | 866 | 93.69 |
| 13.700 | 0.09 | 9.51 | 9.77 | 0.00 | 0.13 | 856 | 93.69 |
| 13.750 | 0.09 | 9.45 | 9.70 | 0.00 | 0.13 | 847 | 93.69 |
| 13.800 | 0.09 | 9.37 | 9.63 | 0.00 | 0.13 | 836 | 93.68 |
| 13.850 | 0.09 | 9.30 | 9.55 | 0.00 | 0.13 | 826 | 93.68 |
| 13.900 | 0.09 | 9.22 | 9.47 | 0.00 | 0.13 | 817 | 93.67 |
| 13.950 | 0.09 | 9.13 | 9.39 | 0.00 | 0.13 | 810 | 93.67 |
| 14.000 | 0.08 | 9.05 | 9.30 | 0.00 | 0.13 | 803 | 93.66 |
| 14.050 | 0.08 | 8.96 | 9.21 | 0.00 | 0.13 | 797 | 93.66 |
| 14.100 | 0.08 | 8.86 | 9.12 | 0.00 | 0.13 | 790 | 93.66 |
| 14.150 | 0.08 | 8.76 | 9.02 | 0.00 | 0.13 | 783 | 93.65 |
| 14.200 | 0.08 | 8.66 | 8.92 | 0.00 | 0.13 | 776 | 93.64 |
| 14.250 | 0.08 | 8.56 | 8.82 | 0.00 | 0.13 | 768 | 93.64 |
| 14.300 | 0.08 | 8.46 | 8.72 | 0.00 | 0.13 | 761 | 93.63 |
| 14.350 | 0.07 | 8.35 | 8.61 | 0.00 | 0.13 | 753 | 93.63 |
| 14.400 | 0.07 | 8.25 | 8.50 | 0.00 | 0.13 | 746 | 93.62 |
| 14.450 | 0.07 | 8.14 | 8.39 | 0.00 | 0.13 | 738 | 93.62 |
| 14.500 | 0.07 | 8.03 | 8.28 | 0.00 | 0.13 | 730 | 93.61 |
| 14.550 | 0.07 | 7.91 | 8.17 | 0.00 | 0.13 | 722 | 93.61 |
| 14.600 | 0.07 | 7.80 | 8.06 | 0.00 | 0.13 | 713 | 93.60 |
| 14.650 | 0.07 | 7.68 | 7.94 | 0.00 | 0.13 | 703 | 93.59 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.07 | 7.57 | 7.82 | 0.00 | 0.13 | 692 | 93.59 |
| 14.750 | 0.07 | 7.45 | 7.70 | 0.00 | 0.13 | 682 | 93.58 |
| 14.800 | 0.07 | 7.32 | 7.58 | 0.00 | 0.13 | 671 | 93.57 |
| 14.850 | 0.07 | 7.20 | 7.46 | 0.00 | 0.13 | 659 | 93.56 |
| 14.900 | 0.06 | 7.07 | 7.33 | 0.00 | 0.13 | 648 | 93.55 |
| 14.950 | 0.06 | 6.95 | 7.20 | 0.00 | 0.13 | 637 | 93.54 |
| 15.000 | 0.06 | 6.82 | 7.07 | 0.00 | 0.13 | 625 | 93.54 |
| 15.050 | 0.06 | 6.68 | 6.94 | 0.00 | 0.13 | 613 | 93.53 |
| 15.100 | 0.06 | 6.55 | 6.81 | 0.00 | 0.13 | 601 | 93.52 |
| 15.150 | 0.06 | 6.42 | 6.67 | 0.00 | 0.13 | 589 | 93.51 |
| 15.200 | 0.06 | 6.28 | 6.53 | 0.00 | 0.13 | 577 | 93.50 |
| 15.250 | 0.06 | 6.14 | 6.40 | 0.00 | 0.13 | 564 | 93.49 |
| 15.300 | 0.06 | 6.00 | 6.26 | 0.00 | 0.13 | 551 | 93.48 |
| 15.350 | 0.06 | 5.86 | 6.11 | 0.00 | 0.13 | 539 | 93.47 |
| 15.400 | 0.06 | 5.71 | 5.97 | 0.00 | 0.13 | 526 | 93.47 |
| 15.450 | 0.05 | 5.57 | 5.82 | 0.00 | 0.13 | 512 | 93.46 |
| 15.500 | 0.05 | 5.42 | 5.67 | 0.00 | 0.13 | 499 | 93.45 |
| 15.550 | 0.05 | 5.27 | 5.52 | 0.00 | 0.13 | 486 | 93.44 |
| 15.600 | 0.05 | 5.11 | 5.37 | 0.00 | 0.13 | 472 | 93.43 |
| 15.650 | 0.05 | 4.96 | 5.22 | 0.00 | 0.13 | 458 | 93.42 |
| 15.700 | 0.05 | 4.80 | 5.06 | 0.00 | 0.13 | 444 | 93.41 |
| 15.750 | 0.05 | 4.65 | 4.90 | 0.00 | 0.13 | 430 | 93.40 |
| 15.800 | 0.05 | 4.49 | 4.74 | 0.00 | 0.13 | 415 | 93.39 |
| 15.850 | 0.05 | 4.33 | 4.58 | 0.00 | 0.13 | 401 | 93.38 |
| 15.900 | 0.05 | 4.16 | 4.42 | 0.00 | 0.13 | 386 | 93.37 |
| 15.950 | 0.04 | 4.00 | 4.25 | 0.00 | 0.13 | 371 | 93.35 |
| 16.000 | 0.04 | 3.83 | 4.09 | 0.00 | 0.13 | 356 | 93.34 |
| 16.050 | 0.04 | 3.66 | 3.92 | 0.00 | 0.13 | 341 | 93.33 |
| 16.100 | 0.04 | 3.49 | 3.75 | 0.00 | 0.13 | 326 | 93.32 |
| 16.150 | 0.04 | 3.32 | 3.58 | 0.00 | 0.13 | 310 | 93.31 |
| 16.200 | 0.04 | 3.15 | 3.40 | 0.00 | 0.13 | 295 | 93.30 |
| 16.250 | 0.04 | 2.97 | 3.23 | 0.00 | 0.13 | 279 | 93.29 |
| 16.300 | 0.04 | 2.80 | 3.06 | 0.00 | 0.13 | 263 | 93.28 |
| 16.350 | 0.04 | 2.62 | 2.88 | 0.00 | 0.13 | 248 | 93.27 |
| 16.400 | 0.04 | 2.45 | 2.70 | 0.00 | 0.13 | 232 | 93.25 |
| 16.450 | 0.04 | 2.27 | 2.53 | 0.00 | 0.13 | 216 | 93.24 |
| 16.500 | 0.04 | 2.09 | 2.35 | 0.00 | 0.13 | 200 | 93.23 |
| 16.550 | 0.04 | 1.92 | 2.17 | 0.00 | 0.13 | 184 | 93.22 |
| 16.600 | 0.04 | 1.74 | 1.99 | 0.00 | 0.13 | 168 | 93.21 |
| 16.650 | 0.04 | 1.56 | 1.81 | 0.00 | 0.13 | 149 | 93.19 |
| 16.700 | 0.04 | 1.38 | 1.63 | 0.00 | 0.13 | 123 | 93.18 |
| 16.750 | 0.04 | 1.19 | 1.45 | 0.00 | 0.13 | 109 | 93.16 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.04 | 1.01 | 1.27 | 0.00 | 0.13 | 96 | 93.14 |
| 16.850 | 0.04 | 0.83 | 1.08 | 0.00 | 0.13 | 83 | 93.12 |
| 16.900 | 0.04 | 0.64 | 0.90 | 0.00 | 0.13 | 70 | 93.10 |
| 16.950 | 0.04 | 0.46 | 0.72 | 0.00 | 0.13 | 53 | 93.08 |
| 17.000 | 0.03 | 0.27 | 0.53 | 0.00 | 0.13 | 36 | 93.05 |
| 17.050 | 0.03 | 0.09 | 0.34 | 0.00 | 0.13 | 19 | 93.03 |
| 17.100 | 0.03 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 93.00 |
| 17.150 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 17.200 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 17.250 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 17.300 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 93.00 |
| 17.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 93.00 |
| 17.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.000 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.050 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.100 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.300 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.350 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.400 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.450 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.500 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 93.00 |
| 18.600 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 18.650 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 18.700 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 18.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 18.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 18.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 18.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.150 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.400 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.450 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.500 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 93.00 |
| 19.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 19.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 20.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 21.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 22.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 22.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 22.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 93.00 |
| 22.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 22.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: 6" Depth Green Roof (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 93.00 |
| 23.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 23.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |
| 24.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 93.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: 6" Depth Green Roof (IN)
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Summary for Hydrograph Addition at '6" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2D |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2D | 1,605 | 12.100 | 0.40 |
| Flow (In) | 6" Depth Green Roof | 1,605 | 12.100 | 0.40 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: 6" Depth Green Roof (IN)

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at '6" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2D |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|---------------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-2D | 3,085 | 12.100 | 0.74 |
| Flow (In) | 6" Depth Green Roof | 3,085 | 12.100 | 0.74 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: 6" Depth Green Roof (IN)

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at '6" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2D |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2D | 3,951 | 12.100 | 0.94 |
| Flow (In) | 6" Depth Green Roof | 3,951 | 12.100 | 0.94 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: 6" Depth Green Roof (IN)
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Summary for Hydrograph Addition at '6" Depth Green Roof'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2D |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2D | 5,727 | 12.100 | 1.35 |
| Flow (In) | 6" Depth Green Roof | 5,727 | 12.100 | 1.35 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 1 years

Label: MC-3500 - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 71.50 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 71.50 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 72.00 | 0.13 | 668 | 0 | 0.00 | 0.13 | 7.55 |
| 72.50 | 0.20 | 1,737 | 0 | 0.00 | 0.20 | 19.50 |
| 72.75 | 0.23 | 2,464 | 0 | 0.00 | 0.23 | 27.61 |
| 73.00 | 0.36 | 3,184 | 0 | 0.00 | 0.36 | 35.74 |
| 73.50 | 0.62 | 4,592 | 0 | 0.00 | 0.62 | 51.64 |
| 74.00 | 0.77 | 5,947 | 0 | 0.00 | 0.77 | 66.85 |
| 74.50 | 0.90 | 7,230 | 0 | 0.00 | 0.90 | 81.23 |
| 75.00 | 1.01 | 8,415 | 0 | 0.00 | 1.01 | 94.51 |
| 75.50 | 1.11 | 9,452 | 0 | 0.00 | 1.11 | 106.13 |
| 76.00 | 1.20 | 10,221 | 0 | 0.00 | 1.20 | 114.77 |
| 76.50 | 1.29 | 10,889 | 0 | 0.00 | 1.29 | 122.27 |
| 77.00 | 1.37 | 11,556 | 0 | 0.00 | 1.37 | 129.77 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 10 years

Label: MC-3500 - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 71.50 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 71.50 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 72.00 | 0.13 | 668 | 0 | 0.00 | 0.13 | 7.55 |
| 72.50 | 0.20 | 1,737 | 0 | 0.00 | 0.20 | 19.50 |
| 72.75 | 0.23 | 2,464 | 0 | 0.00 | 0.23 | 27.61 |
| 73.00 | 0.36 | 3,184 | 0 | 0.00 | 0.36 | 35.74 |
| 73.50 | 0.62 | 4,592 | 0 | 0.00 | 0.62 | 51.64 |
| 74.00 | 0.77 | 5,947 | 0 | 0.00 | 0.77 | 66.85 |
| 74.50 | 0.90 | 7,230 | 0 | 0.00 | 0.90 | 81.23 |
| 75.00 | 1.01 | 8,415 | 0 | 0.00 | 1.01 | 94.51 |
| 75.50 | 1.11 | 9,452 | 0 | 0.00 | 1.11 | 106.13 |
| 76.00 | 1.20 | 10,221 | 0 | 0.00 | 1.20 | 114.77 |
| 76.50 | 1.29 | 10,889 | 0 | 0.00 | 1.29 | 122.27 |
| 77.00 | 1.37 | 11,556 | 0 | 0.00 | 1.37 | 129.77 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 25 years

Label: MC-3500 - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 71.50 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 71.50 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 72.00 | 0.13 | 668 | 0 | 0.00 | 0.13 | 7.55 |
| 72.50 | 0.20 | 1,737 | 0 | 0.00 | 0.20 | 19.50 |
| 72.75 | 0.23 | 2,464 | 0 | 0.00 | 0.23 | 27.61 |
| 73.00 | 0.36 | 3,184 | 0 | 0.00 | 0.36 | 35.74 |
| 73.50 | 0.62 | 4,592 | 0 | 0.00 | 0.62 | 51.64 |
| 74.00 | 0.77 | 5,947 | 0 | 0.00 | 0.77 | 66.85 |
| 74.50 | 0.90 | 7,230 | 0 | 0.00 | 0.90 | 81.23 |
| 75.00 | 1.01 | 8,415 | 0 | 0.00 | 1.01 | 94.51 |
| 75.50 | 1.11 | 9,452 | 0 | 0.00 | 1.11 | 106.13 |
| 76.00 | 1.20 | 10,221 | 0 | 0.00 | 1.20 | 114.77 |
| 76.50 | 1.29 | 10,889 | 0 | 0.00 | 1.29 | 122.27 |
| 77.00 | 1.37 | 11,556 | 0 | 0.00 | 1.37 | 129.77 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 100 years

Label: MC-3500 - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 71.50 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 71.50 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 72.00 | 0.13 | 668 | 0 | 0.00 | 0.13 | 7.55 |
| 72.50 | 0.20 | 1,737 | 0 | 0.00 | 0.20 | 19.50 |
| 72.75 | 0.23 | 2,464 | 0 | 0.00 | 0.23 | 27.61 |
| 73.00 | 0.36 | 3,184 | 0 | 0.00 | 0.36 | 35.74 |
| 73.50 | 0.62 | 4,592 | 0 | 0.00 | 0.62 | 51.64 |
| 74.00 | 0.77 | 5,947 | 0 | 0.00 | 0.77 | 66.85 |
| 74.50 | 0.90 | 7,230 | 0 | 0.00 | 0.90 | 81.23 |
| 75.00 | 1.01 | 8,415 | 0 | 0.00 | 1.01 | 94.51 |
| 75.50 | 1.11 | 9,452 | 0 | 0.00 | 1.11 | 106.13 |
| 76.00 | 1.20 | 10,221 | 0 | 0.00 | 1.20 | 114.77 |
| 76.50 | 1.29 | 10,889 | 0 | 0.00 | 1.29 | 122.27 |
| 77.00 | 1.37 | 11,556 | 0 | 0.00 | 1.37 | 129.77 |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 1 years

Label: MC-3500 - 2 (IN)

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 71.50 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 0.44 ft ³ /s | Time to Peak (Flow, In) | 12.150 hours |
| Flow (Peak Outlet) | 0.23 ft ³ /s | Time to Peak (Flow, Outlet) | 16.500 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 72.74 ft | | |
| Volume (Peak) | 2,429 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 9,644 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 9,398 ft ³ | | |
| Volume (Retained) | 238 ft ³ | | |
| Volume (Unrouted) | -9 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 10 years

Label: MC-3500 - 2 (IN)

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 71.50 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 1.81 ft ³ /s | Time to Peak (Flow, In) | 12.200 hours |
| Flow (Peak Outlet) | 0.42 ft ³ /s | Time to Peak (Flow, Outlet) | 13.550 hours |
| Peak Values | | | |
| Elevation (Water Surface, Peak) | 73.13 ft | | |
| Volume (Peak) | 3,552 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 18,443 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 16,459 ft ³ | | |
| Volume (Retained) | 1,945 ft ³ | | |
| Volume (Unrouted) | -38 ft ³ | | |
| Error (Mass Balance) | 0.2 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 25 years

Label: MC-3500 - 2 (IN)

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 71.50 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 3.33 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.73 ft ³ /s | Time to Peak (Flow, Outlet) | 12.900 hours |
| Peak Values | | | |
| Elevation (Water Surface, Peak) | 73.86 ft | | |
| Volume (Peak) | 5,580 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 23,569 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 21,106 ft ³ | | |
| Volume (Retained) | 2,421 ft ³ | | |
| Volume (Unrouted) | -42 ft ³ | | |
| Error (Mass Balance) | 0.2 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 100 years

Label: MC-3500 - 2 (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 71.50 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 7.23 ft ³ /s | Time to Peak (Flow, In) | 12.150 hours |
| Flow (Peak Outlet) | 1.28 ft ³ /s | Time to Peak (Flow, Outlet) | 12.700 hours |
| Peak Values | | | |
| Elevation (Water Surface, Peak) | 76.44 ft | | |
| Volume (Peak) | 10,803 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 33,660 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 31,039 ft ³ | | |
| Volume (Retained) | 2,575 ft ³ | | |
| Volume (Unrouted) | -46 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 71.50 |
| 0.050 | 0.00 | 0.17 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 0.100 | 0.00 | 0.17 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.150 | 0.00 | 0.16 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.200 | 0.00 | 0.16 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.250 | 0.00 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.300 | 0.00 | 0.15 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.350 | 0.00 | 0.14 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.400 | 0.00 | 0.14 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.450 | 0.00 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.500 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 0.550 | 0.00 | 0.12 | 0.13 | 0.00 | 0.00 | 11 | 71.51 |
| 0.600 | 0.00 | 0.12 | 0.12 | 0.00 | 0.00 | 11 | 71.51 |
| 0.650 | 0.00 | 0.11 | 0.12 | 0.00 | 0.00 | 10 | 71.51 |
| 0.700 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.750 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.800 | 0.00 | 0.10 | 0.11 | 0.00 | 0.00 | 9 | 71.51 |
| 0.850 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 0.900 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 0.950 | 0.00 | 0.09 | 0.10 | 0.00 | 0.00 | 8 | 71.51 |
| 1.000 | 0.00 | 0.09 | 0.09 | 0.00 | 0.00 | 8 | 71.51 |
| 1.050 | 0.00 | 0.09 | 0.09 | 0.00 | 0.00 | 8 | 71.51 |
| 1.100 | 0.00 | 0.08 | 0.09 | 0.00 | 0.00 | 8 | 71.51 |
| 1.150 | 0.00 | 0.08 | 0.08 | 0.00 | 0.00 | 7 | 71.51 |
| 1.200 | 0.00 | 0.08 | 0.08 | 0.00 | 0.00 | 7 | 71.51 |
| 1.250 | 0.00 | 0.07 | 0.08 | 0.00 | 0.00 | 7 | 71.51 |
| 1.300 | 0.00 | 0.07 | 0.07 | 0.00 | 0.00 | 7 | 71.50 |
| 1.350 | 0.00 | 0.07 | 0.07 | 0.00 | 0.00 | 6 | 71.50 |
| 1.400 | 0.00 | 0.07 | 0.07 | 0.00 | 0.00 | 6 | 71.50 |
| 1.450 | 0.00 | 0.06 | 0.07 | 0.00 | 0.00 | 6 | 71.50 |
| 1.500 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 6 | 71.50 |
| 1.550 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 6 | 71.50 |
| 1.600 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 71.50 |
| 1.650 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 71.50 |
| 1.700 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 71.50 |
| 1.750 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 71.50 |
| 1.800 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 71.50 |
| 1.850 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 71.50 |
| 1.900 | 0.00 | 0.06 | 0.06 | 0.00 | 0.00 | 6 | 71.50 |
| 1.950 | 0.00 | 0.06 | 0.07 | 0.00 | 0.00 | 6 | 71.50 |
| 2.000 | 0.00 | 0.07 | 0.07 | 0.00 | 0.00 | 6 | 71.50 |
| 2.050 | 0.00 | 0.07 | 0.07 | 0.00 | 0.00 | 6 | 71.50 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.07 | 0.08 | 0.00 | 0.00 | 7 | 71.51 |
| 2.150 | 0.00 | 0.08 | 0.08 | 0.00 | 0.00 | 7 | 71.51 |
| 2.200 | 0.00 | 0.08 | 0.09 | 0.00 | 0.00 | 8 | 71.51 |
| 2.250 | 0.00 | 0.09 | 0.09 | 0.00 | 0.00 | 8 | 71.51 |
| 2.300 | 0.00 | 0.09 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 2.350 | 0.01 | 0.10 | 0.11 | 0.00 | 0.00 | 9 | 71.51 |
| 2.400 | 0.01 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 2.450 | 0.01 | 0.12 | 0.12 | 0.00 | 0.00 | 11 | 71.51 |
| 2.500 | 0.01 | 0.12 | 0.13 | 0.00 | 0.00 | 11 | 71.51 |
| 2.550 | 0.01 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 2.600 | 0.01 | 0.14 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 2.650 | 0.01 | 0.15 | 0.15 | 0.00 | 0.00 | 14 | 71.51 |
| 2.700 | 0.01 | 0.16 | 0.16 | 0.00 | 0.00 | 15 | 71.51 |
| 2.750 | 0.01 | 0.17 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 2.800 | 0.01 | 0.18 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 2.850 | 0.01 | 0.19 | 0.19 | 0.00 | 0.00 | 17 | 71.51 |
| 2.900 | 0.01 | 0.20 | 0.21 | 0.00 | 0.00 | 18 | 71.51 |
| 2.950 | 0.01 | 0.21 | 0.22 | 0.00 | 0.00 | 19 | 71.51 |
| 3.000 | 0.01 | 0.22 | 0.23 | 0.00 | 0.00 | 20 | 71.52 |
| 3.050 | 0.01 | 0.23 | 0.24 | 0.00 | 0.00 | 21 | 71.52 |
| 3.100 | 0.01 | 0.24 | 0.25 | 0.00 | 0.00 | 22 | 71.52 |
| 3.150 | 0.01 | 0.26 | 0.27 | 0.00 | 0.00 | 23 | 71.52 |
| 3.200 | 0.01 | 0.27 | 0.28 | 0.00 | 0.00 | 25 | 71.52 |
| 3.250 | 0.01 | 0.28 | 0.29 | 0.00 | 0.01 | 26 | 71.52 |
| 3.300 | 0.01 | 0.29 | 0.30 | 0.00 | 0.01 | 27 | 71.52 |
| 3.350 | 0.01 | 0.31 | 0.32 | 0.00 | 0.01 | 28 | 71.52 |
| 3.400 | 0.01 | 0.32 | 0.33 | 0.00 | 0.01 | 29 | 71.52 |
| 3.450 | 0.01 | 0.33 | 0.35 | 0.00 | 0.01 | 31 | 71.52 |
| 3.500 | 0.01 | 0.35 | 0.36 | 0.00 | 0.01 | 32 | 71.52 |
| 3.550 | 0.01 | 0.36 | 0.37 | 0.00 | 0.01 | 33 | 71.52 |
| 3.600 | 0.01 | 0.38 | 0.39 | 0.00 | 0.01 | 34 | 71.53 |
| 3.650 | 0.01 | 0.39 | 0.40 | 0.00 | 0.01 | 36 | 71.53 |
| 3.700 | 0.01 | 0.40 | 0.42 | 0.00 | 0.01 | 37 | 71.53 |
| 3.750 | 0.02 | 0.42 | 0.43 | 0.00 | 0.01 | 38 | 71.53 |
| 3.800 | 0.02 | 0.43 | 0.45 | 0.00 | 0.01 | 40 | 71.53 |
| 3.850 | 0.02 | 0.45 | 0.46 | 0.00 | 0.01 | 41 | 71.53 |
| 3.900 | 0.02 | 0.46 | 0.48 | 0.00 | 0.01 | 42 | 71.53 |
| 3.950 | 0.02 | 0.48 | 0.50 | 0.00 | 0.01 | 44 | 71.53 |
| 4.000 | 0.02 | 0.49 | 0.51 | 0.00 | 0.01 | 45 | 71.53 |
| 4.050 | 0.02 | 0.51 | 0.53 | 0.00 | 0.01 | 47 | 71.53 |
| 4.100 | 0.02 | 0.53 | 0.54 | 0.00 | 0.01 | 48 | 71.54 |
| 4.150 | 0.02 | 0.54 | 0.56 | 0.00 | 0.01 | 50 | 71.54 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.02 | 0.56 | 0.58 | 0.00 | 0.01 | 51 | 71.54 |
| 4.250 | 0.02 | 0.57 | 0.59 | 0.00 | 0.01 | 52 | 71.54 |
| 4.300 | 0.02 | 0.59 | 0.61 | 0.00 | 0.01 | 54 | 71.54 |
| 4.350 | 0.02 | 0.61 | 0.63 | 0.00 | 0.01 | 55 | 71.54 |
| 4.400 | 0.02 | 0.62 | 0.64 | 0.00 | 0.01 | 57 | 71.54 |
| 4.450 | 0.02 | 0.64 | 0.66 | 0.00 | 0.01 | 58 | 71.54 |
| 4.500 | 0.02 | 0.65 | 0.68 | 0.00 | 0.01 | 60 | 71.54 |
| 4.550 | 0.02 | 0.67 | 0.70 | 0.00 | 0.01 | 61 | 71.55 |
| 4.600 | 0.02 | 0.69 | 0.71 | 0.00 | 0.01 | 63 | 71.55 |
| 4.650 | 0.02 | 0.70 | 0.73 | 0.00 | 0.01 | 65 | 71.55 |
| 4.700 | 0.02 | 0.72 | 0.75 | 0.00 | 0.01 | 66 | 71.55 |
| 4.750 | 0.02 | 0.74 | 0.76 | 0.00 | 0.01 | 68 | 71.55 |
| 4.800 | 0.02 | 0.76 | 0.78 | 0.00 | 0.01 | 69 | 71.55 |
| 4.850 | 0.02 | 0.77 | 0.80 | 0.00 | 0.01 | 71 | 71.55 |
| 4.900 | 0.02 | 0.79 | 0.82 | 0.00 | 0.01 | 72 | 71.55 |
| 4.950 | 0.02 | 0.81 | 0.84 | 0.00 | 0.01 | 74 | 71.56 |
| 5.000 | 0.02 | 0.82 | 0.85 | 0.00 | 0.01 | 75 | 71.56 |
| 5.050 | 0.02 | 0.84 | 0.87 | 0.00 | 0.02 | 77 | 71.56 |
| 5.100 | 0.02 | 0.86 | 0.89 | 0.00 | 0.02 | 79 | 71.56 |
| 5.150 | 0.02 | 0.88 | 0.91 | 0.00 | 0.02 | 80 | 71.56 |
| 5.200 | 0.02 | 0.89 | 0.93 | 0.00 | 0.02 | 82 | 71.56 |
| 5.250 | 0.03 | 0.91 | 0.94 | 0.00 | 0.02 | 83 | 71.56 |
| 5.300 | 0.03 | 0.93 | 0.96 | 0.00 | 0.02 | 85 | 71.56 |
| 5.350 | 0.03 | 0.95 | 0.98 | 0.00 | 0.02 | 87 | 71.56 |
| 5.400 | 0.03 | 0.96 | 1.00 | 0.00 | 0.02 | 88 | 71.57 |
| 5.450 | 0.03 | 0.98 | 1.02 | 0.00 | 0.02 | 90 | 71.57 |
| 5.500 | 0.03 | 1.00 | 1.03 | 0.00 | 0.02 | 91 | 71.57 |
| 5.550 | 0.03 | 1.02 | 1.05 | 0.00 | 0.02 | 93 | 71.57 |
| 5.600 | 0.03 | 1.03 | 1.07 | 0.00 | 0.02 | 95 | 71.57 |
| 5.650 | 0.03 | 1.05 | 1.09 | 0.00 | 0.02 | 96 | 71.57 |
| 5.700 | 0.03 | 1.07 | 1.11 | 0.00 | 0.02 | 98 | 71.57 |
| 5.750 | 0.03 | 1.09 | 1.13 | 0.00 | 0.02 | 100 | 71.57 |
| 5.800 | 0.03 | 1.10 | 1.14 | 0.00 | 0.02 | 101 | 71.58 |
| 5.850 | 0.03 | 1.12 | 1.16 | 0.00 | 0.02 | 103 | 71.58 |
| 5.900 | 0.03 | 1.14 | 1.18 | 0.00 | 0.02 | 104 | 71.58 |
| 5.950 | 0.03 | 1.16 | 1.20 | 0.00 | 0.02 | 106 | 71.58 |
| 6.000 | 0.03 | 1.18 | 1.22 | 0.00 | 0.02 | 108 | 71.58 |
| 6.050 | 0.03 | 1.19 | 1.24 | 0.00 | 0.02 | 109 | 71.58 |
| 6.100 | 0.03 | 1.21 | 1.26 | 0.00 | 0.02 | 111 | 71.58 |
| 6.150 | 0.03 | 1.23 | 1.27 | 0.00 | 0.02 | 113 | 71.58 |
| 6.200 | 0.03 | 1.25 | 1.29 | 0.00 | 0.02 | 114 | 71.59 |
| 6.250 | 0.03 | 1.27 | 1.31 | 0.00 | 0.02 | 116 | 71.59 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.03 | 1.29 | 1.33 | 0.00 | 0.02 | 118 | 71.59 |
| 6.350 | 0.03 | 1.31 | 1.36 | 0.00 | 0.02 | 120 | 71.59 |
| 6.400 | 0.03 | 1.33 | 1.38 | 0.00 | 0.02 | 122 | 71.59 |
| 6.450 | 0.04 | 1.35 | 1.40 | 0.00 | 0.02 | 124 | 71.59 |
| 6.500 | 0.04 | 1.37 | 1.42 | 0.00 | 0.02 | 126 | 71.59 |
| 6.550 | 0.04 | 1.40 | 1.45 | 0.00 | 0.03 | 128 | 71.60 |
| 6.600 | 0.04 | 1.42 | 1.47 | 0.00 | 0.03 | 130 | 71.60 |
| 6.650 | 0.04 | 1.44 | 1.50 | 0.00 | 0.03 | 132 | 71.60 |
| 6.700 | 0.04 | 1.47 | 1.52 | 0.00 | 0.03 | 135 | 71.60 |
| 6.750 | 0.04 | 1.49 | 1.55 | 0.00 | 0.03 | 137 | 71.60 |
| 6.800 | 0.04 | 1.52 | 1.57 | 0.00 | 0.03 | 139 | 71.60 |
| 6.850 | 0.04 | 1.55 | 1.60 | 0.00 | 0.03 | 142 | 71.61 |
| 6.900 | 0.04 | 1.57 | 1.63 | 0.00 | 0.03 | 144 | 71.61 |
| 6.950 | 0.04 | 1.60 | 1.66 | 0.00 | 0.03 | 147 | 71.61 |
| 7.000 | 0.04 | 1.63 | 1.69 | 0.00 | 0.03 | 149 | 71.61 |
| 7.050 | 0.04 | 1.65 | 1.71 | 0.00 | 0.03 | 152 | 71.61 |
| 7.100 | 0.04 | 1.68 | 1.74 | 0.00 | 0.03 | 154 | 71.62 |
| 7.150 | 0.05 | 1.71 | 1.77 | 0.00 | 0.03 | 157 | 71.62 |
| 7.200 | 0.05 | 1.74 | 1.80 | 0.00 | 0.03 | 160 | 71.62 |
| 7.250 | 0.05 | 1.77 | 1.83 | 0.00 | 0.03 | 162 | 71.62 |
| 7.300 | 0.05 | 1.80 | 1.87 | 0.00 | 0.03 | 165 | 71.62 |
| 7.350 | 0.05 | 1.83 | 1.90 | 0.00 | 0.03 | 168 | 71.63 |
| 7.400 | 0.05 | 1.86 | 1.93 | 0.00 | 0.03 | 171 | 71.63 |
| 7.450 | 0.05 | 1.89 | 1.96 | 0.00 | 0.03 | 174 | 71.63 |
| 7.500 | 0.05 | 1.93 | 1.99 | 0.00 | 0.03 | 176 | 71.63 |
| 7.550 | 0.05 | 1.96 | 2.03 | 0.00 | 0.04 | 179 | 71.63 |
| 7.600 | 0.05 | 1.99 | 2.06 | 0.00 | 0.04 | 182 | 71.64 |
| 7.650 | 0.05 | 2.02 | 2.10 | 0.00 | 0.04 | 185 | 71.64 |
| 7.700 | 0.05 | 2.06 | 2.13 | 0.00 | 0.04 | 188 | 71.64 |
| 7.750 | 0.05 | 2.09 | 2.16 | 0.00 | 0.04 | 191 | 71.64 |
| 7.800 | 0.06 | 2.12 | 2.20 | 0.00 | 0.04 | 195 | 71.65 |
| 7.850 | 0.06 | 2.16 | 2.23 | 0.00 | 0.04 | 198 | 71.65 |
| 7.900 | 0.06 | 2.19 | 2.27 | 0.00 | 0.04 | 201 | 71.65 |
| 7.950 | 0.06 | 2.23 | 2.31 | 0.00 | 0.04 | 204 | 71.65 |
| 8.000 | 0.06 | 2.26 | 2.34 | 0.00 | 0.04 | 207 | 71.66 |
| 8.050 | 0.06 | 2.30 | 2.38 | 0.00 | 0.04 | 210 | 71.66 |
| 8.100 | 0.06 | 2.33 | 2.42 | 0.00 | 0.04 | 214 | 71.66 |
| 8.150 | 0.06 | 2.37 | 2.45 | 0.00 | 0.04 | 217 | 71.66 |
| 8.200 | 0.06 | 2.41 | 2.49 | 0.00 | 0.04 | 221 | 71.67 |
| 8.250 | 0.06 | 2.45 | 2.54 | 0.00 | 0.04 | 224 | 71.67 |
| 8.300 | 0.07 | 2.49 | 2.58 | 0.00 | 0.04 | 228 | 71.67 |
| 8.350 | 0.07 | 2.53 | 2.62 | 0.00 | 0.05 | 232 | 71.67 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.07 | 2.58 | 2.67 | 0.00 | 0.05 | 236 | 71.68 |
| 8.450 | 0.07 | 2.62 | 2.72 | 0.00 | 0.05 | 240 | 71.68 |
| 8.500 | 0.07 | 2.67 | 2.77 | 0.00 | 0.05 | 245 | 71.68 |
| 8.550 | 0.07 | 2.72 | 2.82 | 0.00 | 0.05 | 249 | 71.69 |
| 8.600 | 0.08 | 2.77 | 2.87 | 0.00 | 0.05 | 254 | 71.69 |
| 8.650 | 0.08 | 2.82 | 2.92 | 0.00 | 0.05 | 258 | 71.69 |
| 8.700 | 0.08 | 2.87 | 2.98 | 0.00 | 0.05 | 263 | 71.70 |
| 8.750 | 0.08 | 2.93 | 3.03 | 0.00 | 0.05 | 268 | 71.70 |
| 8.800 | 0.08 | 2.98 | 3.09 | 0.00 | 0.05 | 273 | 71.70 |
| 8.850 | 0.08 | 3.04 | 3.15 | 0.00 | 0.05 | 279 | 71.71 |
| 8.900 | 0.09 | 3.10 | 3.21 | 0.00 | 0.06 | 284 | 71.71 |
| 8.950 | 0.09 | 3.16 | 3.27 | 0.00 | 0.06 | 289 | 71.72 |
| 9.000 | 0.09 | 3.22 | 3.33 | 0.00 | 0.06 | 295 | 71.72 |
| 9.050 | 0.09 | 3.28 | 3.40 | 0.00 | 0.06 | 301 | 71.73 |
| 9.100 | 0.09 | 3.34 | 3.46 | 0.00 | 0.06 | 306 | 71.73 |
| 9.150 | 0.09 | 3.41 | 3.53 | 0.00 | 0.06 | 312 | 71.73 |
| 9.200 | 0.10 | 3.47 | 3.60 | 0.00 | 0.06 | 318 | 71.74 |
| 9.250 | 0.10 | 3.54 | 3.66 | 0.00 | 0.06 | 324 | 71.74 |
| 9.300 | 0.10 | 3.60 | 3.73 | 0.00 | 0.06 | 330 | 71.75 |
| 9.350 | 0.10 | 3.67 | 3.80 | 0.00 | 0.07 | 336 | 71.75 |
| 9.400 | 0.10 | 3.74 | 3.87 | 0.00 | 0.07 | 343 | 71.76 |
| 9.450 | 0.10 | 3.81 | 3.94 | 0.00 | 0.07 | 349 | 71.76 |
| 9.500 | 0.11 | 3.88 | 4.02 | 0.00 | 0.07 | 355 | 71.77 |
| 9.550 | 0.11 | 3.95 | 4.09 | 0.00 | 0.07 | 362 | 71.77 |
| 9.600 | 0.11 | 4.02 | 4.17 | 0.00 | 0.07 | 368 | 71.78 |
| 9.650 | 0.11 | 4.09 | 4.24 | 0.00 | 0.07 | 375 | 71.78 |
| 9.700 | 0.11 | 4.17 | 4.32 | 0.00 | 0.07 | 382 | 71.79 |
| 9.750 | 0.11 | 4.24 | 4.39 | 0.00 | 0.08 | 389 | 71.79 |
| 9.800 | 0.12 | 4.32 | 4.47 | 0.00 | 0.08 | 395 | 71.80 |
| 9.850 | 0.12 | 4.39 | 4.55 | 0.00 | 0.08 | 402 | 71.80 |
| 9.900 | 0.12 | 4.47 | 4.63 | 0.00 | 0.08 | 409 | 71.81 |
| 9.950 | 0.12 | 4.55 | 4.71 | 0.00 | 0.08 | 416 | 71.81 |
| 10.000 | 0.12 | 4.62 | 4.79 | 0.00 | 0.08 | 424 | 71.82 |
| 10.050 | 0.12 | 4.70 | 4.87 | 0.00 | 0.08 | 431 | 71.82 |
| 10.100 | 0.13 | 4.78 | 4.95 | 0.00 | 0.09 | 438 | 71.83 |
| 10.150 | 0.13 | 4.86 | 5.04 | 0.00 | 0.09 | 446 | 71.83 |
| 10.200 | 0.13 | 4.95 | 5.13 | 0.00 | 0.09 | 453 | 71.84 |
| 10.250 | 0.14 | 5.04 | 5.22 | 0.00 | 0.09 | 461 | 71.85 |
| 10.300 | 0.14 | 5.13 | 5.31 | 0.00 | 0.09 | 470 | 71.85 |
| 10.350 | 0.14 | 5.22 | 5.41 | 0.00 | 0.09 | 478 | 71.86 |
| 10.400 | 0.15 | 5.32 | 5.51 | 0.00 | 0.10 | 487 | 71.87 |
| 10.450 | 0.15 | 5.42 | 5.62 | 0.00 | 0.10 | 497 | 71.87 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.15 | 5.53 | 5.72 | 0.00 | 0.10 | 506 | 71.88 |
| 10.550 | 0.16 | 5.63 | 5.84 | 0.00 | 0.10 | 516 | 71.89 |
| 10.600 | 0.16 | 5.74 | 5.95 | 0.00 | 0.10 | 526 | 71.89 |
| 10.650 | 0.16 | 5.86 | 6.07 | 0.00 | 0.11 | 537 | 71.90 |
| 10.700 | 0.17 | 5.97 | 6.19 | 0.00 | 0.11 | 547 | 71.91 |
| 10.750 | 0.17 | 6.09 | 6.31 | 0.00 | 0.11 | 558 | 71.92 |
| 10.800 | 0.17 | 6.21 | 6.44 | 0.00 | 0.11 | 569 | 71.93 |
| 10.850 | 0.18 | 6.34 | 6.56 | 0.00 | 0.11 | 581 | 71.93 |
| 10.900 | 0.18 | 6.46 | 6.70 | 0.00 | 0.12 | 592 | 71.94 |
| 10.950 | 0.18 | 6.59 | 6.83 | 0.00 | 0.12 | 604 | 71.95 |
| 11.000 | 0.19 | 6.72 | 6.97 | 0.00 | 0.12 | 616 | 71.96 |
| 11.050 | 0.19 | 6.86 | 7.11 | 0.00 | 0.12 | 628 | 71.97 |
| 11.100 | 0.20 | 7.00 | 7.25 | 0.00 | 0.13 | 641 | 71.98 |
| 11.150 | 0.21 | 7.15 | 7.41 | 0.00 | 0.13 | 655 | 71.99 |
| 11.200 | 0.22 | 7.32 | 7.58 | 0.00 | 0.13 | 670 | 72.00 |
| 11.250 | 0.23 | 7.51 | 7.77 | 0.00 | 0.13 | 680 | 72.01 |
| 11.300 | 0.24 | 7.70 | 7.97 | 0.00 | 0.13 | 691 | 72.02 |
| 11.350 | 0.24 | 7.92 | 8.19 | 0.00 | 0.13 | 703 | 72.03 |
| 11.400 | 0.25 | 8.14 | 8.41 | 0.00 | 0.14 | 716 | 72.04 |
| 11.450 | 0.26 | 8.38 | 8.65 | 0.00 | 0.14 | 729 | 72.05 |
| 11.500 | 0.27 | 8.63 | 8.90 | 0.00 | 0.14 | 743 | 72.06 |
| 11.550 | 0.28 | 8.90 | 9.18 | 0.00 | 0.14 | 759 | 72.07 |
| 11.600 | 0.30 | 9.20 | 9.48 | 0.00 | 0.14 | 776 | 72.08 |
| 11.650 | 0.32 | 9.52 | 9.81 | 0.00 | 0.14 | 794 | 72.09 |
| 11.700 | 0.34 | 9.88 | 10.17 | 0.00 | 0.15 | 814 | 72.11 |
| 11.750 | 0.36 | 10.27 | 10.57 | 0.00 | 0.15 | 837 | 72.13 |
| 11.800 | 0.37 | 10.70 | 11.01 | 0.00 | 0.15 | 861 | 72.14 |
| 11.850 | 0.38 | 11.14 | 11.45 | 0.00 | 0.15 | 886 | 72.16 |
| 11.900 | 0.38 | 11.59 | 11.90 | 0.00 | 0.16 | 911 | 72.18 |
| 11.950 | 0.39 | 12.04 | 12.36 | 0.00 | 0.16 | 937 | 72.20 |
| 12.000 | 0.41 | 12.52 | 12.84 | 0.00 | 0.16 | 963 | 72.22 |
| 12.050 | 0.43 | 13.02 | 13.35 | 0.00 | 0.17 | 992 | 72.24 |
| 12.100 | 0.44 | 13.54 | 13.88 | 0.00 | 0.17 | 1,045 | 72.26 |
| 12.150 | 0.44 | 14.07 | 14.41 | 0.00 | 0.17 | 1,111 | 72.29 |
| 12.200 | 0.43 | 14.58 | 14.93 | 0.00 | 0.18 | 1,175 | 72.31 |
| 12.250 | 0.41 | 15.06 | 15.42 | 0.00 | 0.18 | 1,235 | 72.33 |
| 12.300 | 0.41 | 15.52 | 15.88 | 0.00 | 0.18 | 1,292 | 72.35 |
| 12.350 | 0.40 | 15.96 | 16.33 | 0.00 | 0.18 | 1,346 | 72.37 |
| 12.400 | 0.40 | 16.38 | 16.76 | 0.00 | 0.19 | 1,399 | 72.39 |
| 12.450 | 0.39 | 16.79 | 17.17 | 0.00 | 0.19 | 1,450 | 72.40 |
| 12.500 | 0.39 | 17.19 | 17.57 | 0.00 | 0.19 | 1,499 | 72.42 |
| 12.550 | 0.38 | 17.56 | 17.95 | 0.00 | 0.19 | 1,546 | 72.44 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.38 | 17.93 | 18.32 | 0.00 | 0.20 | 1,592 | 72.45 |
| 12.650 | 0.38 | 18.29 | 18.68 | 0.00 | 0.20 | 1,636 | 72.47 |
| 12.700 | 0.37 | 18.63 | 19.04 | 0.00 | 0.20 | 1,679 | 72.48 |
| 12.750 | 0.37 | 18.97 | 19.38 | 0.00 | 0.20 | 1,722 | 72.49 |
| 12.800 | 0.37 | 19.31 | 19.72 | 0.00 | 0.21 | 1,756 | 72.51 |
| 12.850 | 0.37 | 19.64 | 20.05 | 0.00 | 0.21 | 1,786 | 72.52 |
| 12.900 | 0.37 | 19.97 | 20.39 | 0.00 | 0.21 | 1,816 | 72.53 |
| 12.950 | 0.37 | 20.30 | 20.71 | 0.00 | 0.21 | 1,845 | 72.54 |
| 13.000 | 0.37 | 20.62 | 21.04 | 0.00 | 0.21 | 1,874 | 72.55 |
| 13.050 | 0.37 | 20.93 | 21.36 | 0.00 | 0.21 | 1,903 | 72.56 |
| 13.100 | 0.37 | 21.25 | 21.67 | 0.00 | 0.21 | 1,932 | 72.57 |
| 13.150 | 0.37 | 21.56 | 21.99 | 0.00 | 0.21 | 1,960 | 72.58 |
| 13.200 | 0.37 | 21.87 | 22.30 | 0.00 | 0.21 | 1,988 | 72.59 |
| 13.250 | 0.37 | 22.18 | 22.61 | 0.00 | 0.22 | 2,015 | 72.60 |
| 13.300 | 0.37 | 22.48 | 22.91 | 0.00 | 0.22 | 2,043 | 72.61 |
| 13.350 | 0.37 | 22.78 | 23.22 | 0.00 | 0.22 | 2,070 | 72.61 |
| 13.400 | 0.35 | 23.06 | 23.50 | 0.00 | 0.22 | 2,095 | 72.62 |
| 13.450 | 0.27 | 23.24 | 23.68 | 0.00 | 0.22 | 2,112 | 72.63 |
| 13.500 | 0.27 | 23.35 | 23.79 | 0.00 | 0.22 | 2,121 | 72.63 |
| 13.550 | 0.27 | 23.45 | 23.89 | 0.00 | 0.22 | 2,130 | 72.64 |
| 13.600 | 0.27 | 23.54 | 23.99 | 0.00 | 0.22 | 2,139 | 72.64 |
| 13.650 | 0.27 | 23.64 | 24.08 | 0.00 | 0.22 | 2,147 | 72.64 |
| 13.700 | 0.27 | 23.73 | 24.18 | 0.00 | 0.22 | 2,156 | 72.64 |
| 13.750 | 0.27 | 23.82 | 24.27 | 0.00 | 0.22 | 2,164 | 72.65 |
| 13.800 | 0.27 | 23.91 | 24.36 | 0.00 | 0.22 | 2,172 | 72.65 |
| 13.850 | 0.27 | 24.00 | 24.45 | 0.00 | 0.22 | 2,180 | 72.65 |
| 13.900 | 0.26 | 24.09 | 24.53 | 0.00 | 0.22 | 2,188 | 72.66 |
| 13.950 | 0.26 | 24.17 | 24.62 | 0.00 | 0.22 | 2,195 | 72.66 |
| 14.000 | 0.26 | 24.25 | 24.70 | 0.00 | 0.22 | 2,203 | 72.66 |
| 14.050 | 0.26 | 24.33 | 24.78 | 0.00 | 0.22 | 2,210 | 72.66 |
| 14.100 | 0.26 | 24.41 | 24.85 | 0.00 | 0.22 | 2,217 | 72.66 |
| 14.150 | 0.26 | 24.48 | 24.93 | 0.00 | 0.22 | 2,224 | 72.67 |
| 14.200 | 0.26 | 24.56 | 25.00 | 0.00 | 0.22 | 2,230 | 72.67 |
| 14.250 | 0.26 | 24.63 | 25.08 | 0.00 | 0.22 | 2,237 | 72.67 |
| 14.300 | 0.26 | 24.70 | 25.15 | 0.00 | 0.23 | 2,243 | 72.67 |
| 14.350 | 0.26 | 24.77 | 25.22 | 0.00 | 0.23 | 2,250 | 72.68 |
| 14.400 | 0.26 | 24.84 | 25.29 | 0.00 | 0.23 | 2,256 | 72.68 |
| 14.450 | 0.26 | 24.91 | 25.36 | 0.00 | 0.23 | 2,262 | 72.68 |
| 14.500 | 0.26 | 24.97 | 25.42 | 0.00 | 0.23 | 2,268 | 72.68 |
| 14.550 | 0.26 | 25.04 | 25.49 | 0.00 | 0.23 | 2,274 | 72.68 |
| 14.600 | 0.26 | 25.10 | 25.56 | 0.00 | 0.23 | 2,280 | 72.69 |
| 14.650 | 0.26 | 25.17 | 25.62 | 0.00 | 0.23 | 2,285 | 72.69 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.26 | 25.23 | 25.68 | 0.00 | 0.23 | 2,291 | 72.69 |
| 14.750 | 0.26 | 25.29 | 25.74 | 0.00 | 0.23 | 2,296 | 72.69 |
| 14.800 | 0.26 | 25.35 | 25.80 | 0.00 | 0.23 | 2,302 | 72.69 |
| 14.850 | 0.26 | 25.41 | 25.86 | 0.00 | 0.23 | 2,307 | 72.70 |
| 14.900 | 0.26 | 25.46 | 25.92 | 0.00 | 0.23 | 2,312 | 72.70 |
| 14.950 | 0.26 | 25.52 | 25.98 | 0.00 | 0.23 | 2,317 | 72.70 |
| 15.000 | 0.26 | 25.57 | 26.03 | 0.00 | 0.23 | 2,322 | 72.70 |
| 15.050 | 0.26 | 25.63 | 26.09 | 0.00 | 0.23 | 2,327 | 72.70 |
| 15.100 | 0.25 | 25.68 | 26.14 | 0.00 | 0.23 | 2,332 | 72.70 |
| 15.150 | 0.25 | 25.73 | 26.19 | 0.00 | 0.23 | 2,337 | 72.71 |
| 15.200 | 0.25 | 25.78 | 26.24 | 0.00 | 0.23 | 2,341 | 72.71 |
| 15.250 | 0.25 | 25.83 | 26.29 | 0.00 | 0.23 | 2,346 | 72.71 |
| 15.300 | 0.25 | 25.88 | 26.34 | 0.00 | 0.23 | 2,350 | 72.71 |
| 15.350 | 0.25 | 25.93 | 26.39 | 0.00 | 0.23 | 2,354 | 72.71 |
| 15.400 | 0.25 | 25.97 | 26.43 | 0.00 | 0.23 | 2,358 | 72.71 |
| 15.450 | 0.25 | 26.02 | 26.48 | 0.00 | 0.23 | 2,363 | 72.72 |
| 15.500 | 0.25 | 26.06 | 26.52 | 0.00 | 0.23 | 2,366 | 72.72 |
| 15.550 | 0.25 | 26.11 | 26.57 | 0.00 | 0.23 | 2,370 | 72.72 |
| 15.600 | 0.25 | 26.15 | 26.61 | 0.00 | 0.23 | 2,374 | 72.72 |
| 15.650 | 0.25 | 26.19 | 26.65 | 0.00 | 0.23 | 2,378 | 72.72 |
| 15.700 | 0.25 | 26.23 | 26.69 | 0.00 | 0.23 | 2,382 | 72.72 |
| 15.750 | 0.25 | 26.27 | 26.73 | 0.00 | 0.23 | 2,385 | 72.72 |
| 15.800 | 0.25 | 26.31 | 26.77 | 0.00 | 0.23 | 2,388 | 72.72 |
| 15.850 | 0.25 | 26.34 | 26.81 | 0.00 | 0.23 | 2,392 | 72.73 |
| 15.900 | 0.25 | 26.38 | 26.84 | 0.00 | 0.23 | 2,395 | 72.73 |
| 15.950 | 0.25 | 26.42 | 26.88 | 0.00 | 0.23 | 2,398 | 72.73 |
| 16.000 | 0.25 | 26.45 | 26.91 | 0.00 | 0.23 | 2,401 | 72.73 |
| 16.050 | 0.25 | 26.48 | 26.95 | 0.00 | 0.23 | 2,404 | 72.73 |
| 16.100 | 0.25 | 26.52 | 26.98 | 0.00 | 0.23 | 2,407 | 72.73 |
| 16.150 | 0.25 | 26.55 | 27.01 | 0.00 | 0.23 | 2,410 | 72.73 |
| 16.200 | 0.25 | 26.58 | 27.04 | 0.00 | 0.23 | 2,413 | 72.73 |
| 16.250 | 0.25 | 26.61 | 27.07 | 0.00 | 0.23 | 2,416 | 72.73 |
| 16.300 | 0.25 | 26.64 | 27.10 | 0.00 | 0.23 | 2,418 | 72.73 |
| 16.350 | 0.25 | 26.67 | 27.13 | 0.00 | 0.23 | 2,421 | 72.74 |
| 16.400 | 0.25 | 26.70 | 27.16 | 0.00 | 0.23 | 2,424 | 72.74 |
| 16.450 | 0.25 | 26.72 | 27.19 | 0.00 | 0.23 | 2,426 | 72.74 |
| 16.500 | 0.25 | 26.75 | 27.22 | 0.00 | 0.23 | 2,429 | 72.74 |
| 16.550 | 0.22 | 26.75 | 27.21 | 0.00 | 0.23 | 2,428 | 72.74 |
| 16.600 | 0.13 | 26.63 | 27.10 | 0.00 | 0.23 | 2,418 | 72.73 |
| 16.650 | 0.13 | 26.44 | 26.90 | 0.00 | 0.23 | 2,400 | 72.73 |
| 16.700 | 0.13 | 26.24 | 26.70 | 0.00 | 0.23 | 2,382 | 72.72 |
| 16.750 | 0.13 | 26.04 | 26.50 | 0.00 | 0.23 | 2,364 | 72.72 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.13 | 25.85 | 26.30 | 0.00 | 0.23 | 2,347 | 72.71 |
| 16.850 | 0.13 | 25.65 | 26.11 | 0.00 | 0.23 | 2,329 | 72.70 |
| 16.900 | 0.13 | 25.46 | 25.91 | 0.00 | 0.23 | 2,312 | 72.70 |
| 16.950 | 0.13 | 25.26 | 25.72 | 0.00 | 0.23 | 2,294 | 72.69 |
| 17.000 | 0.13 | 25.07 | 25.52 | 0.00 | 0.23 | 2,276 | 72.69 |
| 17.050 | 0.13 | 24.87 | 25.33 | 0.00 | 0.23 | 2,259 | 72.68 |
| 17.100 | 0.13 | 24.68 | 25.13 | 0.00 | 0.22 | 2,242 | 72.67 |
| 17.150 | 0.13 | 24.49 | 24.94 | 0.00 | 0.22 | 2,224 | 72.67 |
| 17.200 | 0.13 | 24.30 | 24.74 | 0.00 | 0.22 | 2,207 | 72.66 |
| 17.250 | 0.13 | 24.11 | 24.55 | 0.00 | 0.22 | 2,190 | 72.66 |
| 17.300 | 0.13 | 23.92 | 24.36 | 0.00 | 0.22 | 2,172 | 72.65 |
| 17.350 | 0.13 | 23.73 | 24.17 | 0.00 | 0.22 | 2,155 | 72.64 |
| 17.400 | 0.13 | 23.54 | 23.98 | 0.00 | 0.22 | 2,138 | 72.64 |
| 17.450 | 0.13 | 23.35 | 23.79 | 0.00 | 0.22 | 2,121 | 72.63 |
| 17.500 | 0.12 | 23.16 | 23.60 | 0.00 | 0.22 | 2,104 | 72.63 |
| 17.550 | 0.12 | 22.97 | 23.41 | 0.00 | 0.22 | 2,087 | 72.62 |
| 17.600 | 0.12 | 22.78 | 23.22 | 0.00 | 0.22 | 2,070 | 72.61 |
| 17.650 | 0.12 | 22.59 | 23.03 | 0.00 | 0.22 | 2,053 | 72.61 |
| 17.700 | 0.12 | 22.41 | 22.84 | 0.00 | 0.22 | 2,036 | 72.60 |
| 17.750 | 0.12 | 22.22 | 22.65 | 0.00 | 0.22 | 2,019 | 72.60 |
| 17.800 | 0.12 | 22.03 | 22.47 | 0.00 | 0.22 | 2,002 | 72.59 |
| 17.850 | 0.12 | 21.85 | 22.28 | 0.00 | 0.21 | 1,986 | 72.59 |
| 17.900 | 0.12 | 21.66 | 22.09 | 0.00 | 0.21 | 1,969 | 72.58 |
| 17.950 | 0.12 | 21.48 | 21.91 | 0.00 | 0.21 | 1,952 | 72.57 |
| 18.000 | 0.12 | 21.30 | 21.72 | 0.00 | 0.21 | 1,936 | 72.57 |
| 18.050 | 0.12 | 21.11 | 21.54 | 0.00 | 0.21 | 1,919 | 72.56 |
| 18.100 | 0.12 | 20.93 | 21.35 | 0.00 | 0.21 | 1,903 | 72.56 |
| 18.150 | 0.12 | 20.75 | 21.17 | 0.00 | 0.21 | 1,886 | 72.55 |
| 18.200 | 0.12 | 20.56 | 20.98 | 0.00 | 0.21 | 1,870 | 72.55 |
| 18.250 | 0.12 | 20.38 | 20.80 | 0.00 | 0.21 | 1,853 | 72.54 |
| 18.300 | 0.12 | 20.20 | 20.62 | 0.00 | 0.21 | 1,837 | 72.53 |
| 18.350 | 0.12 | 20.03 | 20.44 | 0.00 | 0.21 | 1,821 | 72.53 |
| 18.400 | 0.12 | 19.85 | 20.26 | 0.00 | 0.21 | 1,805 | 72.52 |
| 18.450 | 0.12 | 19.67 | 20.09 | 0.00 | 0.21 | 1,789 | 72.52 |
| 18.500 | 0.12 | 19.50 | 19.91 | 0.00 | 0.21 | 1,773 | 72.51 |
| 18.550 | 0.12 | 19.32 | 19.73 | 0.00 | 0.21 | 1,758 | 72.51 |
| 18.600 | 0.12 | 19.15 | 19.56 | 0.00 | 0.20 | 1,742 | 72.50 |
| 18.650 | 0.12 | 18.98 | 19.39 | 0.00 | 0.20 | 1,722 | 72.50 |
| 18.700 | 0.12 | 18.81 | 19.21 | 0.00 | 0.20 | 1,701 | 72.49 |
| 18.750 | 0.12 | 18.64 | 19.04 | 0.00 | 0.20 | 1,680 | 72.48 |
| 18.800 | 0.12 | 18.47 | 18.87 | 0.00 | 0.20 | 1,660 | 72.47 |
| 18.850 | 0.12 | 18.31 | 18.71 | 0.00 | 0.20 | 1,639 | 72.47 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.12 | 18.15 | 18.54 | 0.00 | 0.20 | 1,619 | 72.46 |
| 18.950 | 0.12 | 17.99 | 18.38 | 0.00 | 0.20 | 1,599 | 72.45 |
| 19.000 | 0.12 | 17.83 | 18.22 | 0.00 | 0.20 | 1,579 | 72.45 |
| 19.050 | 0.12 | 17.67 | 18.06 | 0.00 | 0.20 | 1,559 | 72.44 |
| 19.100 | 0.12 | 17.51 | 17.90 | 0.00 | 0.19 | 1,540 | 72.43 |
| 19.150 | 0.12 | 17.36 | 17.75 | 0.00 | 0.19 | 1,521 | 72.43 |
| 19.200 | 0.12 | 17.21 | 17.59 | 0.00 | 0.19 | 1,502 | 72.42 |
| 19.250 | 0.12 | 17.06 | 17.44 | 0.00 | 0.19 | 1,483 | 72.41 |
| 19.300 | 0.12 | 16.91 | 17.29 | 0.00 | 0.19 | 1,464 | 72.41 |
| 19.350 | 0.12 | 16.76 | 17.14 | 0.00 | 0.19 | 1,446 | 72.40 |
| 19.400 | 0.12 | 16.61 | 16.99 | 0.00 | 0.19 | 1,428 | 72.39 |
| 19.450 | 0.12 | 16.47 | 16.84 | 0.00 | 0.19 | 1,410 | 72.39 |
| 19.500 | 0.12 | 16.32 | 16.70 | 0.00 | 0.19 | 1,392 | 72.38 |
| 19.550 | 0.12 | 16.18 | 16.55 | 0.00 | 0.19 | 1,374 | 72.38 |
| 19.600 | 0.12 | 16.04 | 16.41 | 0.00 | 0.19 | 1,357 | 72.37 |
| 19.650 | 0.12 | 15.90 | 16.27 | 0.00 | 0.18 | 1,339 | 72.36 |
| 19.700 | 0.11 | 15.77 | 16.13 | 0.00 | 0.18 | 1,322 | 72.36 |
| 19.750 | 0.11 | 15.63 | 16.00 | 0.00 | 0.18 | 1,305 | 72.35 |
| 19.800 | 0.11 | 15.50 | 15.86 | 0.00 | 0.18 | 1,289 | 72.35 |
| 19.850 | 0.11 | 15.36 | 15.72 | 0.00 | 0.18 | 1,272 | 72.34 |
| 19.900 | 0.11 | 15.23 | 15.59 | 0.00 | 0.18 | 1,256 | 72.34 |
| 19.950 | 0.11 | 15.10 | 15.46 | 0.00 | 0.18 | 1,239 | 72.33 |
| 20.000 | 0.11 | 14.97 | 15.33 | 0.00 | 0.18 | 1,223 | 72.33 |
| 20.050 | 0.04 | 14.77 | 15.13 | 0.00 | 0.18 | 1,198 | 72.32 |
| 20.100 | 0.04 | 14.50 | 14.85 | 0.00 | 0.18 | 1,165 | 72.31 |
| 20.150 | 0.04 | 14.23 | 14.58 | 0.00 | 0.17 | 1,131 | 72.29 |
| 20.200 | 0.04 | 13.96 | 14.31 | 0.00 | 0.17 | 1,097 | 72.28 |
| 20.250 | 0.04 | 13.70 | 14.04 | 0.00 | 0.17 | 1,065 | 72.27 |
| 20.300 | 0.04 | 13.43 | 13.77 | 0.00 | 0.17 | 1,032 | 72.26 |
| 20.350 | 0.04 | 13.18 | 13.51 | 0.00 | 0.17 | 1,001 | 72.25 |
| 20.400 | 0.04 | 12.92 | 13.25 | 0.00 | 0.17 | 986 | 72.24 |
| 20.450 | 0.04 | 12.67 | 12.99 | 0.00 | 0.16 | 972 | 72.23 |
| 20.500 | 0.04 | 12.42 | 12.74 | 0.00 | 0.16 | 958 | 72.22 |
| 20.550 | 0.04 | 12.17 | 12.49 | 0.00 | 0.16 | 944 | 72.21 |
| 20.600 | 0.04 | 11.92 | 12.24 | 0.00 | 0.16 | 930 | 72.20 |
| 20.650 | 0.04 | 11.68 | 12.00 | 0.00 | 0.16 | 916 | 72.19 |
| 20.700 | 0.04 | 11.44 | 11.75 | 0.00 | 0.16 | 903 | 72.18 |
| 20.750 | 0.04 | 11.20 | 11.51 | 0.00 | 0.16 | 889 | 72.17 |
| 20.800 | 0.04 | 10.97 | 11.28 | 0.00 | 0.15 | 876 | 72.16 |
| 20.850 | 0.04 | 10.74 | 11.04 | 0.00 | 0.15 | 863 | 72.15 |
| 20.900 | 0.04 | 10.51 | 10.81 | 0.00 | 0.15 | 850 | 72.14 |
| 20.950 | 0.04 | 10.28 | 10.58 | 0.00 | 0.15 | 837 | 72.13 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.04 | 10.06 | 10.35 | 0.00 | 0.15 | 824 | 72.12 |
| 21.050 | 0.04 | 9.83 | 10.13 | 0.00 | 0.15 | 812 | 72.11 |
| 21.100 | 0.04 | 9.62 | 9.91 | 0.00 | 0.15 | 799 | 72.10 |
| 21.150 | 0.04 | 9.40 | 9.69 | 0.00 | 0.14 | 787 | 72.09 |
| 21.200 | 0.04 | 9.18 | 9.47 | 0.00 | 0.14 | 775 | 72.08 |
| 21.250 | 0.03 | 8.97 | 9.25 | 0.00 | 0.14 | 763 | 72.07 |
| 21.300 | 0.03 | 8.76 | 9.04 | 0.00 | 0.14 | 751 | 72.06 |
| 21.350 | 0.03 | 8.55 | 8.83 | 0.00 | 0.14 | 739 | 72.05 |
| 21.400 | 0.03 | 8.35 | 8.62 | 0.00 | 0.14 | 728 | 72.04 |
| 21.450 | 0.03 | 8.14 | 8.42 | 0.00 | 0.14 | 716 | 72.04 |
| 21.500 | 0.03 | 7.94 | 8.21 | 0.00 | 0.13 | 705 | 72.03 |
| 21.550 | 0.03 | 7.74 | 8.01 | 0.00 | 0.13 | 693 | 72.02 |
| 21.600 | 0.03 | 7.55 | 7.81 | 0.00 | 0.13 | 682 | 72.01 |
| 21.650 | 0.03 | 7.35 | 7.61 | 0.00 | 0.13 | 671 | 72.00 |
| 21.700 | 0.03 | 7.16 | 7.42 | 0.00 | 0.13 | 656 | 71.99 |
| 21.750 | 0.03 | 6.98 | 7.23 | 0.00 | 0.13 | 639 | 71.98 |
| 21.800 | 0.03 | 6.80 | 7.04 | 0.00 | 0.12 | 623 | 71.97 |
| 21.850 | 0.03 | 6.63 | 6.87 | 0.00 | 0.12 | 607 | 71.95 |
| 21.900 | 0.03 | 6.46 | 6.69 | 0.00 | 0.12 | 592 | 71.94 |
| 21.950 | 0.03 | 6.30 | 6.53 | 0.00 | 0.11 | 577 | 71.93 |
| 22.000 | 0.03 | 6.14 | 6.37 | 0.00 | 0.11 | 563 | 71.92 |
| 22.050 | 0.03 | 5.99 | 6.21 | 0.00 | 0.11 | 549 | 71.91 |
| 22.100 | 0.03 | 5.85 | 6.06 | 0.00 | 0.10 | 536 | 71.90 |
| 22.150 | 0.03 | 5.71 | 5.91 | 0.00 | 0.10 | 523 | 71.89 |
| 22.200 | 0.03 | 5.57 | 5.77 | 0.00 | 0.10 | 510 | 71.88 |
| 22.250 | 0.03 | 5.44 | 5.64 | 0.00 | 0.10 | 498 | 71.87 |
| 22.300 | 0.03 | 5.31 | 5.50 | 0.00 | 0.10 | 487 | 71.86 |
| 22.350 | 0.03 | 5.19 | 5.37 | 0.00 | 0.09 | 475 | 71.86 |
| 22.400 | 0.03 | 5.07 | 5.25 | 0.00 | 0.09 | 464 | 71.85 |
| 22.450 | 0.03 | 4.95 | 5.13 | 0.00 | 0.09 | 454 | 71.84 |
| 22.500 | 0.03 | 4.84 | 5.01 | 0.00 | 0.09 | 443 | 71.83 |
| 22.550 | 0.03 | 4.73 | 4.90 | 0.00 | 0.08 | 434 | 71.82 |
| 22.600 | 0.03 | 4.63 | 4.79 | 0.00 | 0.08 | 424 | 71.82 |
| 22.650 | 0.03 | 4.53 | 4.69 | 0.00 | 0.08 | 415 | 71.81 |
| 22.700 | 0.03 | 4.43 | 4.59 | 0.00 | 0.08 | 406 | 71.80 |
| 22.750 | 0.03 | 4.33 | 4.49 | 0.00 | 0.08 | 397 | 71.80 |
| 22.800 | 0.03 | 4.24 | 4.39 | 0.00 | 0.08 | 388 | 71.79 |
| 22.850 | 0.03 | 4.15 | 4.30 | 0.00 | 0.07 | 380 | 71.78 |
| 22.900 | 0.03 | 4.06 | 4.21 | 0.00 | 0.07 | 372 | 71.78 |
| 22.950 | 0.03 | 3.98 | 4.12 | 0.00 | 0.07 | 365 | 71.77 |
| 23.000 | 0.03 | 3.90 | 4.04 | 0.00 | 0.07 | 357 | 71.77 |
| 23.050 | 0.03 | 3.82 | 3.96 | 0.00 | 0.07 | 350 | 71.76 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.03 | 3.74 | 3.88 | 0.00 | 0.07 | 343 | 71.76 |
| 23.150 | 0.03 | 3.67 | 3.80 | 0.00 | 0.07 | 336 | 71.75 |
| 23.200 | 0.03 | 3.59 | 3.72 | 0.00 | 0.06 | 329 | 71.75 |
| 23.250 | 0.03 | 3.52 | 3.65 | 0.00 | 0.06 | 323 | 71.74 |
| 23.300 | 0.03 | 3.46 | 3.58 | 0.00 | 0.06 | 317 | 71.74 |
| 23.350 | 0.03 | 3.39 | 3.51 | 0.00 | 0.06 | 311 | 71.73 |
| 23.400 | 0.03 | 3.33 | 3.45 | 0.00 | 0.06 | 305 | 71.73 |
| 23.450 | 0.03 | 3.27 | 3.38 | 0.00 | 0.06 | 299 | 71.72 |
| 23.500 | 0.03 | 3.21 | 3.32 | 0.00 | 0.06 | 294 | 71.72 |
| 23.550 | 0.03 | 3.15 | 3.26 | 0.00 | 0.06 | 288 | 71.72 |
| 23.600 | 0.03 | 3.09 | 3.20 | 0.00 | 0.06 | 283 | 71.71 |
| 23.650 | 0.03 | 3.04 | 3.14 | 0.00 | 0.05 | 278 | 71.71 |
| 23.700 | 0.03 | 2.98 | 3.09 | 0.00 | 0.05 | 273 | 71.70 |
| 23.750 | 0.03 | 2.93 | 3.04 | 0.00 | 0.05 | 268 | 71.70 |
| 23.800 | 0.03 | 2.88 | 2.98 | 0.00 | 0.05 | 264 | 71.70 |
| 23.850 | 0.03 | 2.83 | 2.93 | 0.00 | 0.05 | 259 | 71.69 |
| 23.900 | 0.03 | 2.78 | 2.88 | 0.00 | 0.05 | 255 | 71.69 |
| 23.950 | 0.03 | 2.74 | 2.84 | 0.00 | 0.05 | 251 | 71.69 |
| 24.000 | 0.03 | 2.69 | 2.79 | 0.00 | 0.05 | 247 | 71.68 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 71.50 |
| 0.050 | 0.00 | 0.17 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 0.100 | 0.00 | 0.17 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.150 | 0.00 | 0.16 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.200 | 0.00 | 0.16 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.250 | 0.00 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.300 | 0.00 | 0.15 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.350 | 0.00 | 0.14 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.400 | 0.00 | 0.14 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.450 | 0.00 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.500 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 0.550 | 0.00 | 0.12 | 0.13 | 0.00 | 0.00 | 11 | 71.51 |
| 0.600 | 0.00 | 0.12 | 0.12 | 0.00 | 0.00 | 11 | 71.51 |
| 0.650 | 0.00 | 0.11 | 0.12 | 0.00 | 0.00 | 10 | 71.51 |
| 0.700 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.750 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.800 | 0.00 | 0.10 | 0.11 | 0.00 | 0.00 | 9 | 71.51 |
| 0.850 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 0.900 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 0.950 | 0.00 | 0.09 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 1.000 | 0.00 | 0.09 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 1.050 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 1.100 | 0.00 | 0.10 | 0.10 | 0.00 | 0.00 | 9 | 71.51 |
| 1.150 | 0.01 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 1.200 | 0.01 | 0.12 | 0.12 | 0.00 | 0.00 | 11 | 71.51 |
| 1.250 | 0.01 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 1.300 | 0.01 | 0.14 | 0.14 | 0.00 | 0.00 | 13 | 71.51 |
| 1.350 | 0.01 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 1.400 | 0.01 | 0.17 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 1.450 | 0.01 | 0.18 | 0.19 | 0.00 | 0.00 | 17 | 71.51 |
| 1.500 | 0.01 | 0.20 | 0.21 | 0.00 | 0.00 | 18 | 71.51 |
| 1.550 | 0.01 | 0.22 | 0.22 | 0.00 | 0.00 | 20 | 71.51 |
| 1.600 | 0.01 | 0.24 | 0.24 | 0.00 | 0.00 | 22 | 71.52 |
| 1.650 | 0.02 | 0.26 | 0.27 | 0.00 | 0.00 | 23 | 71.52 |
| 1.700 | 0.02 | 0.28 | 0.29 | 0.00 | 0.00 | 25 | 71.52 |
| 1.750 | 0.02 | 0.30 | 0.31 | 0.00 | 0.01 | 27 | 71.52 |
| 1.800 | 0.02 | 0.32 | 0.33 | 0.00 | 0.01 | 29 | 71.52 |
| 1.850 | 0.02 | 0.34 | 0.36 | 0.00 | 0.01 | 31 | 71.52 |
| 1.900 | 0.02 | 0.37 | 0.38 | 0.00 | 0.01 | 34 | 71.53 |
| 1.950 | 0.02 | 0.39 | 0.41 | 0.00 | 0.01 | 36 | 71.53 |
| 2.000 | 0.02 | 0.42 | 0.43 | 0.00 | 0.01 | 38 | 71.53 |
| 2.050 | 0.02 | 0.44 | 0.46 | 0.00 | 0.01 | 40 | 71.53 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.02 | 0.47 | 0.48 | 0.00 | 0.01 | 43 | 71.53 |
| 2.150 | 0.02 | 0.49 | 0.51 | 0.00 | 0.01 | 45 | 71.53 |
| 2.200 | 0.02 | 0.52 | 0.54 | 0.00 | 0.01 | 47 | 71.54 |
| 2.250 | 0.02 | 0.54 | 0.56 | 0.00 | 0.01 | 50 | 71.54 |
| 2.300 | 0.02 | 0.57 | 0.59 | 0.00 | 0.01 | 52 | 71.54 |
| 2.350 | 0.02 | 0.60 | 0.62 | 0.00 | 0.01 | 55 | 71.54 |
| 2.400 | 0.03 | 0.63 | 0.65 | 0.00 | 0.01 | 57 | 71.54 |
| 2.450 | 0.03 | 0.65 | 0.68 | 0.00 | 0.01 | 60 | 71.54 |
| 2.500 | 0.03 | 0.68 | 0.71 | 0.00 | 0.01 | 63 | 71.55 |
| 2.550 | 0.03 | 0.71 | 0.74 | 0.00 | 0.01 | 65 | 71.55 |
| 2.600 | 0.03 | 0.74 | 0.77 | 0.00 | 0.01 | 68 | 71.55 |
| 2.650 | 0.03 | 0.77 | 0.80 | 0.00 | 0.01 | 71 | 71.55 |
| 2.700 | 0.03 | 0.80 | 0.83 | 0.00 | 0.01 | 74 | 71.56 |
| 2.750 | 0.03 | 0.83 | 0.86 | 0.00 | 0.01 | 76 | 71.56 |
| 2.800 | 0.03 | 0.87 | 0.90 | 0.00 | 0.02 | 79 | 71.56 |
| 2.850 | 0.03 | 0.90 | 0.93 | 0.00 | 0.02 | 82 | 71.56 |
| 2.900 | 0.03 | 0.93 | 0.96 | 0.00 | 0.02 | 85 | 71.56 |
| 2.950 | 0.03 | 0.96 | 0.99 | 0.00 | 0.02 | 88 | 71.57 |
| 3.000 | 0.03 | 0.99 | 1.03 | 0.00 | 0.02 | 91 | 71.57 |
| 3.050 | 0.03 | 1.02 | 1.06 | 0.00 | 0.02 | 94 | 71.57 |
| 3.100 | 0.04 | 1.06 | 1.09 | 0.00 | 0.02 | 97 | 71.57 |
| 3.150 | 0.04 | 1.09 | 1.13 | 0.00 | 0.02 | 100 | 71.57 |
| 3.200 | 0.04 | 1.12 | 1.16 | 0.00 | 0.02 | 103 | 71.58 |
| 3.250 | 0.04 | 1.15 | 1.20 | 0.00 | 0.02 | 106 | 71.58 |
| 3.300 | 0.04 | 1.19 | 1.23 | 0.00 | 0.02 | 109 | 71.58 |
| 3.350 | 0.04 | 1.22 | 1.26 | 0.00 | 0.02 | 112 | 71.58 |
| 3.400 | 0.04 | 1.25 | 1.30 | 0.00 | 0.02 | 115 | 71.59 |
| 3.450 | 0.04 | 1.29 | 1.33 | 0.00 | 0.02 | 118 | 71.59 |
| 3.500 | 0.04 | 1.32 | 1.37 | 0.00 | 0.02 | 121 | 71.59 |
| 3.550 | 0.04 | 1.36 | 1.40 | 0.00 | 0.02 | 124 | 71.59 |
| 3.600 | 0.04 | 1.39 | 1.44 | 0.00 | 0.02 | 127 | 71.60 |
| 3.650 | 0.04 | 1.42 | 1.47 | 0.00 | 0.03 | 130 | 71.60 |
| 3.700 | 0.04 | 1.46 | 1.51 | 0.00 | 0.03 | 133 | 71.60 |
| 3.750 | 0.04 | 1.49 | 1.54 | 0.00 | 0.03 | 137 | 71.60 |
| 3.800 | 0.04 | 1.53 | 1.58 | 0.00 | 0.03 | 140 | 71.60 |
| 3.850 | 0.05 | 1.56 | 1.62 | 0.00 | 0.03 | 143 | 71.61 |
| 3.900 | 0.05 | 1.59 | 1.65 | 0.00 | 0.03 | 146 | 71.61 |
| 3.950 | 0.05 | 1.63 | 1.69 | 0.00 | 0.03 | 149 | 71.61 |
| 4.000 | 0.05 | 1.66 | 1.72 | 0.00 | 0.03 | 152 | 71.61 |
| 4.050 | 0.05 | 1.70 | 1.76 | 0.00 | 0.03 | 155 | 71.62 |
| 4.100 | 0.05 | 1.73 | 1.79 | 0.00 | 0.03 | 159 | 71.62 |
| 4.150 | 0.05 | 1.76 | 1.83 | 0.00 | 0.03 | 162 | 71.62 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.05 | 1.80 | 1.86 | 0.00 | 0.03 | 165 | 71.62 |
| 4.250 | 0.05 | 1.83 | 1.90 | 0.00 | 0.03 | 168 | 71.63 |
| 4.300 | 0.05 | 1.87 | 1.93 | 0.00 | 0.03 | 171 | 71.63 |
| 4.350 | 0.05 | 1.90 | 1.97 | 0.00 | 0.03 | 174 | 71.63 |
| 4.400 | 0.05 | 1.94 | 2.00 | 0.00 | 0.03 | 177 | 71.63 |
| 4.450 | 0.05 | 1.97 | 2.04 | 0.00 | 0.04 | 180 | 71.64 |
| 4.500 | 0.05 | 2.00 | 2.08 | 0.00 | 0.04 | 184 | 71.64 |
| 4.550 | 0.05 | 2.04 | 2.11 | 0.00 | 0.04 | 187 | 71.64 |
| 4.600 | 0.05 | 2.07 | 2.15 | 0.00 | 0.04 | 190 | 71.64 |
| 4.650 | 0.06 | 2.11 | 2.18 | 0.00 | 0.04 | 193 | 71.64 |
| 4.700 | 0.06 | 2.14 | 2.22 | 0.00 | 0.04 | 196 | 71.65 |
| 4.750 | 0.06 | 2.17 | 2.25 | 0.00 | 0.04 | 199 | 71.65 |
| 4.800 | 0.06 | 2.21 | 2.29 | 0.00 | 0.04 | 202 | 71.65 |
| 4.850 | 0.06 | 2.24 | 2.32 | 0.00 | 0.04 | 205 | 71.65 |
| 4.900 | 0.06 | 2.28 | 2.36 | 0.00 | 0.04 | 208 | 71.66 |
| 4.950 | 0.06 | 2.31 | 2.39 | 0.00 | 0.04 | 212 | 71.66 |
| 5.000 | 0.06 | 2.34 | 2.43 | 0.00 | 0.04 | 215 | 71.66 |
| 5.050 | 0.06 | 2.38 | 2.46 | 0.00 | 0.04 | 218 | 71.66 |
| 5.100 | 0.06 | 2.41 | 2.50 | 0.00 | 0.04 | 221 | 71.67 |
| 5.150 | 0.06 | 2.44 | 2.53 | 0.00 | 0.04 | 224 | 71.67 |
| 5.200 | 0.06 | 2.48 | 2.57 | 0.00 | 0.04 | 227 | 71.67 |
| 5.250 | 0.06 | 2.51 | 2.60 | 0.00 | 0.05 | 230 | 71.67 |
| 5.300 | 0.06 | 2.54 | 2.63 | 0.00 | 0.05 | 233 | 71.67 |
| 5.350 | 0.06 | 2.58 | 2.67 | 0.00 | 0.05 | 236 | 71.68 |
| 5.400 | 0.06 | 2.61 | 2.70 | 0.00 | 0.05 | 239 | 71.68 |
| 5.450 | 0.06 | 2.64 | 2.74 | 0.00 | 0.05 | 242 | 71.68 |
| 5.500 | 0.06 | 2.67 | 2.77 | 0.00 | 0.05 | 245 | 71.68 |
| 5.550 | 0.07 | 2.71 | 2.80 | 0.00 | 0.05 | 248 | 71.69 |
| 5.600 | 0.07 | 2.74 | 2.84 | 0.00 | 0.05 | 251 | 71.69 |
| 5.650 | 0.07 | 2.77 | 2.87 | 0.00 | 0.05 | 254 | 71.69 |
| 5.700 | 0.07 | 2.81 | 2.91 | 0.00 | 0.05 | 257 | 71.69 |
| 5.750 | 0.07 | 2.84 | 2.94 | 0.00 | 0.05 | 260 | 71.69 |
| 5.800 | 0.07 | 2.87 | 2.97 | 0.00 | 0.05 | 263 | 71.70 |
| 5.850 | 0.07 | 2.90 | 3.01 | 0.00 | 0.05 | 266 | 71.70 |
| 5.900 | 0.07 | 2.93 | 3.04 | 0.00 | 0.05 | 269 | 71.70 |
| 5.950 | 0.07 | 2.97 | 3.07 | 0.00 | 0.05 | 272 | 71.70 |
| 6.000 | 0.07 | 3.00 | 3.11 | 0.00 | 0.05 | 275 | 71.71 |
| 6.050 | 0.07 | 3.03 | 3.14 | 0.00 | 0.05 | 278 | 71.71 |
| 6.100 | 0.07 | 3.06 | 3.17 | 0.00 | 0.05 | 281 | 71.71 |
| 6.150 | 0.07 | 3.10 | 3.21 | 0.00 | 0.06 | 284 | 71.71 |
| 6.200 | 0.07 | 3.13 | 3.24 | 0.00 | 0.06 | 287 | 71.71 |
| 6.250 | 0.07 | 3.17 | 3.28 | 0.00 | 0.06 | 290 | 71.72 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.08 | 3.20 | 3.32 | 0.00 | 0.06 | 293 | 71.72 |
| 6.350 | 0.08 | 3.24 | 3.36 | 0.00 | 0.06 | 297 | 71.72 |
| 6.400 | 0.08 | 3.28 | 3.40 | 0.00 | 0.06 | 300 | 71.72 |
| 6.450 | 0.08 | 3.32 | 3.44 | 0.00 | 0.06 | 304 | 71.73 |
| 6.500 | 0.08 | 3.36 | 3.48 | 0.00 | 0.06 | 308 | 71.73 |
| 6.550 | 0.08 | 3.40 | 3.52 | 0.00 | 0.06 | 312 | 71.73 |
| 6.600 | 0.08 | 3.45 | 3.57 | 0.00 | 0.06 | 316 | 71.74 |
| 6.650 | 0.09 | 3.49 | 3.62 | 0.00 | 0.06 | 320 | 71.74 |
| 6.700 | 0.09 | 3.54 | 3.66 | 0.00 | 0.06 | 324 | 71.74 |
| 6.750 | 0.09 | 3.58 | 3.71 | 0.00 | 0.06 | 328 | 71.75 |
| 6.800 | 0.09 | 3.63 | 3.76 | 0.00 | 0.07 | 333 | 71.75 |
| 6.850 | 0.09 | 3.68 | 3.81 | 0.00 | 0.07 | 337 | 71.75 |
| 6.900 | 0.09 | 3.73 | 3.86 | 0.00 | 0.07 | 342 | 71.76 |
| 6.950 | 0.09 | 3.78 | 3.92 | 0.00 | 0.07 | 346 | 71.76 |
| 7.000 | 0.10 | 3.83 | 3.97 | 0.00 | 0.07 | 351 | 71.76 |
| 7.050 | 0.10 | 3.88 | 4.02 | 0.00 | 0.07 | 356 | 71.77 |
| 7.100 | 0.10 | 3.94 | 4.08 | 0.00 | 0.07 | 361 | 71.77 |
| 7.150 | 0.10 | 3.99 | 4.13 | 0.00 | 0.07 | 366 | 71.77 |
| 7.200 | 0.10 | 4.05 | 4.19 | 0.00 | 0.07 | 371 | 71.78 |
| 7.250 | 0.10 | 4.10 | 4.25 | 0.00 | 0.07 | 376 | 71.78 |
| 7.300 | 0.10 | 4.16 | 4.31 | 0.00 | 0.07 | 381 | 71.79 |
| 7.350 | 0.10 | 4.21 | 4.36 | 0.00 | 0.08 | 386 | 71.79 |
| 7.400 | 0.11 | 4.27 | 4.42 | 0.00 | 0.08 | 391 | 71.79 |
| 7.450 | 0.11 | 4.33 | 4.48 | 0.00 | 0.08 | 397 | 71.80 |
| 7.500 | 0.11 | 4.39 | 4.55 | 0.00 | 0.08 | 402 | 71.80 |
| 7.550 | 0.11 | 4.45 | 4.61 | 0.00 | 0.08 | 407 | 71.81 |
| 7.600 | 0.11 | 4.51 | 4.67 | 0.00 | 0.08 | 413 | 71.81 |
| 7.650 | 0.11 | 4.57 | 4.73 | 0.00 | 0.08 | 419 | 71.81 |
| 7.700 | 0.11 | 4.63 | 4.80 | 0.00 | 0.08 | 424 | 71.82 |
| 7.750 | 0.12 | 4.69 | 4.86 | 0.00 | 0.08 | 430 | 71.82 |
| 7.800 | 0.12 | 4.75 | 4.92 | 0.00 | 0.09 | 436 | 71.83 |
| 7.850 | 0.12 | 4.82 | 4.99 | 0.00 | 0.09 | 441 | 71.83 |
| 7.900 | 0.12 | 4.88 | 5.06 | 0.00 | 0.09 | 447 | 71.83 |
| 7.950 | 0.12 | 4.94 | 5.12 | 0.00 | 0.09 | 453 | 71.84 |
| 8.000 | 0.12 | 5.01 | 5.19 | 0.00 | 0.09 | 459 | 71.84 |
| 8.050 | 0.12 | 5.07 | 5.26 | 0.00 | 0.09 | 465 | 71.85 |
| 8.100 | 0.13 | 5.14 | 5.32 | 0.00 | 0.09 | 471 | 71.85 |
| 8.150 | 0.13 | 5.21 | 5.39 | 0.00 | 0.09 | 477 | 71.86 |
| 8.200 | 0.13 | 5.28 | 5.47 | 0.00 | 0.09 | 484 | 71.86 |
| 8.250 | 0.13 | 5.35 | 5.54 | 0.00 | 0.10 | 490 | 71.87 |
| 8.300 | 0.14 | 5.43 | 5.62 | 0.00 | 0.10 | 497 | 71.87 |
| 8.350 | 0.14 | 5.51 | 5.71 | 0.00 | 0.10 | 505 | 71.88 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.14 | 5.59 | 5.79 | 0.00 | 0.10 | 512 | 71.88 |
| 8.450 | 0.15 | 5.68 | 5.88 | 0.00 | 0.10 | 520 | 71.89 |
| 8.500 | 0.15 | 5.77 | 5.97 | 0.00 | 0.10 | 528 | 71.90 |
| 8.550 | 0.15 | 5.86 | 6.07 | 0.00 | 0.11 | 537 | 71.90 |
| 8.600 | 0.16 | 5.95 | 6.17 | 0.00 | 0.11 | 545 | 71.91 |
| 8.650 | 0.16 | 6.05 | 6.27 | 0.00 | 0.11 | 554 | 71.92 |
| 8.700 | 0.16 | 6.15 | 6.37 | 0.00 | 0.11 | 564 | 71.92 |
| 8.750 | 0.17 | 6.25 | 6.48 | 0.00 | 0.11 | 573 | 71.93 |
| 8.800 | 0.17 | 6.36 | 6.59 | 0.00 | 0.11 | 583 | 71.94 |
| 8.850 | 0.17 | 6.47 | 6.70 | 0.00 | 0.12 | 593 | 71.94 |
| 8.900 | 0.17 | 6.58 | 6.81 | 0.00 | 0.12 | 603 | 71.95 |
| 8.950 | 0.18 | 6.69 | 6.93 | 0.00 | 0.12 | 613 | 71.96 |
| 9.000 | 0.18 | 6.80 | 7.05 | 0.00 | 0.12 | 623 | 71.97 |
| 9.050 | 0.18 | 6.92 | 7.17 | 0.00 | 0.12 | 634 | 71.97 |
| 9.100 | 0.19 | 7.04 | 7.29 | 0.00 | 0.13 | 645 | 71.98 |
| 9.150 | 0.19 | 7.16 | 7.42 | 0.00 | 0.13 | 656 | 71.99 |
| 9.200 | 0.19 | 7.28 | 7.55 | 0.00 | 0.13 | 667 | 72.00 |
| 9.250 | 0.20 | 7.41 | 7.67 | 0.00 | 0.13 | 675 | 72.01 |
| 9.300 | 0.20 | 7.54 | 7.81 | 0.00 | 0.13 | 682 | 72.01 |
| 9.350 | 0.20 | 7.68 | 7.95 | 0.00 | 0.13 | 690 | 72.02 |
| 9.400 | 0.21 | 7.82 | 8.09 | 0.00 | 0.13 | 698 | 72.02 |
| 9.450 | 0.21 | 7.97 | 8.24 | 0.00 | 0.14 | 706 | 72.03 |
| 9.500 | 0.21 | 8.12 | 8.39 | 0.00 | 0.14 | 715 | 72.04 |
| 9.550 | 0.22 | 8.28 | 8.55 | 0.00 | 0.14 | 724 | 72.04 |
| 9.600 | 0.22 | 8.44 | 8.71 | 0.00 | 0.14 | 733 | 72.05 |
| 9.650 | 0.22 | 8.60 | 8.88 | 0.00 | 0.14 | 742 | 72.06 |
| 9.700 | 0.22 | 8.77 | 9.05 | 0.00 | 0.14 | 751 | 72.06 |
| 9.750 | 0.23 | 8.94 | 9.22 | 0.00 | 0.14 | 761 | 72.07 |
| 9.800 | 0.23 | 9.11 | 9.39 | 0.00 | 0.14 | 771 | 72.08 |
| 9.850 | 0.23 | 9.28 | 9.57 | 0.00 | 0.14 | 780 | 72.08 |
| 9.900 | 0.23 | 9.46 | 9.75 | 0.00 | 0.14 | 790 | 72.09 |
| 9.950 | 0.23 | 9.63 | 9.93 | 0.00 | 0.15 | 800 | 72.10 |
| 10.000 | 0.24 | 9.81 | 10.11 | 0.00 | 0.15 | 811 | 72.11 |
| 10.050 | 0.24 | 9.99 | 10.29 | 0.00 | 0.15 | 821 | 72.11 |
| 10.100 | 0.24 | 10.18 | 10.48 | 0.00 | 0.15 | 831 | 72.12 |
| 10.150 | 0.25 | 10.36 | 10.66 | 0.00 | 0.15 | 842 | 72.13 |
| 10.200 | 0.25 | 10.56 | 10.86 | 0.00 | 0.15 | 853 | 72.14 |
| 10.250 | 0.25 | 10.75 | 11.06 | 0.00 | 0.15 | 864 | 72.15 |
| 10.300 | 0.26 | 10.96 | 11.26 | 0.00 | 0.15 | 875 | 72.16 |
| 10.350 | 0.26 | 11.16 | 11.47 | 0.00 | 0.15 | 887 | 72.16 |
| 10.400 | 0.26 | 11.38 | 11.69 | 0.00 | 0.16 | 899 | 72.17 |
| 10.450 | 0.27 | 11.59 | 11.91 | 0.00 | 0.16 | 911 | 72.18 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.27 | 11.82 | 12.14 | 0.00 | 0.16 | 924 | 72.19 |
| 10.550 | 0.28 | 12.05 | 12.37 | 0.00 | 0.16 | 937 | 72.20 |
| 10.600 | 0.28 | 12.28 | 12.60 | 0.00 | 0.16 | 950 | 72.21 |
| 10.650 | 0.29 | 12.52 | 12.85 | 0.00 | 0.16 | 964 | 72.22 |
| 10.700 | 0.29 | 12.76 | 13.09 | 0.00 | 0.16 | 977 | 72.23 |
| 10.750 | 0.29 | 13.01 | 13.35 | 0.00 | 0.17 | 992 | 72.24 |
| 10.800 | 0.30 | 13.27 | 13.60 | 0.00 | 0.17 | 1,011 | 72.25 |
| 10.850 | 0.30 | 13.53 | 13.86 | 0.00 | 0.17 | 1,043 | 72.26 |
| 10.900 | 0.30 | 13.78 | 14.13 | 0.00 | 0.17 | 1,075 | 72.28 |
| 10.950 | 0.30 | 14.04 | 14.39 | 0.00 | 0.17 | 1,107 | 72.29 |
| 11.000 | 0.30 | 14.30 | 14.65 | 0.00 | 0.17 | 1,139 | 72.30 |
| 11.050 | 0.31 | 14.55 | 14.91 | 0.00 | 0.18 | 1,171 | 72.31 |
| 11.100 | 0.31 | 14.81 | 15.17 | 0.00 | 0.18 | 1,204 | 72.32 |
| 11.150 | 0.31 | 15.08 | 15.43 | 0.00 | 0.18 | 1,236 | 72.33 |
| 11.200 | 0.32 | 15.34 | 15.70 | 0.00 | 0.18 | 1,270 | 72.34 |
| 11.250 | 0.32 | 15.62 | 15.98 | 0.00 | 0.18 | 1,304 | 72.35 |
| 11.300 | 0.33 | 15.90 | 16.26 | 0.00 | 0.18 | 1,338 | 72.36 |
| 11.350 | 0.33 | 16.18 | 16.55 | 0.00 | 0.19 | 1,374 | 72.38 |
| 11.400 | 0.34 | 16.48 | 16.85 | 0.00 | 0.19 | 1,411 | 72.39 |
| 11.450 | 0.34 | 16.78 | 17.16 | 0.00 | 0.19 | 1,448 | 72.40 |
| 11.500 | 0.35 | 17.08 | 17.47 | 0.00 | 0.19 | 1,487 | 72.41 |
| 11.550 | 0.36 | 17.41 | 17.79 | 0.00 | 0.19 | 1,527 | 72.43 |
| 11.600 | 0.38 | 17.75 | 18.15 | 0.00 | 0.20 | 1,570 | 72.44 |
| 11.650 | 0.39 | 18.13 | 18.53 | 0.00 | 0.20 | 1,617 | 72.46 |
| 11.700 | 0.40 | 18.53 | 18.93 | 0.00 | 0.20 | 1,666 | 72.48 |
| 11.750 | 0.41 | 18.94 | 19.34 | 0.00 | 0.20 | 1,717 | 72.49 |
| 11.800 | 0.43 | 19.36 | 19.77 | 0.00 | 0.21 | 1,761 | 72.51 |
| 11.850 | 0.44 | 19.81 | 20.23 | 0.00 | 0.21 | 1,802 | 72.52 |
| 11.900 | 0.45 | 20.29 | 20.70 | 0.00 | 0.21 | 1,845 | 72.54 |
| 11.950 | 0.48 | 20.80 | 21.22 | 0.00 | 0.21 | 1,891 | 72.55 |
| 12.000 | 0.54 | 21.39 | 21.82 | 0.00 | 0.21 | 1,944 | 72.57 |
| 12.050 | 0.58 | 22.08 | 22.51 | 0.00 | 0.22 | 2,006 | 72.59 |
| 12.100 | 0.60 | 22.82 | 23.26 | 0.00 | 0.22 | 2,074 | 72.62 |
| 12.150 | 0.60 | 23.58 | 24.02 | 0.00 | 0.22 | 2,142 | 72.64 |
| 12.200 | 1.81 | 25.53 | 25.99 | 0.00 | 0.23 | 2,319 | 72.70 |
| 12.250 | 1.37 | 28.21 | 28.71 | 0.00 | 0.25 | 2,561 | 72.78 |
| 12.300 | 1.24 | 30.25 | 30.81 | 0.00 | 0.28 | 2,748 | 72.85 |
| 12.350 | 1.10 | 31.97 | 32.59 | 0.00 | 0.31 | 2,905 | 72.90 |
| 12.400 | 0.99 | 33.39 | 34.06 | 0.00 | 0.33 | 3,035 | 72.95 |
| 12.450 | 0.88 | 34.56 | 35.27 | 0.00 | 0.35 | 3,142 | 72.99 |
| 12.500 | 0.77 | 35.49 | 36.22 | 0.00 | 0.37 | 3,227 | 73.02 |
| 12.550 | 0.68 | 36.18 | 36.94 | 0.00 | 0.38 | 3,291 | 73.04 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.61 | 36.70 | 37.47 | 0.00 | 0.39 | 3,339 | 73.05 |
| 12.650 | 0.57 | 37.09 | 37.88 | 0.00 | 0.39 | 3,375 | 73.07 |
| 12.700 | 0.55 | 37.41 | 38.20 | 0.00 | 0.40 | 3,404 | 73.08 |
| 12.750 | 0.53 | 37.68 | 38.49 | 0.00 | 0.40 | 3,429 | 73.09 |
| 12.800 | 0.52 | 37.92 | 38.73 | 0.00 | 0.41 | 3,451 | 73.09 |
| 12.850 | 0.51 | 38.13 | 38.94 | 0.00 | 0.41 | 3,470 | 73.10 |
| 12.900 | 0.50 | 38.30 | 39.13 | 0.00 | 0.41 | 3,487 | 73.11 |
| 12.950 | 0.48 | 38.45 | 39.28 | 0.00 | 0.42 | 3,500 | 73.11 |
| 13.000 | 0.47 | 38.58 | 39.41 | 0.00 | 0.42 | 3,512 | 73.12 |
| 13.050 | 0.46 | 38.67 | 39.51 | 0.00 | 0.42 | 3,521 | 73.12 |
| 13.100 | 0.46 | 38.75 | 39.59 | 0.00 | 0.42 | 3,528 | 73.12 |
| 13.150 | 0.45 | 38.81 | 39.66 | 0.00 | 0.42 | 3,534 | 73.12 |
| 13.200 | 0.45 | 38.87 | 39.71 | 0.00 | 0.42 | 3,538 | 73.12 |
| 13.250 | 0.44 | 38.91 | 39.75 | 0.00 | 0.42 | 3,542 | 73.13 |
| 13.300 | 0.44 | 38.94 | 39.79 | 0.00 | 0.42 | 3,545 | 73.13 |
| 13.350 | 0.44 | 38.97 | 39.82 | 0.00 | 0.42 | 3,548 | 73.13 |
| 13.400 | 0.43 | 38.99 | 39.84 | 0.00 | 0.42 | 3,550 | 73.13 |
| 13.450 | 0.43 | 39.01 | 39.86 | 0.00 | 0.42 | 3,551 | 73.13 |
| 13.500 | 0.43 | 39.02 | 39.86 | 0.00 | 0.42 | 3,552 | 73.13 |
| 13.550 | 0.42 | 39.02 | 39.87 | 0.00 | 0.42 | 3,552 | 73.13 |
| 13.600 | 0.42 | 39.01 | 39.86 | 0.00 | 0.42 | 3,552 | 73.13 |
| 13.650 | 0.42 | 39.01 | 39.85 | 0.00 | 0.42 | 3,551 | 73.13 |
| 13.700 | 0.42 | 38.99 | 39.84 | 0.00 | 0.42 | 3,550 | 73.13 |
| 13.750 | 0.41 | 38.97 | 39.82 | 0.00 | 0.42 | 3,548 | 73.13 |
| 13.800 | 0.41 | 38.95 | 39.79 | 0.00 | 0.42 | 3,546 | 73.13 |
| 13.850 | 0.41 | 38.92 | 39.76 | 0.00 | 0.42 | 3,543 | 73.13 |
| 13.900 | 0.40 | 38.88 | 39.73 | 0.00 | 0.42 | 3,540 | 73.13 |
| 13.950 | 0.40 | 38.84 | 39.69 | 0.00 | 0.42 | 3,536 | 73.12 |
| 14.000 | 0.40 | 38.80 | 39.64 | 0.00 | 0.42 | 3,532 | 73.12 |
| 14.050 | 0.39 | 38.75 | 39.59 | 0.00 | 0.42 | 3,528 | 73.12 |
| 14.100 | 0.39 | 38.70 | 39.54 | 0.00 | 0.42 | 3,523 | 73.12 |
| 14.150 | 0.39 | 38.65 | 39.48 | 0.00 | 0.42 | 3,518 | 73.12 |
| 14.200 | 0.39 | 38.59 | 39.43 | 0.00 | 0.42 | 3,513 | 73.12 |
| 14.250 | 0.39 | 38.53 | 39.37 | 0.00 | 0.42 | 3,508 | 73.11 |
| 14.300 | 0.39 | 38.48 | 39.31 | 0.00 | 0.42 | 3,503 | 73.11 |
| 14.350 | 0.38 | 38.42 | 39.25 | 0.00 | 0.41 | 3,497 | 73.11 |
| 14.400 | 0.38 | 38.36 | 39.19 | 0.00 | 0.41 | 3,492 | 73.11 |
| 14.450 | 0.38 | 38.30 | 39.12 | 0.00 | 0.41 | 3,486 | 73.11 |
| 14.500 | 0.38 | 38.24 | 39.06 | 0.00 | 0.41 | 3,481 | 73.10 |
| 14.550 | 0.38 | 38.18 | 39.00 | 0.00 | 0.41 | 3,475 | 73.10 |
| 14.600 | 0.38 | 38.11 | 38.93 | 0.00 | 0.41 | 3,469 | 73.10 |
| 14.650 | 0.38 | 38.05 | 38.87 | 0.00 | 0.41 | 3,463 | 73.10 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.37 | 37.99 | 38.80 | 0.00 | 0.41 | 3,457 | 73.10 |
| 14.750 | 0.37 | 37.93 | 38.74 | 0.00 | 0.41 | 3,452 | 73.09 |
| 14.800 | 0.37 | 37.86 | 38.67 | 0.00 | 0.41 | 3,446 | 73.09 |
| 14.850 | 0.37 | 37.80 | 38.61 | 0.00 | 0.40 | 3,441 | 73.09 |
| 14.900 | 0.37 | 37.75 | 38.55 | 0.00 | 0.40 | 3,435 | 73.09 |
| 14.950 | 0.37 | 37.69 | 38.49 | 0.00 | 0.40 | 3,430 | 73.09 |
| 15.000 | 0.37 | 37.63 | 38.44 | 0.00 | 0.40 | 3,425 | 73.08 |
| 15.050 | 0.37 | 37.58 | 38.38 | 0.00 | 0.40 | 3,420 | 73.08 |
| 15.100 | 0.37 | 37.53 | 38.33 | 0.00 | 0.40 | 3,415 | 73.08 |
| 15.150 | 0.37 | 37.48 | 38.27 | 0.00 | 0.40 | 3,410 | 73.08 |
| 15.200 | 0.37 | 37.43 | 38.22 | 0.00 | 0.40 | 3,406 | 73.08 |
| 15.250 | 0.37 | 37.38 | 38.17 | 0.00 | 0.40 | 3,401 | 73.08 |
| 15.300 | 0.37 | 37.33 | 38.12 | 0.00 | 0.40 | 3,397 | 73.08 |
| 15.350 | 0.37 | 37.29 | 38.08 | 0.00 | 0.40 | 3,393 | 73.07 |
| 15.400 | 0.37 | 37.24 | 38.03 | 0.00 | 0.39 | 3,389 | 73.07 |
| 15.450 | 0.37 | 37.20 | 37.98 | 0.00 | 0.39 | 3,384 | 73.07 |
| 15.500 | 0.37 | 37.15 | 37.94 | 0.00 | 0.39 | 3,381 | 73.07 |
| 15.550 | 0.37 | 37.11 | 37.90 | 0.00 | 0.39 | 3,377 | 73.07 |
| 15.600 | 0.34 | 37.04 | 37.82 | 0.00 | 0.39 | 3,370 | 73.07 |
| 15.650 | 0.27 | 36.87 | 37.64 | 0.00 | 0.39 | 3,354 | 73.06 |
| 15.700 | 0.27 | 36.64 | 37.41 | 0.00 | 0.38 | 3,333 | 73.05 |
| 15.750 | 0.27 | 36.41 | 37.18 | 0.00 | 0.38 | 3,313 | 73.05 |
| 15.800 | 0.27 | 36.20 | 36.95 | 0.00 | 0.38 | 3,293 | 73.04 |
| 15.850 | 0.27 | 35.99 | 36.74 | 0.00 | 0.37 | 3,273 | 73.03 |
| 15.900 | 0.27 | 35.78 | 36.52 | 0.00 | 0.37 | 3,254 | 73.02 |
| 15.950 | 0.27 | 35.58 | 36.32 | 0.00 | 0.37 | 3,236 | 73.02 |
| 16.000 | 0.27 | 35.39 | 36.11 | 0.00 | 0.36 | 3,218 | 73.01 |
| 16.050 | 0.27 | 35.20 | 35.92 | 0.00 | 0.36 | 3,200 | 73.01 |
| 16.100 | 0.26 | 35.01 | 35.73 | 0.00 | 0.36 | 3,183 | 73.00 |
| 16.150 | 0.26 | 34.83 | 35.54 | 0.00 | 0.35 | 3,167 | 72.99 |
| 16.200 | 0.26 | 34.66 | 35.36 | 0.00 | 0.35 | 3,151 | 72.99 |
| 16.250 | 0.26 | 34.49 | 35.18 | 0.00 | 0.35 | 3,135 | 72.98 |
| 16.300 | 0.26 | 34.32 | 35.01 | 0.00 | 0.35 | 3,120 | 72.98 |
| 16.350 | 0.26 | 34.16 | 34.84 | 0.00 | 0.34 | 3,105 | 72.97 |
| 16.400 | 0.26 | 34.00 | 34.68 | 0.00 | 0.34 | 3,091 | 72.97 |
| 16.450 | 0.26 | 33.84 | 34.52 | 0.00 | 0.34 | 3,077 | 72.96 |
| 16.500 | 0.26 | 33.70 | 34.37 | 0.00 | 0.34 | 3,063 | 72.96 |
| 16.550 | 0.26 | 33.55 | 34.22 | 0.00 | 0.33 | 3,050 | 72.95 |
| 16.600 | 0.26 | 33.41 | 34.07 | 0.00 | 0.33 | 3,037 | 72.95 |
| 16.650 | 0.26 | 33.27 | 33.93 | 0.00 | 0.33 | 3,024 | 72.94 |
| 16.700 | 0.26 | 33.13 | 33.79 | 0.00 | 0.33 | 3,012 | 72.94 |
| 16.750 | 0.26 | 33.00 | 33.66 | 0.00 | 0.33 | 3,000 | 72.94 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.26 | 32.88 | 33.52 | 0.00 | 0.32 | 2,988 | 72.93 |
| 16.850 | 0.26 | 32.75 | 33.40 | 0.00 | 0.32 | 2,977 | 72.93 |
| 16.900 | 0.26 | 32.63 | 33.27 | 0.00 | 0.32 | 2,966 | 72.92 |
| 16.950 | 0.26 | 32.51 | 33.15 | 0.00 | 0.32 | 2,955 | 72.92 |
| 17.000 | 0.26 | 32.40 | 33.03 | 0.00 | 0.32 | 2,944 | 72.92 |
| 17.050 | 0.26 | 32.28 | 32.91 | 0.00 | 0.31 | 2,934 | 72.91 |
| 17.100 | 0.26 | 32.17 | 32.80 | 0.00 | 0.31 | 2,924 | 72.91 |
| 17.150 | 0.26 | 32.07 | 32.69 | 0.00 | 0.31 | 2,914 | 72.91 |
| 17.200 | 0.26 | 31.96 | 32.58 | 0.00 | 0.31 | 2,905 | 72.90 |
| 17.250 | 0.26 | 31.86 | 32.48 | 0.00 | 0.31 | 2,895 | 72.90 |
| 17.300 | 0.26 | 31.76 | 32.38 | 0.00 | 0.31 | 2,886 | 72.90 |
| 17.350 | 0.26 | 31.67 | 32.28 | 0.00 | 0.30 | 2,877 | 72.89 |
| 17.400 | 0.26 | 31.57 | 32.18 | 0.00 | 0.30 | 2,869 | 72.89 |
| 17.450 | 0.26 | 31.48 | 32.08 | 0.00 | 0.30 | 2,860 | 72.89 |
| 17.500 | 0.26 | 31.39 | 31.99 | 0.00 | 0.30 | 2,852 | 72.88 |
| 17.550 | 0.26 | 31.30 | 31.90 | 0.00 | 0.30 | 2,844 | 72.88 |
| 17.600 | 0.25 | 31.22 | 31.81 | 0.00 | 0.30 | 2,836 | 72.88 |
| 17.650 | 0.25 | 31.13 | 31.72 | 0.00 | 0.30 | 2,828 | 72.88 |
| 17.700 | 0.25 | 31.05 | 31.64 | 0.00 | 0.30 | 2,821 | 72.87 |
| 17.750 | 0.25 | 30.97 | 31.56 | 0.00 | 0.29 | 2,814 | 72.87 |
| 17.800 | 0.25 | 30.89 | 31.48 | 0.00 | 0.29 | 2,807 | 72.87 |
| 17.850 | 0.25 | 30.81 | 31.40 | 0.00 | 0.29 | 2,800 | 72.87 |
| 17.900 | 0.25 | 30.74 | 31.32 | 0.00 | 0.29 | 2,793 | 72.86 |
| 17.950 | 0.25 | 30.67 | 31.24 | 0.00 | 0.29 | 2,786 | 72.86 |
| 18.000 | 0.25 | 30.59 | 31.17 | 0.00 | 0.29 | 2,779 | 72.86 |
| 18.050 | 0.25 | 30.52 | 31.10 | 0.00 | 0.29 | 2,773 | 72.86 |
| 18.100 | 0.25 | 30.46 | 31.03 | 0.00 | 0.29 | 2,767 | 72.86 |
| 18.150 | 0.25 | 30.39 | 30.96 | 0.00 | 0.28 | 2,761 | 72.85 |
| 18.200 | 0.25 | 30.32 | 30.89 | 0.00 | 0.28 | 2,755 | 72.85 |
| 18.250 | 0.25 | 30.26 | 30.83 | 0.00 | 0.28 | 2,749 | 72.85 |
| 18.300 | 0.25 | 30.20 | 30.76 | 0.00 | 0.28 | 2,743 | 72.85 |
| 18.350 | 0.25 | 30.14 | 30.70 | 0.00 | 0.28 | 2,738 | 72.85 |
| 18.400 | 0.25 | 30.08 | 30.64 | 0.00 | 0.28 | 2,733 | 72.84 |
| 18.450 | 0.25 | 30.03 | 30.58 | 0.00 | 0.28 | 2,727 | 72.84 |
| 18.500 | 0.25 | 29.97 | 30.53 | 0.00 | 0.28 | 2,722 | 72.84 |
| 18.550 | 0.25 | 29.92 | 30.47 | 0.00 | 0.28 | 2,717 | 72.84 |
| 18.600 | 0.25 | 29.86 | 30.42 | 0.00 | 0.28 | 2,713 | 72.84 |
| 18.650 | 0.25 | 29.81 | 30.37 | 0.00 | 0.28 | 2,708 | 72.83 |
| 18.700 | 0.25 | 29.76 | 30.31 | 0.00 | 0.28 | 2,704 | 72.83 |
| 18.750 | 0.25 | 29.72 | 30.26 | 0.00 | 0.27 | 2,699 | 72.83 |
| 18.800 | 0.25 | 29.67 | 30.22 | 0.00 | 0.27 | 2,695 | 72.83 |
| 18.850 | 0.25 | 29.62 | 30.17 | 0.00 | 0.27 | 2,691 | 72.83 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.25 | 29.58 | 30.12 | 0.00 | 0.27 | 2,687 | 72.83 |
| 18.950 | 0.25 | 29.54 | 30.08 | 0.00 | 0.27 | 2,683 | 72.83 |
| 19.000 | 0.25 | 29.49 | 30.04 | 0.00 | 0.27 | 2,679 | 72.82 |
| 19.050 | 0.25 | 29.45 | 29.99 | 0.00 | 0.27 | 2,675 | 72.82 |
| 19.100 | 0.25 | 29.41 | 29.95 | 0.00 | 0.27 | 2,671 | 72.82 |
| 19.150 | 0.25 | 29.37 | 29.91 | 0.00 | 0.27 | 2,668 | 72.82 |
| 19.200 | 0.25 | 29.34 | 29.87 | 0.00 | 0.27 | 2,664 | 72.82 |
| 19.250 | 0.25 | 29.30 | 29.84 | 0.00 | 0.27 | 2,661 | 72.82 |
| 19.300 | 0.25 | 29.26 | 29.80 | 0.00 | 0.27 | 2,658 | 72.82 |
| 19.350 | 0.25 | 29.23 | 29.76 | 0.00 | 0.27 | 2,655 | 72.82 |
| 19.400 | 0.25 | 29.19 | 29.73 | 0.00 | 0.27 | 2,651 | 72.82 |
| 19.450 | 0.25 | 29.16 | 29.69 | 0.00 | 0.27 | 2,648 | 72.81 |
| 19.500 | 0.25 | 29.13 | 29.66 | 0.00 | 0.27 | 2,645 | 72.81 |
| 19.550 | 0.25 | 29.10 | 29.63 | 0.00 | 0.26 | 2,643 | 72.81 |
| 19.600 | 0.25 | 29.07 | 29.59 | 0.00 | 0.26 | 2,640 | 72.81 |
| 19.650 | 0.25 | 29.04 | 29.56 | 0.00 | 0.26 | 2,637 | 72.81 |
| 19.700 | 0.25 | 29.01 | 29.53 | 0.00 | 0.26 | 2,634 | 72.81 |
| 19.750 | 0.25 | 28.98 | 29.50 | 0.00 | 0.26 | 2,632 | 72.81 |
| 19.800 | 0.25 | 28.95 | 29.47 | 0.00 | 0.26 | 2,629 | 72.81 |
| 19.850 | 0.25 | 28.92 | 29.45 | 0.00 | 0.26 | 2,627 | 72.81 |
| 19.900 | 0.25 | 28.90 | 29.42 | 0.00 | 0.26 | 2,624 | 72.81 |
| 19.950 | 0.25 | 28.87 | 29.39 | 0.00 | 0.26 | 2,622 | 72.80 |
| 20.000 | 0.25 | 28.84 | 29.36 | 0.00 | 0.26 | 2,619 | 72.80 |
| 20.050 | 0.25 | 28.82 | 29.34 | 0.00 | 0.26 | 2,617 | 72.80 |
| 20.100 | 0.25 | 28.79 | 29.31 | 0.00 | 0.26 | 2,615 | 72.80 |
| 20.150 | 0.25 | 28.77 | 29.29 | 0.00 | 0.26 | 2,613 | 72.80 |
| 20.200 | 0.25 | 28.75 | 29.27 | 0.00 | 0.26 | 2,611 | 72.80 |
| 20.250 | 0.25 | 28.72 | 29.24 | 0.00 | 0.26 | 2,609 | 72.80 |
| 20.300 | 0.25 | 28.70 | 29.22 | 0.00 | 0.26 | 2,607 | 72.80 |
| 20.350 | 0.25 | 28.68 | 29.20 | 0.00 | 0.26 | 2,605 | 72.80 |
| 20.400 | 0.25 | 28.66 | 29.18 | 0.00 | 0.26 | 2,603 | 72.80 |
| 20.450 | 0.25 | 28.64 | 29.15 | 0.00 | 0.26 | 2,601 | 72.80 |
| 20.500 | 0.25 | 28.62 | 29.13 | 0.00 | 0.26 | 2,599 | 72.80 |
| 20.550 | 0.25 | 28.60 | 29.11 | 0.00 | 0.26 | 2,597 | 72.80 |
| 20.600 | 0.25 | 28.58 | 29.09 | 0.00 | 0.26 | 2,595 | 72.80 |
| 20.650 | 0.25 | 28.56 | 29.07 | 0.00 | 0.26 | 2,594 | 72.80 |
| 20.700 | 0.25 | 28.54 | 29.06 | 0.00 | 0.26 | 2,592 | 72.79 |
| 20.750 | 0.25 | 28.53 | 29.04 | 0.00 | 0.26 | 2,590 | 72.79 |
| 20.800 | 0.25 | 28.51 | 29.02 | 0.00 | 0.26 | 2,589 | 72.79 |
| 20.850 | 0.25 | 28.49 | 29.00 | 0.00 | 0.26 | 2,587 | 72.79 |
| 20.900 | 0.25 | 28.47 | 28.98 | 0.00 | 0.25 | 2,586 | 72.79 |
| 20.950 | 0.25 | 28.46 | 28.97 | 0.00 | 0.25 | 2,584 | 72.79 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.25 | 28.44 | 28.95 | 0.00 | 0.25 | 2,583 | 72.79 |
| 21.050 | 0.25 | 28.43 | 28.94 | 0.00 | 0.25 | 2,581 | 72.79 |
| 21.100 | 0.25 | 28.41 | 28.92 | 0.00 | 0.25 | 2,580 | 72.79 |
| 21.150 | 0.25 | 28.40 | 28.90 | 0.00 | 0.25 | 2,579 | 72.79 |
| 21.200 | 0.25 | 28.38 | 28.89 | 0.00 | 0.25 | 2,577 | 72.79 |
| 21.250 | 0.25 | 28.37 | 28.87 | 0.00 | 0.25 | 2,576 | 72.79 |
| 21.300 | 0.25 | 28.35 | 28.86 | 0.00 | 0.25 | 2,575 | 72.79 |
| 21.350 | 0.25 | 28.34 | 28.85 | 0.00 | 0.25 | 2,573 | 72.79 |
| 21.400 | 0.25 | 28.33 | 28.83 | 0.00 | 0.25 | 2,572 | 72.79 |
| 21.450 | 0.25 | 28.31 | 28.82 | 0.00 | 0.25 | 2,571 | 72.79 |
| 21.500 | 0.25 | 28.30 | 28.81 | 0.00 | 0.25 | 2,570 | 72.79 |
| 21.550 | 0.25 | 28.29 | 28.79 | 0.00 | 0.25 | 2,569 | 72.79 |
| 21.600 | 0.25 | 28.28 | 28.78 | 0.00 | 0.25 | 2,567 | 72.79 |
| 21.650 | 0.25 | 28.26 | 28.77 | 0.00 | 0.25 | 2,566 | 72.79 |
| 21.700 | 0.25 | 28.25 | 28.75 | 0.00 | 0.25 | 2,565 | 72.79 |
| 21.750 | 0.25 | 28.24 | 28.74 | 0.00 | 0.25 | 2,564 | 72.78 |
| 21.800 | 0.25 | 28.23 | 28.73 | 0.00 | 0.25 | 2,563 | 72.78 |
| 21.850 | 0.25 | 28.22 | 28.72 | 0.00 | 0.25 | 2,562 | 72.78 |
| 21.900 | 0.25 | 28.21 | 28.71 | 0.00 | 0.25 | 2,561 | 72.78 |
| 21.950 | 0.25 | 28.19 | 28.70 | 0.00 | 0.25 | 2,560 | 72.78 |
| 22.000 | 0.24 | 28.18 | 28.68 | 0.00 | 0.25 | 2,559 | 72.78 |
| 22.050 | 0.24 | 28.17 | 28.67 | 0.00 | 0.25 | 2,558 | 72.78 |
| 22.100 | 0.24 | 28.16 | 28.66 | 0.00 | 0.25 | 2,557 | 72.78 |
| 22.150 | 0.24 | 28.15 | 28.65 | 0.00 | 0.25 | 2,556 | 72.78 |
| 22.200 | 0.24 | 28.14 | 28.64 | 0.00 | 0.25 | 2,555 | 72.78 |
| 22.250 | 0.24 | 28.13 | 28.63 | 0.00 | 0.25 | 2,554 | 72.78 |
| 22.300 | 0.24 | 28.12 | 28.62 | 0.00 | 0.25 | 2,554 | 72.78 |
| 22.350 | 0.24 | 28.11 | 28.61 | 0.00 | 0.25 | 2,553 | 72.78 |
| 22.400 | 0.24 | 28.10 | 28.60 | 0.00 | 0.25 | 2,552 | 72.78 |
| 22.450 | 0.24 | 28.10 | 28.59 | 0.00 | 0.25 | 2,551 | 72.78 |
| 22.500 | 0.13 | 27.98 | 28.47 | 0.00 | 0.25 | 2,540 | 72.78 |
| 22.550 | 0.13 | 27.74 | 28.23 | 0.00 | 0.24 | 2,519 | 72.77 |
| 22.600 | 0.13 | 27.52 | 27.99 | 0.00 | 0.24 | 2,498 | 72.76 |
| 22.650 | 0.13 | 27.29 | 27.77 | 0.00 | 0.24 | 2,478 | 72.75 |
| 22.700 | 0.13 | 27.08 | 27.54 | 0.00 | 0.23 | 2,458 | 72.75 |
| 22.750 | 0.12 | 26.86 | 27.33 | 0.00 | 0.23 | 2,438 | 72.74 |
| 22.800 | 0.12 | 26.65 | 27.11 | 0.00 | 0.23 | 2,419 | 72.73 |
| 22.850 | 0.12 | 26.43 | 26.90 | 0.00 | 0.23 | 2,400 | 72.73 |
| 22.900 | 0.12 | 26.22 | 26.68 | 0.00 | 0.23 | 2,381 | 72.72 |
| 22.950 | 0.12 | 26.01 | 26.47 | 0.00 | 0.23 | 2,361 | 72.71 |
| 23.000 | 0.12 | 25.80 | 26.26 | 0.00 | 0.23 | 2,342 | 72.71 |
| 23.050 | 0.12 | 25.59 | 26.05 | 0.00 | 0.23 | 2,324 | 72.70 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.12 | 25.38 | 25.84 | 0.00 | 0.23 | 2,305 | 72.70 |
| 23.150 | 0.12 | 25.17 | 25.63 | 0.00 | 0.23 | 2,286 | 72.69 |
| 23.200 | 0.12 | 24.97 | 25.42 | 0.00 | 0.23 | 2,268 | 72.68 |
| 23.250 | 0.12 | 24.76 | 25.22 | 0.00 | 0.23 | 2,249 | 72.68 |
| 23.300 | 0.12 | 24.56 | 25.01 | 0.00 | 0.22 | 2,231 | 72.67 |
| 23.350 | 0.12 | 24.36 | 24.81 | 0.00 | 0.22 | 2,212 | 72.66 |
| 23.400 | 0.12 | 24.16 | 24.60 | 0.00 | 0.22 | 2,194 | 72.66 |
| 23.450 | 0.12 | 23.96 | 24.40 | 0.00 | 0.22 | 2,176 | 72.65 |
| 23.500 | 0.12 | 23.76 | 24.20 | 0.00 | 0.22 | 2,158 | 72.64 |
| 23.550 | 0.12 | 23.56 | 24.00 | 0.00 | 0.22 | 2,140 | 72.64 |
| 23.600 | 0.12 | 23.36 | 23.80 | 0.00 | 0.22 | 2,123 | 72.63 |
| 23.650 | 0.12 | 23.17 | 23.61 | 0.00 | 0.22 | 2,105 | 72.63 |
| 23.700 | 0.12 | 22.97 | 23.41 | 0.00 | 0.22 | 2,087 | 72.62 |
| 23.750 | 0.12 | 22.78 | 23.22 | 0.00 | 0.22 | 2,070 | 72.61 |
| 23.800 | 0.12 | 22.59 | 23.02 | 0.00 | 0.22 | 2,052 | 72.61 |
| 23.850 | 0.12 | 22.40 | 22.83 | 0.00 | 0.22 | 2,035 | 72.60 |
| 23.900 | 0.12 | 22.21 | 22.64 | 0.00 | 0.22 | 2,018 | 72.60 |
| 23.950 | 0.12 | 22.02 | 22.45 | 0.00 | 0.22 | 2,001 | 72.59 |
| 24.000 | 0.12 | 21.83 | 22.26 | 0.00 | 0.21 | 1,984 | 72.58 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 71.50 |
| 0.050 | 0.00 | 0.17 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 0.100 | 0.00 | 0.17 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.150 | 0.00 | 0.16 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.200 | 0.00 | 0.16 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.250 | 0.00 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.300 | 0.00 | 0.15 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.350 | 0.00 | 0.14 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.400 | 0.00 | 0.14 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.450 | 0.00 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.500 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 0.550 | 0.00 | 0.12 | 0.13 | 0.00 | 0.00 | 11 | 71.51 |
| 0.600 | 0.00 | 0.12 | 0.12 | 0.00 | 0.00 | 11 | 71.51 |
| 0.650 | 0.00 | 0.11 | 0.12 | 0.00 | 0.00 | 10 | 71.51 |
| 0.700 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.750 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.800 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.850 | 0.00 | 0.11 | 0.11 | 0.00 | 0.00 | 10 | 71.51 |
| 0.900 | 0.01 | 0.12 | 0.12 | 0.00 | 0.00 | 11 | 71.51 |
| 0.950 | 0.01 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 1.000 | 0.01 | 0.14 | 0.14 | 0.00 | 0.00 | 13 | 71.51 |
| 1.050 | 0.01 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 1.100 | 0.01 | 0.17 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 1.150 | 0.01 | 0.19 | 0.20 | 0.00 | 0.00 | 18 | 71.51 |
| 1.200 | 0.02 | 0.22 | 0.22 | 0.00 | 0.00 | 20 | 71.51 |
| 1.250 | 0.02 | 0.24 | 0.25 | 0.00 | 0.00 | 22 | 71.52 |
| 1.300 | 0.02 | 0.27 | 0.27 | 0.00 | 0.00 | 24 | 71.52 |
| 1.350 | 0.02 | 0.29 | 0.30 | 0.00 | 0.01 | 27 | 71.52 |
| 1.400 | 0.02 | 0.32 | 0.33 | 0.00 | 0.01 | 30 | 71.52 |
| 1.450 | 0.02 | 0.35 | 0.37 | 0.00 | 0.01 | 32 | 71.52 |
| 1.500 | 0.02 | 0.38 | 0.40 | 0.00 | 0.01 | 35 | 71.53 |
| 1.550 | 0.02 | 0.42 | 0.43 | 0.00 | 0.01 | 38 | 71.53 |
| 1.600 | 0.03 | 0.45 | 0.47 | 0.00 | 0.01 | 41 | 71.53 |
| 1.650 | 0.03 | 0.48 | 0.50 | 0.00 | 0.01 | 44 | 71.53 |
| 1.700 | 0.03 | 0.52 | 0.54 | 0.00 | 0.01 | 48 | 71.54 |
| 1.750 | 0.03 | 0.55 | 0.57 | 0.00 | 0.01 | 51 | 71.54 |
| 1.800 | 0.03 | 0.59 | 0.61 | 0.00 | 0.01 | 54 | 71.54 |
| 1.850 | 0.03 | 0.63 | 0.65 | 0.00 | 0.01 | 57 | 71.54 |
| 1.900 | 0.03 | 0.66 | 0.69 | 0.00 | 0.01 | 61 | 71.55 |
| 1.950 | 0.03 | 0.70 | 0.73 | 0.00 | 0.01 | 64 | 71.55 |
| 2.000 | 0.03 | 0.74 | 0.76 | 0.00 | 0.01 | 68 | 71.55 |
| 2.050 | 0.03 | 0.78 | 0.80 | 0.00 | 0.01 | 71 | 71.55 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.03 | 0.81 | 0.84 | 0.00 | 0.01 | 75 | 71.56 |
| 2.150 | 0.03 | 0.85 | 0.88 | 0.00 | 0.02 | 78 | 71.56 |
| 2.200 | 0.04 | 0.89 | 0.92 | 0.00 | 0.02 | 82 | 71.56 |
| 2.250 | 0.04 | 0.93 | 0.96 | 0.00 | 0.02 | 85 | 71.56 |
| 2.300 | 0.04 | 0.97 | 1.00 | 0.00 | 0.02 | 89 | 71.57 |
| 2.350 | 0.04 | 1.01 | 1.05 | 0.00 | 0.02 | 92 | 71.57 |
| 2.400 | 0.04 | 1.05 | 1.09 | 0.00 | 0.02 | 96 | 71.57 |
| 2.450 | 0.04 | 1.09 | 1.13 | 0.00 | 0.02 | 100 | 71.57 |
| 2.500 | 0.04 | 1.13 | 1.17 | 0.00 | 0.02 | 104 | 71.58 |
| 2.550 | 0.04 | 1.17 | 1.22 | 0.00 | 0.02 | 107 | 71.58 |
| 2.600 | 0.04 | 1.22 | 1.26 | 0.00 | 0.02 | 111 | 71.58 |
| 2.650 | 0.04 | 1.26 | 1.30 | 0.00 | 0.02 | 115 | 71.59 |
| 2.700 | 0.04 | 1.30 | 1.35 | 0.00 | 0.02 | 119 | 71.59 |
| 2.750 | 0.05 | 1.34 | 1.39 | 0.00 | 0.02 | 123 | 71.59 |
| 2.800 | 0.05 | 1.38 | 1.43 | 0.00 | 0.02 | 127 | 71.60 |
| 2.850 | 0.05 | 1.43 | 1.48 | 0.00 | 0.03 | 131 | 71.60 |
| 2.900 | 0.05 | 1.47 | 1.52 | 0.00 | 0.03 | 135 | 71.60 |
| 2.950 | 0.05 | 1.51 | 1.57 | 0.00 | 0.03 | 139 | 71.60 |
| 3.000 | 0.05 | 1.56 | 1.61 | 0.00 | 0.03 | 143 | 71.61 |
| 3.050 | 0.05 | 1.60 | 1.66 | 0.00 | 0.03 | 147 | 71.61 |
| 3.100 | 0.05 | 1.65 | 1.70 | 0.00 | 0.03 | 151 | 71.61 |
| 3.150 | 0.05 | 1.69 | 1.75 | 0.00 | 0.03 | 155 | 71.62 |
| 3.200 | 0.05 | 1.73 | 1.80 | 0.00 | 0.03 | 159 | 71.62 |
| 3.250 | 0.05 | 1.78 | 1.84 | 0.00 | 0.03 | 163 | 71.62 |
| 3.300 | 0.06 | 1.82 | 1.89 | 0.00 | 0.03 | 167 | 71.62 |
| 3.350 | 0.06 | 1.87 | 1.93 | 0.00 | 0.03 | 171 | 71.63 |
| 3.400 | 0.06 | 1.91 | 1.98 | 0.00 | 0.03 | 175 | 71.63 |
| 3.450 | 0.06 | 1.95 | 2.02 | 0.00 | 0.04 | 179 | 71.63 |
| 3.500 | 0.06 | 2.00 | 2.07 | 0.00 | 0.04 | 183 | 71.64 |
| 3.550 | 0.06 | 2.04 | 2.12 | 0.00 | 0.04 | 187 | 71.64 |
| 3.600 | 0.06 | 2.09 | 2.16 | 0.00 | 0.04 | 191 | 71.64 |
| 3.650 | 0.06 | 2.13 | 2.21 | 0.00 | 0.04 | 195 | 71.65 |
| 3.700 | 0.06 | 2.17 | 2.25 | 0.00 | 0.04 | 199 | 71.65 |
| 3.750 | 0.06 | 2.22 | 2.30 | 0.00 | 0.04 | 203 | 71.65 |
| 3.800 | 0.06 | 2.26 | 2.34 | 0.00 | 0.04 | 207 | 71.66 |
| 3.850 | 0.06 | 2.31 | 2.39 | 0.00 | 0.04 | 211 | 71.66 |
| 3.900 | 0.06 | 2.35 | 2.43 | 0.00 | 0.04 | 215 | 71.66 |
| 3.950 | 0.07 | 2.39 | 2.48 | 0.00 | 0.04 | 219 | 71.66 |
| 4.000 | 0.07 | 2.44 | 2.53 | 0.00 | 0.04 | 223 | 71.67 |
| 4.050 | 0.07 | 2.48 | 2.57 | 0.00 | 0.04 | 227 | 71.67 |
| 4.100 | 0.07 | 2.53 | 2.62 | 0.00 | 0.05 | 231 | 71.67 |
| 4.150 | 0.07 | 2.57 | 2.66 | 0.00 | 0.05 | 235 | 71.68 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.07 | 2.61 | 2.71 | 0.00 | 0.05 | 239 | 71.68 |
| 4.250 | 0.07 | 2.66 | 2.75 | 0.00 | 0.05 | 243 | 71.68 |
| 4.300 | 0.07 | 2.70 | 2.80 | 0.00 | 0.05 | 247 | 71.69 |
| 4.350 | 0.07 | 2.74 | 2.84 | 0.00 | 0.05 | 251 | 71.69 |
| 4.400 | 0.07 | 2.79 | 2.89 | 0.00 | 0.05 | 255 | 71.69 |
| 4.450 | 0.07 | 2.83 | 2.93 | 0.00 | 0.05 | 259 | 71.69 |
| 4.500 | 0.07 | 2.87 | 2.98 | 0.00 | 0.05 | 263 | 71.70 |
| 4.550 | 0.07 | 2.92 | 3.02 | 0.00 | 0.05 | 267 | 71.70 |
| 4.600 | 0.07 | 2.96 | 3.06 | 0.00 | 0.05 | 271 | 71.70 |
| 4.650 | 0.08 | 3.00 | 3.11 | 0.00 | 0.05 | 275 | 71.71 |
| 4.700 | 0.08 | 3.04 | 3.15 | 0.00 | 0.05 | 279 | 71.71 |
| 4.750 | 0.08 | 3.09 | 3.20 | 0.00 | 0.06 | 283 | 71.71 |
| 4.800 | 0.08 | 3.13 | 3.24 | 0.00 | 0.06 | 287 | 71.71 |
| 4.850 | 0.08 | 3.17 | 3.28 | 0.00 | 0.06 | 290 | 71.72 |
| 4.900 | 0.08 | 3.21 | 3.33 | 0.00 | 0.06 | 294 | 71.72 |
| 4.950 | 0.08 | 3.25 | 3.37 | 0.00 | 0.06 | 298 | 71.72 |
| 5.000 | 0.08 | 3.30 | 3.41 | 0.00 | 0.06 | 302 | 71.73 |
| 5.050 | 0.08 | 3.34 | 3.46 | 0.00 | 0.06 | 306 | 71.73 |
| 5.100 | 0.08 | 3.38 | 3.50 | 0.00 | 0.06 | 310 | 71.73 |
| 5.150 | 0.08 | 3.42 | 3.54 | 0.00 | 0.06 | 313 | 71.73 |
| 5.200 | 0.08 | 3.46 | 3.59 | 0.00 | 0.06 | 317 | 71.74 |
| 5.250 | 0.08 | 3.50 | 3.63 | 0.00 | 0.06 | 321 | 71.74 |
| 5.300 | 0.08 | 3.54 | 3.67 | 0.00 | 0.06 | 325 | 71.74 |
| 5.350 | 0.09 | 3.58 | 3.71 | 0.00 | 0.06 | 328 | 71.75 |
| 5.400 | 0.09 | 3.62 | 3.75 | 0.00 | 0.07 | 332 | 71.75 |
| 5.450 | 0.09 | 3.67 | 3.80 | 0.00 | 0.07 | 336 | 71.75 |
| 5.500 | 0.09 | 3.71 | 3.84 | 0.00 | 0.07 | 339 | 71.75 |
| 5.550 | 0.09 | 3.75 | 3.88 | 0.00 | 0.07 | 343 | 71.76 |
| 5.600 | 0.09 | 3.79 | 3.92 | 0.00 | 0.07 | 347 | 71.76 |
| 5.650 | 0.09 | 3.83 | 3.96 | 0.00 | 0.07 | 351 | 71.76 |
| 5.700 | 0.09 | 3.87 | 4.00 | 0.00 | 0.07 | 354 | 71.77 |
| 5.750 | 0.09 | 3.91 | 4.05 | 0.00 | 0.07 | 358 | 71.77 |
| 5.800 | 0.09 | 3.95 | 4.09 | 0.00 | 0.07 | 361 | 71.77 |
| 5.850 | 0.09 | 3.98 | 4.13 | 0.00 | 0.07 | 365 | 71.77 |
| 5.900 | 0.09 | 4.02 | 4.17 | 0.00 | 0.07 | 369 | 71.78 |
| 5.950 | 0.09 | 4.06 | 4.21 | 0.00 | 0.07 | 372 | 71.78 |
| 6.000 | 0.09 | 4.10 | 4.25 | 0.00 | 0.07 | 376 | 71.78 |
| 6.050 | 0.09 | 4.14 | 4.29 | 0.00 | 0.07 | 379 | 71.78 |
| 6.100 | 0.10 | 4.18 | 4.33 | 0.00 | 0.08 | 383 | 71.79 |
| 6.150 | 0.10 | 4.22 | 4.37 | 0.00 | 0.08 | 387 | 71.79 |
| 6.200 | 0.10 | 4.26 | 4.42 | 0.00 | 0.08 | 391 | 71.79 |
| 6.250 | 0.10 | 4.31 | 4.46 | 0.00 | 0.08 | 394 | 71.80 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.10 | 4.35 | 4.51 | 0.00 | 0.08 | 399 | 71.80 |
| 6.350 | 0.10 | 4.40 | 4.56 | 0.00 | 0.08 | 403 | 71.80 |
| 6.400 | 0.10 | 4.45 | 4.61 | 0.00 | 0.08 | 407 | 71.80 |
| 6.450 | 0.11 | 4.50 | 4.66 | 0.00 | 0.08 | 412 | 71.81 |
| 6.500 | 0.11 | 4.55 | 4.71 | 0.00 | 0.08 | 417 | 71.81 |
| 6.550 | 0.11 | 4.60 | 4.76 | 0.00 | 0.08 | 421 | 71.82 |
| 6.600 | 0.11 | 4.65 | 4.82 | 0.00 | 0.08 | 426 | 71.82 |
| 6.650 | 0.11 | 4.71 | 4.88 | 0.00 | 0.08 | 431 | 71.82 |
| 6.700 | 0.11 | 4.77 | 4.94 | 0.00 | 0.09 | 437 | 71.83 |
| 6.750 | 0.12 | 4.82 | 5.00 | 0.00 | 0.09 | 442 | 71.83 |
| 6.800 | 0.12 | 4.88 | 5.06 | 0.00 | 0.09 | 447 | 71.84 |
| 6.850 | 0.12 | 4.94 | 5.12 | 0.00 | 0.09 | 453 | 71.84 |
| 6.900 | 0.12 | 5.01 | 5.19 | 0.00 | 0.09 | 459 | 71.84 |
| 6.950 | 0.12 | 5.07 | 5.25 | 0.00 | 0.09 | 465 | 71.85 |
| 7.000 | 0.13 | 5.13 | 5.32 | 0.00 | 0.09 | 470 | 71.85 |
| 7.050 | 0.13 | 5.20 | 5.39 | 0.00 | 0.09 | 476 | 71.86 |
| 7.100 | 0.13 | 5.27 | 5.46 | 0.00 | 0.09 | 482 | 71.86 |
| 7.150 | 0.13 | 5.33 | 5.53 | 0.00 | 0.10 | 489 | 71.87 |
| 7.200 | 0.13 | 5.40 | 5.60 | 0.00 | 0.10 | 495 | 71.87 |
| 7.250 | 0.13 | 5.47 | 5.67 | 0.00 | 0.10 | 501 | 71.88 |
| 7.300 | 0.14 | 5.54 | 5.74 | 0.00 | 0.10 | 508 | 71.88 |
| 7.350 | 0.14 | 5.61 | 5.82 | 0.00 | 0.10 | 514 | 71.89 |
| 7.400 | 0.14 | 5.69 | 5.89 | 0.00 | 0.10 | 521 | 71.89 |
| 7.450 | 0.14 | 5.76 | 5.97 | 0.00 | 0.10 | 528 | 71.90 |
| 7.500 | 0.14 | 5.83 | 6.04 | 0.00 | 0.10 | 534 | 71.90 |
| 7.550 | 0.14 | 5.91 | 6.12 | 0.00 | 0.11 | 541 | 71.91 |
| 7.600 | 0.15 | 5.99 | 6.20 | 0.00 | 0.11 | 548 | 71.91 |
| 7.650 | 0.15 | 6.06 | 6.28 | 0.00 | 0.11 | 555 | 71.92 |
| 7.700 | 0.15 | 6.14 | 6.36 | 0.00 | 0.11 | 563 | 71.92 |
| 7.750 | 0.15 | 6.22 | 6.44 | 0.00 | 0.11 | 570 | 71.93 |
| 7.800 | 0.15 | 6.30 | 6.52 | 0.00 | 0.11 | 577 | 71.93 |
| 7.850 | 0.16 | 6.38 | 6.61 | 0.00 | 0.11 | 584 | 71.94 |
| 7.900 | 0.16 | 6.46 | 6.69 | 0.00 | 0.12 | 592 | 71.94 |
| 7.950 | 0.16 | 6.54 | 6.78 | 0.00 | 0.12 | 599 | 71.95 |
| 8.000 | 0.16 | 6.62 | 6.86 | 0.00 | 0.12 | 607 | 71.95 |
| 8.050 | 0.16 | 6.71 | 6.95 | 0.00 | 0.12 | 614 | 71.96 |
| 8.100 | 0.17 | 6.79 | 7.03 | 0.00 | 0.12 | 622 | 71.97 |
| 8.150 | 0.17 | 6.88 | 7.13 | 0.00 | 0.12 | 630 | 71.97 |
| 8.200 | 0.17 | 6.97 | 7.22 | 0.00 | 0.13 | 639 | 71.98 |
| 8.250 | 0.18 | 7.06 | 7.32 | 0.00 | 0.13 | 647 | 71.98 |
| 8.300 | 0.18 | 7.16 | 7.42 | 0.00 | 0.13 | 656 | 71.99 |
| 8.350 | 0.18 | 7.27 | 7.53 | 0.00 | 0.13 | 666 | 72.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|-----------------|--|----------------------------------|----------------------------------|--------------------------------------|---------------------------------------|------------------------------|-------------------|
| 8.400 | 0.19 | 7.38 | 7.64 | 0.00 | 0.13 | 673 | 72.00 |
| 8.450 | 0.19 | 7.49 | 7.76 | 0.00 | 0.13 | 679 | 72.01 |
| 8.500 | 0.20 | 7.61 | 7.88 | 0.00 | 0.13 | 686 | 72.01 |
| 8.550 | 0.20 | 7.74 | 8.01 | 0.00 | 0.13 | 693 | 72.02 |
| 8.600 | 0.20 | 7.88 | 8.15 | 0.00 | 0.13 | 701 | 72.02 |
| 8.650 | 0.21 | 8.02 | 8.29 | 0.00 | 0.14 | 709 | 72.03 |
| 8.700 | 0.21 | 8.16 | 8.44 | 0.00 | 0.14 | 717 | 72.04 |
| 8.750 | 0.22 | 8.32 | 8.59 | 0.00 | 0.14 | 726 | 72.04 |
| 8.800 | 0.22 | 8.48 | 8.75 | 0.00 | 0.14 | 735 | 72.05 |
| 8.850 | 0.22 | 8.64 | 8.92 | 0.00 | 0.14 | 744 | 72.06 |
| 8.900 | 0.23 | 8.81 | 9.09 | 0.00 | 0.14 | 754 | 72.06 |
| 8.950 | 0.23 | 8.98 | 9.27 | 0.00 | 0.14 | 764 | 72.07 |
| 9.000 | 0.23 | 9.16 | 9.44 | 0.00 | 0.14 | 773 | 72.08 |
| 9.050 | 0.23 | 9.34 | 9.62 | 0.00 | 0.14 | 783 | 72.09 |
| 9.100 | 0.24 | 9.52 | 9.80 | 0.00 | 0.14 | 794 | 72.09 |
| 9.150 | 0.24 | 9.70 | 9.99 | 0.00 | 0.15 | 804 | 72.10 |
| 9.200 | 0.24 | 9.88 | 10.18 | 0.00 | 0.15 | 815 | 72.11 |
| 9.250 | 0.24 | 10.07 | 10.37 | 0.00 | 0.15 | 825 | 72.12 |
| 9.300 | 0.25 | 10.26 | 10.56 | 0.00 | 0.15 | 836 | 72.13 |
| 9.350 | 0.25 | 10.46 | 10.76 | 0.00 | 0.15 | 847 | 72.13 |
| 9.400 | 0.25 | 10.65 | 10.96 | 0.00 | 0.15 | 858 | 72.14 |
| 9.450 | 0.25 | 10.85 | 11.16 | 0.00 | 0.15 | 869 | 72.15 |
| 9.500 | 0.26 | 11.05 | 11.36 | 0.00 | 0.15 | 881 | 72.16 |
| 9.550 | 0.26 | 11.26 | 11.57 | 0.00 | 0.16 | 892 | 72.17 |
| 9.600 | 0.26 | 11.46 | 11.78 | 0.00 | 0.16 | 904 | 72.18 |
| 9.650 | 0.26 | 11.67 | 11.99 | 0.00 | 0.16 | 916 | 72.19 |
| 9.700 | 0.27 | 11.88 | 12.20 | 0.00 | 0.16 | 928 | 72.19 |
| 9.750 | 0.27 | 12.10 | 12.42 | 0.00 | 0.16 | 940 | 72.20 |
| 9.800 | 0.27 | 12.31 | 12.64 | 0.00 | 0.16 | 952 | 72.21 |
| 9.850 | 0.27 | 12.53 | 12.86 | 0.00 | 0.16 | 964 | 72.22 |
| 9.900 | 0.28 | 12.75 | 13.08 | 0.00 | 0.16 | 977 | 72.23 |
| 9.950 | 0.28 | 12.97 | 13.31 | 0.00 | 0.17 | 989 | 72.24 |
| 10.000 | 0.28 | 13.20 | 13.53 | 0.00 | 0.17 | 1,003 | 72.25 |
| 10.050 | 0.28 | 13.43 | 13.77 | 0.00 | 0.17 | 1,031 | 72.26 |
| 10.100 | 0.29 | 13.66 | 14.00 | 0.00 | 0.17 | 1,060 | 72.27 |
| 10.150 | 0.29 | 13.89 | 14.24 | 0.00 | 0.17 | 1,089 | 72.28 |
| 10.200 | 0.30 | 14.14 | 14.48 | 0.00 | 0.17 | 1,119 | 72.29 |
| 10.250 | 0.30 | 14.38 | 14.73 | 0.00 | 0.18 | 1,150 | 72.30 |
| 10.300 | 0.30 | 14.63 | 14.99 | 0.00 | 0.18 | 1,181 | 72.31 |
| 10.350 | 0.30 | 14.88 | 15.24 | 0.00 | 0.18 | 1,212 | 72.32 |
| 10.400 | 0.31 | 15.13 | 15.49 | 0.00 | 0.18 | 1,243 | 72.33 |
| 10.450 | 0.31 | 15.38 | 15.74 | 0.00 | 0.18 | 1,275 | 72.34 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.31 | 15.63 | 16.00 | 0.00 | 0.18 | 1,306 | 72.35 |
| 10.550 | 0.31 | 15.89 | 16.25 | 0.00 | 0.18 | 1,337 | 72.36 |
| 10.600 | 0.31 | 16.14 | 16.51 | 0.00 | 0.19 | 1,369 | 72.37 |
| 10.650 | 0.31 | 16.39 | 16.77 | 0.00 | 0.19 | 1,400 | 72.39 |
| 10.700 | 0.32 | 16.64 | 17.02 | 0.00 | 0.19 | 1,432 | 72.40 |
| 10.750 | 0.32 | 16.90 | 17.28 | 0.00 | 0.19 | 1,463 | 72.41 |
| 10.800 | 0.32 | 17.15 | 17.54 | 0.00 | 0.19 | 1,495 | 72.42 |
| 10.850 | 0.32 | 17.41 | 17.80 | 0.00 | 0.19 | 1,527 | 72.43 |
| 10.900 | 0.32 | 17.66 | 18.05 | 0.00 | 0.20 | 1,559 | 72.44 |
| 10.950 | 0.33 | 17.92 | 18.31 | 0.00 | 0.20 | 1,591 | 72.45 |
| 11.000 | 0.33 | 18.18 | 18.58 | 0.00 | 0.20 | 1,623 | 72.46 |
| 11.050 | 0.33 | 18.44 | 18.84 | 0.00 | 0.20 | 1,655 | 72.47 |
| 11.100 | 0.33 | 18.70 | 19.10 | 0.00 | 0.20 | 1,688 | 72.48 |
| 11.150 | 0.34 | 18.97 | 19.37 | 0.00 | 0.20 | 1,721 | 72.49 |
| 11.200 | 0.35 | 19.24 | 19.65 | 0.00 | 0.20 | 1,750 | 72.50 |
| 11.250 | 0.35 | 19.53 | 19.94 | 0.00 | 0.21 | 1,776 | 72.51 |
| 11.300 | 0.36 | 19.83 | 20.24 | 0.00 | 0.21 | 1,803 | 72.52 |
| 11.350 | 0.37 | 20.14 | 20.55 | 0.00 | 0.21 | 1,831 | 72.53 |
| 11.400 | 0.37 | 20.46 | 20.88 | 0.00 | 0.21 | 1,860 | 72.54 |
| 11.450 | 0.38 | 20.79 | 21.21 | 0.00 | 0.21 | 1,890 | 72.55 |
| 11.500 | 0.39 | 21.13 | 21.56 | 0.00 | 0.21 | 1,921 | 72.56 |
| 11.550 | 0.40 | 21.49 | 21.92 | 0.00 | 0.21 | 1,953 | 72.57 |
| 11.600 | 0.40 | 21.86 | 22.29 | 0.00 | 0.21 | 1,987 | 72.59 |
| 11.650 | 0.41 | 22.25 | 22.68 | 0.00 | 0.22 | 2,021 | 72.60 |
| 11.700 | 0.43 | 22.65 | 23.09 | 0.00 | 0.22 | 2,058 | 72.61 |
| 11.750 | 0.44 | 23.08 | 23.52 | 0.00 | 0.22 | 2,097 | 72.62 |
| 11.800 | 0.46 | 23.55 | 23.99 | 0.00 | 0.22 | 2,139 | 72.64 |
| 11.850 | 0.48 | 24.04 | 24.49 | 0.00 | 0.22 | 2,184 | 72.65 |
| 11.900 | 0.50 | 24.57 | 25.02 | 0.00 | 0.22 | 2,232 | 72.67 |
| 11.950 | 0.54 | 25.16 | 25.61 | 0.00 | 0.23 | 2,285 | 72.69 |
| 12.000 | 0.62 | 25.86 | 26.32 | 0.00 | 0.23 | 2,348 | 72.71 |
| 12.050 | 1.04 | 27.06 | 27.52 | 0.00 | 0.23 | 2,456 | 72.75 |
| 12.100 | 3.33 | 30.85 | 31.43 | 0.00 | 0.29 | 2,802 | 72.87 |
| 12.150 | 2.54 | 35.97 | 36.72 | 0.00 | 0.37 | 3,272 | 73.03 |
| 12.200 | 2.18 | 39.82 | 40.70 | 0.00 | 0.44 | 3,626 | 73.16 |
| 12.250 | 2.21 | 43.22 | 44.21 | 0.00 | 0.49 | 3,939 | 73.27 |
| 12.300 | 2.20 | 46.53 | 47.63 | 0.00 | 0.55 | 4,240 | 73.37 |
| 12.350 | 2.11 | 49.64 | 50.84 | 0.00 | 0.60 | 4,522 | 73.47 |
| 12.400 | 1.97 | 52.44 | 53.71 | 0.00 | 0.64 | 4,779 | 73.57 |
| 12.450 | 1.78 | 54.86 | 56.18 | 0.00 | 0.66 | 5,001 | 73.65 |
| 12.500 | 1.55 | 56.82 | 58.18 | 0.00 | 0.68 | 5,182 | 73.72 |
| 12.550 | 1.33 | 58.30 | 59.70 | 0.00 | 0.70 | 5,317 | 73.77 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 1.15 | 59.36 | 60.78 | 0.00 | 0.71 | 5,413 | 73.80 |
| 12.650 | 1.00 | 60.08 | 61.52 | 0.00 | 0.72 | 5,477 | 73.82 |
| 12.700 | 0.92 | 60.56 | 62.00 | 0.00 | 0.72 | 5,520 | 73.84 |
| 12.750 | 0.86 | 60.88 | 62.33 | 0.00 | 0.73 | 5,549 | 73.85 |
| 12.800 | 0.81 | 61.08 | 62.54 | 0.00 | 0.73 | 5,567 | 73.86 |
| 12.850 | 0.76 | 61.20 | 62.65 | 0.00 | 0.73 | 5,577 | 73.86 |
| 12.900 | 0.73 | 61.23 | 62.69 | 0.00 | 0.73 | 5,580 | 73.86 |
| 12.950 | 0.69 | 61.19 | 62.65 | 0.00 | 0.73 | 5,577 | 73.86 |
| 13.000 | 0.66 | 61.09 | 62.54 | 0.00 | 0.73 | 5,568 | 73.86 |
| 13.050 | 0.63 | 60.93 | 62.38 | 0.00 | 0.73 | 5,553 | 73.85 |
| 13.100 | 0.61 | 60.72 | 62.17 | 0.00 | 0.72 | 5,535 | 73.85 |
| 13.150 | 0.59 | 60.47 | 61.92 | 0.00 | 0.72 | 5,512 | 73.84 |
| 13.200 | 0.57 | 60.20 | 61.64 | 0.00 | 0.72 | 5,488 | 73.83 |
| 13.250 | 0.56 | 59.91 | 61.34 | 0.00 | 0.72 | 5,461 | 73.82 |
| 13.300 | 0.55 | 59.59 | 61.02 | 0.00 | 0.71 | 5,433 | 73.81 |
| 13.350 | 0.54 | 59.27 | 60.69 | 0.00 | 0.71 | 5,404 | 73.80 |
| 13.400 | 0.53 | 58.93 | 60.35 | 0.00 | 0.71 | 5,374 | 73.79 |
| 13.450 | 0.52 | 58.59 | 59.99 | 0.00 | 0.70 | 5,343 | 73.77 |
| 13.500 | 0.52 | 58.24 | 59.63 | 0.00 | 0.70 | 5,311 | 73.76 |
| 13.550 | 0.51 | 57.87 | 59.26 | 0.00 | 0.69 | 5,279 | 73.75 |
| 13.600 | 0.50 | 57.51 | 58.89 | 0.00 | 0.69 | 5,245 | 73.74 |
| 13.650 | 0.49 | 57.13 | 58.50 | 0.00 | 0.69 | 5,210 | 73.73 |
| 13.700 | 0.49 | 56.75 | 58.11 | 0.00 | 0.68 | 5,175 | 73.71 |
| 13.750 | 0.48 | 56.36 | 57.71 | 0.00 | 0.68 | 5,139 | 73.70 |
| 13.800 | 0.47 | 55.96 | 57.31 | 0.00 | 0.67 | 5,103 | 73.69 |
| 13.850 | 0.47 | 55.56 | 56.90 | 0.00 | 0.67 | 5,066 | 73.67 |
| 13.900 | 0.46 | 55.15 | 56.48 | 0.00 | 0.67 | 5,028 | 73.66 |
| 13.950 | 0.45 | 54.74 | 56.06 | 0.00 | 0.66 | 4,990 | 73.65 |
| 14.000 | 0.44 | 54.32 | 55.63 | 0.00 | 0.66 | 4,952 | 73.63 |
| 14.050 | 0.44 | 53.90 | 55.20 | 0.00 | 0.65 | 4,913 | 73.62 |
| 14.100 | 0.43 | 53.47 | 54.76 | 0.00 | 0.65 | 4,874 | 73.60 |
| 14.150 | 0.43 | 53.04 | 54.33 | 0.00 | 0.64 | 4,834 | 73.59 |
| 14.200 | 0.42 | 52.61 | 53.89 | 0.00 | 0.64 | 4,795 | 73.57 |
| 14.250 | 0.42 | 52.19 | 53.45 | 0.00 | 0.63 | 4,756 | 73.56 |
| 14.300 | 0.42 | 51.77 | 53.03 | 0.00 | 0.63 | 4,717 | 73.55 |
| 14.350 | 0.42 | 51.35 | 52.60 | 0.00 | 0.63 | 4,679 | 73.53 |
| 14.400 | 0.42 | 50.94 | 52.18 | 0.00 | 0.62 | 4,641 | 73.52 |
| 14.450 | 0.41 | 50.54 | 51.77 | 0.00 | 0.62 | 4,604 | 73.50 |
| 14.500 | 0.41 | 50.14 | 51.36 | 0.00 | 0.61 | 4,568 | 73.49 |
| 14.550 | 0.41 | 49.75 | 50.96 | 0.00 | 0.60 | 4,533 | 73.48 |
| 14.600 | 0.41 | 49.38 | 50.57 | 0.00 | 0.60 | 4,498 | 73.47 |
| 14.650 | 0.41 | 49.01 | 50.19 | 0.00 | 0.59 | 4,465 | 73.45 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.40 | 48.64 | 49.82 | 0.00 | 0.59 | 4,432 | 73.44 |
| 14.750 | 0.40 | 48.29 | 49.45 | 0.00 | 0.58 | 4,400 | 73.43 |
| 14.800 | 0.40 | 47.95 | 49.09 | 0.00 | 0.57 | 4,368 | 73.42 |
| 14.850 | 0.40 | 47.61 | 48.75 | 0.00 | 0.57 | 4,338 | 73.41 |
| 14.900 | 0.40 | 47.28 | 48.40 | 0.00 | 0.56 | 4,308 | 73.40 |
| 14.950 | 0.40 | 46.96 | 48.07 | 0.00 | 0.56 | 4,278 | 73.39 |
| 15.000 | 0.39 | 46.64 | 47.74 | 0.00 | 0.55 | 4,250 | 73.38 |
| 15.050 | 0.39 | 46.33 | 47.42 | 0.00 | 0.55 | 4,222 | 73.37 |
| 15.100 | 0.39 | 46.03 | 47.11 | 0.00 | 0.54 | 4,194 | 73.36 |
| 15.150 | 0.39 | 45.73 | 46.80 | 0.00 | 0.54 | 4,167 | 73.35 |
| 15.200 | 0.39 | 45.44 | 46.50 | 0.00 | 0.53 | 4,141 | 73.34 |
| 15.250 | 0.38 | 45.16 | 46.21 | 0.00 | 0.53 | 4,115 | 73.33 |
| 15.300 | 0.38 | 44.88 | 45.92 | 0.00 | 0.52 | 4,089 | 73.32 |
| 15.350 | 0.38 | 44.60 | 45.64 | 0.00 | 0.52 | 4,065 | 73.31 |
| 15.400 | 0.38 | 44.33 | 45.36 | 0.00 | 0.51 | 4,040 | 73.30 |
| 15.450 | 0.38 | 44.07 | 45.09 | 0.00 | 0.51 | 4,016 | 73.29 |
| 15.500 | 0.38 | 43.81 | 44.82 | 0.00 | 0.50 | 3,993 | 73.29 |
| 15.550 | 0.38 | 43.56 | 44.57 | 0.00 | 0.50 | 3,970 | 73.28 |
| 15.600 | 0.38 | 43.32 | 44.32 | 0.00 | 0.50 | 3,948 | 73.27 |
| 15.650 | 0.38 | 43.09 | 44.07 | 0.00 | 0.49 | 3,927 | 73.26 |
| 15.700 | 0.37 | 42.86 | 43.84 | 0.00 | 0.49 | 3,906 | 73.25 |
| 15.750 | 0.37 | 42.64 | 43.61 | 0.00 | 0.49 | 3,886 | 73.25 |
| 15.800 | 0.37 | 42.42 | 43.39 | 0.00 | 0.48 | 3,866 | 73.24 |
| 15.850 | 0.37 | 42.22 | 43.17 | 0.00 | 0.48 | 3,847 | 73.23 |
| 15.900 | 0.37 | 42.01 | 42.96 | 0.00 | 0.47 | 3,829 | 73.23 |
| 15.950 | 0.37 | 41.82 | 42.76 | 0.00 | 0.47 | 3,810 | 73.22 |
| 16.000 | 0.37 | 41.63 | 42.56 | 0.00 | 0.47 | 3,793 | 73.21 |
| 16.050 | 0.37 | 41.44 | 42.37 | 0.00 | 0.47 | 3,776 | 73.21 |
| 16.100 | 0.37 | 41.26 | 42.19 | 0.00 | 0.46 | 3,759 | 73.20 |
| 16.150 | 0.37 | 41.09 | 42.01 | 0.00 | 0.46 | 3,743 | 73.20 |
| 16.200 | 0.37 | 40.92 | 41.84 | 0.00 | 0.46 | 3,728 | 73.19 |
| 16.250 | 0.28 | 40.67 | 41.58 | 0.00 | 0.45 | 3,705 | 73.18 |
| 16.300 | 0.27 | 40.34 | 41.23 | 0.00 | 0.45 | 3,674 | 73.17 |
| 16.350 | 0.27 | 40.00 | 40.88 | 0.00 | 0.44 | 3,643 | 73.16 |
| 16.400 | 0.27 | 39.67 | 40.54 | 0.00 | 0.44 | 3,613 | 73.15 |
| 16.450 | 0.27 | 39.36 | 40.22 | 0.00 | 0.43 | 3,583 | 73.14 |
| 16.500 | 0.27 | 39.05 | 39.90 | 0.00 | 0.43 | 3,555 | 73.13 |
| 16.550 | 0.27 | 38.75 | 39.59 | 0.00 | 0.42 | 3,528 | 73.12 |
| 16.600 | 0.27 | 38.46 | 39.29 | 0.00 | 0.42 | 3,501 | 73.11 |
| 16.650 | 0.27 | 38.18 | 39.00 | 0.00 | 0.41 | 3,475 | 73.10 |
| 16.700 | 0.27 | 37.90 | 38.72 | 0.00 | 0.41 | 3,450 | 73.09 |
| 16.750 | 0.27 | 37.64 | 38.44 | 0.00 | 0.40 | 3,425 | 73.09 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.27 | 37.38 | 38.18 | 0.00 | 0.40 | 3,402 | 73.08 |
| 16.850 | 0.27 | 37.13 | 37.92 | 0.00 | 0.39 | 3,379 | 73.07 |
| 16.900 | 0.27 | 36.89 | 37.67 | 0.00 | 0.39 | 3,356 | 73.06 |
| 16.950 | 0.27 | 36.66 | 37.42 | 0.00 | 0.38 | 3,335 | 73.05 |
| 17.000 | 0.27 | 36.43 | 37.19 | 0.00 | 0.38 | 3,314 | 73.05 |
| 17.050 | 0.27 | 36.20 | 36.96 | 0.00 | 0.38 | 3,293 | 73.04 |
| 17.100 | 0.27 | 35.99 | 36.74 | 0.00 | 0.37 | 3,273 | 73.03 |
| 17.150 | 0.27 | 35.78 | 36.52 | 0.00 | 0.37 | 3,254 | 73.02 |
| 17.200 | 0.27 | 35.58 | 36.31 | 0.00 | 0.37 | 3,235 | 73.02 |
| 17.250 | 0.26 | 35.38 | 36.11 | 0.00 | 0.36 | 3,217 | 73.01 |
| 17.300 | 0.26 | 35.19 | 35.91 | 0.00 | 0.36 | 3,199 | 73.01 |
| 17.350 | 0.26 | 35.00 | 35.72 | 0.00 | 0.36 | 3,182 | 73.00 |
| 17.400 | 0.26 | 34.82 | 35.53 | 0.00 | 0.35 | 3,166 | 72.99 |
| 17.450 | 0.26 | 34.64 | 35.35 | 0.00 | 0.35 | 3,150 | 72.99 |
| 17.500 | 0.26 | 34.47 | 35.17 | 0.00 | 0.35 | 3,134 | 72.98 |
| 17.550 | 0.26 | 34.30 | 35.00 | 0.00 | 0.35 | 3,118 | 72.98 |
| 17.600 | 0.26 | 34.14 | 34.83 | 0.00 | 0.34 | 3,103 | 72.97 |
| 17.650 | 0.26 | 33.98 | 34.66 | 0.00 | 0.34 | 3,089 | 72.97 |
| 17.700 | 0.26 | 33.82 | 34.50 | 0.00 | 0.34 | 3,075 | 72.96 |
| 17.750 | 0.26 | 33.67 | 34.35 | 0.00 | 0.34 | 3,061 | 72.96 |
| 17.800 | 0.26 | 33.53 | 34.19 | 0.00 | 0.33 | 3,047 | 72.95 |
| 17.850 | 0.26 | 33.38 | 34.05 | 0.00 | 0.33 | 3,034 | 72.95 |
| 17.900 | 0.26 | 33.24 | 33.90 | 0.00 | 0.33 | 3,021 | 72.94 |
| 17.950 | 0.26 | 33.10 | 33.76 | 0.00 | 0.33 | 3,009 | 72.94 |
| 18.000 | 0.26 | 32.97 | 33.62 | 0.00 | 0.33 | 2,997 | 72.93 |
| 18.050 | 0.26 | 32.84 | 33.49 | 0.00 | 0.32 | 2,985 | 72.93 |
| 18.100 | 0.26 | 32.71 | 33.36 | 0.00 | 0.32 | 2,973 | 72.93 |
| 18.150 | 0.26 | 32.59 | 33.23 | 0.00 | 0.32 | 2,962 | 72.92 |
| 18.200 | 0.26 | 32.47 | 33.10 | 0.00 | 0.32 | 2,951 | 72.92 |
| 18.250 | 0.26 | 32.35 | 32.98 | 0.00 | 0.32 | 2,940 | 72.92 |
| 18.300 | 0.26 | 32.24 | 32.87 | 0.00 | 0.31 | 2,930 | 72.91 |
| 18.350 | 0.26 | 32.13 | 32.75 | 0.00 | 0.31 | 2,920 | 72.91 |
| 18.400 | 0.26 | 32.02 | 32.64 | 0.00 | 0.31 | 2,910 | 72.90 |
| 18.450 | 0.26 | 31.92 | 32.53 | 0.00 | 0.31 | 2,900 | 72.90 |
| 18.500 | 0.26 | 31.82 | 32.43 | 0.00 | 0.31 | 2,891 | 72.90 |
| 18.550 | 0.26 | 31.72 | 32.33 | 0.00 | 0.31 | 2,882 | 72.90 |
| 18.600 | 0.26 | 31.62 | 32.23 | 0.00 | 0.30 | 2,873 | 72.89 |
| 18.650 | 0.26 | 31.53 | 32.13 | 0.00 | 0.30 | 2,865 | 72.89 |
| 18.700 | 0.26 | 31.44 | 32.04 | 0.00 | 0.30 | 2,857 | 72.89 |
| 18.750 | 0.26 | 31.35 | 31.95 | 0.00 | 0.30 | 2,849 | 72.88 |
| 18.800 | 0.26 | 31.26 | 31.86 | 0.00 | 0.30 | 2,841 | 72.88 |
| 18.850 | 0.26 | 31.18 | 31.78 | 0.00 | 0.30 | 2,833 | 72.88 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.26 | 31.10 | 31.69 | 0.00 | 0.30 | 2,826 | 72.88 |
| 18.950 | 0.26 | 31.02 | 31.61 | 0.00 | 0.29 | 2,819 | 72.87 |
| 19.000 | 0.26 | 30.95 | 31.53 | 0.00 | 0.29 | 2,812 | 72.87 |
| 19.050 | 0.26 | 30.87 | 31.46 | 0.00 | 0.29 | 2,805 | 72.87 |
| 19.100 | 0.26 | 30.80 | 31.38 | 0.00 | 0.29 | 2,798 | 72.87 |
| 19.150 | 0.25 | 30.73 | 31.31 | 0.00 | 0.29 | 2,792 | 72.86 |
| 19.200 | 0.25 | 30.66 | 31.24 | 0.00 | 0.29 | 2,785 | 72.86 |
| 19.250 | 0.25 | 30.59 | 31.17 | 0.00 | 0.29 | 2,779 | 72.86 |
| 19.300 | 0.25 | 30.53 | 31.10 | 0.00 | 0.29 | 2,773 | 72.86 |
| 19.350 | 0.25 | 30.46 | 31.04 | 0.00 | 0.29 | 2,768 | 72.86 |
| 19.400 | 0.25 | 30.40 | 30.97 | 0.00 | 0.29 | 2,762 | 72.85 |
| 19.450 | 0.25 | 30.34 | 30.91 | 0.00 | 0.28 | 2,756 | 72.85 |
| 19.500 | 0.25 | 30.29 | 30.85 | 0.00 | 0.28 | 2,751 | 72.85 |
| 19.550 | 0.25 | 30.23 | 30.79 | 0.00 | 0.28 | 2,746 | 72.85 |
| 19.600 | 0.25 | 30.17 | 30.74 | 0.00 | 0.28 | 2,741 | 72.85 |
| 19.650 | 0.25 | 30.12 | 30.68 | 0.00 | 0.28 | 2,736 | 72.84 |
| 19.700 | 0.25 | 30.07 | 30.63 | 0.00 | 0.28 | 2,731 | 72.84 |
| 19.750 | 0.25 | 30.02 | 30.57 | 0.00 | 0.28 | 2,727 | 72.84 |
| 19.800 | 0.25 | 29.97 | 30.52 | 0.00 | 0.28 | 2,722 | 72.84 |
| 19.850 | 0.25 | 29.92 | 30.47 | 0.00 | 0.28 | 2,718 | 72.84 |
| 19.900 | 0.25 | 29.87 | 30.42 | 0.00 | 0.28 | 2,713 | 72.84 |
| 19.950 | 0.25 | 29.82 | 30.38 | 0.00 | 0.28 | 2,709 | 72.84 |
| 20.000 | 0.25 | 29.78 | 30.33 | 0.00 | 0.28 | 2,705 | 72.83 |
| 20.050 | 0.25 | 29.74 | 30.28 | 0.00 | 0.27 | 2,701 | 72.83 |
| 20.100 | 0.25 | 29.69 | 30.24 | 0.00 | 0.27 | 2,697 | 72.83 |
| 20.150 | 0.25 | 29.65 | 30.20 | 0.00 | 0.27 | 2,693 | 72.83 |
| 20.200 | 0.25 | 29.61 | 30.16 | 0.00 | 0.27 | 2,689 | 72.83 |
| 20.250 | 0.25 | 29.57 | 30.12 | 0.00 | 0.27 | 2,686 | 72.83 |
| 20.300 | 0.25 | 29.53 | 30.08 | 0.00 | 0.27 | 2,682 | 72.83 |
| 20.350 | 0.25 | 29.50 | 30.04 | 0.00 | 0.27 | 2,679 | 72.82 |
| 20.400 | 0.25 | 29.46 | 30.00 | 0.00 | 0.27 | 2,676 | 72.82 |
| 20.450 | 0.25 | 29.42 | 29.96 | 0.00 | 0.27 | 2,672 | 72.82 |
| 20.500 | 0.25 | 29.39 | 29.93 | 0.00 | 0.27 | 2,669 | 72.82 |
| 20.550 | 0.25 | 29.35 | 29.89 | 0.00 | 0.27 | 2,666 | 72.82 |
| 20.600 | 0.25 | 29.32 | 29.86 | 0.00 | 0.27 | 2,663 | 72.82 |
| 20.650 | 0.25 | 29.29 | 29.83 | 0.00 | 0.27 | 2,660 | 72.82 |
| 20.700 | 0.25 | 29.26 | 29.79 | 0.00 | 0.27 | 2,657 | 72.82 |
| 20.750 | 0.25 | 29.23 | 29.76 | 0.00 | 0.27 | 2,654 | 72.82 |
| 20.800 | 0.25 | 29.20 | 29.73 | 0.00 | 0.27 | 2,652 | 72.82 |
| 20.850 | 0.25 | 29.17 | 29.70 | 0.00 | 0.27 | 2,649 | 72.81 |
| 20.900 | 0.25 | 29.14 | 29.67 | 0.00 | 0.27 | 2,647 | 72.81 |
| 20.950 | 0.25 | 29.11 | 29.64 | 0.00 | 0.26 | 2,644 | 72.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.25 | 29.09 | 29.61 | 0.00 | 0.26 | 2,641 | 72.81 |
| 21.050 | 0.25 | 29.06 | 29.59 | 0.00 | 0.26 | 2,639 | 72.81 |
| 21.100 | 0.25 | 29.03 | 29.56 | 0.00 | 0.26 | 2,637 | 72.81 |
| 21.150 | 0.25 | 29.01 | 29.53 | 0.00 | 0.26 | 2,634 | 72.81 |
| 21.200 | 0.25 | 28.98 | 29.51 | 0.00 | 0.26 | 2,632 | 72.81 |
| 21.250 | 0.25 | 28.96 | 29.48 | 0.00 | 0.26 | 2,630 | 72.81 |
| 21.300 | 0.25 | 28.94 | 29.46 | 0.00 | 0.26 | 2,628 | 72.81 |
| 21.350 | 0.25 | 28.91 | 29.44 | 0.00 | 0.26 | 2,626 | 72.81 |
| 21.400 | 0.25 | 28.89 | 29.41 | 0.00 | 0.26 | 2,624 | 72.81 |
| 21.450 | 0.25 | 28.87 | 29.39 | 0.00 | 0.26 | 2,622 | 72.80 |
| 21.500 | 0.25 | 28.85 | 29.37 | 0.00 | 0.26 | 2,620 | 72.80 |
| 21.550 | 0.25 | 28.83 | 29.35 | 0.00 | 0.26 | 2,618 | 72.80 |
| 21.600 | 0.25 | 28.81 | 29.33 | 0.00 | 0.26 | 2,616 | 72.80 |
| 21.650 | 0.25 | 28.79 | 29.31 | 0.00 | 0.26 | 2,614 | 72.80 |
| 21.700 | 0.25 | 28.77 | 29.28 | 0.00 | 0.26 | 2,612 | 72.80 |
| 21.750 | 0.25 | 28.75 | 29.27 | 0.00 | 0.26 | 2,611 | 72.80 |
| 21.800 | 0.25 | 28.73 | 29.25 | 0.00 | 0.26 | 2,609 | 72.80 |
| 21.850 | 0.25 | 28.71 | 29.23 | 0.00 | 0.26 | 2,607 | 72.80 |
| 21.900 | 0.25 | 28.69 | 29.21 | 0.00 | 0.26 | 2,605 | 72.80 |
| 21.950 | 0.25 | 28.67 | 29.19 | 0.00 | 0.26 | 2,604 | 72.80 |
| 22.000 | 0.25 | 28.66 | 29.17 | 0.00 | 0.26 | 2,602 | 72.80 |
| 22.050 | 0.25 | 28.64 | 29.15 | 0.00 | 0.26 | 2,601 | 72.80 |
| 22.100 | 0.25 | 28.62 | 29.14 | 0.00 | 0.26 | 2,599 | 72.80 |
| 22.150 | 0.25 | 28.61 | 29.12 | 0.00 | 0.26 | 2,598 | 72.80 |
| 22.200 | 0.25 | 28.59 | 29.10 | 0.00 | 0.26 | 2,596 | 72.80 |
| 22.250 | 0.25 | 28.57 | 29.09 | 0.00 | 0.26 | 2,595 | 72.80 |
| 22.300 | 0.25 | 28.56 | 29.07 | 0.00 | 0.26 | 2,593 | 72.79 |
| 22.350 | 0.25 | 28.54 | 29.06 | 0.00 | 0.26 | 2,592 | 72.79 |
| 22.400 | 0.25 | 28.53 | 29.04 | 0.00 | 0.26 | 2,591 | 72.79 |
| 22.450 | 0.25 | 28.51 | 29.03 | 0.00 | 0.26 | 2,589 | 72.79 |
| 22.500 | 0.25 | 28.50 | 29.01 | 0.00 | 0.26 | 2,588 | 72.79 |
| 22.550 | 0.25 | 28.49 | 29.00 | 0.00 | 0.26 | 2,587 | 72.79 |
| 22.600 | 0.25 | 28.47 | 28.98 | 0.00 | 0.25 | 2,585 | 72.79 |
| 22.650 | 0.25 | 28.46 | 28.97 | 0.00 | 0.25 | 2,584 | 72.79 |
| 22.700 | 0.25 | 28.45 | 28.95 | 0.00 | 0.25 | 2,583 | 72.79 |
| 22.750 | 0.25 | 28.43 | 28.94 | 0.00 | 0.25 | 2,582 | 72.79 |
| 22.800 | 0.25 | 28.42 | 28.93 | 0.00 | 0.25 | 2,581 | 72.79 |
| 22.850 | 0.25 | 28.41 | 28.91 | 0.00 | 0.25 | 2,579 | 72.79 |
| 22.900 | 0.25 | 28.39 | 28.90 | 0.00 | 0.25 | 2,578 | 72.79 |
| 22.950 | 0.25 | 28.38 | 28.89 | 0.00 | 0.25 | 2,577 | 72.79 |
| 23.000 | 0.25 | 28.37 | 28.88 | 0.00 | 0.25 | 2,576 | 72.79 |
| 23.050 | 0.25 | 28.36 | 28.86 | 0.00 | 0.25 | 2,575 | 72.79 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.25 | 28.35 | 28.85 | 0.00 | 0.25 | 2,574 | 72.79 |
| 23.150 | 0.25 | 28.33 | 28.84 | 0.00 | 0.25 | 2,573 | 72.79 |
| 23.200 | 0.25 | 28.32 | 28.83 | 0.00 | 0.25 | 2,572 | 72.79 |
| 23.250 | 0.25 | 28.31 | 28.82 | 0.00 | 0.25 | 2,571 | 72.79 |
| 23.300 | 0.25 | 28.30 | 28.81 | 0.00 | 0.25 | 2,570 | 72.79 |
| 23.350 | 0.25 | 28.29 | 28.79 | 0.00 | 0.25 | 2,569 | 72.79 |
| 23.400 | 0.25 | 28.28 | 28.78 | 0.00 | 0.25 | 2,568 | 72.79 |
| 23.450 | 0.25 | 28.27 | 28.77 | 0.00 | 0.25 | 2,567 | 72.79 |
| 23.500 | 0.25 | 28.26 | 28.76 | 0.00 | 0.25 | 2,566 | 72.79 |
| 23.550 | 0.25 | 28.25 | 28.75 | 0.00 | 0.25 | 2,565 | 72.79 |
| 23.600 | 0.25 | 28.24 | 28.74 | 0.00 | 0.25 | 2,564 | 72.78 |
| 23.650 | 0.25 | 28.23 | 28.73 | 0.00 | 0.25 | 2,563 | 72.78 |
| 23.700 | 0.25 | 28.22 | 28.72 | 0.00 | 0.25 | 2,562 | 72.78 |
| 23.750 | 0.21 | 28.17 | 28.67 | 0.00 | 0.25 | 2,558 | 72.78 |
| 23.800 | 0.13 | 28.01 | 28.51 | 0.00 | 0.25 | 2,544 | 72.78 |
| 23.850 | 0.13 | 27.78 | 28.27 | 0.00 | 0.24 | 2,523 | 72.77 |
| 23.900 | 0.13 | 27.56 | 28.04 | 0.00 | 0.24 | 2,502 | 72.76 |
| 23.950 | 0.13 | 27.34 | 27.82 | 0.00 | 0.24 | 2,482 | 72.76 |
| 24.000 | 0.13 | 27.13 | 27.60 | 0.00 | 0.23 | 2,463 | 72.75 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.18 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 71.50 |
| 0.050 | 0.00 | 0.17 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 0.100 | 0.00 | 0.17 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.150 | 0.00 | 0.16 | 0.17 | 0.00 | 0.00 | 15 | 71.51 |
| 0.200 | 0.00 | 0.16 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.250 | 0.00 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 71.51 |
| 0.300 | 0.00 | 0.15 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.350 | 0.00 | 0.14 | 0.15 | 0.00 | 0.00 | 13 | 71.51 |
| 0.400 | 0.00 | 0.14 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.450 | 0.00 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.500 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 0.550 | 0.00 | 0.12 | 0.13 | 0.00 | 0.00 | 11 | 71.51 |
| 0.600 | 0.00 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 71.51 |
| 0.650 | 0.01 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 71.51 |
| 0.700 | 0.01 | 0.15 | 0.15 | 0.00 | 0.00 | 14 | 71.51 |
| 0.750 | 0.02 | 0.17 | 0.18 | 0.00 | 0.00 | 16 | 71.51 |
| 0.800 | 0.02 | 0.20 | 0.20 | 0.00 | 0.00 | 18 | 71.51 |
| 0.850 | 0.02 | 0.23 | 0.24 | 0.00 | 0.00 | 21 | 71.52 |
| 0.900 | 0.02 | 0.26 | 0.27 | 0.00 | 0.00 | 24 | 71.52 |
| 0.950 | 0.03 | 0.30 | 0.32 | 0.00 | 0.01 | 28 | 71.52 |
| 1.000 | 0.03 | 0.35 | 0.36 | 0.00 | 0.01 | 32 | 71.52 |
| 1.050 | 0.03 | 0.40 | 0.41 | 0.00 | 0.01 | 36 | 71.53 |
| 1.100 | 0.03 | 0.45 | 0.46 | 0.00 | 0.01 | 41 | 71.53 |
| 1.150 | 0.04 | 0.50 | 0.52 | 0.00 | 0.01 | 46 | 71.53 |
| 1.200 | 0.04 | 0.55 | 0.57 | 0.00 | 0.01 | 51 | 71.54 |
| 1.250 | 0.04 | 0.61 | 0.63 | 0.00 | 0.01 | 56 | 71.54 |
| 1.300 | 0.04 | 0.67 | 0.69 | 0.00 | 0.01 | 61 | 71.55 |
| 1.350 | 0.04 | 0.73 | 0.75 | 0.00 | 0.01 | 67 | 71.55 |
| 1.400 | 0.05 | 0.79 | 0.82 | 0.00 | 0.01 | 72 | 71.55 |
| 1.450 | 0.05 | 0.85 | 0.88 | 0.00 | 0.02 | 78 | 71.56 |
| 1.500 | 0.05 | 0.91 | 0.95 | 0.00 | 0.02 | 84 | 71.56 |
| 1.550 | 0.05 | 0.98 | 1.01 | 0.00 | 0.02 | 90 | 71.57 |
| 1.600 | 0.05 | 1.04 | 1.08 | 0.00 | 0.02 | 95 | 71.57 |
| 1.650 | 0.05 | 1.11 | 1.15 | 0.00 | 0.02 | 101 | 71.58 |
| 1.700 | 0.05 | 1.17 | 1.21 | 0.00 | 0.02 | 107 | 71.58 |
| 1.750 | 0.06 | 1.24 | 1.28 | 0.00 | 0.02 | 113 | 71.58 |
| 1.800 | 0.06 | 1.30 | 1.35 | 0.00 | 0.02 | 119 | 71.59 |
| 1.850 | 0.06 | 1.36 | 1.41 | 0.00 | 0.02 | 125 | 71.59 |
| 1.900 | 0.06 | 1.43 | 1.48 | 0.00 | 0.03 | 131 | 71.60 |
| 1.950 | 0.06 | 1.49 | 1.55 | 0.00 | 0.03 | 137 | 71.60 |
| 2.000 | 0.06 | 1.56 | 1.61 | 0.00 | 0.03 | 143 | 71.61 |
| 2.050 | 0.06 | 1.62 | 1.68 | 0.00 | 0.03 | 148 | 71.61 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.06 | 1.68 | 1.74 | 0.00 | 0.03 | 154 | 71.62 |
| 2.150 | 0.06 | 1.75 | 1.81 | 0.00 | 0.03 | 160 | 71.62 |
| 2.200 | 0.06 | 1.81 | 1.88 | 0.00 | 0.03 | 166 | 71.62 |
| 2.250 | 0.07 | 1.87 | 1.94 | 0.00 | 0.03 | 172 | 71.63 |
| 2.300 | 0.07 | 1.94 | 2.01 | 0.00 | 0.03 | 178 | 71.63 |
| 2.350 | 0.07 | 2.00 | 2.07 | 0.00 | 0.04 | 183 | 71.64 |
| 2.400 | 0.07 | 2.07 | 2.14 | 0.00 | 0.04 | 189 | 71.64 |
| 2.450 | 0.07 | 2.13 | 2.21 | 0.00 | 0.04 | 195 | 71.65 |
| 2.500 | 0.07 | 2.20 | 2.28 | 0.00 | 0.04 | 201 | 71.65 |
| 2.550 | 0.07 | 2.26 | 2.34 | 0.00 | 0.04 | 207 | 71.66 |
| 2.600 | 0.07 | 2.33 | 2.41 | 0.00 | 0.04 | 213 | 71.66 |
| 2.650 | 0.08 | 2.39 | 2.48 | 0.00 | 0.04 | 219 | 71.66 |
| 2.700 | 0.08 | 2.46 | 2.54 | 0.00 | 0.04 | 225 | 71.67 |
| 2.750 | 0.08 | 2.52 | 2.61 | 0.00 | 0.05 | 231 | 71.67 |
| 2.800 | 0.08 | 2.59 | 2.68 | 0.00 | 0.05 | 237 | 71.68 |
| 2.850 | 0.08 | 2.65 | 2.75 | 0.00 | 0.05 | 243 | 71.68 |
| 2.900 | 0.08 | 2.72 | 2.81 | 0.00 | 0.05 | 249 | 71.69 |
| 2.950 | 0.08 | 2.78 | 2.88 | 0.00 | 0.05 | 255 | 71.69 |
| 3.000 | 0.08 | 2.85 | 2.95 | 0.00 | 0.05 | 261 | 71.70 |
| 3.050 | 0.09 | 2.91 | 3.02 | 0.00 | 0.05 | 267 | 71.70 |
| 3.100 | 0.09 | 2.98 | 3.08 | 0.00 | 0.05 | 273 | 71.70 |
| 3.150 | 0.09 | 3.04 | 3.15 | 0.00 | 0.05 | 279 | 71.71 |
| 3.200 | 0.09 | 3.11 | 3.22 | 0.00 | 0.06 | 285 | 71.71 |
| 3.250 | 0.09 | 3.17 | 3.28 | 0.00 | 0.06 | 290 | 71.72 |
| 3.300 | 0.09 | 3.23 | 3.35 | 0.00 | 0.06 | 296 | 71.72 |
| 3.350 | 0.09 | 3.30 | 3.42 | 0.00 | 0.06 | 302 | 71.73 |
| 3.400 | 0.09 | 3.36 | 3.48 | 0.00 | 0.06 | 308 | 71.73 |
| 3.450 | 0.09 | 3.43 | 3.55 | 0.00 | 0.06 | 314 | 71.74 |
| 3.500 | 0.09 | 3.49 | 3.61 | 0.00 | 0.06 | 320 | 71.74 |
| 3.550 | 0.10 | 3.55 | 3.68 | 0.00 | 0.06 | 326 | 71.74 |
| 3.600 | 0.10 | 3.62 | 3.75 | 0.00 | 0.06 | 331 | 71.75 |
| 3.650 | 0.10 | 3.68 | 3.81 | 0.00 | 0.07 | 337 | 71.75 |
| 3.700 | 0.10 | 3.74 | 3.88 | 0.00 | 0.07 | 343 | 71.76 |
| 3.750 | 0.10 | 3.80 | 3.94 | 0.00 | 0.07 | 349 | 71.76 |
| 3.800 | 0.10 | 3.87 | 4.01 | 0.00 | 0.07 | 354 | 71.77 |
| 3.850 | 0.10 | 3.93 | 4.07 | 0.00 | 0.07 | 360 | 71.77 |
| 3.900 | 0.10 | 3.99 | 4.13 | 0.00 | 0.07 | 366 | 71.77 |
| 3.950 | 0.10 | 4.05 | 4.20 | 0.00 | 0.07 | 371 | 71.78 |
| 4.000 | 0.11 | 4.11 | 4.26 | 0.00 | 0.07 | 377 | 71.78 |
| 4.050 | 0.11 | 4.18 | 4.33 | 0.00 | 0.07 | 383 | 71.79 |
| 4.100 | 0.11 | 4.24 | 4.39 | 0.00 | 0.08 | 388 | 71.79 |
| 4.150 | 0.11 | 4.30 | 4.45 | 0.00 | 0.08 | 394 | 71.79 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.11 | 4.36 | 4.51 | 0.00 | 0.08 | 399 | 71.80 |
| 4.250 | 0.11 | 4.42 | 4.58 | 0.00 | 0.08 | 405 | 71.80 |
| 4.300 | 0.11 | 4.48 | 4.64 | 0.00 | 0.08 | 410 | 71.81 |
| 4.350 | 0.11 | 4.54 | 4.70 | 0.00 | 0.08 | 416 | 71.81 |
| 4.400 | 0.11 | 4.60 | 4.76 | 0.00 | 0.08 | 421 | 71.82 |
| 4.450 | 0.11 | 4.66 | 4.82 | 0.00 | 0.08 | 427 | 71.82 |
| 4.500 | 0.11 | 4.72 | 4.88 | 0.00 | 0.08 | 432 | 71.82 |
| 4.550 | 0.12 | 4.77 | 4.95 | 0.00 | 0.09 | 437 | 71.83 |
| 4.600 | 0.12 | 4.83 | 5.01 | 0.00 | 0.09 | 443 | 71.83 |
| 4.650 | 0.12 | 4.89 | 5.07 | 0.00 | 0.09 | 448 | 71.84 |
| 4.700 | 0.12 | 4.95 | 5.13 | 0.00 | 0.09 | 453 | 71.84 |
| 4.750 | 0.12 | 5.01 | 5.19 | 0.00 | 0.09 | 459 | 71.84 |
| 4.800 | 0.12 | 5.06 | 5.25 | 0.00 | 0.09 | 464 | 71.85 |
| 4.850 | 0.12 | 5.12 | 5.31 | 0.00 | 0.09 | 469 | 71.85 |
| 4.900 | 0.12 | 5.18 | 5.36 | 0.00 | 0.09 | 474 | 71.86 |
| 4.950 | 0.12 | 5.24 | 5.42 | 0.00 | 0.09 | 480 | 71.86 |
| 5.000 | 0.12 | 5.29 | 5.48 | 0.00 | 0.09 | 485 | 71.86 |
| 5.050 | 0.12 | 5.35 | 5.54 | 0.00 | 0.10 | 490 | 71.87 |
| 5.100 | 0.13 | 5.40 | 5.60 | 0.00 | 0.10 | 495 | 71.87 |
| 5.150 | 0.13 | 5.46 | 5.66 | 0.00 | 0.10 | 500 | 71.87 |
| 5.200 | 0.13 | 5.52 | 5.71 | 0.00 | 0.10 | 505 | 71.88 |
| 5.250 | 0.13 | 5.57 | 5.77 | 0.00 | 0.10 | 510 | 71.88 |
| 5.300 | 0.13 | 5.63 | 5.83 | 0.00 | 0.10 | 515 | 71.89 |
| 5.350 | 0.13 | 5.68 | 5.89 | 0.00 | 0.10 | 520 | 71.89 |
| 5.400 | 0.13 | 5.74 | 5.94 | 0.00 | 0.10 | 526 | 71.89 |
| 5.450 | 0.13 | 5.79 | 6.00 | 0.00 | 0.10 | 530 | 71.90 |
| 5.500 | 0.13 | 5.84 | 6.05 | 0.00 | 0.10 | 535 | 71.90 |
| 5.550 | 0.13 | 5.90 | 6.11 | 0.00 | 0.11 | 540 | 71.90 |
| 5.600 | 0.13 | 5.95 | 6.17 | 0.00 | 0.11 | 545 | 71.91 |
| 5.650 | 0.13 | 6.01 | 6.22 | 0.00 | 0.11 | 550 | 71.91 |
| 5.700 | 0.14 | 6.06 | 6.28 | 0.00 | 0.11 | 555 | 71.92 |
| 5.750 | 0.14 | 6.11 | 6.33 | 0.00 | 0.11 | 560 | 71.92 |
| 5.800 | 0.14 | 6.17 | 6.39 | 0.00 | 0.11 | 565 | 71.92 |
| 5.850 | 0.14 | 6.22 | 6.44 | 0.00 | 0.11 | 570 | 71.93 |
| 5.900 | 0.14 | 6.27 | 6.50 | 0.00 | 0.11 | 575 | 71.93 |
| 5.950 | 0.14 | 6.33 | 6.55 | 0.00 | 0.11 | 580 | 71.93 |
| 6.000 | 0.14 | 6.38 | 6.61 | 0.00 | 0.11 | 584 | 71.94 |
| 6.050 | 0.14 | 6.43 | 6.66 | 0.00 | 0.12 | 589 | 71.94 |
| 6.100 | 0.14 | 6.49 | 6.72 | 0.00 | 0.12 | 594 | 71.94 |
| 6.150 | 0.15 | 6.54 | 6.78 | 0.00 | 0.12 | 599 | 71.95 |
| 6.200 | 0.15 | 6.60 | 6.84 | 0.00 | 0.12 | 605 | 71.95 |
| 6.250 | 0.15 | 6.66 | 6.90 | 0.00 | 0.12 | 610 | 71.96 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.15 | 6.72 | 6.96 | 0.00 | 0.12 | 616 | 71.96 |
| 6.350 | 0.16 | 6.79 | 7.03 | 0.00 | 0.12 | 622 | 71.97 |
| 6.400 | 0.16 | 6.85 | 7.10 | 0.00 | 0.12 | 628 | 71.97 |
| 6.450 | 0.16 | 6.92 | 7.17 | 0.00 | 0.12 | 634 | 71.97 |
| 6.500 | 0.16 | 7.00 | 7.25 | 0.00 | 0.13 | 641 | 71.98 |
| 6.550 | 0.17 | 7.07 | 7.32 | 0.00 | 0.13 | 648 | 71.99 |
| 6.600 | 0.17 | 7.15 | 7.40 | 0.00 | 0.13 | 655 | 71.99 |
| 6.650 | 0.17 | 7.23 | 7.49 | 0.00 | 0.13 | 662 | 72.00 |
| 6.700 | 0.17 | 7.31 | 7.57 | 0.00 | 0.13 | 669 | 72.00 |
| 6.750 | 0.18 | 7.39 | 7.66 | 0.00 | 0.13 | 674 | 72.00 |
| 6.800 | 0.18 | 7.48 | 7.75 | 0.00 | 0.13 | 679 | 72.01 |
| 6.850 | 0.18 | 7.58 | 7.84 | 0.00 | 0.13 | 684 | 72.01 |
| 6.900 | 0.18 | 7.68 | 7.94 | 0.00 | 0.13 | 690 | 72.02 |
| 6.950 | 0.19 | 7.78 | 8.05 | 0.00 | 0.13 | 695 | 72.02 |
| 7.000 | 0.19 | 7.88 | 8.15 | 0.00 | 0.13 | 701 | 72.03 |
| 7.050 | 0.19 | 7.99 | 8.26 | 0.00 | 0.14 | 707 | 72.03 |
| 7.100 | 0.19 | 8.10 | 8.38 | 0.00 | 0.14 | 714 | 72.03 |
| 7.150 | 0.20 | 8.22 | 8.49 | 0.00 | 0.14 | 720 | 72.04 |
| 7.200 | 0.20 | 8.34 | 8.62 | 0.00 | 0.14 | 727 | 72.04 |
| 7.250 | 0.20 | 8.46 | 8.74 | 0.00 | 0.14 | 734 | 72.05 |
| 7.300 | 0.20 | 8.59 | 8.87 | 0.00 | 0.14 | 741 | 72.06 |
| 7.350 | 0.21 | 8.72 | 9.00 | 0.00 | 0.14 | 749 | 72.06 |
| 7.400 | 0.21 | 8.86 | 9.14 | 0.00 | 0.14 | 756 | 72.07 |
| 7.450 | 0.21 | 8.99 | 9.28 | 0.00 | 0.14 | 764 | 72.07 |
| 7.500 | 0.21 | 9.13 | 9.42 | 0.00 | 0.14 | 772 | 72.08 |
| 7.550 | 0.22 | 9.28 | 9.57 | 0.00 | 0.14 | 780 | 72.08 |
| 7.600 | 0.22 | 9.43 | 9.71 | 0.00 | 0.14 | 789 | 72.09 |
| 7.650 | 0.22 | 9.58 | 9.87 | 0.00 | 0.15 | 797 | 72.10 |
| 7.700 | 0.22 | 9.73 | 10.02 | 0.00 | 0.15 | 806 | 72.10 |
| 7.750 | 0.23 | 9.89 | 10.18 | 0.00 | 0.15 | 815 | 72.11 |
| 7.800 | 0.23 | 10.05 | 10.34 | 0.00 | 0.15 | 824 | 72.12 |
| 7.850 | 0.23 | 10.20 | 10.50 | 0.00 | 0.15 | 833 | 72.12 |
| 7.900 | 0.23 | 10.36 | 10.66 | 0.00 | 0.15 | 842 | 72.13 |
| 7.950 | 0.23 | 10.53 | 10.83 | 0.00 | 0.15 | 851 | 72.14 |
| 8.000 | 0.23 | 10.69 | 10.99 | 0.00 | 0.15 | 860 | 72.14 |
| 8.050 | 0.24 | 10.85 | 11.16 | 0.00 | 0.15 | 869 | 72.15 |
| 8.100 | 0.24 | 11.02 | 11.33 | 0.00 | 0.15 | 879 | 72.16 |
| 8.150 | 0.24 | 11.19 | 11.50 | 0.00 | 0.16 | 888 | 72.17 |
| 8.200 | 0.24 | 11.36 | 11.67 | 0.00 | 0.16 | 898 | 72.17 |
| 8.250 | 0.25 | 11.54 | 11.85 | 0.00 | 0.16 | 908 | 72.18 |
| 8.300 | 0.25 | 11.72 | 12.03 | 0.00 | 0.16 | 918 | 72.19 |
| 8.350 | 0.25 | 11.90 | 12.22 | 0.00 | 0.16 | 929 | 72.20 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.26 | 12.10 | 12.42 | 0.00 | 0.16 | 940 | 72.20 |
| 8.450 | 0.26 | 12.29 | 12.62 | 0.00 | 0.16 | 951 | 72.21 |
| 8.500 | 0.27 | 12.49 | 12.82 | 0.00 | 0.16 | 962 | 72.22 |
| 8.550 | 0.27 | 12.70 | 13.03 | 0.00 | 0.16 | 974 | 72.23 |
| 8.600 | 0.27 | 12.91 | 13.24 | 0.00 | 0.17 | 985 | 72.24 |
| 8.650 | 0.28 | 13.12 | 13.45 | 0.00 | 0.17 | 997 | 72.25 |
| 8.700 | 0.28 | 13.34 | 13.67 | 0.00 | 0.17 | 1,020 | 72.26 |
| 8.750 | 0.28 | 13.56 | 13.90 | 0.00 | 0.17 | 1,047 | 72.27 |
| 8.800 | 0.29 | 13.79 | 14.13 | 0.00 | 0.17 | 1,076 | 72.28 |
| 8.850 | 0.29 | 14.02 | 14.36 | 0.00 | 0.17 | 1,104 | 72.28 |
| 8.900 | 0.29 | 14.25 | 14.60 | 0.00 | 0.17 | 1,134 | 72.29 |
| 8.950 | 0.30 | 14.49 | 14.84 | 0.00 | 0.18 | 1,164 | 72.31 |
| 9.000 | 0.30 | 14.73 | 15.09 | 0.00 | 0.18 | 1,194 | 72.32 |
| 9.050 | 0.30 | 14.98 | 15.34 | 0.00 | 0.18 | 1,224 | 72.33 |
| 9.100 | 0.30 | 15.22 | 15.58 | 0.00 | 0.18 | 1,255 | 72.34 |
| 9.150 | 0.30 | 15.46 | 15.83 | 0.00 | 0.18 | 1,285 | 72.35 |
| 9.200 | 0.31 | 15.71 | 16.07 | 0.00 | 0.18 | 1,315 | 72.36 |
| 9.250 | 0.31 | 15.95 | 16.32 | 0.00 | 0.18 | 1,345 | 72.37 |
| 9.300 | 0.31 | 16.19 | 16.56 | 0.00 | 0.19 | 1,375 | 72.38 |
| 9.350 | 0.31 | 16.43 | 16.81 | 0.00 | 0.19 | 1,405 | 72.39 |
| 9.400 | 0.31 | 16.67 | 17.05 | 0.00 | 0.19 | 1,436 | 72.40 |
| 9.450 | 0.31 | 16.92 | 17.30 | 0.00 | 0.19 | 1,466 | 72.41 |
| 9.500 | 0.31 | 17.16 | 17.54 | 0.00 | 0.19 | 1,496 | 72.42 |
| 9.550 | 0.31 | 17.40 | 17.79 | 0.00 | 0.19 | 1,526 | 72.43 |
| 9.600 | 0.32 | 17.64 | 18.03 | 0.00 | 0.20 | 1,555 | 72.44 |
| 9.650 | 0.32 | 17.88 | 18.27 | 0.00 | 0.20 | 1,585 | 72.45 |
| 9.700 | 0.32 | 18.12 | 18.51 | 0.00 | 0.20 | 1,615 | 72.46 |
| 9.750 | 0.32 | 18.36 | 18.76 | 0.00 | 0.20 | 1,645 | 72.47 |
| 9.800 | 0.32 | 18.60 | 19.00 | 0.00 | 0.20 | 1,675 | 72.48 |
| 9.850 | 0.32 | 18.84 | 19.24 | 0.00 | 0.20 | 1,705 | 72.49 |
| 9.900 | 0.32 | 19.08 | 19.48 | 0.00 | 0.20 | 1,735 | 72.50 |
| 9.950 | 0.33 | 19.32 | 19.73 | 0.00 | 0.21 | 1,757 | 72.51 |
| 10.000 | 0.33 | 19.56 | 19.97 | 0.00 | 0.21 | 1,779 | 72.51 |
| 10.050 | 0.33 | 19.80 | 20.21 | 0.00 | 0.21 | 1,801 | 72.52 |
| 10.100 | 0.33 | 20.04 | 20.46 | 0.00 | 0.21 | 1,823 | 72.53 |
| 10.150 | 0.33 | 20.29 | 20.71 | 0.00 | 0.21 | 1,845 | 72.54 |
| 10.200 | 0.34 | 20.54 | 20.96 | 0.00 | 0.21 | 1,867 | 72.54 |
| 10.250 | 0.34 | 20.79 | 21.21 | 0.00 | 0.21 | 1,890 | 72.55 |
| 10.300 | 0.34 | 21.05 | 21.47 | 0.00 | 0.21 | 1,913 | 72.56 |
| 10.350 | 0.34 | 21.31 | 21.73 | 0.00 | 0.21 | 1,937 | 72.57 |
| 10.400 | 0.35 | 21.57 | 22.00 | 0.00 | 0.21 | 1,961 | 72.58 |
| 10.450 | 0.35 | 21.84 | 22.27 | 0.00 | 0.21 | 1,985 | 72.59 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.35 | 22.11 | 22.54 | 0.00 | 0.22 | 2,009 | 72.59 |
| 10.550 | 0.36 | 22.38 | 22.82 | 0.00 | 0.22 | 2,034 | 72.60 |
| 10.600 | 0.36 | 22.66 | 23.10 | 0.00 | 0.22 | 2,059 | 72.61 |
| 10.650 | 0.36 | 22.94 | 23.38 | 0.00 | 0.22 | 2,084 | 72.62 |
| 10.700 | 0.36 | 23.23 | 23.67 | 0.00 | 0.22 | 2,110 | 72.63 |
| 10.750 | 0.37 | 23.52 | 23.96 | 0.00 | 0.22 | 2,136 | 72.64 |
| 10.800 | 0.37 | 23.81 | 24.25 | 0.00 | 0.22 | 2,163 | 72.65 |
| 10.850 | 0.37 | 24.10 | 24.55 | 0.00 | 0.22 | 2,189 | 72.66 |
| 10.900 | 0.38 | 24.40 | 24.85 | 0.00 | 0.22 | 2,216 | 72.66 |
| 10.950 | 0.38 | 24.71 | 25.16 | 0.00 | 0.23 | 2,244 | 72.67 |
| 11.000 | 0.38 | 25.01 | 25.46 | 0.00 | 0.23 | 2,271 | 72.68 |
| 11.050 | 0.38 | 25.32 | 25.78 | 0.00 | 0.23 | 2,300 | 72.69 |
| 11.100 | 0.39 | 25.64 | 26.10 | 0.00 | 0.23 | 2,328 | 72.70 |
| 11.150 | 0.40 | 25.97 | 26.43 | 0.00 | 0.23 | 2,358 | 72.71 |
| 11.200 | 0.40 | 26.31 | 26.77 | 0.00 | 0.23 | 2,389 | 72.72 |
| 11.250 | 0.40 | 26.65 | 27.12 | 0.00 | 0.23 | 2,420 | 72.73 |
| 11.300 | 0.41 | 27.00 | 27.46 | 0.00 | 0.23 | 2,451 | 72.75 |
| 11.350 | 0.41 | 27.34 | 27.82 | 0.00 | 0.24 | 2,482 | 72.76 |
| 11.400 | 0.41 | 27.68 | 28.17 | 0.00 | 0.24 | 2,513 | 72.77 |
| 11.450 | 0.42 | 28.02 | 28.51 | 0.00 | 0.25 | 2,544 | 72.78 |
| 11.500 | 0.42 | 28.35 | 28.86 | 0.00 | 0.25 | 2,574 | 72.79 |
| 11.550 | 0.43 | 28.68 | 29.20 | 0.00 | 0.26 | 2,604 | 72.80 |
| 11.600 | 0.44 | 29.02 | 29.55 | 0.00 | 0.26 | 2,636 | 72.81 |
| 11.650 | 0.46 | 29.38 | 29.92 | 0.00 | 0.27 | 2,668 | 72.82 |
| 11.700 | 0.48 | 29.77 | 30.32 | 0.00 | 0.28 | 2,704 | 72.83 |
| 11.750 | 0.51 | 30.19 | 30.76 | 0.00 | 0.28 | 2,743 | 72.85 |
| 11.800 | 0.54 | 30.66 | 31.24 | 0.00 | 0.29 | 2,786 | 72.86 |
| 11.850 | 1.05 | 31.64 | 32.25 | 0.00 | 0.30 | 2,875 | 72.89 |
| 11.900 | 2.24 | 34.24 | 34.94 | 0.00 | 0.35 | 3,113 | 72.98 |
| 11.950 | 2.41 | 38.08 | 38.90 | 0.00 | 0.41 | 3,466 | 73.10 |
| 12.000 | 3.33 | 42.85 | 43.82 | 0.00 | 0.49 | 3,905 | 73.25 |
| 12.050 | 4.18 | 49.16 | 50.35 | 0.00 | 0.59 | 4,479 | 73.46 |
| 12.100 | 6.61 | 58.54 | 59.94 | 0.00 | 0.70 | 5,339 | 73.77 |
| 12.150 | 7.23 | 70.74 | 72.38 | 0.00 | 0.82 | 6,448 | 74.19 |
| 12.200 | 6.24 | 82.35 | 84.20 | 0.00 | 0.92 | 7,501 | 74.61 |
| 12.250 | 5.04 | 91.62 | 93.63 | 0.00 | 1.00 | 8,338 | 74.97 |
| 12.300 | 4.29 | 98.82 | 100.96 | 0.00 | 1.07 | 9,011 | 75.28 |
| 12.350 | 3.74 | 104.61 | 106.85 | 0.00 | 1.12 | 9,521 | 75.54 |
| 12.400 | 3.24 | 109.26 | 111.60 | 0.00 | 1.17 | 9,960 | 75.82 |
| 12.450 | 2.78 | 112.86 | 115.28 | 0.00 | 1.21 | 10,266 | 76.03 |
| 12.500 | 2.31 | 115.48 | 117.95 | 0.00 | 1.24 | 10,504 | 76.21 |
| 12.550 | 1.91 | 117.18 | 119.70 | 0.00 | 1.26 | 10,660 | 76.33 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 1.60 | 118.15 | 120.69 | 0.00 | 1.27 | 10,748 | 76.39 |
| 12.650 | 1.41 | 118.61 | 121.16 | 0.00 | 1.28 | 10,790 | 76.43 |
| 12.700 | 1.29 | 118.75 | 121.31 | 0.00 | 1.28 | 10,803 | 76.44 |
| 12.750 | 1.20 | 118.70 | 121.25 | 0.00 | 1.28 | 10,798 | 76.43 |
| 12.800 | 1.13 | 118.48 | 121.03 | 0.00 | 1.27 | 10,778 | 76.42 |
| 12.850 | 1.07 | 118.14 | 120.68 | 0.00 | 1.27 | 10,747 | 76.39 |
| 12.900 | 1.01 | 117.69 | 120.22 | 0.00 | 1.26 | 10,706 | 76.36 |
| 12.950 | 0.95 | 117.13 | 119.65 | 0.00 | 1.26 | 10,655 | 76.33 |
| 13.000 | 0.90 | 116.48 | 118.98 | 0.00 | 1.25 | 10,596 | 76.28 |
| 13.050 | 0.85 | 115.75 | 118.24 | 0.00 | 1.24 | 10,529 | 76.23 |
| 13.100 | 0.82 | 114.96 | 117.42 | 0.00 | 1.23 | 10,457 | 76.18 |
| 13.150 | 0.79 | 114.12 | 116.57 | 0.00 | 1.22 | 10,381 | 76.12 |
| 13.200 | 0.77 | 113.26 | 115.68 | 0.00 | 1.21 | 10,302 | 76.06 |
| 13.250 | 0.75 | 112.38 | 114.78 | 0.00 | 1.20 | 10,222 | 76.00 |
| 13.300 | 0.74 | 111.48 | 113.87 | 0.00 | 1.19 | 10,147 | 75.95 |
| 13.350 | 0.73 | 110.58 | 112.95 | 0.00 | 1.18 | 10,071 | 75.89 |
| 13.400 | 0.71 | 109.67 | 112.02 | 0.00 | 1.17 | 9,995 | 75.84 |
| 13.450 | 0.70 | 108.76 | 111.08 | 0.00 | 1.16 | 9,918 | 75.79 |
| 13.500 | 0.69 | 107.84 | 110.15 | 0.00 | 1.15 | 9,837 | 75.73 |
| 13.550 | 0.68 | 106.92 | 109.21 | 0.00 | 1.14 | 9,747 | 75.68 |
| 13.600 | 0.67 | 106.00 | 108.27 | 0.00 | 1.13 | 9,656 | 75.62 |
| 13.650 | 0.66 | 105.07 | 107.32 | 0.00 | 1.12 | 9,566 | 75.57 |
| 13.700 | 0.65 | 104.15 | 106.38 | 0.00 | 1.11 | 9,475 | 75.51 |
| 13.750 | 0.64 | 103.22 | 105.43 | 0.00 | 1.10 | 9,392 | 75.47 |
| 13.800 | 0.63 | 102.29 | 104.48 | 0.00 | 1.10 | 9,311 | 75.43 |
| 13.850 | 0.61 | 101.35 | 103.53 | 0.00 | 1.09 | 9,230 | 75.39 |
| 13.900 | 0.60 | 100.41 | 102.57 | 0.00 | 1.08 | 9,149 | 75.35 |
| 13.950 | 0.59 | 99.47 | 101.61 | 0.00 | 1.07 | 9,067 | 75.31 |
| 14.000 | 0.58 | 98.52 | 100.64 | 0.00 | 1.06 | 8,984 | 75.26 |
| 14.050 | 0.57 | 97.56 | 99.67 | 0.00 | 1.06 | 8,896 | 75.22 |
| 14.100 | 0.56 | 96.61 | 98.70 | 0.00 | 1.05 | 8,806 | 75.18 |
| 14.150 | 0.56 | 95.65 | 97.73 | 0.00 | 1.04 | 8,715 | 75.14 |
| 14.200 | 0.55 | 94.70 | 96.76 | 0.00 | 1.03 | 8,625 | 75.10 |
| 14.250 | 0.54 | 93.75 | 95.80 | 0.00 | 1.02 | 8,535 | 75.06 |
| 14.300 | 0.54 | 92.81 | 94.84 | 0.00 | 1.01 | 8,445 | 75.01 |
| 14.350 | 0.53 | 91.87 | 93.88 | 0.00 | 1.01 | 8,360 | 74.98 |
| 14.400 | 0.53 | 90.94 | 92.93 | 0.00 | 1.00 | 8,278 | 74.94 |
| 14.450 | 0.52 | 90.01 | 91.99 | 0.00 | 0.99 | 8,196 | 74.91 |
| 14.500 | 0.52 | 89.09 | 91.05 | 0.00 | 0.98 | 8,114 | 74.87 |
| 14.550 | 0.51 | 88.17 | 90.12 | 0.00 | 0.97 | 8,033 | 74.83 |
| 14.600 | 0.51 | 87.26 | 89.19 | 0.00 | 0.97 | 7,952 | 74.80 |
| 14.650 | 0.50 | 86.35 | 88.27 | 0.00 | 0.96 | 7,872 | 74.76 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.50 | 85.45 | 87.35 | 0.00 | 0.95 | 7,790 | 74.73 |
| 14.750 | 0.49 | 84.56 | 86.44 | 0.00 | 0.94 | 7,706 | 74.70 |
| 14.800 | 0.49 | 83.66 | 85.54 | 0.00 | 0.94 | 7,623 | 74.66 |
| 14.850 | 0.48 | 82.78 | 84.63 | 0.00 | 0.93 | 7,541 | 74.63 |
| 14.900 | 0.48 | 81.90 | 83.74 | 0.00 | 0.92 | 7,459 | 74.59 |
| 14.950 | 0.47 | 81.02 | 82.85 | 0.00 | 0.91 | 7,378 | 74.56 |
| 15.000 | 0.47 | 80.15 | 81.96 | 0.00 | 0.91 | 7,297 | 74.53 |
| 15.050 | 0.46 | 79.28 | 81.08 | 0.00 | 0.90 | 7,217 | 74.49 |
| 15.100 | 0.46 | 78.42 | 80.20 | 0.00 | 0.89 | 7,140 | 74.46 |
| 15.150 | 0.45 | 77.57 | 79.33 | 0.00 | 0.88 | 7,063 | 74.43 |
| 15.200 | 0.45 | 76.72 | 78.47 | 0.00 | 0.88 | 6,987 | 74.40 |
| 15.250 | 0.44 | 75.87 | 77.61 | 0.00 | 0.87 | 6,912 | 74.37 |
| 15.300 | 0.44 | 75.03 | 76.75 | 0.00 | 0.86 | 6,837 | 74.34 |
| 15.350 | 0.43 | 74.20 | 75.90 | 0.00 | 0.85 | 6,762 | 74.31 |
| 15.400 | 0.43 | 73.37 | 75.06 | 0.00 | 0.84 | 6,688 | 74.29 |
| 15.450 | 0.43 | 72.55 | 74.22 | 0.00 | 0.84 | 6,615 | 74.26 |
| 15.500 | 0.42 | 71.74 | 73.40 | 0.00 | 0.83 | 6,540 | 74.23 |
| 15.550 | 0.42 | 70.93 | 72.58 | 0.00 | 0.82 | 6,466 | 74.20 |
| 15.600 | 0.42 | 70.14 | 71.77 | 0.00 | 0.82 | 6,393 | 74.17 |
| 15.650 | 0.41 | 69.35 | 70.97 | 0.00 | 0.81 | 6,320 | 74.14 |
| 15.700 | 0.41 | 68.58 | 70.18 | 0.00 | 0.80 | 6,249 | 74.12 |
| 15.750 | 0.41 | 67.81 | 69.40 | 0.00 | 0.79 | 6,178 | 74.09 |
| 15.800 | 0.41 | 67.05 | 68.62 | 0.00 | 0.79 | 6,108 | 74.06 |
| 15.850 | 0.40 | 66.30 | 67.86 | 0.00 | 0.78 | 6,038 | 74.04 |
| 15.900 | 0.40 | 65.55 | 67.10 | 0.00 | 0.77 | 5,970 | 74.01 |
| 15.950 | 0.40 | 64.82 | 66.35 | 0.00 | 0.77 | 5,903 | 73.98 |
| 16.000 | 0.40 | 64.09 | 65.61 | 0.00 | 0.76 | 5,838 | 73.96 |
| 16.050 | 0.39 | 63.38 | 64.88 | 0.00 | 0.75 | 5,774 | 73.94 |
| 16.100 | 0.39 | 62.67 | 64.16 | 0.00 | 0.74 | 5,710 | 73.91 |
| 16.150 | 0.39 | 61.98 | 63.46 | 0.00 | 0.74 | 5,648 | 73.89 |
| 16.200 | 0.39 | 61.30 | 62.76 | 0.00 | 0.73 | 5,587 | 73.87 |
| 16.250 | 0.39 | 60.63 | 62.07 | 0.00 | 0.72 | 5,526 | 73.84 |
| 16.300 | 0.39 | 59.97 | 61.40 | 0.00 | 0.72 | 5,467 | 73.82 |
| 16.350 | 0.38 | 59.32 | 60.74 | 0.00 | 0.71 | 5,409 | 73.80 |
| 16.400 | 0.38 | 58.68 | 60.09 | 0.00 | 0.70 | 5,352 | 73.78 |
| 16.450 | 0.38 | 58.06 | 59.45 | 0.00 | 0.70 | 5,295 | 73.76 |
| 16.500 | 0.38 | 57.44 | 58.82 | 0.00 | 0.69 | 5,239 | 73.74 |
| 16.550 | 0.38 | 56.84 | 58.20 | 0.00 | 0.68 | 5,183 | 73.72 |
| 16.600 | 0.38 | 56.24 | 57.60 | 0.00 | 0.68 | 5,129 | 73.70 |
| 16.650 | 0.38 | 55.66 | 57.00 | 0.00 | 0.67 | 5,075 | 73.68 |
| 16.700 | 0.38 | 55.08 | 56.41 | 0.00 | 0.66 | 5,022 | 73.66 |
| 16.750 | 0.38 | 54.52 | 55.84 | 0.00 | 0.66 | 4,970 | 73.64 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.38 | 53.97 | 55.28 | 0.00 | 0.65 | 4,920 | 73.62 |
| 16.850 | 0.38 | 53.43 | 54.72 | 0.00 | 0.65 | 4,870 | 73.60 |
| 16.900 | 0.38 | 52.90 | 54.18 | 0.00 | 0.64 | 4,821 | 73.58 |
| 16.950 | 0.38 | 52.38 | 53.65 | 0.00 | 0.64 | 4,773 | 73.57 |
| 17.000 | 0.38 | 51.87 | 53.13 | 0.00 | 0.63 | 4,727 | 73.55 |
| 17.050 | 0.38 | 51.37 | 52.62 | 0.00 | 0.63 | 4,681 | 73.53 |
| 17.100 | 0.33 | 50.83 | 52.07 | 0.00 | 0.62 | 4,631 | 73.51 |
| 17.150 | 0.28 | 50.22 | 51.44 | 0.00 | 0.61 | 4,575 | 73.49 |
| 17.200 | 0.28 | 49.57 | 50.78 | 0.00 | 0.60 | 4,516 | 73.47 |
| 17.250 | 0.28 | 48.95 | 50.14 | 0.00 | 0.59 | 4,460 | 73.45 |
| 17.300 | 0.28 | 48.35 | 49.51 | 0.00 | 0.58 | 4,405 | 73.43 |
| 17.350 | 0.28 | 47.77 | 48.91 | 0.00 | 0.57 | 4,352 | 73.41 |
| 17.400 | 0.28 | 47.20 | 48.33 | 0.00 | 0.56 | 4,301 | 73.40 |
| 17.450 | 0.28 | 46.65 | 47.76 | 0.00 | 0.55 | 4,251 | 73.38 |
| 17.500 | 0.28 | 46.12 | 47.21 | 0.00 | 0.54 | 4,203 | 73.36 |
| 17.550 | 0.28 | 45.60 | 46.67 | 0.00 | 0.53 | 4,156 | 73.34 |
| 17.600 | 0.28 | 45.10 | 46.16 | 0.00 | 0.53 | 4,110 | 73.33 |
| 17.650 | 0.28 | 44.62 | 45.66 | 0.00 | 0.52 | 4,066 | 73.31 |
| 17.700 | 0.27 | 44.15 | 45.17 | 0.00 | 0.51 | 4,023 | 73.30 |
| 17.750 | 0.27 | 43.69 | 44.70 | 0.00 | 0.50 | 3,982 | 73.28 |
| 17.800 | 0.27 | 43.25 | 44.24 | 0.00 | 0.50 | 3,942 | 73.27 |
| 17.850 | 0.27 | 42.82 | 43.79 | 0.00 | 0.49 | 3,902 | 73.25 |
| 17.900 | 0.27 | 42.40 | 43.36 | 0.00 | 0.48 | 3,864 | 73.24 |
| 17.950 | 0.27 | 42.00 | 42.94 | 0.00 | 0.47 | 3,827 | 73.23 |
| 18.000 | 0.27 | 41.60 | 42.54 | 0.00 | 0.47 | 3,791 | 73.21 |
| 18.050 | 0.27 | 41.22 | 42.14 | 0.00 | 0.46 | 3,756 | 73.20 |
| 18.100 | 0.27 | 40.85 | 41.76 | 0.00 | 0.46 | 3,721 | 73.19 |
| 18.150 | 0.27 | 40.49 | 41.39 | 0.00 | 0.45 | 3,688 | 73.18 |
| 18.200 | 0.27 | 40.15 | 41.03 | 0.00 | 0.44 | 3,656 | 73.17 |
| 18.250 | 0.27 | 39.81 | 40.68 | 0.00 | 0.44 | 3,625 | 73.16 |
| 18.300 | 0.27 | 39.48 | 40.35 | 0.00 | 0.43 | 3,595 | 73.15 |
| 18.350 | 0.27 | 39.17 | 40.02 | 0.00 | 0.43 | 3,566 | 73.13 |
| 18.400 | 0.27 | 38.86 | 39.70 | 0.00 | 0.42 | 3,538 | 73.12 |
| 18.450 | 0.27 | 38.56 | 39.40 | 0.00 | 0.42 | 3,511 | 73.12 |
| 18.500 | 0.27 | 38.28 | 39.10 | 0.00 | 0.41 | 3,484 | 73.11 |
| 18.550 | 0.27 | 38.00 | 38.81 | 0.00 | 0.41 | 3,458 | 73.10 |
| 18.600 | 0.27 | 37.73 | 38.54 | 0.00 | 0.40 | 3,434 | 73.09 |
| 18.650 | 0.27 | 37.47 | 38.27 | 0.00 | 0.40 | 3,410 | 73.08 |
| 18.700 | 0.27 | 37.22 | 38.00 | 0.00 | 0.39 | 3,386 | 73.07 |
| 18.750 | 0.27 | 36.97 | 37.75 | 0.00 | 0.39 | 3,364 | 73.06 |
| 18.800 | 0.27 | 36.73 | 37.50 | 0.00 | 0.39 | 3,342 | 73.06 |
| 18.850 | 0.27 | 36.50 | 37.27 | 0.00 | 0.38 | 3,321 | 73.05 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.27 | 36.28 | 37.04 | 0.00 | 0.38 | 3,300 | 73.04 |
| 18.950 | 0.27 | 36.06 | 36.81 | 0.00 | 0.37 | 3,280 | 73.03 |
| 19.000 | 0.27 | 35.85 | 36.60 | 0.00 | 0.37 | 3,261 | 73.03 |
| 19.050 | 0.27 | 35.65 | 36.39 | 0.00 | 0.37 | 3,242 | 73.02 |
| 19.100 | 0.27 | 35.45 | 36.18 | 0.00 | 0.36 | 3,224 | 73.01 |
| 19.150 | 0.27 | 35.26 | 35.99 | 0.00 | 0.36 | 3,206 | 73.01 |
| 19.200 | 0.27 | 35.08 | 35.79 | 0.00 | 0.36 | 3,189 | 73.00 |
| 19.250 | 0.27 | 34.90 | 35.61 | 0.00 | 0.36 | 3,173 | 73.00 |
| 19.300 | 0.27 | 34.72 | 35.43 | 0.00 | 0.35 | 3,157 | 72.99 |
| 19.350 | 0.27 | 34.55 | 35.25 | 0.00 | 0.35 | 3,141 | 72.99 |
| 19.400 | 0.27 | 34.39 | 35.08 | 0.00 | 0.35 | 3,126 | 72.98 |
| 19.450 | 0.26 | 34.23 | 34.92 | 0.00 | 0.35 | 3,112 | 72.97 |
| 19.500 | 0.26 | 34.07 | 34.76 | 0.00 | 0.34 | 3,097 | 72.97 |
| 19.550 | 0.26 | 33.92 | 34.60 | 0.00 | 0.34 | 3,084 | 72.97 |
| 19.600 | 0.26 | 33.77 | 34.45 | 0.00 | 0.34 | 3,070 | 72.96 |
| 19.650 | 0.26 | 33.63 | 34.30 | 0.00 | 0.34 | 3,057 | 72.96 |
| 19.700 | 0.26 | 33.49 | 34.16 | 0.00 | 0.33 | 3,044 | 72.95 |
| 19.750 | 0.26 | 33.36 | 34.02 | 0.00 | 0.33 | 3,032 | 72.95 |
| 19.800 | 0.26 | 33.23 | 33.89 | 0.00 | 0.33 | 3,020 | 72.94 |
| 19.850 | 0.26 | 33.10 | 33.75 | 0.00 | 0.33 | 3,008 | 72.94 |
| 19.900 | 0.26 | 32.98 | 33.63 | 0.00 | 0.33 | 2,997 | 72.94 |
| 19.950 | 0.26 | 32.85 | 33.50 | 0.00 | 0.32 | 2,986 | 72.93 |
| 20.000 | 0.26 | 32.74 | 33.38 | 0.00 | 0.32 | 2,975 | 72.93 |
| 20.050 | 0.26 | 32.62 | 33.26 | 0.00 | 0.32 | 2,965 | 72.92 |
| 20.100 | 0.26 | 32.51 | 33.15 | 0.00 | 0.32 | 2,955 | 72.92 |
| 20.150 | 0.26 | 32.40 | 33.04 | 0.00 | 0.32 | 2,945 | 72.92 |
| 20.200 | 0.26 | 32.30 | 32.93 | 0.00 | 0.31 | 2,935 | 72.91 |
| 20.250 | 0.26 | 32.20 | 32.82 | 0.00 | 0.31 | 2,926 | 72.91 |
| 20.300 | 0.26 | 32.10 | 32.72 | 0.00 | 0.31 | 2,917 | 72.91 |
| 20.350 | 0.26 | 32.00 | 32.62 | 0.00 | 0.31 | 2,908 | 72.90 |
| 20.400 | 0.26 | 31.91 | 32.53 | 0.00 | 0.31 | 2,900 | 72.90 |
| 20.450 | 0.26 | 31.82 | 32.43 | 0.00 | 0.31 | 2,891 | 72.90 |
| 20.500 | 0.26 | 31.73 | 32.34 | 0.00 | 0.31 | 2,883 | 72.90 |
| 20.550 | 0.26 | 31.64 | 32.25 | 0.00 | 0.30 | 2,875 | 72.89 |
| 20.600 | 0.26 | 31.56 | 32.16 | 0.00 | 0.30 | 2,868 | 72.89 |
| 20.650 | 0.26 | 31.48 | 32.08 | 0.00 | 0.30 | 2,860 | 72.89 |
| 20.700 | 0.26 | 31.40 | 32.00 | 0.00 | 0.30 | 2,853 | 72.88 |
| 20.750 | 0.26 | 31.32 | 31.92 | 0.00 | 0.30 | 2,846 | 72.88 |
| 20.800 | 0.26 | 31.24 | 31.84 | 0.00 | 0.30 | 2,839 | 72.88 |
| 20.850 | 0.26 | 31.17 | 31.77 | 0.00 | 0.30 | 2,832 | 72.88 |
| 20.900 | 0.26 | 31.10 | 31.69 | 0.00 | 0.30 | 2,826 | 72.88 |
| 20.950 | 0.26 | 31.03 | 31.62 | 0.00 | 0.29 | 2,819 | 72.87 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.26 | 30.96 | 31.55 | 0.00 | 0.29 | 2,813 | 72.87 |
| 21.050 | 0.26 | 30.90 | 31.48 | 0.00 | 0.29 | 2,807 | 72.87 |
| 21.100 | 0.26 | 30.83 | 31.42 | 0.00 | 0.29 | 2,801 | 72.87 |
| 21.150 | 0.26 | 30.77 | 31.35 | 0.00 | 0.29 | 2,796 | 72.87 |
| 21.200 | 0.26 | 30.71 | 31.29 | 0.00 | 0.29 | 2,790 | 72.86 |
| 21.250 | 0.26 | 30.65 | 31.23 | 0.00 | 0.29 | 2,785 | 72.86 |
| 21.300 | 0.26 | 30.59 | 31.17 | 0.00 | 0.29 | 2,779 | 72.86 |
| 21.350 | 0.26 | 30.54 | 31.11 | 0.00 | 0.29 | 2,774 | 72.86 |
| 21.400 | 0.26 | 30.48 | 31.06 | 0.00 | 0.29 | 2,769 | 72.86 |
| 21.450 | 0.26 | 30.43 | 31.00 | 0.00 | 0.29 | 2,764 | 72.85 |
| 21.500 | 0.26 | 30.38 | 30.95 | 0.00 | 0.28 | 2,760 | 72.85 |
| 21.550 | 0.26 | 30.33 | 30.90 | 0.00 | 0.28 | 2,755 | 72.85 |
| 21.600 | 0.26 | 30.28 | 30.85 | 0.00 | 0.28 | 2,751 | 72.85 |
| 21.650 | 0.26 | 30.23 | 30.80 | 0.00 | 0.28 | 2,746 | 72.85 |
| 21.700 | 0.26 | 30.18 | 30.75 | 0.00 | 0.28 | 2,742 | 72.85 |
| 21.750 | 0.26 | 30.14 | 30.70 | 0.00 | 0.28 | 2,738 | 72.85 |
| 21.800 | 0.26 | 30.09 | 30.65 | 0.00 | 0.28 | 2,734 | 72.84 |
| 21.850 | 0.26 | 30.05 | 30.61 | 0.00 | 0.28 | 2,730 | 72.84 |
| 21.900 | 0.26 | 30.01 | 30.57 | 0.00 | 0.28 | 2,726 | 72.84 |
| 21.950 | 0.26 | 29.97 | 30.52 | 0.00 | 0.28 | 2,722 | 72.84 |
| 22.000 | 0.26 | 29.93 | 30.48 | 0.00 | 0.28 | 2,718 | 72.84 |
| 22.050 | 0.26 | 29.89 | 30.44 | 0.00 | 0.28 | 2,715 | 72.84 |
| 22.100 | 0.26 | 29.85 | 30.40 | 0.00 | 0.28 | 2,711 | 72.84 |
| 22.150 | 0.26 | 29.81 | 30.36 | 0.00 | 0.28 | 2,708 | 72.83 |
| 22.200 | 0.26 | 29.77 | 30.32 | 0.00 | 0.28 | 2,704 | 72.83 |
| 22.250 | 0.26 | 29.74 | 30.29 | 0.00 | 0.27 | 2,701 | 72.83 |
| 22.300 | 0.26 | 29.70 | 30.25 | 0.00 | 0.27 | 2,698 | 72.83 |
| 22.350 | 0.26 | 29.67 | 30.22 | 0.00 | 0.27 | 2,695 | 72.83 |
| 22.400 | 0.26 | 29.64 | 30.18 | 0.00 | 0.27 | 2,692 | 72.83 |
| 22.450 | 0.26 | 29.60 | 30.15 | 0.00 | 0.27 | 2,689 | 72.83 |
| 22.500 | 0.26 | 29.57 | 30.11 | 0.00 | 0.27 | 2,686 | 72.83 |
| 22.550 | 0.26 | 29.54 | 30.08 | 0.00 | 0.27 | 2,683 | 72.83 |
| 22.600 | 0.26 | 29.51 | 30.05 | 0.00 | 0.27 | 2,680 | 72.83 |
| 22.650 | 0.26 | 29.48 | 30.02 | 0.00 | 0.27 | 2,677 | 72.82 |
| 22.700 | 0.26 | 29.45 | 29.99 | 0.00 | 0.27 | 2,675 | 72.82 |
| 22.750 | 0.26 | 29.42 | 29.96 | 0.00 | 0.27 | 2,672 | 72.82 |
| 22.800 | 0.26 | 29.39 | 29.93 | 0.00 | 0.27 | 2,670 | 72.82 |
| 22.850 | 0.26 | 29.37 | 29.90 | 0.00 | 0.27 | 2,667 | 72.82 |
| 22.900 | 0.25 | 29.34 | 29.88 | 0.00 | 0.27 | 2,665 | 72.82 |
| 22.950 | 0.25 | 29.31 | 29.85 | 0.00 | 0.27 | 2,662 | 72.82 |
| 23.000 | 0.25 | 29.29 | 29.82 | 0.00 | 0.27 | 2,660 | 72.82 |
| 23.050 | 0.25 | 29.26 | 29.80 | 0.00 | 0.27 | 2,658 | 72.82 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.25 | 29.24 | 29.77 | 0.00 | 0.27 | 2,655 | 72.82 |
| 23.150 | 0.25 | 29.21 | 29.74 | 0.00 | 0.27 | 2,653 | 72.82 |
| 23.200 | 0.25 | 29.19 | 29.72 | 0.00 | 0.27 | 2,651 | 72.81 |
| 23.250 | 0.25 | 29.16 | 29.70 | 0.00 | 0.27 | 2,649 | 72.81 |
| 23.300 | 0.25 | 29.14 | 29.67 | 0.00 | 0.27 | 2,647 | 72.81 |
| 23.350 | 0.25 | 29.12 | 29.65 | 0.00 | 0.27 | 2,645 | 72.81 |
| 23.400 | 0.25 | 29.10 | 29.63 | 0.00 | 0.26 | 2,643 | 72.81 |
| 23.450 | 0.25 | 29.08 | 29.60 | 0.00 | 0.26 | 2,641 | 72.81 |
| 23.500 | 0.25 | 29.05 | 29.58 | 0.00 | 0.26 | 2,639 | 72.81 |
| 23.550 | 0.25 | 29.03 | 29.56 | 0.00 | 0.26 | 2,637 | 72.81 |
| 23.600 | 0.25 | 29.01 | 29.54 | 0.00 | 0.26 | 2,635 | 72.81 |
| 23.650 | 0.25 | 28.99 | 29.52 | 0.00 | 0.26 | 2,633 | 72.81 |
| 23.700 | 0.25 | 28.97 | 29.50 | 0.00 | 0.26 | 2,631 | 72.81 |
| 23.750 | 0.25 | 28.95 | 29.48 | 0.00 | 0.26 | 2,629 | 72.81 |
| 23.800 | 0.25 | 28.93 | 29.46 | 0.00 | 0.26 | 2,628 | 72.81 |
| 23.850 | 0.25 | 28.92 | 29.44 | 0.00 | 0.26 | 2,626 | 72.81 |
| 23.900 | 0.25 | 28.90 | 29.42 | 0.00 | 0.26 | 2,624 | 72.81 |
| 23.950 | 0.25 | 28.88 | 29.40 | 0.00 | 0.26 | 2,623 | 72.81 |
| 24.000 | 0.25 | 28.86 | 29.38 | 0.00 | 0.26 | 2,621 | 72.80 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: MC-3500 - 2 (IN)

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'MC-3500 - 2'

| Upstream Link | Upstream Node |
|-----------------------------|-------------------------|
| 24-GR OUT | 24" Depth Green Roof |
| <Catchment to Outflow Node> | PDA-2E |
| 6-GR OUT | 6" Depth Green Roof |
| SP-2 OUT | Stormwater Planters - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | 24-GR OUT | 3,817 | 11.250 | 0.09 |
| Flow (From) | PDA-2E | 305 | 12.150 | 0.08 |
| Flow (From) | 6-GR OUT | 1,610 | 11.800 | 0.13 |
| Flow (From) | SP-2 OUT | 3,912 | 11.600 | 0.14 |
| Flow (In) | MC-3500 - 2 | 9,644 | 12.150 | 0.44 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: MC-3500 - 2 (IN)

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'MC-3500 - 2'

| Upstream Link | Upstream Node |
|-----------------------------|-------------------------|
| 24-GR OUT | 24" Depth Green Roof |
| <Catchment to Outflow Node> | PDA-2E |
| 6-GR OUT | 6" Depth Green Roof |
| SP-2 OUT | Stormwater Planters - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | 24-GR OUT | 6,928 | 12.200 | 1.34 |
| Flow (From) | PDA-2E | 909 | 12.100 | 0.24 |
| Flow (From) | 6-GR OUT | 3,090 | 11.650 | 0.13 |
| Flow (From) | SP-2 OUT | 7,515 | 10.850 | 0.14 |
| Flow (In) | MC-3500 - 2 | 18,443 | 12.200 | 1.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: MC-3500 - 2 (IN)

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'MC-3500 - 2'

| Upstream Link | Upstream Node |
|-----------------------------|-------------------------|
| 24-GR OUT | 24" Depth Green Roof |
| <Catchment to Outflow Node> | PDA-2E |
| 6-GR OUT | 6" Depth Green Roof |
| SP-2 OUT | Stormwater Planters - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | 24-GR OUT | 8,686 | 12.100 | 2.71 |
| Flow (From) | PDA-2E | 1,306 | 12.100 | 0.35 |
| Flow (From) | 6-GR OUT | 3,955 | 12.250 | 0.53 |
| Flow (From) | SP-2 OUT | 9,621 | 12.450 | 0.70 |
| Flow (In) | MC-3500 - 2 | 23,569 | 12.100 | 3.33 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Return Event: 100 years

Label: MC-3500 - 2 (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

Summary for Hydrograph Addition at 'MC-3500 - 2'

| Upstream Link | Upstream Node |
|-----------------------------|-------------------------|
| 24-GR OUT | 24" Depth Green Roof |
| <Catchment to Outflow Node> | PDA-2E |
| 6-GR OUT | 6" Depth Green Roof |
| SP-2 OUT | Stormwater Planters - 2 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | 24-GR OUT | 12,417 | 12.100 | 3.20 |
| Flow (From) | PDA-2E | 2,167 | 12.100 | 0.57 |
| Flow (From) | 6-GR OUT | 5,731 | 12.150 | 1.27 |
| Flow (From) | SP-2 OUT | 13,345 | 12.200 | 2.47 |
| Flow (In) | MC-3500 - 2 | 33,660 | 12.150 | 7.23 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 1 years

Label: MC-3500 - 3

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 63.15 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 63.15 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 63.65 | 0.41 | 1,486 | 0 | 0.00 | 0.41 | 16.92 |
| 64.15 | 1.23 | 3,865 | 0 | 0.00 | 1.23 | 44.17 |
| 64.65 | 2.32 | 7,084 | 0 | 0.00 | 2.32 | 81.04 |
| 65.15 | 3.63 | 10,217 | 0 | 0.00 | 3.63 | 117.15 |
| 65.65 | 5.12 | 13,232 | 0 | 0.00 | 5.12 | 152.15 |
| 66.15 | 6.78 | 16,086 | 0 | 0.00 | 6.78 | 185.52 |
| 66.65 | 8.59 | 18,721 | 0 | 0.00 | 8.59 | 216.60 |
| 67.15 | 10.55 | 21,030 | 0 | 0.00 | 10.55 | 244.22 |
| 67.65 | 12.61 | 22,741 | 0 | 0.00 | 12.61 | 265.29 |
| 68.15 | 14.78 | 24,227 | 0 | 0.00 | 14.78 | 283.97 |
| 68.65 | 17.00 | 25,712 | 0 | 0.00 | 17.00 | 302.69 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 10 years

Label: MC-3500 - 3

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 63.15 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 63.15 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 63.65 | 0.41 | 1,486 | 0 | 0.00 | 0.41 | 16.92 |
| 64.15 | 1.23 | 3,865 | 0 | 0.00 | 1.23 | 44.17 |
| 64.65 | 2.32 | 7,084 | 0 | 0.00 | 2.32 | 81.04 |
| 65.15 | 3.63 | 10,217 | 0 | 0.00 | 3.63 | 117.15 |
| 65.65 | 5.12 | 13,232 | 0 | 0.00 | 5.12 | 152.15 |
| 66.15 | 6.78 | 16,086 | 0 | 0.00 | 6.78 | 185.52 |
| 66.65 | 8.59 | 18,721 | 0 | 0.00 | 8.59 | 216.60 |
| 67.15 | 10.55 | 21,030 | 0 | 0.00 | 10.55 | 244.22 |
| 67.65 | 12.61 | 22,741 | 0 | 0.00 | 12.61 | 265.29 |
| 68.15 | 14.78 | 24,227 | 0 | 0.00 | 14.78 | 283.97 |
| 68.65 | 17.00 | 25,712 | 0 | 0.00 | 17.00 | 302.69 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 25 years

Label: MC-3500 - 3

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 63.15 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 63.15 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 63.65 | 0.41 | 1,486 | 0 | 0.00 | 0.41 | 16.92 |
| 64.15 | 1.23 | 3,865 | 0 | 0.00 | 1.23 | 44.17 |
| 64.65 | 2.32 | 7,084 | 0 | 0.00 | 2.32 | 81.04 |
| 65.15 | 3.63 | 10,217 | 0 | 0.00 | 3.63 | 117.15 |
| 65.65 | 5.12 | 13,232 | 0 | 0.00 | 5.12 | 152.15 |
| 66.15 | 6.78 | 16,086 | 0 | 0.00 | 6.78 | 185.52 |
| 66.65 | 8.59 | 18,721 | 0 | 0.00 | 8.59 | 216.60 |
| 67.15 | 10.55 | 21,030 | 0 | 0.00 | 10.55 | 244.22 |
| 67.65 | 12.61 | 22,741 | 0 | 0.00 | 12.61 | 265.29 |
| 68.15 | 14.78 | 24,227 | 0 | 0.00 | 14.78 | 283.97 |
| 68.65 | 17.00 | 25,712 | 0 | 0.00 | 17.00 | 302.69 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 100 years

Label: MC-3500 - 3

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 63.15 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 63.15 | 0.00 | 0 | 0 | 0.00 | 0.00 | 0.00 |
| 63.65 | 0.41 | 1,486 | 0 | 0.00 | 0.41 | 16.92 |
| 64.15 | 1.23 | 3,865 | 0 | 0.00 | 1.23 | 44.17 |
| 64.65 | 2.32 | 7,084 | 0 | 0.00 | 2.32 | 81.04 |
| 65.15 | 3.63 | 10,217 | 0 | 0.00 | 3.63 | 117.15 |
| 65.65 | 5.12 | 13,232 | 0 | 0.00 | 5.12 | 152.15 |
| 66.15 | 6.78 | 16,086 | 0 | 0.00 | 6.78 | 185.52 |
| 66.65 | 8.59 | 18,721 | 0 | 0.00 | 8.59 | 216.60 |
| 67.15 | 10.55 | 21,030 | 0 | 0.00 | 10.55 | 244.22 |
| 67.65 | 12.61 | 22,741 | 0 | 0.00 | 12.61 | 265.29 |
| 68.15 | 14.78 | 24,227 | 0 | 0.00 | 14.78 | 283.97 |
| 68.65 | 17.00 | 25,712 | 0 | 0.00 | 17.00 | 302.69 |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 1 years

Label: MC-3500 - 3 (IN)

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 63.15 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 5.21 ft ³ /s | Time to Peak (Flow, In) | 12.150 hours |
| Flow (Peak Outlet) | 2.00 ft ³ /s | Time to Peak (Flow, Outlet) | 12.450 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 64.50 ft | | |
| Volume (Peak) | 6,135 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 19,897 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 19,594 ft ³ | | |
| Volume (Retained) | 288 ft ³ | | |
| Volume (Unrouted) | -15 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 10 years

Label: MC-3500 - 3 (IN)

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | | | |
|------------------------------------|--------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 63.15 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 12.08 ft ³ /s | Time to Peak (Flow, In) | 12.150 hours |
| Flow (Peak Outlet) | 5.48 ft ³ /s | Time to Peak (Flow, Outlet) | 12.400 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 65.76 ft | | |
| Volume (Peak) | 13,858 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 47,606 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 46,990 ft ³ | | |
| Volume (Retained) | 587 ft ³ | | |
| Volume (Unrouted) | -30 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 25 years

Label: MC-3500 - 3 (IN)

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | | | |
|------------------------------------|--------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 63.15 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 16.18 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 8.01 ft ³ /s | Time to Peak (Flow, Outlet) | 12.350 hours |
| Elevation (Water Surface, Peak) | 66.49 ft | | |
| Volume (Peak) | 17,897 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 64,556 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 63,759 ft ³ | | |
| Volume (Retained) | 758 ft ³ | | |
| Volume (Unrouted) | -39 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 100 years

Label: MC-3500 - 3 (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | | | |
|------------------------------------|--------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 63.15 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.00 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.00 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 24.51 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 15.14 ft ³ /s | Time to Peak (Flow, Outlet) | 12.300 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 68.23 ft | | |
| Volume (Peak) | 24,465 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 100,006 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 98,845 ft ³ | | |
| Volume (Retained) | 1,105 ft ³ | | |
| Volume (Unrouted) | -56 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 6.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 7.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 8.000 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 0 | 63.15 |
| 8.050 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 1 | 63.15 |
| 8.100 | 0.00 | 0.02 | 0.02 | 0.00 | 0.00 | 2 | 63.15 |
| 8.150 | 0.01 | 0.03 | 0.03 | 0.00 | 0.00 | 2 | 63.15 |
| 8.200 | 0.01 | 0.04 | 0.04 | 0.00 | 0.00 | 3 | 63.15 |
| 8.250 | 0.01 | 0.05 | 0.05 | 0.00 | 0.00 | 5 | 63.15 |
| 8.300 | 0.01 | 0.07 | 0.07 | 0.00 | 0.00 | 6 | 63.15 |
| 8.350 | 0.01 | 0.08 | 0.09 | 0.00 | 0.00 | 8 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.01 | 0.10 | 0.11 | 0.00 | 0.00 | 10 | 63.15 |
| 8.450 | 0.02 | 0.13 | 0.13 | 0.00 | 0.00 | 12 | 63.15 |
| 8.500 | 0.02 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 63.15 |
| 8.550 | 0.02 | 0.18 | 0.19 | 0.00 | 0.00 | 16 | 63.16 |
| 8.600 | 0.02 | 0.21 | 0.22 | 0.00 | 0.01 | 19 | 63.16 |
| 8.650 | 0.02 | 0.24 | 0.25 | 0.00 | 0.01 | 22 | 63.16 |
| 8.700 | 0.03 | 0.27 | 0.29 | 0.00 | 0.01 | 25 | 63.16 |
| 8.750 | 0.03 | 0.31 | 0.33 | 0.00 | 0.01 | 29 | 63.16 |
| 8.800 | 0.03 | 0.35 | 0.37 | 0.00 | 0.01 | 32 | 63.16 |
| 8.850 | 0.03 | 0.39 | 0.41 | 0.00 | 0.01 | 36 | 63.16 |
| 8.900 | 0.03 | 0.44 | 0.46 | 0.00 | 0.01 | 40 | 63.16 |
| 8.950 | 0.04 | 0.48 | 0.51 | 0.00 | 0.01 | 45 | 63.17 |
| 9.000 | 0.04 | 0.53 | 0.56 | 0.00 | 0.01 | 49 | 63.17 |
| 9.050 | 0.04 | 0.58 | 0.61 | 0.00 | 0.01 | 54 | 63.17 |
| 9.100 | 0.05 | 0.64 | 0.67 | 0.00 | 0.02 | 59 | 63.17 |
| 9.150 | 0.05 | 0.70 | 0.73 | 0.00 | 0.02 | 64 | 63.17 |
| 9.200 | 0.05 | 0.76 | 0.80 | 0.00 | 0.02 | 70 | 63.17 |
| 9.250 | 0.05 | 0.82 | 0.86 | 0.00 | 0.02 | 76 | 63.18 |
| 9.300 | 0.06 | 0.89 | 0.93 | 0.00 | 0.02 | 82 | 63.18 |
| 9.350 | 0.06 | 0.95 | 1.00 | 0.00 | 0.02 | 88 | 63.18 |
| 9.400 | 0.06 | 1.03 | 1.08 | 0.00 | 0.03 | 95 | 63.18 |
| 9.450 | 0.07 | 1.10 | 1.16 | 0.00 | 0.03 | 101 | 63.18 |
| 9.500 | 0.07 | 1.18 | 1.24 | 0.00 | 0.03 | 109 | 63.19 |
| 9.550 | 0.07 | 1.26 | 1.32 | 0.00 | 0.03 | 116 | 63.19 |
| 9.600 | 0.08 | 1.34 | 1.41 | 0.00 | 0.03 | 123 | 63.19 |
| 9.650 | 0.08 | 1.42 | 1.49 | 0.00 | 0.04 | 131 | 63.19 |
| 9.700 | 0.08 | 1.51 | 1.59 | 0.00 | 0.04 | 139 | 63.20 |
| 9.750 | 0.09 | 1.60 | 1.68 | 0.00 | 0.04 | 148 | 63.20 |
| 9.800 | 0.09 | 1.69 | 1.78 | 0.00 | 0.04 | 156 | 63.20 |
| 9.850 | 0.10 | 1.79 | 1.88 | 0.00 | 0.05 | 165 | 63.21 |
| 9.900 | 0.10 | 1.89 | 1.99 | 0.00 | 0.05 | 174 | 63.21 |
| 9.950 | 0.10 | 1.99 | 2.09 | 0.00 | 0.05 | 184 | 63.21 |
| 10.000 | 0.11 | 2.10 | 2.20 | 0.00 | 0.05 | 193 | 63.22 |
| 10.050 | 0.11 | 2.20 | 2.31 | 0.00 | 0.06 | 203 | 63.22 |
| 10.100 | 0.12 | 2.31 | 2.43 | 0.00 | 0.06 | 214 | 63.22 |
| 10.150 | 0.12 | 2.43 | 2.55 | 0.00 | 0.06 | 224 | 63.23 |
| 10.200 | 0.13 | 2.55 | 2.68 | 0.00 | 0.06 | 235 | 63.23 |
| 10.250 | 0.13 | 2.67 | 2.81 | 0.00 | 0.07 | 247 | 63.23 |
| 10.300 | 0.14 | 2.80 | 2.95 | 0.00 | 0.07 | 259 | 63.24 |
| 10.350 | 0.15 | 2.94 | 3.09 | 0.00 | 0.07 | 271 | 63.24 |
| 10.400 | 0.15 | 3.08 | 3.24 | 0.00 | 0.08 | 285 | 63.25 |
| 10.450 | 0.16 | 3.23 | 3.40 | 0.00 | 0.08 | 298 | 63.25 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.17 | 3.39 | 3.56 | 0.00 | 0.09 | 312 | 63.26 |
| 10.550 | 0.17 | 3.55 | 3.73 | 0.00 | 0.09 | 327 | 63.26 |
| 10.600 | 0.18 | 3.71 | 3.90 | 0.00 | 0.09 | 343 | 63.27 |
| 10.650 | 0.19 | 3.89 | 4.08 | 0.00 | 0.10 | 359 | 63.27 |
| 10.700 | 0.20 | 4.07 | 4.27 | 0.00 | 0.10 | 375 | 63.28 |
| 10.750 | 0.21 | 4.25 | 4.47 | 0.00 | 0.11 | 392 | 63.28 |
| 10.800 | 0.21 | 4.44 | 4.67 | 0.00 | 0.11 | 410 | 63.29 |
| 10.850 | 0.22 | 4.64 | 4.88 | 0.00 | 0.12 | 429 | 63.29 |
| 10.900 | 0.23 | 4.85 | 5.09 | 0.00 | 0.12 | 447 | 63.30 |
| 10.950 | 0.24 | 5.06 | 5.32 | 0.00 | 0.13 | 467 | 63.31 |
| 11.000 | 0.25 | 5.28 | 5.55 | 0.00 | 0.13 | 487 | 63.31 |
| 11.050 | 0.26 | 5.50 | 5.78 | 0.00 | 0.14 | 508 | 63.32 |
| 11.100 | 0.27 | 5.74 | 6.03 | 0.00 | 0.15 | 530 | 63.33 |
| 11.150 | 0.29 | 5.99 | 6.30 | 0.00 | 0.15 | 553 | 63.34 |
| 11.200 | 0.31 | 6.27 | 6.59 | 0.00 | 0.16 | 579 | 63.34 |
| 11.250 | 0.33 | 6.57 | 6.91 | 0.00 | 0.17 | 607 | 63.35 |
| 11.300 | 0.35 | 6.91 | 7.26 | 0.00 | 0.18 | 637 | 63.36 |
| 11.350 | 0.38 | 7.27 | 7.64 | 0.00 | 0.19 | 671 | 63.38 |
| 11.400 | 0.41 | 7.66 | 8.05 | 0.00 | 0.20 | 707 | 63.39 |
| 11.450 | 0.43 | 8.09 | 8.50 | 0.00 | 0.21 | 747 | 63.40 |
| 11.500 | 0.46 | 8.55 | 8.99 | 0.00 | 0.22 | 789 | 63.42 |
| 11.550 | 0.51 | 9.06 | 9.53 | 0.00 | 0.23 | 836 | 63.43 |
| 11.600 | 0.60 | 9.68 | 10.17 | 0.00 | 0.25 | 893 | 63.45 |
| 11.650 | 0.73 | 10.47 | 11.01 | 0.00 | 0.27 | 967 | 63.48 |
| 11.700 | 0.92 | 11.53 | 12.12 | 0.00 | 0.29 | 1,064 | 63.51 |
| 11.750 | 1.14 | 12.93 | 13.59 | 0.00 | 0.33 | 1,194 | 63.55 |
| 11.800 | 1.40 | 14.72 | 15.47 | 0.00 | 0.38 | 1,358 | 63.61 |
| 11.850 | 1.67 | 16.91 | 17.79 | 0.00 | 0.44 | 1,533 | 63.67 |
| 11.900 | 1.98 | 19.53 | 20.57 | 0.00 | 0.52 | 1,685 | 63.72 |
| 11.950 | 2.50 | 22.76 | 24.01 | 0.00 | 0.62 | 1,873 | 63.78 |
| 12.000 | 3.51 | 27.24 | 28.77 | 0.00 | 0.77 | 2,132 | 63.87 |
| 12.050 | 4.49 | 33.31 | 35.24 | 0.00 | 0.96 | 2,792 | 63.99 |
| 12.100 | 5.12 | 40.53 | 42.92 | 0.00 | 1.19 | 3,714 | 64.13 |
| 12.150 | 5.21 | 48.01 | 50.86 | 0.00 | 1.43 | 4,452 | 64.24 |
| 12.200 | 4.54 | 54.49 | 57.76 | 0.00 | 1.63 | 5,058 | 64.33 |
| 12.250 | 3.75 | 59.21 | 62.78 | 0.00 | 1.78 | 5,498 | 64.40 |
| 12.300 | 3.18 | 62.37 | 66.14 | 0.00 | 1.88 | 5,790 | 64.45 |
| 12.350 | 2.77 | 64.43 | 68.32 | 0.00 | 1.95 | 5,980 | 64.48 |
| 12.400 | 2.40 | 65.63 | 69.60 | 0.00 | 1.99 | 6,091 | 64.49 |
| 12.450 | 2.07 | 66.11 | 70.11 | 0.00 | 2.00 | 6,135 | 64.50 |
| 12.500 | 1.73 | 65.92 | 69.91 | 0.00 | 1.99 | 6,118 | 64.50 |
| 12.550 | 1.44 | 65.16 | 69.10 | 0.00 | 1.97 | 6,047 | 64.49 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 1.20 | 63.93 | 67.80 | 0.00 | 1.93 | 5,934 | 64.47 |
| 12.650 | 1.03 | 62.39 | 66.16 | 0.00 | 1.88 | 5,791 | 64.45 |
| 12.700 | 0.92 | 60.68 | 64.34 | 0.00 | 1.83 | 5,633 | 64.42 |
| 12.750 | 0.86 | 58.91 | 62.46 | 0.00 | 1.77 | 5,470 | 64.40 |
| 12.800 | 0.81 | 57.14 | 60.58 | 0.00 | 1.72 | 5,305 | 64.37 |
| 12.850 | 0.77 | 55.40 | 58.73 | 0.00 | 1.66 | 5,142 | 64.35 |
| 12.900 | 0.73 | 53.69 | 56.90 | 0.00 | 1.61 | 4,982 | 64.32 |
| 12.950 | 0.70 | 52.00 | 55.12 | 0.00 | 1.56 | 4,826 | 64.30 |
| 13.000 | 0.66 | 50.36 | 53.37 | 0.00 | 1.50 | 4,672 | 64.27 |
| 13.050 | 0.63 | 48.74 | 51.65 | 0.00 | 1.45 | 4,521 | 64.25 |
| 13.100 | 0.60 | 47.17 | 49.98 | 0.00 | 1.40 | 4,375 | 64.23 |
| 13.150 | 0.58 | 45.65 | 48.36 | 0.00 | 1.36 | 4,232 | 64.21 |
| 13.200 | 0.57 | 44.18 | 46.80 | 0.00 | 1.31 | 4,095 | 64.19 |
| 13.250 | 0.56 | 42.77 | 45.30 | 0.00 | 1.27 | 3,964 | 64.17 |
| 13.300 | 0.55 | 41.43 | 43.88 | 0.00 | 1.22 | 3,829 | 64.14 |
| 13.350 | 0.54 | 40.15 | 42.52 | 0.00 | 1.18 | 3,666 | 64.12 |
| 13.400 | 0.53 | 38.93 | 41.22 | 0.00 | 1.14 | 3,510 | 64.10 |
| 13.450 | 0.52 | 37.77 | 39.98 | 0.00 | 1.11 | 3,362 | 64.07 |
| 13.500 | 0.51 | 36.66 | 38.80 | 0.00 | 1.07 | 3,220 | 64.05 |
| 13.550 | 0.50 | 35.60 | 37.67 | 0.00 | 1.04 | 3,085 | 64.03 |
| 13.600 | 0.49 | 34.59 | 36.60 | 0.00 | 1.00 | 2,955 | 64.01 |
| 13.650 | 0.48 | 33.62 | 35.57 | 0.00 | 0.97 | 2,832 | 63.99 |
| 13.700 | 0.47 | 32.70 | 34.58 | 0.00 | 0.94 | 2,713 | 63.97 |
| 13.750 | 0.47 | 31.81 | 33.64 | 0.00 | 0.91 | 2,600 | 63.96 |
| 13.800 | 0.46 | 30.96 | 32.73 | 0.00 | 0.89 | 2,491 | 63.94 |
| 13.850 | 0.45 | 30.14 | 31.86 | 0.00 | 0.86 | 2,387 | 63.92 |
| 13.900 | 0.44 | 29.35 | 31.03 | 0.00 | 0.84 | 2,286 | 63.91 |
| 13.950 | 0.43 | 28.60 | 30.22 | 0.00 | 0.81 | 2,211 | 63.89 |
| 14.000 | 0.42 | 27.87 | 29.45 | 0.00 | 0.79 | 2,169 | 63.88 |
| 14.050 | 0.41 | 27.17 | 28.70 | 0.00 | 0.77 | 2,128 | 63.87 |
| 14.100 | 0.40 | 26.50 | 27.99 | 0.00 | 0.74 | 2,089 | 63.85 |
| 14.150 | 0.40 | 25.85 | 27.30 | 0.00 | 0.72 | 2,052 | 63.84 |
| 14.200 | 0.39 | 25.23 | 26.64 | 0.00 | 0.70 | 2,016 | 63.83 |
| 14.250 | 0.39 | 24.64 | 26.01 | 0.00 | 0.68 | 1,982 | 63.82 |
| 14.300 | 0.38 | 24.08 | 25.41 | 0.00 | 0.67 | 1,949 | 63.81 |
| 14.350 | 0.38 | 23.54 | 24.84 | 0.00 | 0.65 | 1,918 | 63.80 |
| 14.400 | 0.37 | 23.02 | 24.29 | 0.00 | 0.63 | 1,888 | 63.79 |
| 14.450 | 0.37 | 22.53 | 23.76 | 0.00 | 0.62 | 1,859 | 63.78 |
| 14.500 | 0.36 | 22.06 | 23.26 | 0.00 | 0.60 | 1,832 | 63.77 |
| 14.550 | 0.36 | 21.61 | 22.78 | 0.00 | 0.59 | 1,806 | 63.76 |
| 14.600 | 0.36 | 21.18 | 22.32 | 0.00 | 0.57 | 1,781 | 63.75 |
| 14.650 | 0.35 | 20.76 | 21.88 | 0.00 | 0.56 | 1,757 | 63.74 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.35 | 20.37 | 21.46 | 0.00 | 0.55 | 1,734 | 63.73 |
| 14.750 | 0.34 | 19.98 | 21.05 | 0.00 | 0.53 | 1,711 | 63.73 |
| 14.800 | 0.34 | 19.62 | 20.66 | 0.00 | 0.52 | 1,690 | 63.72 |
| 14.850 | 0.33 | 19.26 | 20.29 | 0.00 | 0.51 | 1,670 | 63.71 |
| 14.900 | 0.33 | 18.92 | 19.93 | 0.00 | 0.50 | 1,650 | 63.71 |
| 14.950 | 0.32 | 18.60 | 19.58 | 0.00 | 0.49 | 1,631 | 63.70 |
| 15.000 | 0.32 | 18.28 | 19.24 | 0.00 | 0.48 | 1,612 | 63.69 |
| 15.050 | 0.32 | 17.97 | 18.91 | 0.00 | 0.47 | 1,595 | 63.69 |
| 15.100 | 0.31 | 17.68 | 18.60 | 0.00 | 0.46 | 1,577 | 63.68 |
| 15.150 | 0.31 | 17.39 | 18.29 | 0.00 | 0.45 | 1,561 | 63.68 |
| 15.200 | 0.30 | 17.11 | 18.00 | 0.00 | 0.44 | 1,545 | 63.67 |
| 15.250 | 0.30 | 16.84 | 17.71 | 0.00 | 0.43 | 1,529 | 63.66 |
| 15.300 | 0.29 | 16.58 | 17.43 | 0.00 | 0.43 | 1,514 | 63.66 |
| 15.350 | 0.29 | 16.32 | 17.16 | 0.00 | 0.42 | 1,499 | 63.65 |
| 15.400 | 0.28 | 16.07 | 16.89 | 0.00 | 0.41 | 1,484 | 63.65 |
| 15.450 | 0.28 | 15.83 | 16.64 | 0.00 | 0.40 | 1,461 | 63.64 |
| 15.500 | 0.27 | 15.59 | 16.38 | 0.00 | 0.40 | 1,439 | 63.63 |
| 15.550 | 0.27 | 15.35 | 16.13 | 0.00 | 0.39 | 1,416 | 63.63 |
| 15.600 | 0.26 | 15.11 | 15.88 | 0.00 | 0.39 | 1,395 | 63.62 |
| 15.650 | 0.26 | 14.88 | 15.64 | 0.00 | 0.38 | 1,373 | 63.61 |
| 15.700 | 0.26 | 14.65 | 15.39 | 0.00 | 0.37 | 1,352 | 63.60 |
| 15.750 | 0.25 | 14.42 | 15.15 | 0.00 | 0.37 | 1,331 | 63.60 |
| 15.800 | 0.25 | 14.19 | 14.91 | 0.00 | 0.36 | 1,310 | 63.59 |
| 15.850 | 0.24 | 13.97 | 14.68 | 0.00 | 0.36 | 1,289 | 63.58 |
| 15.900 | 0.24 | 13.74 | 14.44 | 0.00 | 0.35 | 1,268 | 63.58 |
| 15.950 | 0.23 | 13.52 | 14.21 | 0.00 | 0.34 | 1,248 | 63.57 |
| 16.000 | 0.23 | 13.30 | 13.98 | 0.00 | 0.34 | 1,228 | 63.56 |
| 16.050 | 0.22 | 13.09 | 13.76 | 0.00 | 0.33 | 1,208 | 63.56 |
| 16.100 | 0.22 | 12.87 | 13.53 | 0.00 | 0.33 | 1,188 | 63.55 |
| 16.150 | 0.22 | 12.66 | 13.31 | 0.00 | 0.32 | 1,169 | 63.54 |
| 16.200 | 0.21 | 12.46 | 13.09 | 0.00 | 0.32 | 1,150 | 63.54 |
| 16.250 | 0.21 | 12.26 | 12.88 | 0.00 | 0.31 | 1,131 | 63.53 |
| 16.300 | 0.21 | 12.06 | 12.68 | 0.00 | 0.31 | 1,113 | 63.52 |
| 16.350 | 0.21 | 11.87 | 12.48 | 0.00 | 0.30 | 1,096 | 63.52 |
| 16.400 | 0.20 | 11.69 | 12.29 | 0.00 | 0.30 | 1,079 | 63.51 |
| 16.450 | 0.20 | 11.51 | 12.10 | 0.00 | 0.29 | 1,062 | 63.51 |
| 16.500 | 0.20 | 11.34 | 11.91 | 0.00 | 0.29 | 1,046 | 63.50 |
| 16.550 | 0.20 | 11.17 | 11.74 | 0.00 | 0.28 | 1,031 | 63.50 |
| 16.600 | 0.20 | 11.00 | 11.56 | 0.00 | 0.28 | 1,015 | 63.49 |
| 16.650 | 0.19 | 10.84 | 11.39 | 0.00 | 0.28 | 1,001 | 63.49 |
| 16.700 | 0.19 | 10.68 | 11.23 | 0.00 | 0.27 | 986 | 63.48 |
| 16.750 | 0.19 | 10.53 | 11.07 | 0.00 | 0.27 | 972 | 63.48 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.19 | 10.38 | 10.91 | 0.00 | 0.26 | 958 | 63.47 |
| 16.850 | 0.19 | 10.24 | 10.76 | 0.00 | 0.26 | 945 | 63.47 |
| 16.900 | 0.18 | 10.09 | 10.61 | 0.00 | 0.26 | 931 | 63.46 |
| 16.950 | 0.18 | 9.95 | 10.46 | 0.00 | 0.25 | 919 | 63.46 |
| 17.000 | 0.18 | 9.82 | 10.32 | 0.00 | 0.25 | 906 | 63.45 |
| 17.050 | 0.18 | 9.68 | 10.17 | 0.00 | 0.25 | 893 | 63.45 |
| 17.100 | 0.18 | 9.55 | 10.04 | 0.00 | 0.24 | 881 | 63.45 |
| 17.150 | 0.17 | 9.42 | 9.90 | 0.00 | 0.24 | 869 | 63.44 |
| 17.200 | 0.17 | 9.29 | 9.77 | 0.00 | 0.24 | 858 | 63.44 |
| 17.250 | 0.17 | 9.17 | 9.64 | 0.00 | 0.23 | 846 | 63.43 |
| 17.300 | 0.17 | 9.05 | 9.51 | 0.00 | 0.23 | 835 | 63.43 |
| 17.350 | 0.17 | 8.93 | 9.38 | 0.00 | 0.23 | 824 | 63.43 |
| 17.400 | 0.16 | 8.81 | 9.26 | 0.00 | 0.22 | 813 | 63.42 |
| 17.450 | 0.16 | 8.69 | 9.13 | 0.00 | 0.22 | 802 | 63.42 |
| 17.500 | 0.16 | 8.58 | 9.01 | 0.00 | 0.22 | 792 | 63.42 |
| 17.550 | 0.16 | 8.46 | 8.90 | 0.00 | 0.22 | 781 | 63.41 |
| 17.600 | 0.16 | 8.35 | 8.78 | 0.00 | 0.21 | 771 | 63.41 |
| 17.650 | 0.15 | 8.24 | 8.66 | 0.00 | 0.21 | 761 | 63.41 |
| 17.700 | 0.15 | 8.13 | 8.55 | 0.00 | 0.21 | 751 | 63.40 |
| 17.750 | 0.15 | 8.03 | 8.44 | 0.00 | 0.20 | 741 | 63.40 |
| 17.800 | 0.15 | 7.92 | 8.32 | 0.00 | 0.20 | 731 | 63.40 |
| 17.850 | 0.15 | 7.82 | 8.21 | 0.00 | 0.20 | 721 | 63.39 |
| 17.900 | 0.14 | 7.71 | 8.11 | 0.00 | 0.20 | 712 | 63.39 |
| 17.950 | 0.14 | 7.61 | 8.00 | 0.00 | 0.19 | 702 | 63.39 |
| 18.000 | 0.14 | 7.51 | 7.89 | 0.00 | 0.19 | 693 | 63.38 |
| 18.050 | 0.14 | 7.41 | 7.79 | 0.00 | 0.19 | 684 | 63.38 |
| 18.100 | 0.14 | 7.31 | 7.68 | 0.00 | 0.19 | 675 | 63.38 |
| 18.150 | 0.13 | 7.21 | 7.58 | 0.00 | 0.18 | 666 | 63.37 |
| 18.200 | 0.13 | 7.12 | 7.48 | 0.00 | 0.18 | 657 | 63.37 |
| 18.250 | 0.13 | 7.03 | 7.38 | 0.00 | 0.18 | 648 | 63.37 |
| 18.300 | 0.13 | 6.94 | 7.29 | 0.00 | 0.18 | 640 | 63.37 |
| 18.350 | 0.13 | 6.85 | 7.20 | 0.00 | 0.17 | 632 | 63.36 |
| 18.400 | 0.13 | 6.77 | 7.12 | 0.00 | 0.17 | 625 | 63.36 |
| 18.450 | 0.13 | 6.69 | 7.03 | 0.00 | 0.17 | 618 | 63.36 |
| 18.500 | 0.13 | 6.61 | 6.95 | 0.00 | 0.17 | 611 | 63.36 |
| 18.550 | 0.13 | 6.54 | 6.87 | 0.00 | 0.17 | 604 | 63.35 |
| 18.600 | 0.13 | 6.47 | 6.80 | 0.00 | 0.16 | 597 | 63.35 |
| 18.650 | 0.13 | 6.40 | 6.73 | 0.00 | 0.16 | 591 | 63.35 |
| 18.700 | 0.13 | 6.33 | 6.66 | 0.00 | 0.16 | 584 | 63.35 |
| 18.750 | 0.13 | 6.27 | 6.59 | 0.00 | 0.16 | 578 | 63.34 |
| 18.800 | 0.13 | 6.20 | 6.52 | 0.00 | 0.16 | 573 | 63.34 |
| 18.850 | 0.13 | 6.14 | 6.46 | 0.00 | 0.16 | 567 | 63.34 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.13 | 6.08 | 6.39 | 0.00 | 0.16 | 562 | 63.34 |
| 18.950 | 0.12 | 6.03 | 6.33 | 0.00 | 0.15 | 556 | 63.34 |
| 19.000 | 0.12 | 5.97 | 6.28 | 0.00 | 0.15 | 551 | 63.34 |
| 19.050 | 0.12 | 5.92 | 6.22 | 0.00 | 0.15 | 546 | 63.33 |
| 19.100 | 0.12 | 5.86 | 6.16 | 0.00 | 0.15 | 541 | 63.33 |
| 19.150 | 0.12 | 5.81 | 6.11 | 0.00 | 0.15 | 536 | 63.33 |
| 19.200 | 0.12 | 5.76 | 6.06 | 0.00 | 0.15 | 532 | 63.33 |
| 19.250 | 0.12 | 5.71 | 6.00 | 0.00 | 0.15 | 527 | 63.33 |
| 19.300 | 0.12 | 5.67 | 5.95 | 0.00 | 0.14 | 523 | 63.33 |
| 19.350 | 0.12 | 5.62 | 5.91 | 0.00 | 0.14 | 519 | 63.32 |
| 19.400 | 0.12 | 5.57 | 5.86 | 0.00 | 0.14 | 514 | 63.32 |
| 19.450 | 0.12 | 5.53 | 5.81 | 0.00 | 0.14 | 510 | 63.32 |
| 19.500 | 0.12 | 5.49 | 5.77 | 0.00 | 0.14 | 506 | 63.32 |
| 19.550 | 0.12 | 5.44 | 5.72 | 0.00 | 0.14 | 502 | 63.32 |
| 19.600 | 0.12 | 5.40 | 5.68 | 0.00 | 0.14 | 499 | 63.32 |
| 19.650 | 0.12 | 5.36 | 5.63 | 0.00 | 0.14 | 495 | 63.32 |
| 19.700 | 0.12 | 5.32 | 5.59 | 0.00 | 0.14 | 491 | 63.32 |
| 19.750 | 0.11 | 5.28 | 5.55 | 0.00 | 0.13 | 487 | 63.31 |
| 19.800 | 0.11 | 5.24 | 5.51 | 0.00 | 0.13 | 484 | 63.31 |
| 19.850 | 0.11 | 5.21 | 5.47 | 0.00 | 0.13 | 480 | 63.31 |
| 19.900 | 0.11 | 5.17 | 5.43 | 0.00 | 0.13 | 477 | 63.31 |
| 19.950 | 0.11 | 5.13 | 5.39 | 0.00 | 0.13 | 474 | 63.31 |
| 20.000 | 0.11 | 5.10 | 5.36 | 0.00 | 0.13 | 470 | 63.31 |
| 20.050 | 0.11 | 5.06 | 5.32 | 0.00 | 0.13 | 467 | 63.31 |
| 20.100 | 0.11 | 5.03 | 5.28 | 0.00 | 0.13 | 464 | 63.31 |
| 20.150 | 0.11 | 4.99 | 5.25 | 0.00 | 0.13 | 461 | 63.31 |
| 20.200 | 0.11 | 4.96 | 5.21 | 0.00 | 0.13 | 458 | 63.30 |
| 20.250 | 0.11 | 4.93 | 5.18 | 0.00 | 0.13 | 455 | 63.30 |
| 20.300 | 0.11 | 4.90 | 5.14 | 0.00 | 0.12 | 452 | 63.30 |
| 20.350 | 0.11 | 4.86 | 5.11 | 0.00 | 0.12 | 449 | 63.30 |
| 20.400 | 0.11 | 4.83 | 5.08 | 0.00 | 0.12 | 446 | 63.30 |
| 20.450 | 0.11 | 4.80 | 5.05 | 0.00 | 0.12 | 443 | 63.30 |
| 20.500 | 0.11 | 4.77 | 5.02 | 0.00 | 0.12 | 441 | 63.30 |
| 20.550 | 0.11 | 4.74 | 4.99 | 0.00 | 0.12 | 438 | 63.30 |
| 20.600 | 0.11 | 4.72 | 4.96 | 0.00 | 0.12 | 435 | 63.30 |
| 20.650 | 0.11 | 4.69 | 4.93 | 0.00 | 0.12 | 433 | 63.30 |
| 20.700 | 0.10 | 4.66 | 4.90 | 0.00 | 0.12 | 430 | 63.29 |
| 20.750 | 0.10 | 4.63 | 4.87 | 0.00 | 0.12 | 428 | 63.29 |
| 20.800 | 0.10 | 4.61 | 4.84 | 0.00 | 0.12 | 425 | 63.29 |
| 20.850 | 0.10 | 4.58 | 4.81 | 0.00 | 0.12 | 423 | 63.29 |
| 20.900 | 0.10 | 4.55 | 4.79 | 0.00 | 0.12 | 420 | 63.29 |
| 20.950 | 0.10 | 4.53 | 4.76 | 0.00 | 0.12 | 418 | 63.29 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.10 | 4.50 | 4.73 | 0.00 | 0.11 | 416 | 63.29 |
| 21.050 | 0.10 | 4.48 | 4.71 | 0.00 | 0.11 | 413 | 63.29 |
| 21.100 | 0.10 | 4.46 | 4.68 | 0.00 | 0.11 | 411 | 63.29 |
| 21.150 | 0.10 | 4.43 | 4.66 | 0.00 | 0.11 | 409 | 63.29 |
| 21.200 | 0.10 | 4.41 | 4.63 | 0.00 | 0.11 | 407 | 63.29 |
| 21.250 | 0.10 | 4.38 | 4.61 | 0.00 | 0.11 | 405 | 63.29 |
| 21.300 | 0.10 | 4.36 | 4.58 | 0.00 | 0.11 | 403 | 63.29 |
| 21.350 | 0.10 | 4.34 | 4.56 | 0.00 | 0.11 | 400 | 63.28 |
| 21.400 | 0.10 | 4.32 | 4.54 | 0.00 | 0.11 | 398 | 63.28 |
| 21.450 | 0.10 | 4.29 | 4.51 | 0.00 | 0.11 | 396 | 63.28 |
| 21.500 | 0.10 | 4.27 | 4.49 | 0.00 | 0.11 | 394 | 63.28 |
| 21.550 | 0.10 | 4.25 | 4.46 | 0.00 | 0.11 | 392 | 63.28 |
| 21.600 | 0.10 | 4.23 | 4.44 | 0.00 | 0.11 | 390 | 63.28 |
| 21.650 | 0.10 | 4.20 | 4.42 | 0.00 | 0.11 | 388 | 63.28 |
| 21.700 | 0.10 | 4.18 | 4.40 | 0.00 | 0.11 | 386 | 63.28 |
| 21.750 | 0.10 | 4.16 | 4.37 | 0.00 | 0.11 | 384 | 63.28 |
| 21.800 | 0.09 | 4.14 | 4.35 | 0.00 | 0.11 | 382 | 63.28 |
| 21.850 | 0.09 | 4.12 | 4.33 | 0.00 | 0.10 | 380 | 63.28 |
| 21.900 | 0.09 | 4.10 | 4.31 | 0.00 | 0.10 | 378 | 63.28 |
| 21.950 | 0.09 | 4.08 | 4.29 | 0.00 | 0.10 | 376 | 63.28 |
| 22.000 | 0.09 | 4.06 | 4.26 | 0.00 | 0.10 | 374 | 63.28 |
| 22.050 | 0.09 | 4.04 | 4.24 | 0.00 | 0.10 | 373 | 63.28 |
| 22.100 | 0.09 | 4.02 | 4.22 | 0.00 | 0.10 | 371 | 63.27 |
| 22.150 | 0.09 | 4.00 | 4.20 | 0.00 | 0.10 | 369 | 63.27 |
| 22.200 | 0.09 | 3.97 | 4.18 | 0.00 | 0.10 | 367 | 63.27 |
| 22.250 | 0.09 | 3.95 | 4.16 | 0.00 | 0.10 | 365 | 63.27 |
| 22.300 | 0.09 | 3.93 | 4.14 | 0.00 | 0.10 | 363 | 63.27 |
| 22.350 | 0.09 | 3.91 | 4.11 | 0.00 | 0.10 | 361 | 63.27 |
| 22.400 | 0.09 | 3.89 | 4.09 | 0.00 | 0.10 | 359 | 63.27 |
| 22.450 | 0.09 | 3.87 | 4.07 | 0.00 | 0.10 | 358 | 63.27 |
| 22.500 | 0.09 | 3.85 | 4.05 | 0.00 | 0.10 | 356 | 63.27 |
| 22.550 | 0.09 | 3.83 | 4.03 | 0.00 | 0.10 | 354 | 63.27 |
| 22.600 | 0.09 | 3.81 | 4.01 | 0.00 | 0.10 | 352 | 63.27 |
| 22.650 | 0.09 | 3.80 | 3.99 | 0.00 | 0.10 | 350 | 63.27 |
| 22.700 | 0.09 | 3.78 | 3.97 | 0.00 | 0.10 | 349 | 63.27 |
| 22.750 | 0.09 | 3.76 | 3.95 | 0.00 | 0.10 | 347 | 63.27 |
| 22.800 | 0.09 | 3.74 | 3.93 | 0.00 | 0.10 | 345 | 63.27 |
| 22.850 | 0.08 | 3.72 | 3.91 | 0.00 | 0.09 | 343 | 63.27 |
| 22.900 | 0.08 | 3.70 | 3.89 | 0.00 | 0.09 | 341 | 63.26 |
| 22.950 | 0.08 | 3.68 | 3.87 | 0.00 | 0.09 | 340 | 63.26 |
| 23.000 | 0.08 | 3.66 | 3.85 | 0.00 | 0.09 | 338 | 63.26 |
| 23.050 | 0.08 | 3.64 | 3.83 | 0.00 | 0.09 | 336 | 63.26 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: MC-3500 - 3 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.08 | 3.62 | 3.81 | 0.00 | 0.09 | 334 | 63.26 |
| 23.150 | 0.08 | 3.60 | 3.79 | 0.00 | 0.09 | 332 | 63.26 |
| 23.200 | 0.08 | 3.58 | 3.77 | 0.00 | 0.09 | 331 | 63.26 |
| 23.250 | 0.08 | 3.56 | 3.74 | 0.00 | 0.09 | 329 | 63.26 |
| 23.300 | 0.08 | 3.54 | 3.72 | 0.00 | 0.09 | 327 | 63.26 |
| 23.350 | 0.08 | 3.53 | 3.70 | 0.00 | 0.09 | 325 | 63.26 |
| 23.400 | 0.08 | 3.51 | 3.68 | 0.00 | 0.09 | 324 | 63.26 |
| 23.450 | 0.08 | 3.49 | 3.67 | 0.00 | 0.09 | 322 | 63.26 |
| 23.500 | 0.08 | 3.47 | 3.65 | 0.00 | 0.09 | 320 | 63.26 |
| 23.550 | 0.08 | 3.45 | 3.63 | 0.00 | 0.09 | 318 | 63.26 |
| 23.600 | 0.08 | 3.43 | 3.61 | 0.00 | 0.09 | 317 | 63.26 |
| 23.650 | 0.08 | 3.41 | 3.59 | 0.00 | 0.09 | 315 | 63.26 |
| 23.700 | 0.08 | 3.39 | 3.57 | 0.00 | 0.09 | 313 | 63.26 |
| 23.750 | 0.08 | 3.37 | 3.55 | 0.00 | 0.09 | 311 | 63.25 |
| 23.800 | 0.08 | 3.36 | 3.53 | 0.00 | 0.09 | 310 | 63.25 |
| 23.850 | 0.08 | 3.34 | 3.51 | 0.00 | 0.09 | 308 | 63.25 |
| 23.900 | 0.07 | 3.32 | 3.49 | 0.00 | 0.08 | 306 | 63.25 |
| 23.950 | 0.07 | 3.30 | 3.47 | 0.00 | 0.08 | 304 | 63.25 |
| 24.000 | 0.07 | 3.28 | 3.45 | 0.00 | 0.08 | 303 | 63.25 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 5.350 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 1 | 63.15 |
| 5.400 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 1 | 63.15 |
| 5.450 | 0.01 | 0.02 | 0.02 | 0.00 | 0.00 | 2 | 63.15 |
| 5.500 | 0.01 | 0.03 | 0.03 | 0.00 | 0.00 | 3 | 63.15 |
| 5.550 | 0.01 | 0.04 | 0.04 | 0.00 | 0.00 | 4 | 63.15 |
| 5.600 | 0.01 | 0.06 | 0.06 | 0.00 | 0.00 | 5 | 63.15 |
| 5.650 | 0.01 | 0.07 | 0.08 | 0.00 | 0.00 | 7 | 63.15 |
| 5.700 | 0.01 | 0.09 | 0.10 | 0.00 | 0.00 | 8 | 63.15 |
| 5.750 | 0.01 | 0.11 | 0.12 | 0.00 | 0.00 | 10 | 63.15 |
| 5.800 | 0.02 | 0.13 | 0.14 | 0.00 | 0.00 | 12 | 63.15 |
| 5.850 | 0.02 | 0.16 | 0.16 | 0.00 | 0.00 | 14 | 63.15 |
| 5.900 | 0.02 | 0.18 | 0.19 | 0.00 | 0.00 | 17 | 63.16 |
| 5.950 | 0.02 | 0.21 | 0.22 | 0.00 | 0.01 | 19 | 63.16 |
| 6.000 | 0.02 | 0.24 | 0.25 | 0.00 | 0.01 | 22 | 63.16 |
| 6.050 | 0.02 | 0.27 | 0.28 | 0.00 | 0.01 | 25 | 63.16 |
| 6.100 | 0.02 | 0.30 | 0.31 | 0.00 | 0.01 | 28 | 63.16 |
| 6.150 | 0.03 | 0.33 | 0.35 | 0.00 | 0.01 | 31 | 63.16 |
| 6.200 | 0.03 | 0.37 | 0.39 | 0.00 | 0.01 | 34 | 63.16 |
| 6.250 | 0.03 | 0.40 | 0.42 | 0.00 | 0.01 | 37 | 63.16 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.03 | 0.44 | 0.47 | 0.00 | 0.01 | 41 | 63.16 |
| 6.350 | 0.03 | 0.48 | 0.51 | 0.00 | 0.01 | 45 | 63.17 |
| 6.400 | 0.04 | 0.53 | 0.55 | 0.00 | 0.01 | 49 | 63.17 |
| 6.450 | 0.04 | 0.57 | 0.60 | 0.00 | 0.01 | 53 | 63.17 |
| 6.500 | 0.04 | 0.62 | 0.65 | 0.00 | 0.02 | 57 | 63.17 |
| 6.550 | 0.04 | 0.66 | 0.70 | 0.00 | 0.02 | 61 | 63.17 |
| 6.600 | 0.04 | 0.71 | 0.75 | 0.00 | 0.02 | 66 | 63.17 |
| 6.650 | 0.05 | 0.77 | 0.81 | 0.00 | 0.02 | 71 | 63.17 |
| 6.700 | 0.05 | 0.82 | 0.86 | 0.00 | 0.02 | 76 | 63.18 |
| 6.750 | 0.05 | 0.88 | 0.92 | 0.00 | 0.02 | 81 | 63.18 |
| 6.800 | 0.05 | 0.94 | 0.98 | 0.00 | 0.02 | 86 | 63.18 |
| 6.850 | 0.06 | 1.00 | 1.05 | 0.00 | 0.03 | 92 | 63.18 |
| 6.900 | 0.06 | 1.06 | 1.11 | 0.00 | 0.03 | 98 | 63.18 |
| 6.950 | 0.06 | 1.12 | 1.18 | 0.00 | 0.03 | 104 | 63.18 |
| 7.000 | 0.06 | 1.19 | 1.25 | 0.00 | 0.03 | 110 | 63.19 |
| 7.050 | 0.07 | 1.26 | 1.32 | 0.00 | 0.03 | 116 | 63.19 |
| 7.100 | 0.07 | 1.33 | 1.39 | 0.00 | 0.03 | 123 | 63.19 |
| 7.150 | 0.07 | 1.40 | 1.47 | 0.00 | 0.04 | 129 | 63.19 |
| 7.200 | 0.08 | 1.47 | 1.55 | 0.00 | 0.04 | 136 | 63.20 |
| 7.250 | 0.08 | 1.55 | 1.63 | 0.00 | 0.04 | 143 | 63.20 |
| 7.300 | 0.08 | 1.63 | 1.71 | 0.00 | 0.04 | 150 | 63.20 |
| 7.350 | 0.09 | 1.71 | 1.80 | 0.00 | 0.04 | 158 | 63.20 |
| 7.400 | 0.09 | 1.79 | 1.88 | 0.00 | 0.05 | 165 | 63.21 |
| 7.450 | 0.09 | 1.88 | 1.97 | 0.00 | 0.05 | 173 | 63.21 |
| 7.500 | 0.10 | 1.96 | 2.06 | 0.00 | 0.05 | 181 | 63.21 |
| 7.550 | 0.10 | 2.05 | 2.16 | 0.00 | 0.05 | 189 | 63.21 |
| 7.600 | 0.10 | 2.14 | 2.25 | 0.00 | 0.05 | 198 | 63.22 |
| 7.650 | 0.11 | 2.24 | 2.35 | 0.00 | 0.06 | 206 | 63.22 |
| 7.700 | 0.11 | 2.33 | 2.45 | 0.00 | 0.06 | 215 | 63.22 |
| 7.750 | 0.11 | 2.43 | 2.55 | 0.00 | 0.06 | 224 | 63.23 |
| 7.800 | 0.12 | 2.53 | 2.66 | 0.00 | 0.06 | 233 | 63.23 |
| 7.850 | 0.12 | 2.63 | 2.76 | 0.00 | 0.07 | 243 | 63.23 |
| 7.900 | 0.12 | 2.73 | 2.87 | 0.00 | 0.07 | 252 | 63.23 |
| 7.950 | 0.13 | 2.84 | 2.98 | 0.00 | 0.07 | 262 | 63.24 |
| 8.000 | 0.13 | 2.94 | 3.09 | 0.00 | 0.08 | 272 | 63.24 |
| 8.050 | 0.13 | 3.05 | 3.21 | 0.00 | 0.08 | 282 | 63.24 |
| 8.100 | 0.14 | 3.16 | 3.32 | 0.00 | 0.08 | 292 | 63.25 |
| 8.150 | 0.14 | 3.28 | 3.45 | 0.00 | 0.08 | 303 | 63.25 |
| 8.200 | 0.15 | 3.40 | 3.57 | 0.00 | 0.09 | 314 | 63.26 |
| 8.250 | 0.15 | 3.52 | 3.70 | 0.00 | 0.09 | 325 | 63.26 |
| 8.300 | 0.16 | 3.65 | 3.84 | 0.00 | 0.09 | 337 | 63.26 |
| 8.350 | 0.17 | 3.79 | 3.98 | 0.00 | 0.10 | 349 | 63.27 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.17 | 3.92 | 4.13 | 0.00 | 0.10 | 362 | 63.27 |
| 8.450 | 0.18 | 4.07 | 4.28 | 0.00 | 0.10 | 376 | 63.28 |
| 8.500 | 0.19 | 4.22 | 4.44 | 0.00 | 0.11 | 390 | 63.28 |
| 8.550 | 0.19 | 4.38 | 4.60 | 0.00 | 0.11 | 404 | 63.29 |
| 8.600 | 0.20 | 4.54 | 4.77 | 0.00 | 0.12 | 419 | 63.29 |
| 8.650 | 0.21 | 4.70 | 4.94 | 0.00 | 0.12 | 434 | 63.30 |
| 8.700 | 0.21 | 4.88 | 5.13 | 0.00 | 0.12 | 450 | 63.30 |
| 8.750 | 0.22 | 5.05 | 5.31 | 0.00 | 0.13 | 467 | 63.31 |
| 8.800 | 0.23 | 5.24 | 5.50 | 0.00 | 0.13 | 483 | 63.31 |
| 8.850 | 0.24 | 5.43 | 5.70 | 0.00 | 0.14 | 501 | 63.32 |
| 8.900 | 0.24 | 5.62 | 5.91 | 0.00 | 0.14 | 519 | 63.32 |
| 8.950 | 0.25 | 5.82 | 6.12 | 0.00 | 0.15 | 537 | 63.33 |
| 9.000 | 0.26 | 6.02 | 6.33 | 0.00 | 0.15 | 556 | 63.34 |
| 9.050 | 0.27 | 6.23 | 6.55 | 0.00 | 0.16 | 575 | 63.34 |
| 9.100 | 0.28 | 6.45 | 6.78 | 0.00 | 0.16 | 595 | 63.35 |
| 9.150 | 0.28 | 6.67 | 7.01 | 0.00 | 0.17 | 616 | 63.36 |
| 9.200 | 0.29 | 6.90 | 7.25 | 0.00 | 0.18 | 636 | 63.36 |
| 9.250 | 0.30 | 7.13 | 7.49 | 0.00 | 0.18 | 658 | 63.37 |
| 9.300 | 0.31 | 7.36 | 7.74 | 0.00 | 0.19 | 680 | 63.38 |
| 9.350 | 0.32 | 7.61 | 7.99 | 0.00 | 0.19 | 702 | 63.39 |
| 9.400 | 0.33 | 7.85 | 8.25 | 0.00 | 0.20 | 725 | 63.39 |
| 9.450 | 0.34 | 8.10 | 8.52 | 0.00 | 0.21 | 748 | 63.40 |
| 9.500 | 0.35 | 8.36 | 8.79 | 0.00 | 0.21 | 772 | 63.41 |
| 9.550 | 0.36 | 8.62 | 9.06 | 0.00 | 0.22 | 796 | 63.42 |
| 9.600 | 0.37 | 8.89 | 9.35 | 0.00 | 0.23 | 821 | 63.43 |
| 9.650 | 0.37 | 9.16 | 9.63 | 0.00 | 0.23 | 846 | 63.43 |
| 9.700 | 0.38 | 9.44 | 9.92 | 0.00 | 0.24 | 871 | 63.44 |
| 9.750 | 0.39 | 9.72 | 10.22 | 0.00 | 0.25 | 898 | 63.45 |
| 9.800 | 0.40 | 10.01 | 10.52 | 0.00 | 0.26 | 924 | 63.46 |
| 9.850 | 0.41 | 10.31 | 10.83 | 0.00 | 0.26 | 951 | 63.47 |
| 9.900 | 0.42 | 10.60 | 11.14 | 0.00 | 0.27 | 979 | 63.48 |
| 9.950 | 0.43 | 10.90 | 11.46 | 0.00 | 0.28 | 1,006 | 63.49 |
| 10.000 | 0.44 | 11.21 | 11.78 | 0.00 | 0.29 | 1,035 | 63.50 |
| 10.050 | 0.46 | 11.52 | 12.11 | 0.00 | 0.29 | 1,064 | 63.51 |
| 10.100 | 0.47 | 11.84 | 12.45 | 0.00 | 0.30 | 1,093 | 63.52 |
| 10.150 | 0.48 | 12.17 | 12.79 | 0.00 | 0.31 | 1,123 | 63.53 |
| 10.200 | 0.50 | 12.51 | 13.15 | 0.00 | 0.32 | 1,155 | 63.54 |
| 10.250 | 0.51 | 12.87 | 13.52 | 0.00 | 0.33 | 1,188 | 63.55 |
| 10.300 | 0.53 | 13.24 | 13.91 | 0.00 | 0.34 | 1,222 | 63.56 |
| 10.350 | 0.55 | 13.62 | 14.32 | 0.00 | 0.35 | 1,257 | 63.57 |
| 10.400 | 0.57 | 14.02 | 14.74 | 0.00 | 0.36 | 1,294 | 63.59 |
| 10.450 | 0.58 | 14.44 | 15.17 | 0.00 | 0.37 | 1,332 | 63.60 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.60 | 14.86 | 15.62 | 0.00 | 0.38 | 1,372 | 63.61 |
| 10.550 | 0.62 | 15.31 | 16.09 | 0.00 | 0.39 | 1,413 | 63.63 |
| 10.600 | 0.64 | 15.77 | 16.57 | 0.00 | 0.40 | 1,455 | 63.64 |
| 10.650 | 0.66 | 16.24 | 17.07 | 0.00 | 0.41 | 1,494 | 63.65 |
| 10.700 | 0.68 | 16.71 | 17.58 | 0.00 | 0.43 | 1,522 | 63.66 |
| 10.750 | 0.70 | 17.20 | 18.09 | 0.00 | 0.45 | 1,550 | 63.67 |
| 10.800 | 0.72 | 17.70 | 18.62 | 0.00 | 0.46 | 1,579 | 63.68 |
| 10.850 | 0.74 | 18.20 | 19.15 | 0.00 | 0.48 | 1,608 | 63.69 |
| 10.900 | 0.76 | 18.71 | 19.70 | 0.00 | 0.49 | 1,637 | 63.70 |
| 10.950 | 0.78 | 19.23 | 20.25 | 0.00 | 0.51 | 1,667 | 63.71 |
| 11.000 | 0.80 | 19.75 | 20.81 | 0.00 | 0.53 | 1,698 | 63.72 |
| 11.050 | 0.83 | 20.29 | 21.38 | 0.00 | 0.54 | 1,729 | 63.73 |
| 11.100 | 0.86 | 20.85 | 21.98 | 0.00 | 0.56 | 1,762 | 63.74 |
| 11.150 | 0.90 | 21.45 | 22.61 | 0.00 | 0.58 | 1,796 | 63.75 |
| 11.200 | 0.96 | 22.10 | 23.31 | 0.00 | 0.60 | 1,834 | 63.77 |
| 11.250 | 1.02 | 22.82 | 24.08 | 0.00 | 0.63 | 1,876 | 63.78 |
| 11.300 | 1.08 | 23.62 | 24.92 | 0.00 | 0.65 | 1,922 | 63.80 |
| 11.350 | 1.14 | 24.48 | 25.84 | 0.00 | 0.68 | 1,972 | 63.81 |
| 11.400 | 1.21 | 25.42 | 26.84 | 0.00 | 0.71 | 2,027 | 63.83 |
| 11.450 | 1.28 | 26.43 | 27.92 | 0.00 | 0.74 | 2,086 | 63.85 |
| 11.500 | 1.35 | 27.51 | 29.07 | 0.00 | 0.78 | 2,148 | 63.87 |
| 11.550 | 1.48 | 28.72 | 30.34 | 0.00 | 0.81 | 2,218 | 63.90 |
| 11.600 | 1.71 | 30.18 | 31.91 | 0.00 | 0.86 | 2,392 | 63.92 |
| 11.650 | 2.05 | 32.10 | 33.95 | 0.00 | 0.92 | 2,637 | 63.96 |
| 11.700 | 2.56 | 34.70 | 36.71 | 0.00 | 1.01 | 2,969 | 64.01 |
| 11.750 | 3.12 | 38.14 | 40.38 | 0.00 | 1.12 | 3,409 | 64.08 |
| 11.800 | 3.76 | 42.51 | 45.02 | 0.00 | 1.26 | 3,939 | 64.16 |
| 11.850 | 4.41 | 47.83 | 50.68 | 0.00 | 1.42 | 4,436 | 64.24 |
| 11.900 | 5.14 | 54.14 | 57.38 | 0.00 | 1.62 | 5,024 | 64.33 |
| 11.950 | 6.34 | 61.88 | 65.61 | 0.00 | 1.87 | 5,744 | 64.44 |
| 12.000 | 8.67 | 72.48 | 76.89 | 0.00 | 2.20 | 6,723 | 64.59 |
| 12.050 | 10.84 | 86.56 | 92.00 | 0.00 | 2.72 | 8,042 | 64.80 |
| 12.100 | 12.08 | 102.78 | 109.48 | 0.00 | 3.35 | 9,556 | 65.04 |
| 12.150 | 12.08 | 118.85 | 126.94 | 0.00 | 4.05 | 11,070 | 65.29 |
| 12.200 | 10.38 | 131.99 | 141.31 | 0.00 | 4.66 | 12,309 | 65.50 |
| 12.250 | 8.46 | 140.69 | 150.83 | 0.00 | 5.07 | 13,119 | 65.63 |
| 12.300 | 7.10 | 145.60 | 156.25 | 0.00 | 5.33 | 13,589 | 65.71 |
| 12.350 | 6.14 | 147.92 | 158.84 | 0.00 | 5.46 | 13,813 | 65.75 |
| 12.400 | 5.29 | 148.38 | 159.35 | 0.00 | 5.48 | 13,858 | 65.76 |
| 12.450 | 4.53 | 147.36 | 158.21 | 0.00 | 5.43 | 13,759 | 65.74 |
| 12.500 | 3.78 | 145.07 | 155.67 | 0.00 | 5.30 | 13,538 | 65.70 |
| 12.550 | 3.13 | 141.74 | 151.98 | 0.00 | 5.12 | 13,218 | 65.65 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 2.59 | 137.61 | 147.46 | 0.00 | 4.92 | 12,833 | 65.58 |
| 12.650 | 2.21 | 133.00 | 142.42 | 0.00 | 4.71 | 12,403 | 65.51 |
| 12.700 | 1.99 | 128.23 | 137.20 | 0.00 | 4.49 | 11,959 | 65.44 |
| 12.750 | 1.85 | 123.53 | 132.07 | 0.00 | 4.27 | 11,516 | 65.36 |
| 12.800 | 1.74 | 119.01 | 127.12 | 0.00 | 4.06 | 11,085 | 65.29 |
| 12.850 | 1.65 | 114.69 | 122.40 | 0.00 | 3.85 | 10,674 | 65.22 |
| 12.900 | 1.57 | 110.59 | 117.91 | 0.00 | 3.66 | 10,283 | 65.16 |
| 12.950 | 1.49 | 106.65 | 113.65 | 0.00 | 3.50 | 9,916 | 65.10 |
| 13.000 | 1.42 | 102.84 | 109.55 | 0.00 | 3.36 | 9,563 | 65.04 |
| 13.050 | 1.35 | 99.18 | 105.61 | 0.00 | 3.21 | 9,223 | 64.99 |
| 13.100 | 1.29 | 95.67 | 101.82 | 0.00 | 3.08 | 8,896 | 64.94 |
| 13.150 | 1.24 | 92.31 | 98.19 | 0.00 | 2.94 | 8,583 | 64.89 |
| 13.200 | 1.21 | 89.12 | 94.76 | 0.00 | 2.82 | 8,283 | 64.84 |
| 13.250 | 1.18 | 86.10 | 91.51 | 0.00 | 2.70 | 7,999 | 64.79 |
| 13.300 | 1.16 | 83.26 | 88.45 | 0.00 | 2.59 | 7,732 | 64.75 |
| 13.350 | 1.14 | 80.59 | 85.57 | 0.00 | 2.49 | 7,480 | 64.71 |
| 13.400 | 1.12 | 78.07 | 82.85 | 0.00 | 2.39 | 7,243 | 64.68 |
| 13.450 | 1.10 | 75.69 | 80.29 | 0.00 | 2.30 | 7,020 | 64.64 |
| 13.500 | 1.08 | 73.41 | 77.87 | 0.00 | 2.23 | 6,809 | 64.61 |
| 13.550 | 1.06 | 71.23 | 75.55 | 0.00 | 2.16 | 6,608 | 64.58 |
| 13.600 | 1.04 | 69.14 | 73.33 | 0.00 | 2.10 | 6,415 | 64.55 |
| 13.650 | 1.02 | 67.14 | 71.21 | 0.00 | 2.03 | 6,230 | 64.52 |
| 13.700 | 1.00 | 65.22 | 69.17 | 0.00 | 1.97 | 6,053 | 64.49 |
| 13.750 | 0.98 | 63.38 | 67.21 | 0.00 | 1.91 | 5,883 | 64.46 |
| 13.800 | 0.96 | 61.61 | 65.32 | 0.00 | 1.86 | 5,719 | 64.44 |
| 13.850 | 0.94 | 59.90 | 63.51 | 0.00 | 1.80 | 5,562 | 64.41 |
| 13.900 | 0.92 | 58.26 | 61.77 | 0.00 | 1.75 | 5,410 | 64.39 |
| 13.950 | 0.90 | 56.68 | 60.09 | 0.00 | 1.70 | 5,262 | 64.37 |
| 14.000 | 0.88 | 55.16 | 58.47 | 0.00 | 1.66 | 5,120 | 64.34 |
| 14.050 | 0.86 | 53.69 | 56.90 | 0.00 | 1.61 | 4,982 | 64.32 |
| 14.100 | 0.85 | 52.27 | 55.40 | 0.00 | 1.56 | 4,850 | 64.30 |
| 14.150 | 0.83 | 50.91 | 53.95 | 0.00 | 1.52 | 4,723 | 64.28 |
| 14.200 | 0.82 | 49.60 | 52.56 | 0.00 | 1.48 | 4,601 | 64.26 |
| 14.250 | 0.81 | 48.35 | 51.23 | 0.00 | 1.44 | 4,484 | 64.25 |
| 14.300 | 0.80 | 47.15 | 49.96 | 0.00 | 1.40 | 4,373 | 64.23 |
| 14.350 | 0.79 | 46.01 | 48.74 | 0.00 | 1.37 | 4,266 | 64.21 |
| 14.400 | 0.78 | 44.92 | 47.58 | 0.00 | 1.33 | 4,164 | 64.20 |
| 14.450 | 0.77 | 43.87 | 46.47 | 0.00 | 1.30 | 4,066 | 64.18 |
| 14.500 | 0.76 | 42.87 | 45.40 | 0.00 | 1.27 | 3,973 | 64.17 |
| 14.550 | 0.75 | 41.91 | 44.38 | 0.00 | 1.24 | 3,883 | 64.15 |
| 14.600 | 0.74 | 40.99 | 43.40 | 0.00 | 1.21 | 3,772 | 64.14 |
| 14.650 | 0.73 | 40.10 | 42.46 | 0.00 | 1.18 | 3,659 | 64.12 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.72 | 39.25 | 41.56 | 0.00 | 1.15 | 3,551 | 64.10 |
| 14.750 | 0.71 | 38.44 | 40.69 | 0.00 | 1.13 | 3,447 | 64.09 |
| 14.800 | 0.70 | 37.65 | 39.86 | 0.00 | 1.10 | 3,346 | 64.07 |
| 14.850 | 0.70 | 36.90 | 39.05 | 0.00 | 1.08 | 3,250 | 64.06 |
| 14.900 | 0.69 | 36.17 | 38.28 | 0.00 | 1.05 | 3,157 | 64.04 |
| 14.950 | 0.68 | 35.47 | 37.53 | 0.00 | 1.03 | 3,067 | 64.03 |
| 15.000 | 0.67 | 34.79 | 36.81 | 0.00 | 1.01 | 2,981 | 64.01 |
| 15.050 | 0.66 | 34.14 | 36.11 | 0.00 | 0.99 | 2,897 | 64.00 |
| 15.100 | 0.65 | 33.50 | 35.44 | 0.00 | 0.97 | 2,816 | 63.99 |
| 15.150 | 0.64 | 32.89 | 34.79 | 0.00 | 0.95 | 2,738 | 63.98 |
| 15.200 | 0.63 | 32.29 | 34.15 | 0.00 | 0.93 | 2,662 | 63.97 |
| 15.250 | 0.62 | 31.72 | 33.54 | 0.00 | 0.91 | 2,588 | 63.95 |
| 15.300 | 0.61 | 31.16 | 32.94 | 0.00 | 0.89 | 2,516 | 63.94 |
| 15.350 | 0.60 | 30.61 | 32.36 | 0.00 | 0.88 | 2,447 | 63.93 |
| 15.400 | 0.59 | 30.08 | 31.80 | 0.00 | 0.86 | 2,379 | 63.92 |
| 15.450 | 0.58 | 29.56 | 31.25 | 0.00 | 0.84 | 2,313 | 63.91 |
| 15.500 | 0.57 | 29.06 | 30.71 | 0.00 | 0.83 | 2,249 | 63.90 |
| 15.550 | 0.56 | 28.57 | 30.19 | 0.00 | 0.81 | 2,209 | 63.89 |
| 15.600 | 0.55 | 28.09 | 29.68 | 0.00 | 0.79 | 2,181 | 63.88 |
| 15.650 | 0.54 | 27.62 | 29.18 | 0.00 | 0.78 | 2,154 | 63.87 |
| 15.700 | 0.53 | 27.16 | 28.69 | 0.00 | 0.76 | 2,128 | 63.87 |
| 15.750 | 0.52 | 26.71 | 28.21 | 0.00 | 0.75 | 2,101 | 63.86 |
| 15.800 | 0.51 | 26.26 | 27.74 | 0.00 | 0.74 | 2,076 | 63.85 |
| 15.850 | 0.50 | 25.83 | 27.28 | 0.00 | 0.72 | 2,051 | 63.84 |
| 15.900 | 0.49 | 25.40 | 26.82 | 0.00 | 0.71 | 2,026 | 63.83 |
| 15.950 | 0.48 | 24.99 | 26.38 | 0.00 | 0.70 | 2,002 | 63.82 |
| 16.000 | 0.47 | 24.57 | 25.94 | 0.00 | 0.68 | 1,978 | 63.82 |
| 16.050 | 0.46 | 24.17 | 25.51 | 0.00 | 0.67 | 1,954 | 63.81 |
| 16.100 | 0.45 | 23.77 | 25.09 | 0.00 | 0.66 | 1,931 | 63.80 |
| 16.150 | 0.45 | 23.39 | 24.68 | 0.00 | 0.64 | 1,909 | 63.79 |
| 16.200 | 0.44 | 23.01 | 24.28 | 0.00 | 0.63 | 1,887 | 63.78 |
| 16.250 | 0.44 | 22.65 | 23.89 | 0.00 | 0.62 | 1,866 | 63.78 |
| 16.300 | 0.43 | 22.30 | 23.52 | 0.00 | 0.61 | 1,846 | 63.77 |
| 16.350 | 0.43 | 21.97 | 23.16 | 0.00 | 0.60 | 1,826 | 63.76 |
| 16.400 | 0.42 | 21.64 | 22.82 | 0.00 | 0.59 | 1,808 | 63.76 |
| 16.450 | 0.42 | 21.33 | 22.48 | 0.00 | 0.58 | 1,789 | 63.75 |
| 16.500 | 0.42 | 21.03 | 22.16 | 0.00 | 0.57 | 1,772 | 63.75 |
| 16.550 | 0.41 | 20.74 | 21.85 | 0.00 | 0.56 | 1,755 | 63.74 |
| 16.600 | 0.41 | 20.45 | 21.55 | 0.00 | 0.55 | 1,739 | 63.73 |
| 16.650 | 0.40 | 20.18 | 21.26 | 0.00 | 0.54 | 1,723 | 63.73 |
| 16.700 | 0.40 | 19.92 | 20.98 | 0.00 | 0.53 | 1,707 | 63.72 |
| 16.750 | 0.39 | 19.66 | 20.71 | 0.00 | 0.52 | 1,692 | 63.72 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.39 | 19.41 | 20.44 | 0.00 | 0.52 | 1,678 | 63.71 |
| 16.850 | 0.39 | 19.17 | 20.18 | 0.00 | 0.51 | 1,664 | 63.71 |
| 16.900 | 0.38 | 18.93 | 19.93 | 0.00 | 0.50 | 1,650 | 63.71 |
| 16.950 | 0.38 | 18.70 | 19.69 | 0.00 | 0.49 | 1,637 | 63.70 |
| 17.000 | 0.37 | 18.48 | 19.45 | 0.00 | 0.49 | 1,624 | 63.70 |
| 17.050 | 0.37 | 18.26 | 19.22 | 0.00 | 0.48 | 1,611 | 63.69 |
| 17.100 | 0.36 | 18.05 | 18.99 | 0.00 | 0.47 | 1,599 | 63.69 |
| 17.150 | 0.36 | 17.84 | 18.77 | 0.00 | 0.47 | 1,587 | 63.68 |
| 17.200 | 0.36 | 17.64 | 18.56 | 0.00 | 0.46 | 1,575 | 63.68 |
| 17.250 | 0.35 | 17.44 | 18.34 | 0.00 | 0.45 | 1,564 | 63.68 |
| 17.300 | 0.35 | 17.24 | 18.14 | 0.00 | 0.45 | 1,552 | 63.67 |
| 17.350 | 0.34 | 17.05 | 17.93 | 0.00 | 0.44 | 1,541 | 63.67 |
| 17.400 | 0.34 | 16.86 | 17.73 | 0.00 | 0.43 | 1,530 | 63.66 |
| 17.450 | 0.33 | 16.68 | 17.53 | 0.00 | 0.43 | 1,519 | 63.66 |
| 17.500 | 0.33 | 16.50 | 17.34 | 0.00 | 0.42 | 1,509 | 63.66 |
| 17.550 | 0.33 | 16.32 | 17.15 | 0.00 | 0.42 | 1,499 | 63.65 |
| 17.600 | 0.32 | 16.14 | 16.96 | 0.00 | 0.41 | 1,488 | 63.65 |
| 17.650 | 0.32 | 15.97 | 16.78 | 0.00 | 0.41 | 1,473 | 63.65 |
| 17.700 | 0.31 | 15.79 | 16.60 | 0.00 | 0.40 | 1,457 | 63.64 |
| 17.750 | 0.31 | 15.62 | 16.41 | 0.00 | 0.40 | 1,441 | 63.63 |
| 17.800 | 0.30 | 15.44 | 16.23 | 0.00 | 0.39 | 1,425 | 63.63 |
| 17.850 | 0.30 | 15.27 | 16.05 | 0.00 | 0.39 | 1,409 | 63.62 |
| 17.900 | 0.30 | 15.09 | 15.86 | 0.00 | 0.38 | 1,393 | 63.62 |
| 17.950 | 0.29 | 14.92 | 15.68 | 0.00 | 0.38 | 1,377 | 63.61 |
| 18.000 | 0.29 | 14.75 | 15.50 | 0.00 | 0.38 | 1,361 | 63.61 |
| 18.050 | 0.28 | 14.57 | 15.32 | 0.00 | 0.37 | 1,345 | 63.60 |
| 18.100 | 0.28 | 14.40 | 15.14 | 0.00 | 0.37 | 1,329 | 63.60 |
| 18.150 | 0.28 | 14.23 | 14.96 | 0.00 | 0.36 | 1,314 | 63.59 |
| 18.200 | 0.28 | 14.07 | 14.79 | 0.00 | 0.36 | 1,298 | 63.59 |
| 18.250 | 0.27 | 13.91 | 14.62 | 0.00 | 0.35 | 1,284 | 63.58 |
| 18.300 | 0.27 | 13.75 | 14.45 | 0.00 | 0.35 | 1,269 | 63.58 |
| 18.350 | 0.27 | 13.60 | 14.30 | 0.00 | 0.35 | 1,255 | 63.57 |
| 18.400 | 0.27 | 13.46 | 14.14 | 0.00 | 0.34 | 1,242 | 63.57 |
| 18.450 | 0.27 | 13.32 | 13.99 | 0.00 | 0.34 | 1,229 | 63.56 |
| 18.500 | 0.27 | 13.18 | 13.85 | 0.00 | 0.34 | 1,216 | 63.56 |
| 18.550 | 0.27 | 13.05 | 13.71 | 0.00 | 0.33 | 1,204 | 63.56 |
| 18.600 | 0.26 | 12.92 | 13.58 | 0.00 | 0.33 | 1,192 | 63.55 |
| 18.650 | 0.26 | 12.79 | 13.45 | 0.00 | 0.33 | 1,181 | 63.55 |
| 18.700 | 0.26 | 12.67 | 13.32 | 0.00 | 0.32 | 1,170 | 63.54 |
| 18.750 | 0.26 | 12.56 | 13.20 | 0.00 | 0.32 | 1,159 | 63.54 |
| 18.800 | 0.26 | 12.44 | 13.08 | 0.00 | 0.32 | 1,148 | 63.54 |
| 18.850 | 0.26 | 12.33 | 12.96 | 0.00 | 0.31 | 1,138 | 63.53 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.26 | 12.22 | 12.85 | 0.00 | 0.31 | 1,128 | 63.53 |
| 18.950 | 0.26 | 12.12 | 12.73 | 0.00 | 0.31 | 1,118 | 63.53 |
| 19.000 | 0.25 | 12.01 | 12.63 | 0.00 | 0.31 | 1,109 | 63.52 |
| 19.050 | 0.25 | 11.91 | 12.52 | 0.00 | 0.30 | 1,100 | 63.52 |
| 19.100 | 0.25 | 11.82 | 12.42 | 0.00 | 0.30 | 1,091 | 63.52 |
| 19.150 | 0.25 | 11.72 | 12.32 | 0.00 | 0.30 | 1,082 | 63.51 |
| 19.200 | 0.25 | 11.63 | 12.22 | 0.00 | 0.30 | 1,073 | 63.51 |
| 19.250 | 0.25 | 11.54 | 12.12 | 0.00 | 0.29 | 1,065 | 63.51 |
| 19.300 | 0.25 | 11.45 | 12.03 | 0.00 | 0.29 | 1,057 | 63.51 |
| 19.350 | 0.25 | 11.36 | 11.94 | 0.00 | 0.29 | 1,048 | 63.50 |
| 19.400 | 0.24 | 11.27 | 11.85 | 0.00 | 0.29 | 1,041 | 63.50 |
| 19.450 | 0.24 | 11.19 | 11.76 | 0.00 | 0.29 | 1,033 | 63.50 |
| 19.500 | 0.24 | 11.11 | 11.68 | 0.00 | 0.28 | 1,025 | 63.49 |
| 19.550 | 0.24 | 11.03 | 11.59 | 0.00 | 0.28 | 1,018 | 63.49 |
| 19.600 | 0.24 | 10.95 | 11.51 | 0.00 | 0.28 | 1,011 | 63.49 |
| 19.650 | 0.24 | 10.87 | 11.43 | 0.00 | 0.28 | 1,003 | 63.49 |
| 19.700 | 0.24 | 10.80 | 11.35 | 0.00 | 0.28 | 996 | 63.49 |
| 19.750 | 0.23 | 10.72 | 11.27 | 0.00 | 0.27 | 989 | 63.48 |
| 19.800 | 0.23 | 10.65 | 11.19 | 0.00 | 0.27 | 983 | 63.48 |
| 19.850 | 0.23 | 10.57 | 11.11 | 0.00 | 0.27 | 976 | 63.48 |
| 19.900 | 0.23 | 10.50 | 11.04 | 0.00 | 0.27 | 969 | 63.48 |
| 19.950 | 0.23 | 10.43 | 10.96 | 0.00 | 0.27 | 963 | 63.47 |
| 20.000 | 0.23 | 10.36 | 10.89 | 0.00 | 0.26 | 956 | 63.47 |
| 20.050 | 0.23 | 10.29 | 10.82 | 0.00 | 0.26 | 950 | 63.47 |
| 20.100 | 0.23 | 10.23 | 10.75 | 0.00 | 0.26 | 944 | 63.47 |
| 20.150 | 0.22 | 10.16 | 10.68 | 0.00 | 0.26 | 938 | 63.47 |
| 20.200 | 0.22 | 10.09 | 10.61 | 0.00 | 0.26 | 931 | 63.46 |
| 20.250 | 0.22 | 10.03 | 10.54 | 0.00 | 0.26 | 926 | 63.46 |
| 20.300 | 0.22 | 9.97 | 10.48 | 0.00 | 0.25 | 920 | 63.46 |
| 20.350 | 0.22 | 9.91 | 10.41 | 0.00 | 0.25 | 914 | 63.46 |
| 20.400 | 0.22 | 9.85 | 10.35 | 0.00 | 0.25 | 909 | 63.46 |
| 20.450 | 0.22 | 9.79 | 10.28 | 0.00 | 0.25 | 903 | 63.45 |
| 20.500 | 0.22 | 9.73 | 10.22 | 0.00 | 0.25 | 898 | 63.45 |
| 20.550 | 0.22 | 9.67 | 10.16 | 0.00 | 0.25 | 892 | 63.45 |
| 20.600 | 0.22 | 9.61 | 10.10 | 0.00 | 0.25 | 887 | 63.45 |
| 20.650 | 0.22 | 9.56 | 10.05 | 0.00 | 0.24 | 882 | 63.45 |
| 20.700 | 0.21 | 9.50 | 9.99 | 0.00 | 0.24 | 877 | 63.45 |
| 20.750 | 0.21 | 9.45 | 9.93 | 0.00 | 0.24 | 872 | 63.44 |
| 20.800 | 0.21 | 9.39 | 9.87 | 0.00 | 0.24 | 867 | 63.44 |
| 20.850 | 0.21 | 9.34 | 9.82 | 0.00 | 0.24 | 862 | 63.44 |
| 20.900 | 0.21 | 9.29 | 9.76 | 0.00 | 0.24 | 857 | 63.44 |
| 20.950 | 0.21 | 9.24 | 9.71 | 0.00 | 0.24 | 853 | 63.44 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.21 | 9.19 | 9.66 | 0.00 | 0.23 | 848 | 63.44 |
| 21.050 | 0.21 | 9.14 | 9.61 | 0.00 | 0.23 | 844 | 63.43 |
| 21.100 | 0.21 | 9.09 | 9.56 | 0.00 | 0.23 | 839 | 63.43 |
| 21.150 | 0.21 | 9.04 | 9.50 | 0.00 | 0.23 | 835 | 63.43 |
| 21.200 | 0.20 | 9.00 | 9.45 | 0.00 | 0.23 | 830 | 63.43 |
| 21.250 | 0.20 | 8.95 | 9.40 | 0.00 | 0.23 | 826 | 63.43 |
| 21.300 | 0.20 | 8.90 | 9.35 | 0.00 | 0.23 | 821 | 63.43 |
| 21.350 | 0.20 | 8.85 | 9.31 | 0.00 | 0.23 | 817 | 63.42 |
| 21.400 | 0.20 | 8.81 | 9.26 | 0.00 | 0.22 | 813 | 63.42 |
| 21.450 | 0.20 | 8.76 | 9.21 | 0.00 | 0.22 | 809 | 63.42 |
| 21.500 | 0.20 | 8.72 | 9.16 | 0.00 | 0.22 | 804 | 63.42 |
| 21.550 | 0.20 | 8.67 | 9.11 | 0.00 | 0.22 | 800 | 63.42 |
| 21.600 | 0.20 | 8.63 | 9.06 | 0.00 | 0.22 | 796 | 63.42 |
| 21.650 | 0.20 | 8.58 | 9.02 | 0.00 | 0.22 | 792 | 63.42 |
| 21.700 | 0.20 | 8.54 | 8.97 | 0.00 | 0.22 | 788 | 63.42 |
| 21.750 | 0.19 | 8.49 | 8.93 | 0.00 | 0.22 | 784 | 63.41 |
| 21.800 | 0.19 | 8.45 | 8.88 | 0.00 | 0.22 | 780 | 63.41 |
| 21.850 | 0.19 | 8.41 | 8.84 | 0.00 | 0.21 | 776 | 63.41 |
| 21.900 | 0.19 | 8.36 | 8.79 | 0.00 | 0.21 | 772 | 63.41 |
| 21.950 | 0.19 | 8.32 | 8.75 | 0.00 | 0.21 | 768 | 63.41 |
| 22.000 | 0.19 | 8.28 | 8.70 | 0.00 | 0.21 | 764 | 63.41 |
| 22.050 | 0.19 | 8.24 | 8.66 | 0.00 | 0.21 | 760 | 63.41 |
| 22.100 | 0.19 | 8.20 | 8.61 | 0.00 | 0.21 | 756 | 63.40 |
| 22.150 | 0.19 | 8.15 | 8.57 | 0.00 | 0.21 | 753 | 63.40 |
| 22.200 | 0.19 | 8.11 | 8.53 | 0.00 | 0.21 | 749 | 63.40 |
| 22.250 | 0.18 | 8.07 | 8.48 | 0.00 | 0.21 | 745 | 63.40 |
| 22.300 | 0.18 | 8.03 | 8.44 | 0.00 | 0.20 | 741 | 63.40 |
| 22.350 | 0.18 | 7.99 | 8.39 | 0.00 | 0.20 | 737 | 63.40 |
| 22.400 | 0.18 | 7.95 | 8.35 | 0.00 | 0.20 | 733 | 63.40 |
| 22.450 | 0.18 | 7.90 | 8.31 | 0.00 | 0.20 | 730 | 63.40 |
| 22.500 | 0.18 | 7.86 | 8.26 | 0.00 | 0.20 | 726 | 63.39 |
| 22.550 | 0.18 | 7.82 | 8.22 | 0.00 | 0.20 | 722 | 63.39 |
| 22.600 | 0.18 | 7.78 | 8.18 | 0.00 | 0.20 | 718 | 63.39 |
| 22.650 | 0.18 | 7.74 | 8.14 | 0.00 | 0.20 | 715 | 63.39 |
| 22.700 | 0.18 | 7.70 | 8.10 | 0.00 | 0.20 | 711 | 63.39 |
| 22.750 | 0.17 | 7.66 | 8.05 | 0.00 | 0.20 | 707 | 63.39 |
| 22.800 | 0.17 | 7.62 | 8.01 | 0.00 | 0.19 | 704 | 63.39 |
| 22.850 | 0.17 | 7.58 | 7.97 | 0.00 | 0.19 | 700 | 63.39 |
| 22.900 | 0.17 | 7.54 | 7.93 | 0.00 | 0.19 | 696 | 63.38 |
| 22.950 | 0.17 | 7.50 | 7.89 | 0.00 | 0.19 | 693 | 63.38 |
| 23.000 | 0.17 | 7.46 | 7.84 | 0.00 | 0.19 | 689 | 63.38 |
| 23.050 | 0.17 | 7.43 | 7.80 | 0.00 | 0.19 | 685 | 63.38 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: MC-3500 - 3 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.17 | 7.39 | 7.76 | 0.00 | 0.19 | 682 | 63.38 |
| 23.150 | 0.17 | 7.34 | 7.72 | 0.00 | 0.19 | 678 | 63.38 |
| 23.200 | 0.17 | 7.30 | 7.68 | 0.00 | 0.19 | 674 | 63.38 |
| 23.250 | 0.17 | 7.27 | 7.64 | 0.00 | 0.19 | 671 | 63.38 |
| 23.300 | 0.16 | 7.23 | 7.59 | 0.00 | 0.18 | 667 | 63.37 |
| 23.350 | 0.16 | 7.19 | 7.55 | 0.00 | 0.18 | 663 | 63.37 |
| 23.400 | 0.16 | 7.15 | 7.51 | 0.00 | 0.18 | 660 | 63.37 |
| 23.450 | 0.16 | 7.11 | 7.47 | 0.00 | 0.18 | 656 | 63.37 |
| 23.500 | 0.16 | 7.07 | 7.43 | 0.00 | 0.18 | 653 | 63.37 |
| 23.550 | 0.16 | 7.03 | 7.39 | 0.00 | 0.18 | 649 | 63.37 |
| 23.600 | 0.16 | 6.99 | 7.35 | 0.00 | 0.18 | 645 | 63.37 |
| 23.650 | 0.16 | 6.95 | 7.31 | 0.00 | 0.18 | 642 | 63.37 |
| 23.700 | 0.16 | 6.92 | 7.27 | 0.00 | 0.18 | 638 | 63.36 |
| 23.750 | 0.16 | 6.88 | 7.23 | 0.00 | 0.18 | 635 | 63.36 |
| 23.800 | 0.15 | 6.84 | 7.19 | 0.00 | 0.17 | 631 | 63.36 |
| 23.850 | 0.15 | 6.80 | 7.15 | 0.00 | 0.17 | 628 | 63.36 |
| 23.900 | 0.15 | 6.76 | 7.10 | 0.00 | 0.17 | 624 | 63.36 |
| 23.950 | 0.15 | 6.72 | 7.06 | 0.00 | 0.17 | 620 | 63.36 |
| 24.000 | 0.15 | 6.68 | 7.02 | 0.00 | 0.17 | 617 | 63.36 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 4.450 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 1 | 63.15 |
| 4.500 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 1 | 63.15 |
| 4.550 | 0.01 | 0.02 | 0.02 | 0.00 | 0.00 | 2 | 63.15 |
| 4.600 | 0.01 | 0.03 | 0.04 | 0.00 | 0.00 | 3 | 63.15 |
| 4.650 | 0.01 | 0.05 | 0.05 | 0.00 | 0.00 | 5 | 63.15 |
| 4.700 | 0.01 | 0.07 | 0.07 | 0.00 | 0.00 | 6 | 63.15 |
| 4.750 | 0.01 | 0.09 | 0.09 | 0.00 | 0.00 | 8 | 63.15 |
| 4.800 | 0.02 | 0.11 | 0.12 | 0.00 | 0.00 | 10 | 63.15 |
| 4.850 | 0.02 | 0.14 | 0.15 | 0.00 | 0.00 | 13 | 63.15 |
| 4.900 | 0.02 | 0.17 | 0.18 | 0.00 | 0.00 | 15 | 63.16 |
| 4.950 | 0.02 | 0.20 | 0.21 | 0.00 | 0.01 | 18 | 63.16 |
| 5.000 | 0.02 | 0.23 | 0.24 | 0.00 | 0.01 | 21 | 63.16 |
| 5.050 | 0.03 | 0.27 | 0.28 | 0.00 | 0.01 | 25 | 63.16 |
| 5.100 | 0.03 | 0.30 | 0.32 | 0.00 | 0.01 | 28 | 63.16 |
| 5.150 | 0.03 | 0.34 | 0.36 | 0.00 | 0.01 | 32 | 63.16 |
| 5.200 | 0.03 | 0.39 | 0.40 | 0.00 | 0.01 | 36 | 63.16 |
| 5.250 | 0.03 | 0.43 | 0.45 | 0.00 | 0.01 | 40 | 63.16 |
| 5.300 | 0.04 | 0.47 | 0.50 | 0.00 | 0.01 | 44 | 63.16 |
| 5.350 | 0.04 | 0.52 | 0.55 | 0.00 | 0.01 | 48 | 63.17 |
| 5.400 | 0.04 | 0.57 | 0.60 | 0.00 | 0.01 | 52 | 63.17 |
| 5.450 | 0.04 | 0.62 | 0.65 | 0.00 | 0.02 | 57 | 63.17 |
| 5.500 | 0.04 | 0.67 | 0.70 | 0.00 | 0.02 | 62 | 63.17 |
| 5.550 | 0.05 | 0.72 | 0.76 | 0.00 | 0.02 | 67 | 63.17 |
| 5.600 | 0.05 | 0.78 | 0.82 | 0.00 | 0.02 | 72 | 63.17 |
| 5.650 | 0.05 | 0.83 | 0.87 | 0.00 | 0.02 | 77 | 63.18 |
| 5.700 | 0.05 | 0.89 | 0.93 | 0.00 | 0.02 | 82 | 63.18 |
| 5.750 | 0.05 | 0.95 | 1.00 | 0.00 | 0.02 | 87 | 63.18 |
| 5.800 | 0.06 | 1.01 | 1.06 | 0.00 | 0.03 | 93 | 63.18 |
| 5.850 | 0.06 | 1.07 | 1.12 | 0.00 | 0.03 | 99 | 63.18 |
| 5.900 | 0.06 | 1.13 | 1.19 | 0.00 | 0.03 | 104 | 63.19 |
| 5.950 | 0.06 | 1.19 | 1.25 | 0.00 | 0.03 | 110 | 63.19 |
| 6.000 | 0.07 | 1.26 | 1.32 | 0.00 | 0.03 | 116 | 63.19 |
| 6.050 | 0.07 | 1.32 | 1.39 | 0.00 | 0.03 | 122 | 63.19 |
| 6.100 | 0.07 | 1.39 | 1.46 | 0.00 | 0.04 | 128 | 63.19 |
| 6.150 | 0.07 | 1.46 | 1.53 | 0.00 | 0.04 | 135 | 63.20 |
| 6.200 | 0.08 | 1.53 | 1.61 | 0.00 | 0.04 | 141 | 63.20 |
| 6.250 | 0.08 | 1.60 | 1.68 | 0.00 | 0.04 | 148 | 63.20 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.08 | 1.68 | 1.76 | 0.00 | 0.04 | 155 | 63.20 |
| 6.350 | 0.09 | 1.75 | 1.84 | 0.00 | 0.04 | 162 | 63.20 |
| 6.400 | 0.09 | 1.83 | 1.93 | 0.00 | 0.05 | 169 | 63.21 |
| 6.450 | 0.09 | 1.92 | 2.01 | 0.00 | 0.05 | 177 | 63.21 |
| 6.500 | 0.10 | 2.00 | 2.10 | 0.00 | 0.05 | 185 | 63.21 |
| 6.550 | 0.10 | 2.09 | 2.20 | 0.00 | 0.05 | 193 | 63.21 |
| 6.600 | 0.10 | 2.18 | 2.29 | 0.00 | 0.06 | 201 | 63.22 |
| 6.650 | 0.11 | 2.27 | 2.39 | 0.00 | 0.06 | 210 | 63.22 |
| 6.700 | 0.11 | 2.37 | 2.49 | 0.00 | 0.06 | 219 | 63.22 |
| 6.750 | 0.11 | 2.47 | 2.59 | 0.00 | 0.06 | 228 | 63.23 |
| 6.800 | 0.12 | 2.57 | 2.70 | 0.00 | 0.07 | 237 | 63.23 |
| 6.850 | 0.12 | 2.67 | 2.81 | 0.00 | 0.07 | 246 | 63.23 |
| 6.900 | 0.13 | 2.78 | 2.92 | 0.00 | 0.07 | 256 | 63.24 |
| 6.950 | 0.13 | 2.88 | 3.03 | 0.00 | 0.07 | 266 | 63.24 |
| 7.000 | 0.13 | 3.00 | 3.15 | 0.00 | 0.08 | 277 | 63.24 |
| 7.050 | 0.14 | 3.11 | 3.27 | 0.00 | 0.08 | 287 | 63.25 |
| 7.100 | 0.14 | 3.23 | 3.39 | 0.00 | 0.08 | 298 | 63.25 |
| 7.150 | 0.15 | 3.34 | 3.52 | 0.00 | 0.09 | 309 | 63.25 |
| 7.200 | 0.15 | 3.47 | 3.64 | 0.00 | 0.09 | 320 | 63.26 |
| 7.250 | 0.16 | 3.59 | 3.77 | 0.00 | 0.09 | 331 | 63.26 |
| 7.300 | 0.16 | 3.72 | 3.91 | 0.00 | 0.09 | 343 | 63.27 |
| 7.350 | 0.17 | 3.85 | 4.04 | 0.00 | 0.10 | 355 | 63.27 |
| 7.400 | 0.17 | 3.98 | 4.18 | 0.00 | 0.10 | 367 | 63.27 |
| 7.450 | 0.17 | 4.11 | 4.32 | 0.00 | 0.10 | 380 | 63.28 |
| 7.500 | 0.18 | 4.25 | 4.47 | 0.00 | 0.11 | 392 | 63.28 |
| 7.550 | 0.18 | 4.39 | 4.61 | 0.00 | 0.11 | 405 | 63.29 |
| 7.600 | 0.19 | 4.53 | 4.76 | 0.00 | 0.12 | 418 | 63.29 |
| 7.650 | 0.19 | 4.68 | 4.91 | 0.00 | 0.12 | 432 | 63.30 |
| 7.700 | 0.20 | 4.82 | 5.07 | 0.00 | 0.12 | 445 | 63.30 |
| 7.750 | 0.20 | 4.97 | 5.23 | 0.00 | 0.13 | 459 | 63.30 |
| 7.800 | 0.21 | 5.12 | 5.39 | 0.00 | 0.13 | 473 | 63.31 |
| 7.850 | 0.21 | 5.28 | 5.55 | 0.00 | 0.13 | 487 | 63.31 |
| 7.900 | 0.22 | 5.44 | 5.71 | 0.00 | 0.14 | 502 | 63.32 |
| 7.950 | 0.23 | 5.59 | 5.88 | 0.00 | 0.14 | 516 | 63.32 |
| 8.000 | 0.23 | 5.76 | 6.05 | 0.00 | 0.15 | 531 | 63.33 |
| 8.050 | 0.24 | 5.92 | 6.22 | 0.00 | 0.15 | 546 | 63.33 |
| 8.100 | 0.24 | 6.09 | 6.40 | 0.00 | 0.16 | 562 | 63.34 |
| 8.150 | 0.25 | 6.26 | 6.58 | 0.00 | 0.16 | 578 | 63.34 |
| 8.200 | 0.26 | 6.44 | 6.77 | 0.00 | 0.16 | 594 | 63.35 |
| 8.250 | 0.27 | 6.63 | 6.96 | 0.00 | 0.17 | 612 | 63.36 |
| 8.300 | 0.28 | 6.82 | 7.17 | 0.00 | 0.17 | 629 | 63.36 |
| 8.350 | 0.28 | 7.02 | 7.38 | 0.00 | 0.18 | 648 | 63.37 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.29 | 7.23 | 7.60 | 0.00 | 0.18 | 667 | 63.37 |
| 8.450 | 0.30 | 7.45 | 7.83 | 0.00 | 0.19 | 687 | 63.38 |
| 8.500 | 0.31 | 7.67 | 8.07 | 0.00 | 0.20 | 708 | 63.39 |
| 8.550 | 0.32 | 7.91 | 8.31 | 0.00 | 0.20 | 730 | 63.40 |
| 8.600 | 0.33 | 8.15 | 8.56 | 0.00 | 0.21 | 752 | 63.40 |
| 8.650 | 0.34 | 8.40 | 8.82 | 0.00 | 0.21 | 775 | 63.41 |
| 8.700 | 0.35 | 8.65 | 9.09 | 0.00 | 0.22 | 798 | 63.42 |
| 8.750 | 0.36 | 8.91 | 9.37 | 0.00 | 0.23 | 823 | 63.43 |
| 8.800 | 0.37 | 9.19 | 9.65 | 0.00 | 0.23 | 848 | 63.44 |
| 8.850 | 0.39 | 9.46 | 9.95 | 0.00 | 0.24 | 873 | 63.44 |
| 8.900 | 0.40 | 9.75 | 10.25 | 0.00 | 0.25 | 900 | 63.45 |
| 8.950 | 0.41 | 10.04 | 10.55 | 0.00 | 0.26 | 927 | 63.46 |
| 9.000 | 0.42 | 10.34 | 10.87 | 0.00 | 0.26 | 954 | 63.47 |
| 9.050 | 0.43 | 10.65 | 11.19 | 0.00 | 0.27 | 983 | 63.48 |
| 9.100 | 0.44 | 10.96 | 11.52 | 0.00 | 0.28 | 1,012 | 63.49 |
| 9.150 | 0.45 | 11.28 | 11.86 | 0.00 | 0.29 | 1,041 | 63.50 |
| 9.200 | 0.47 | 11.61 | 12.20 | 0.00 | 0.30 | 1,072 | 63.51 |
| 9.250 | 0.48 | 11.95 | 12.55 | 0.00 | 0.30 | 1,102 | 63.52 |
| 9.300 | 0.49 | 12.29 | 12.91 | 0.00 | 0.31 | 1,134 | 63.53 |
| 9.350 | 0.50 | 12.63 | 13.28 | 0.00 | 0.32 | 1,166 | 63.54 |
| 9.400 | 0.51 | 12.99 | 13.65 | 0.00 | 0.33 | 1,199 | 63.55 |
| 9.450 | 0.53 | 13.35 | 14.03 | 0.00 | 0.34 | 1,232 | 63.56 |
| 9.500 | 0.54 | 13.72 | 14.42 | 0.00 | 0.35 | 1,266 | 63.58 |
| 9.550 | 0.55 | 14.09 | 14.81 | 0.00 | 0.36 | 1,301 | 63.59 |
| 9.600 | 0.57 | 14.47 | 15.21 | 0.00 | 0.37 | 1,336 | 63.60 |
| 9.650 | 0.58 | 14.86 | 15.62 | 0.00 | 0.38 | 1,371 | 63.61 |
| 9.700 | 0.59 | 15.25 | 16.03 | 0.00 | 0.39 | 1,408 | 63.62 |
| 9.750 | 0.61 | 15.65 | 16.45 | 0.00 | 0.40 | 1,444 | 63.64 |
| 9.800 | 0.62 | 16.06 | 16.87 | 0.00 | 0.41 | 1,482 | 63.65 |
| 9.850 | 0.63 | 16.46 | 17.31 | 0.00 | 0.42 | 1,507 | 63.66 |
| 9.900 | 0.65 | 16.87 | 17.74 | 0.00 | 0.44 | 1,531 | 63.66 |
| 9.950 | 0.66 | 17.28 | 18.17 | 0.00 | 0.45 | 1,554 | 63.67 |
| 10.000 | 0.67 | 17.69 | 18.61 | 0.00 | 0.46 | 1,578 | 63.68 |
| 10.050 | 0.69 | 18.10 | 19.05 | 0.00 | 0.47 | 1,602 | 63.69 |
| 10.100 | 0.70 | 18.51 | 19.49 | 0.00 | 0.49 | 1,626 | 63.70 |
| 10.150 | 0.72 | 18.94 | 19.94 | 0.00 | 0.50 | 1,651 | 63.71 |
| 10.200 | 0.74 | 19.38 | 20.41 | 0.00 | 0.52 | 1,676 | 63.71 |
| 10.250 | 0.77 | 19.83 | 20.89 | 0.00 | 0.53 | 1,702 | 63.72 |
| 10.300 | 0.79 | 20.30 | 21.39 | 0.00 | 0.54 | 1,730 | 63.73 |
| 10.350 | 0.82 | 20.78 | 21.90 | 0.00 | 0.56 | 1,758 | 63.74 |
| 10.400 | 0.84 | 21.28 | 22.44 | 0.00 | 0.58 | 1,787 | 63.75 |
| 10.450 | 0.86 | 21.80 | 22.99 | 0.00 | 0.59 | 1,817 | 63.76 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.89 | 22.34 | 23.56 | 0.00 | 0.61 | 1,848 | 63.77 |
| 10.550 | 0.91 | 22.88 | 24.14 | 0.00 | 0.63 | 1,880 | 63.78 |
| 10.600 | 0.94 | 23.45 | 24.74 | 0.00 | 0.65 | 1,912 | 63.79 |
| 10.650 | 0.97 | 24.03 | 25.36 | 0.00 | 0.66 | 1,946 | 63.80 |
| 10.700 | 0.99 | 24.62 | 25.99 | 0.00 | 0.68 | 1,980 | 63.82 |
| 10.750 | 1.02 | 25.23 | 26.63 | 0.00 | 0.70 | 2,016 | 63.83 |
| 10.800 | 1.05 | 25.85 | 27.29 | 0.00 | 0.72 | 2,052 | 63.84 |
| 10.850 | 1.07 | 26.48 | 27.97 | 0.00 | 0.74 | 2,088 | 63.85 |
| 10.900 | 1.10 | 27.12 | 28.65 | 0.00 | 0.76 | 2,126 | 63.87 |
| 10.950 | 1.13 | 27.78 | 29.35 | 0.00 | 0.78 | 2,164 | 63.88 |
| 11.000 | 1.16 | 28.45 | 30.07 | 0.00 | 0.81 | 2,203 | 63.89 |
| 11.050 | 1.19 | 29.14 | 30.80 | 0.00 | 0.83 | 2,259 | 63.90 |
| 11.100 | 1.24 | 29.86 | 31.57 | 0.00 | 0.85 | 2,351 | 63.92 |
| 11.150 | 1.29 | 30.64 | 32.39 | 0.00 | 0.88 | 2,450 | 63.93 |
| 11.200 | 1.37 | 31.49 | 33.30 | 0.00 | 0.90 | 2,559 | 63.95 |
| 11.250 | 1.45 | 32.44 | 34.31 | 0.00 | 0.93 | 2,681 | 63.97 |
| 11.300 | 1.54 | 33.49 | 35.43 | 0.00 | 0.97 | 2,815 | 63.99 |
| 11.350 | 1.63 | 34.65 | 36.66 | 0.00 | 1.01 | 2,962 | 64.01 |
| 11.400 | 1.72 | 35.90 | 37.99 | 0.00 | 1.05 | 3,123 | 64.04 |
| 11.450 | 1.81 | 37.25 | 39.43 | 0.00 | 1.09 | 3,296 | 64.06 |
| 11.500 | 1.91 | 38.70 | 40.97 | 0.00 | 1.14 | 3,481 | 64.09 |
| 11.550 | 2.08 | 40.32 | 42.69 | 0.00 | 1.19 | 3,687 | 64.12 |
| 11.600 | 2.41 | 42.30 | 44.80 | 0.00 | 1.25 | 3,920 | 64.16 |
| 11.650 | 2.87 | 44.91 | 47.58 | 0.00 | 1.33 | 4,164 | 64.20 |
| 11.700 | 3.56 | 48.46 | 51.35 | 0.00 | 1.44 | 4,495 | 64.25 |
| 11.750 | 4.33 | 53.17 | 56.35 | 0.00 | 1.59 | 4,934 | 64.32 |
| 11.800 | 5.20 | 59.14 | 62.70 | 0.00 | 1.78 | 5,491 | 64.40 |
| 11.850 | 6.07 | 66.39 | 70.41 | 0.00 | 2.01 | 6,161 | 64.51 |
| 11.900 | 7.04 | 74.94 | 79.50 | 0.00 | 2.28 | 6,951 | 64.63 |
| 11.950 | 8.64 | 85.28 | 90.62 | 0.00 | 2.67 | 7,922 | 64.78 |
| 12.000 | 11.74 | 99.22 | 105.65 | 0.00 | 3.21 | 9,227 | 64.99 |
| 12.050 | 14.60 | 117.58 | 125.56 | 0.00 | 3.99 | 10,950 | 65.27 |
| 12.100 | 16.18 | 138.44 | 148.36 | 0.00 | 4.96 | 12,909 | 65.60 |
| 12.150 | 16.11 | 158.62 | 170.72 | 0.00 | 6.05 | 14,841 | 65.93 |
| 12.200 | 13.79 | 174.60 | 188.52 | 0.00 | 6.96 | 16,347 | 66.20 |
| 12.250 | 11.21 | 184.39 | 199.59 | 0.00 | 7.60 | 17,309 | 66.38 |
| 12.300 | 9.39 | 189.16 | 204.98 | 0.00 | 7.91 | 17,760 | 66.46 |
| 12.350 | 8.09 | 190.61 | 206.63 | 0.00 | 8.01 | 17,897 | 66.49 |
| 12.400 | 6.96 | 189.76 | 205.67 | 0.00 | 7.95 | 17,817 | 66.47 |
| 12.450 | 5.96 | 187.12 | 202.68 | 0.00 | 7.78 | 17,570 | 66.43 |
| 12.500 | 4.96 | 183.03 | 198.05 | 0.00 | 7.51 | 17,174 | 66.35 |
| 12.550 | 4.10 | 177.76 | 192.09 | 0.00 | 7.17 | 16,657 | 66.26 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|-----------------|--|----------------------------------|----------------------------------|--------------------------------------|---------------------------------------|------------------------------|-------------------|
| 12.600 | 3.40 | 171.72 | 185.26 | 0.00 | 6.77 | 16,064 | 66.15 |
| 12.650 | 2.90 | 165.19 | 178.02 | 0.00 | 6.41 | 15,455 | 66.04 |
| 12.700 | 2.60 | 158.60 | 170.70 | 0.00 | 6.05 | 14,839 | 65.93 |
| 12.750 | 2.42 | 152.23 | 163.62 | 0.00 | 5.70 | 14,229 | 65.82 |
| 12.800 | 2.28 | 146.20 | 156.93 | 0.00 | 5.36 | 13,647 | 65.72 |
| 12.850 | 2.16 | 140.52 | 150.64 | 0.00 | 5.06 | 13,104 | 65.63 |
| 12.900 | 2.05 | 135.12 | 144.73 | 0.00 | 4.81 | 12,600 | 65.54 |
| 12.950 | 1.95 | 129.99 | 139.12 | 0.00 | 4.57 | 12,122 | 65.46 |
| 13.000 | 1.85 | 125.11 | 133.79 | 0.00 | 4.34 | 11,666 | 65.39 |
| 13.050 | 1.76 | 120.47 | 128.72 | 0.00 | 4.12 | 11,224 | 65.32 |
| 13.100 | 1.68 | 116.08 | 123.91 | 0.00 | 3.92 | 10,806 | 65.25 |
| 13.150 | 1.62 | 111.93 | 119.38 | 0.00 | 3.73 | 10,411 | 65.18 |
| 13.200 | 1.58 | 108.02 | 115.13 | 0.00 | 3.56 | 10,043 | 65.12 |
| 13.250 | 1.55 | 104.31 | 111.14 | 0.00 | 3.41 | 9,699 | 65.07 |
| 13.300 | 1.52 | 100.82 | 107.38 | 0.00 | 3.28 | 9,375 | 65.01 |
| 13.350 | 1.49 | 97.53 | 103.83 | 0.00 | 3.15 | 9,070 | 64.97 |
| 13.400 | 1.46 | 94.43 | 100.48 | 0.00 | 3.03 | 8,782 | 64.92 |
| 13.450 | 1.44 | 91.50 | 97.33 | 0.00 | 2.91 | 8,508 | 64.88 |
| 13.500 | 1.41 | 88.74 | 94.35 | 0.00 | 2.81 | 8,247 | 64.83 |
| 13.550 | 1.38 | 86.12 | 91.53 | 0.00 | 2.70 | 8,001 | 64.80 |
| 13.600 | 1.36 | 83.65 | 88.87 | 0.00 | 2.61 | 7,768 | 64.76 |
| 13.650 | 1.33 | 81.31 | 86.34 | 0.00 | 2.52 | 7,548 | 64.72 |
| 13.700 | 1.31 | 79.09 | 83.95 | 0.00 | 2.43 | 7,339 | 64.69 |
| 13.750 | 1.28 | 76.98 | 81.68 | 0.00 | 2.35 | 7,140 | 64.66 |
| 13.800 | 1.25 | 74.96 | 79.52 | 0.00 | 2.28 | 6,952 | 64.63 |
| 13.850 | 1.23 | 73.01 | 77.44 | 0.00 | 2.22 | 6,772 | 64.60 |
| 13.900 | 1.20 | 71.12 | 75.44 | 0.00 | 2.16 | 6,598 | 64.57 |
| 13.950 | 1.18 | 69.30 | 73.50 | 0.00 | 2.10 | 6,430 | 64.55 |
| 14.000 | 1.15 | 67.53 | 71.63 | 0.00 | 2.05 | 6,267 | 64.52 |
| 14.050 | 1.13 | 65.83 | 69.81 | 0.00 | 1.99 | 6,109 | 64.50 |
| 14.100 | 1.10 | 64.18 | 68.05 | 0.00 | 1.94 | 5,956 | 64.47 |
| 14.150 | 1.08 | 62.58 | 66.36 | 0.00 | 1.89 | 5,809 | 64.45 |
| 14.200 | 1.07 | 61.05 | 64.74 | 0.00 | 1.84 | 5,668 | 64.43 |
| 14.250 | 1.05 | 59.59 | 63.18 | 0.00 | 1.79 | 5,533 | 64.41 |
| 14.300 | 1.04 | 58.18 | 61.68 | 0.00 | 1.75 | 5,402 | 64.39 |
| 14.350 | 1.03 | 56.84 | 60.25 | 0.00 | 1.71 | 5,277 | 64.37 |
| 14.400 | 1.02 | 55.55 | 58.88 | 0.00 | 1.67 | 5,156 | 64.35 |
| 14.450 | 1.00 | 54.31 | 57.57 | 0.00 | 1.63 | 5,041 | 64.33 |
| 14.500 | 0.99 | 53.12 | 56.31 | 0.00 | 1.59 | 4,930 | 64.31 |
| 14.550 | 0.98 | 51.98 | 55.09 | 0.00 | 1.56 | 4,823 | 64.30 |
| 14.600 | 0.97 | 50.89 | 53.93 | 0.00 | 1.52 | 4,721 | 64.28 |
| 14.650 | 0.95 | 49.83 | 52.81 | 0.00 | 1.49 | 4,623 | 64.27 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.94 | 48.81 | 51.73 | 0.00 | 1.46 | 4,528 | 64.25 |
| 14.750 | 0.93 | 47.83 | 50.68 | 0.00 | 1.42 | 4,436 | 64.24 |
| 14.800 | 0.92 | 46.89 | 49.68 | 0.00 | 1.39 | 4,348 | 64.22 |
| 14.850 | 0.90 | 45.98 | 48.71 | 0.00 | 1.37 | 4,263 | 64.21 |
| 14.900 | 0.89 | 45.09 | 47.77 | 0.00 | 1.34 | 4,181 | 64.20 |
| 14.950 | 0.88 | 44.24 | 46.86 | 0.00 | 1.31 | 4,101 | 64.19 |
| 15.000 | 0.87 | 43.41 | 45.98 | 0.00 | 1.29 | 4,024 | 64.17 |
| 15.050 | 0.85 | 42.61 | 45.13 | 0.00 | 1.26 | 3,949 | 64.16 |
| 15.100 | 0.84 | 41.83 | 44.31 | 0.00 | 1.24 | 3,876 | 64.15 |
| 15.150 | 0.83 | 41.08 | 43.50 | 0.00 | 1.21 | 3,784 | 64.14 |
| 15.200 | 0.81 | 40.35 | 42.72 | 0.00 | 1.19 | 3,690 | 64.12 |
| 15.250 | 0.80 | 39.63 | 41.96 | 0.00 | 1.16 | 3,599 | 64.11 |
| 15.300 | 0.79 | 38.94 | 41.23 | 0.00 | 1.14 | 3,511 | 64.10 |
| 15.350 | 0.78 | 38.26 | 40.51 | 0.00 | 1.12 | 3,425 | 64.08 |
| 15.400 | 0.76 | 37.61 | 39.81 | 0.00 | 1.10 | 3,340 | 64.07 |
| 15.450 | 0.75 | 36.96 | 39.12 | 0.00 | 1.08 | 3,258 | 64.06 |
| 15.500 | 0.74 | 36.34 | 38.45 | 0.00 | 1.06 | 3,178 | 64.05 |
| 15.550 | 0.73 | 35.72 | 37.80 | 0.00 | 1.04 | 3,100 | 64.03 |
| 15.600 | 0.71 | 35.12 | 37.16 | 0.00 | 1.02 | 3,023 | 64.02 |
| 15.650 | 0.70 | 34.53 | 36.54 | 0.00 | 1.00 | 2,948 | 64.01 |
| 15.700 | 0.69 | 33.96 | 35.92 | 0.00 | 0.98 | 2,874 | 64.00 |
| 15.750 | 0.68 | 33.39 | 35.32 | 0.00 | 0.96 | 2,802 | 63.99 |
| 15.800 | 0.66 | 32.83 | 34.73 | 0.00 | 0.95 | 2,731 | 63.98 |
| 15.850 | 0.65 | 32.29 | 34.15 | 0.00 | 0.93 | 2,661 | 63.97 |
| 15.900 | 0.64 | 31.75 | 33.57 | 0.00 | 0.91 | 2,592 | 63.96 |
| 15.950 | 0.62 | 31.22 | 33.01 | 0.00 | 0.90 | 2,525 | 63.95 |
| 16.000 | 0.61 | 30.70 | 32.46 | 0.00 | 0.88 | 2,458 | 63.94 |
| 16.050 | 0.60 | 30.19 | 31.91 | 0.00 | 0.86 | 2,393 | 63.93 |
| 16.100 | 0.59 | 29.69 | 31.38 | 0.00 | 0.85 | 2,329 | 63.92 |
| 16.150 | 0.58 | 29.20 | 30.86 | 0.00 | 0.83 | 2,266 | 63.91 |
| 16.200 | 0.57 | 28.72 | 30.35 | 0.00 | 0.82 | 2,218 | 63.90 |
| 16.250 | 0.57 | 28.26 | 29.86 | 0.00 | 0.80 | 2,192 | 63.89 |
| 16.300 | 0.56 | 27.82 | 29.39 | 0.00 | 0.79 | 2,166 | 63.88 |
| 16.350 | 0.56 | 27.39 | 28.93 | 0.00 | 0.77 | 2,141 | 63.87 |
| 16.400 | 0.55 | 26.97 | 28.49 | 0.00 | 0.76 | 2,117 | 63.86 |
| 16.450 | 0.54 | 26.58 | 28.07 | 0.00 | 0.75 | 2,094 | 63.85 |
| 16.500 | 0.54 | 26.19 | 27.66 | 0.00 | 0.73 | 2,071 | 63.85 |
| 16.550 | 0.53 | 25.82 | 27.26 | 0.00 | 0.72 | 2,050 | 63.84 |
| 16.600 | 0.53 | 25.46 | 26.88 | 0.00 | 0.71 | 2,029 | 63.83 |
| 16.650 | 0.52 | 25.11 | 26.51 | 0.00 | 0.70 | 2,009 | 63.83 |
| 16.700 | 0.52 | 24.77 | 26.15 | 0.00 | 0.69 | 1,989 | 63.82 |
| 16.750 | 0.51 | 24.44 | 25.80 | 0.00 | 0.68 | 1,970 | 63.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.51 | 24.12 | 25.46 | 0.00 | 0.67 | 1,952 | 63.81 |
| 16.850 | 0.50 | 23.81 | 25.13 | 0.00 | 0.66 | 1,934 | 63.80 |
| 16.900 | 0.49 | 23.51 | 24.81 | 0.00 | 0.65 | 1,916 | 63.79 |
| 16.950 | 0.49 | 23.22 | 24.50 | 0.00 | 0.64 | 1,899 | 63.79 |
| 17.000 | 0.48 | 22.93 | 24.19 | 0.00 | 0.63 | 1,882 | 63.78 |
| 17.050 | 0.48 | 22.65 | 23.89 | 0.00 | 0.62 | 1,866 | 63.78 |
| 17.100 | 0.47 | 22.38 | 23.60 | 0.00 | 0.61 | 1,850 | 63.77 |
| 17.150 | 0.47 | 22.11 | 23.32 | 0.00 | 0.60 | 1,835 | 63.77 |
| 17.200 | 0.46 | 21.85 | 23.04 | 0.00 | 0.59 | 1,820 | 63.76 |
| 17.250 | 0.46 | 21.59 | 22.77 | 0.00 | 0.59 | 1,805 | 63.76 |
| 17.300 | 0.45 | 21.34 | 22.50 | 0.00 | 0.58 | 1,790 | 63.75 |
| 17.350 | 0.44 | 21.10 | 22.24 | 0.00 | 0.57 | 1,776 | 63.75 |
| 17.400 | 0.44 | 20.85 | 21.98 | 0.00 | 0.56 | 1,762 | 63.74 |
| 17.450 | 0.43 | 20.61 | 21.72 | 0.00 | 0.56 | 1,748 | 63.74 |
| 17.500 | 0.43 | 20.38 | 21.48 | 0.00 | 0.55 | 1,734 | 63.73 |
| 17.550 | 0.42 | 20.15 | 21.23 | 0.00 | 0.54 | 1,721 | 63.73 |
| 17.600 | 0.42 | 19.92 | 20.99 | 0.00 | 0.53 | 1,708 | 63.72 |
| 17.650 | 0.41 | 19.70 | 20.75 | 0.00 | 0.53 | 1,695 | 63.72 |
| 17.700 | 0.41 | 19.48 | 20.52 | 0.00 | 0.52 | 1,682 | 63.72 |
| 17.750 | 0.40 | 19.26 | 20.28 | 0.00 | 0.51 | 1,669 | 63.71 |
| 17.800 | 0.39 | 19.05 | 20.06 | 0.00 | 0.50 | 1,657 | 63.71 |
| 17.850 | 0.39 | 18.83 | 19.83 | 0.00 | 0.50 | 1,645 | 63.70 |
| 17.900 | 0.38 | 18.62 | 19.60 | 0.00 | 0.49 | 1,632 | 63.70 |
| 17.950 | 0.38 | 18.41 | 19.38 | 0.00 | 0.48 | 1,620 | 63.70 |
| 18.000 | 0.37 | 18.21 | 19.16 | 0.00 | 0.48 | 1,608 | 63.69 |
| 18.050 | 0.37 | 18.00 | 18.95 | 0.00 | 0.47 | 1,596 | 63.69 |
| 18.100 | 0.36 | 17.80 | 18.73 | 0.00 | 0.46 | 1,585 | 63.68 |
| 18.150 | 0.36 | 17.61 | 18.52 | 0.00 | 0.46 | 1,573 | 63.68 |
| 18.200 | 0.36 | 17.42 | 18.32 | 0.00 | 0.45 | 1,562 | 63.68 |
| 18.250 | 0.35 | 17.23 | 18.13 | 0.00 | 0.45 | 1,552 | 63.67 |
| 18.300 | 0.35 | 17.06 | 17.94 | 0.00 | 0.44 | 1,542 | 63.67 |
| 18.350 | 0.35 | 16.89 | 17.76 | 0.00 | 0.44 | 1,532 | 63.67 |
| 18.400 | 0.35 | 16.73 | 17.59 | 0.00 | 0.43 | 1,522 | 63.66 |
| 18.450 | 0.35 | 16.57 | 17.43 | 0.00 | 0.43 | 1,514 | 63.66 |
| 18.500 | 0.35 | 16.43 | 17.27 | 0.00 | 0.42 | 1,505 | 63.66 |
| 18.550 | 0.34 | 16.28 | 17.12 | 0.00 | 0.42 | 1,497 | 63.65 |
| 18.600 | 0.34 | 16.15 | 16.97 | 0.00 | 0.41 | 1,489 | 63.65 |
| 18.650 | 0.34 | 16.01 | 16.83 | 0.00 | 0.41 | 1,478 | 63.65 |
| 18.700 | 0.34 | 15.88 | 16.69 | 0.00 | 0.40 | 1,466 | 63.64 |
| 18.750 | 0.34 | 15.76 | 16.56 | 0.00 | 0.40 | 1,454 | 63.64 |
| 18.800 | 0.34 | 15.63 | 16.43 | 0.00 | 0.40 | 1,443 | 63.64 |
| 18.850 | 0.33 | 15.51 | 16.30 | 0.00 | 0.40 | 1,432 | 63.63 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.33 | 15.40 | 16.18 | 0.00 | 0.39 | 1,421 | 63.63 |
| 18.950 | 0.33 | 15.28 | 16.06 | 0.00 | 0.39 | 1,410 | 63.62 |
| 19.000 | 0.33 | 15.17 | 15.94 | 0.00 | 0.39 | 1,400 | 63.62 |
| 19.050 | 0.33 | 15.06 | 15.82 | 0.00 | 0.38 | 1,390 | 63.62 |
| 19.100 | 0.33 | 14.95 | 15.71 | 0.00 | 0.38 | 1,380 | 63.61 |
| 19.150 | 0.32 | 14.84 | 15.60 | 0.00 | 0.38 | 1,370 | 63.61 |
| 19.200 | 0.32 | 14.74 | 15.49 | 0.00 | 0.38 | 1,360 | 63.61 |
| 19.250 | 0.32 | 14.63 | 15.38 | 0.00 | 0.37 | 1,351 | 63.60 |
| 19.300 | 0.32 | 14.53 | 15.27 | 0.00 | 0.37 | 1,341 | 63.60 |
| 19.350 | 0.32 | 14.43 | 15.17 | 0.00 | 0.37 | 1,332 | 63.60 |
| 19.400 | 0.32 | 14.34 | 15.07 | 0.00 | 0.37 | 1,323 | 63.60 |
| 19.450 | 0.31 | 14.24 | 14.97 | 0.00 | 0.36 | 1,314 | 63.59 |
| 19.500 | 0.31 | 14.15 | 14.87 | 0.00 | 0.36 | 1,306 | 63.59 |
| 19.550 | 0.31 | 14.05 | 14.77 | 0.00 | 0.36 | 1,297 | 63.59 |
| 19.600 | 0.31 | 13.96 | 14.67 | 0.00 | 0.36 | 1,289 | 63.58 |
| 19.650 | 0.31 | 13.87 | 14.58 | 0.00 | 0.35 | 1,280 | 63.58 |
| 19.700 | 0.31 | 13.78 | 14.49 | 0.00 | 0.35 | 1,272 | 63.58 |
| 19.750 | 0.30 | 13.69 | 14.39 | 0.00 | 0.35 | 1,264 | 63.58 |
| 19.800 | 0.30 | 13.61 | 14.30 | 0.00 | 0.35 | 1,256 | 63.57 |
| 19.850 | 0.30 | 13.52 | 14.21 | 0.00 | 0.34 | 1,248 | 63.57 |
| 19.900 | 0.30 | 13.44 | 14.12 | 0.00 | 0.34 | 1,240 | 63.57 |
| 19.950 | 0.30 | 13.35 | 14.03 | 0.00 | 0.34 | 1,232 | 63.56 |
| 20.000 | 0.30 | 13.27 | 13.95 | 0.00 | 0.34 | 1,225 | 63.56 |
| 20.050 | 0.29 | 13.19 | 13.86 | 0.00 | 0.34 | 1,217 | 63.56 |
| 20.100 | 0.29 | 13.11 | 13.78 | 0.00 | 0.33 | 1,210 | 63.56 |
| 20.150 | 0.29 | 13.03 | 13.69 | 0.00 | 0.33 | 1,202 | 63.55 |
| 20.200 | 0.29 | 12.95 | 13.61 | 0.00 | 0.33 | 1,195 | 63.55 |
| 20.250 | 0.29 | 12.87 | 13.53 | 0.00 | 0.33 | 1,188 | 63.55 |
| 20.300 | 0.29 | 12.80 | 13.45 | 0.00 | 0.33 | 1,181 | 63.55 |
| 20.350 | 0.29 | 12.72 | 13.37 | 0.00 | 0.32 | 1,174 | 63.55 |
| 20.400 | 0.28 | 12.65 | 13.29 | 0.00 | 0.32 | 1,167 | 63.54 |
| 20.450 | 0.28 | 12.58 | 13.22 | 0.00 | 0.32 | 1,161 | 63.54 |
| 20.500 | 0.28 | 12.50 | 13.14 | 0.00 | 0.32 | 1,154 | 63.54 |
| 20.550 | 0.28 | 12.43 | 13.07 | 0.00 | 0.32 | 1,148 | 63.54 |
| 20.600 | 0.28 | 12.36 | 12.99 | 0.00 | 0.32 | 1,141 | 63.53 |
| 20.650 | 0.28 | 12.30 | 12.92 | 0.00 | 0.31 | 1,135 | 63.53 |
| 20.700 | 0.28 | 12.23 | 12.85 | 0.00 | 0.31 | 1,129 | 63.53 |
| 20.750 | 0.28 | 12.16 | 12.78 | 0.00 | 0.31 | 1,122 | 63.53 |
| 20.800 | 0.27 | 12.09 | 12.71 | 0.00 | 0.31 | 1,116 | 63.53 |
| 20.850 | 0.27 | 12.03 | 12.64 | 0.00 | 0.31 | 1,110 | 63.52 |
| 20.900 | 0.27 | 11.97 | 12.58 | 0.00 | 0.31 | 1,104 | 63.52 |
| 20.950 | 0.27 | 11.90 | 12.51 | 0.00 | 0.30 | 1,099 | 63.52 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.27 | 11.84 | 12.44 | 0.00 | 0.30 | 1,093 | 63.52 |
| 21.050 | 0.27 | 11.78 | 12.38 | 0.00 | 0.30 | 1,087 | 63.52 |
| 21.100 | 0.27 | 11.72 | 12.32 | 0.00 | 0.30 | 1,082 | 63.51 |
| 21.150 | 0.27 | 11.66 | 12.25 | 0.00 | 0.30 | 1,076 | 63.51 |
| 21.200 | 0.26 | 11.60 | 12.19 | 0.00 | 0.30 | 1,070 | 63.51 |
| 21.250 | 0.26 | 11.54 | 12.13 | 0.00 | 0.29 | 1,065 | 63.51 |
| 21.300 | 0.26 | 11.48 | 12.06 | 0.00 | 0.29 | 1,059 | 63.51 |
| 21.350 | 0.26 | 11.42 | 12.00 | 0.00 | 0.29 | 1,054 | 63.50 |
| 21.400 | 0.26 | 11.36 | 11.94 | 0.00 | 0.29 | 1,049 | 63.50 |
| 21.450 | 0.26 | 11.30 | 11.88 | 0.00 | 0.29 | 1,043 | 63.50 |
| 21.500 | 0.26 | 11.25 | 11.82 | 0.00 | 0.29 | 1,038 | 63.50 |
| 21.550 | 0.26 | 11.19 | 11.76 | 0.00 | 0.29 | 1,033 | 63.50 |
| 21.600 | 0.25 | 11.13 | 11.70 | 0.00 | 0.28 | 1,027 | 63.50 |
| 21.650 | 0.25 | 11.08 | 11.64 | 0.00 | 0.28 | 1,022 | 63.49 |
| 21.700 | 0.25 | 11.02 | 11.58 | 0.00 | 0.28 | 1,017 | 63.49 |
| 21.750 | 0.25 | 10.96 | 11.52 | 0.00 | 0.28 | 1,012 | 63.49 |
| 21.800 | 0.25 | 10.91 | 11.46 | 0.00 | 0.28 | 1,007 | 63.49 |
| 21.850 | 0.25 | 10.85 | 11.41 | 0.00 | 0.28 | 1,002 | 63.49 |
| 21.900 | 0.25 | 10.80 | 11.35 | 0.00 | 0.28 | 997 | 63.49 |
| 21.950 | 0.25 | 10.75 | 11.29 | 0.00 | 0.27 | 992 | 63.48 |
| 22.000 | 0.24 | 10.69 | 11.24 | 0.00 | 0.27 | 987 | 63.48 |
| 22.050 | 0.24 | 10.64 | 11.18 | 0.00 | 0.27 | 982 | 63.48 |
| 22.100 | 0.24 | 10.58 | 11.12 | 0.00 | 0.27 | 977 | 63.48 |
| 22.150 | 0.24 | 10.53 | 11.07 | 0.00 | 0.27 | 972 | 63.48 |
| 22.200 | 0.24 | 10.48 | 11.01 | 0.00 | 0.27 | 967 | 63.48 |
| 22.250 | 0.24 | 10.43 | 10.96 | 0.00 | 0.27 | 962 | 63.47 |
| 22.300 | 0.24 | 10.37 | 10.90 | 0.00 | 0.26 | 957 | 63.47 |
| 22.350 | 0.24 | 10.32 | 10.84 | 0.00 | 0.26 | 952 | 63.47 |
| 22.400 | 0.23 | 10.26 | 10.79 | 0.00 | 0.26 | 947 | 63.47 |
| 22.450 | 0.23 | 10.21 | 10.73 | 0.00 | 0.26 | 943 | 63.47 |
| 22.500 | 0.23 | 10.16 | 10.68 | 0.00 | 0.26 | 938 | 63.47 |
| 22.550 | 0.23 | 10.11 | 10.62 | 0.00 | 0.26 | 933 | 63.46 |
| 22.600 | 0.23 | 10.06 | 10.57 | 0.00 | 0.26 | 928 | 63.46 |
| 22.650 | 0.23 | 10.01 | 10.52 | 0.00 | 0.26 | 923 | 63.46 |
| 22.700 | 0.23 | 9.95 | 10.46 | 0.00 | 0.25 | 919 | 63.46 |
| 22.750 | 0.23 | 9.90 | 10.41 | 0.00 | 0.25 | 914 | 63.46 |
| 22.800 | 0.22 | 9.85 | 10.35 | 0.00 | 0.25 | 909 | 63.46 |
| 22.850 | 0.22 | 9.80 | 10.30 | 0.00 | 0.25 | 904 | 63.45 |
| 22.900 | 0.22 | 9.75 | 10.25 | 0.00 | 0.25 | 900 | 63.45 |
| 22.950 | 0.22 | 9.70 | 10.19 | 0.00 | 0.25 | 895 | 63.45 |
| 23.000 | 0.22 | 9.65 | 10.14 | 0.00 | 0.25 | 890 | 63.45 |
| 23.050 | 0.22 | 9.60 | 10.09 | 0.00 | 0.24 | 886 | 63.45 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: MC-3500 - 3 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.22 | 9.54 | 10.03 | 0.00 | 0.24 | 881 | 63.45 |
| 23.150 | 0.22 | 9.49 | 9.98 | 0.00 | 0.24 | 876 | 63.44 |
| 23.200 | 0.21 | 9.44 | 9.92 | 0.00 | 0.24 | 871 | 63.44 |
| 23.250 | 0.21 | 9.39 | 9.87 | 0.00 | 0.24 | 867 | 63.44 |
| 23.300 | 0.21 | 9.34 | 9.82 | 0.00 | 0.24 | 862 | 63.44 |
| 23.350 | 0.21 | 9.29 | 9.76 | 0.00 | 0.24 | 857 | 63.44 |
| 23.400 | 0.21 | 9.24 | 9.71 | 0.00 | 0.24 | 853 | 63.44 |
| 23.450 | 0.21 | 9.19 | 9.66 | 0.00 | 0.23 | 848 | 63.44 |
| 23.500 | 0.21 | 9.14 | 9.61 | 0.00 | 0.23 | 844 | 63.43 |
| 23.550 | 0.21 | 9.09 | 9.55 | 0.00 | 0.23 | 839 | 63.43 |
| 23.600 | 0.20 | 9.04 | 9.50 | 0.00 | 0.23 | 834 | 63.43 |
| 23.650 | 0.20 | 8.99 | 9.45 | 0.00 | 0.23 | 830 | 63.43 |
| 23.700 | 0.20 | 8.94 | 9.39 | 0.00 | 0.23 | 825 | 63.43 |
| 23.750 | 0.20 | 8.89 | 9.34 | 0.00 | 0.23 | 820 | 63.43 |
| 23.800 | 0.20 | 8.84 | 9.29 | 0.00 | 0.23 | 816 | 63.42 |
| 23.850 | 0.20 | 8.79 | 9.24 | 0.00 | 0.22 | 811 | 63.42 |
| 23.900 | 0.20 | 8.74 | 9.18 | 0.00 | 0.22 | 806 | 63.42 |
| 23.950 | 0.20 | 8.69 | 9.13 | 0.00 | 0.22 | 802 | 63.42 |
| 24.000 | 0.19 | 8.63 | 9.08 | 0.00 | 0.22 | 797 | 63.42 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 2.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 63.15 |
| 3.300 | 0.00 | 0.01 | 0.01 | 0.00 | 0.00 | 0 | 63.15 |
| 3.350 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 | 1 | 63.15 |
| 3.400 | 0.01 | 0.02 | 0.03 | 0.00 | 0.00 | 2 | 63.15 |
| 3.450 | 0.01 | 0.04 | 0.04 | 0.00 | 0.00 | 4 | 63.15 |
| 3.500 | 0.01 | 0.06 | 0.07 | 0.00 | 0.00 | 6 | 63.15 |
| 3.550 | 0.02 | 0.09 | 0.09 | 0.00 | 0.00 | 8 | 63.15 |
| 3.600 | 0.02 | 0.12 | 0.13 | 0.00 | 0.00 | 11 | 63.15 |
| 3.650 | 0.02 | 0.15 | 0.16 | 0.00 | 0.00 | 14 | 63.15 |
| 3.700 | 0.03 | 0.19 | 0.20 | 0.00 | 0.00 | 18 | 63.16 |
| 3.750 | 0.03 | 0.23 | 0.25 | 0.00 | 0.01 | 22 | 63.16 |
| 3.800 | 0.03 | 0.28 | 0.30 | 0.00 | 0.01 | 26 | 63.16 |
| 3.850 | 0.03 | 0.33 | 0.35 | 0.00 | 0.01 | 31 | 63.16 |
| 3.900 | 0.04 | 0.38 | 0.40 | 0.00 | 0.01 | 35 | 63.16 |
| 3.950 | 0.04 | 0.44 | 0.46 | 0.00 | 0.01 | 41 | 63.16 |
| 4.000 | 0.04 | 0.50 | 0.53 | 0.00 | 0.01 | 46 | 63.17 |
| 4.050 | 0.05 | 0.56 | 0.59 | 0.00 | 0.01 | 52 | 63.17 |
| 4.100 | 0.05 | 0.63 | 0.66 | 0.00 | 0.02 | 58 | 63.17 |
| 4.150 | 0.05 | 0.70 | 0.73 | 0.00 | 0.02 | 64 | 63.17 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.06 | 0.77 | 0.81 | 0.00 | 0.02 | 71 | 63.17 |
| 4.250 | 0.06 | 0.84 | 0.89 | 0.00 | 0.02 | 78 | 63.18 |
| 4.300 | 0.06 | 0.92 | 0.97 | 0.00 | 0.02 | 85 | 63.18 |
| 4.350 | 0.07 | 1.00 | 1.05 | 0.00 | 0.03 | 92 | 63.18 |
| 4.400 | 0.07 | 1.08 | 1.14 | 0.00 | 0.03 | 100 | 63.18 |
| 4.450 | 0.07 | 1.17 | 1.22 | 0.00 | 0.03 | 108 | 63.19 |
| 4.500 | 0.08 | 1.25 | 1.32 | 0.00 | 0.03 | 116 | 63.19 |
| 4.550 | 0.08 | 1.34 | 1.41 | 0.00 | 0.03 | 124 | 63.19 |
| 4.600 | 0.08 | 1.43 | 1.50 | 0.00 | 0.04 | 132 | 63.19 |
| 4.650 | 0.09 | 1.52 | 1.60 | 0.00 | 0.04 | 141 | 63.20 |
| 4.700 | 0.09 | 1.62 | 1.70 | 0.00 | 0.04 | 149 | 63.20 |
| 4.750 | 0.09 | 1.71 | 1.80 | 0.00 | 0.04 | 158 | 63.20 |
| 4.800 | 0.10 | 1.81 | 1.90 | 0.00 | 0.05 | 167 | 63.21 |
| 4.850 | 0.10 | 1.91 | 2.01 | 0.00 | 0.05 | 176 | 63.21 |
| 4.900 | 0.10 | 2.01 | 2.11 | 0.00 | 0.05 | 186 | 63.21 |
| 4.950 | 0.11 | 2.11 | 2.22 | 0.00 | 0.05 | 195 | 63.22 |
| 5.000 | 0.11 | 2.22 | 2.33 | 0.00 | 0.06 | 205 | 63.22 |
| 5.050 | 0.11 | 2.32 | 2.44 | 0.00 | 0.06 | 215 | 63.22 |
| 5.100 | 0.12 | 2.43 | 2.56 | 0.00 | 0.06 | 224 | 63.23 |
| 5.150 | 0.12 | 2.54 | 2.67 | 0.00 | 0.06 | 234 | 63.23 |
| 5.200 | 0.12 | 2.65 | 2.79 | 0.00 | 0.07 | 245 | 63.23 |
| 5.250 | 0.13 | 2.76 | 2.90 | 0.00 | 0.07 | 255 | 63.24 |
| 5.300 | 0.13 | 2.87 | 3.02 | 0.00 | 0.07 | 265 | 63.24 |
| 5.350 | 0.13 | 2.99 | 3.14 | 0.00 | 0.08 | 276 | 63.24 |
| 5.400 | 0.14 | 3.10 | 3.26 | 0.00 | 0.08 | 286 | 63.25 |
| 5.450 | 0.14 | 3.22 | 3.38 | 0.00 | 0.08 | 297 | 63.25 |
| 5.500 | 0.15 | 3.34 | 3.51 | 0.00 | 0.09 | 308 | 63.25 |
| 5.550 | 0.15 | 3.46 | 3.63 | 0.00 | 0.09 | 319 | 63.26 |
| 5.600 | 0.15 | 3.57 | 3.76 | 0.00 | 0.09 | 330 | 63.26 |
| 5.650 | 0.16 | 3.70 | 3.88 | 0.00 | 0.09 | 341 | 63.26 |
| 5.700 | 0.16 | 3.82 | 4.01 | 0.00 | 0.10 | 352 | 63.27 |
| 5.750 | 0.16 | 3.94 | 4.14 | 0.00 | 0.10 | 364 | 63.27 |
| 5.800 | 0.17 | 4.06 | 4.27 | 0.00 | 0.10 | 375 | 63.28 |
| 5.850 | 0.17 | 4.19 | 4.40 | 0.00 | 0.11 | 386 | 63.28 |
| 5.900 | 0.17 | 4.31 | 4.53 | 0.00 | 0.11 | 398 | 63.28 |
| 5.950 | 0.18 | 4.44 | 4.66 | 0.00 | 0.11 | 410 | 63.29 |
| 6.000 | 0.18 | 4.56 | 4.80 | 0.00 | 0.12 | 421 | 63.29 |
| 6.050 | 0.19 | 4.69 | 4.93 | 0.00 | 0.12 | 433 | 63.30 |
| 6.100 | 0.19 | 4.82 | 5.07 | 0.00 | 0.12 | 445 | 63.30 |
| 6.150 | 0.19 | 4.95 | 5.20 | 0.00 | 0.13 | 457 | 63.30 |
| 6.200 | 0.20 | 5.09 | 5.35 | 0.00 | 0.13 | 469 | 63.31 |
| 6.250 | 0.21 | 5.23 | 5.49 | 0.00 | 0.13 | 482 | 63.31 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.21 | 5.37 | 5.64 | 0.00 | 0.14 | 495 | 63.32 |
| 6.350 | 0.22 | 5.52 | 5.80 | 0.00 | 0.14 | 509 | 63.32 |
| 6.400 | 0.22 | 5.67 | 5.96 | 0.00 | 0.14 | 523 | 63.33 |
| 6.450 | 0.23 | 5.82 | 6.12 | 0.00 | 0.15 | 538 | 63.33 |
| 6.500 | 0.24 | 5.99 | 6.29 | 0.00 | 0.15 | 552 | 63.34 |
| 6.550 | 0.24 | 6.15 | 6.47 | 0.00 | 0.16 | 568 | 63.34 |
| 6.600 | 0.25 | 6.32 | 6.64 | 0.00 | 0.16 | 583 | 63.35 |
| 6.650 | 0.26 | 6.50 | 6.83 | 0.00 | 0.17 | 599 | 63.35 |
| 6.700 | 0.26 | 6.67 | 7.01 | 0.00 | 0.17 | 616 | 63.36 |
| 6.750 | 0.27 | 6.86 | 7.21 | 0.00 | 0.17 | 633 | 63.36 |
| 6.800 | 0.28 | 7.04 | 7.40 | 0.00 | 0.18 | 650 | 63.37 |
| 6.850 | 0.28 | 7.23 | 7.60 | 0.00 | 0.18 | 668 | 63.37 |
| 6.900 | 0.29 | 7.43 | 7.81 | 0.00 | 0.19 | 686 | 63.38 |
| 6.950 | 0.30 | 7.63 | 8.02 | 0.00 | 0.19 | 704 | 63.39 |
| 7.000 | 0.30 | 7.83 | 8.23 | 0.00 | 0.20 | 723 | 63.39 |
| 7.050 | 0.31 | 8.04 | 8.45 | 0.00 | 0.20 | 742 | 63.40 |
| 7.100 | 0.32 | 8.25 | 8.67 | 0.00 | 0.21 | 762 | 63.41 |
| 7.150 | 0.33 | 8.47 | 8.90 | 0.00 | 0.22 | 781 | 63.41 |
| 7.200 | 0.33 | 8.69 | 9.13 | 0.00 | 0.22 | 802 | 63.42 |
| 7.250 | 0.34 | 8.91 | 9.36 | 0.00 | 0.23 | 822 | 63.43 |
| 7.300 | 0.35 | 9.14 | 9.60 | 0.00 | 0.23 | 843 | 63.43 |
| 7.350 | 0.36 | 9.37 | 9.84 | 0.00 | 0.24 | 864 | 63.44 |
| 7.400 | 0.37 | 9.60 | 10.09 | 0.00 | 0.24 | 886 | 63.45 |
| 7.450 | 0.37 | 9.84 | 10.34 | 0.00 | 0.25 | 908 | 63.46 |
| 7.500 | 0.38 | 10.08 | 10.59 | 0.00 | 0.26 | 930 | 63.46 |
| 7.550 | 0.39 | 10.33 | 10.85 | 0.00 | 0.26 | 953 | 63.47 |
| 7.600 | 0.40 | 10.57 | 11.11 | 0.00 | 0.27 | 976 | 63.48 |
| 7.650 | 0.41 | 10.83 | 11.38 | 0.00 | 0.28 | 999 | 63.49 |
| 7.700 | 0.41 | 11.08 | 11.65 | 0.00 | 0.28 | 1,023 | 63.49 |
| 7.750 | 0.42 | 11.34 | 11.92 | 0.00 | 0.29 | 1,047 | 63.50 |
| 7.800 | 0.43 | 11.60 | 12.20 | 0.00 | 0.30 | 1,071 | 63.51 |
| 7.850 | 0.44 | 11.87 | 12.47 | 0.00 | 0.30 | 1,095 | 63.52 |
| 7.900 | 0.45 | 12.14 | 12.76 | 0.00 | 0.31 | 1,120 | 63.53 |
| 7.950 | 0.46 | 12.41 | 13.04 | 0.00 | 0.32 | 1,145 | 63.54 |
| 8.000 | 0.47 | 12.69 | 13.33 | 0.00 | 0.32 | 1,171 | 63.54 |
| 8.050 | 0.47 | 12.96 | 13.63 | 0.00 | 0.33 | 1,197 | 63.55 |
| 8.100 | 0.49 | 13.25 | 13.92 | 0.00 | 0.34 | 1,223 | 63.56 |
| 8.150 | 0.50 | 13.54 | 14.23 | 0.00 | 0.35 | 1,250 | 63.57 |
| 8.200 | 0.51 | 13.84 | 14.55 | 0.00 | 0.35 | 1,278 | 63.58 |
| 8.250 | 0.53 | 14.16 | 14.88 | 0.00 | 0.36 | 1,307 | 63.59 |
| 8.300 | 0.54 | 14.49 | 15.23 | 0.00 | 0.37 | 1,337 | 63.60 |
| 8.350 | 0.56 | 14.83 | 15.58 | 0.00 | 0.38 | 1,369 | 63.61 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.57 | 15.18 | 15.96 | 0.00 | 0.39 | 1,401 | 63.62 |
| 8.450 | 0.59 | 15.55 | 16.35 | 0.00 | 0.40 | 1,435 | 63.63 |
| 8.500 | 0.61 | 15.93 | 16.75 | 0.00 | 0.41 | 1,471 | 63.64 |
| 8.550 | 0.62 | 16.32 | 17.16 | 0.00 | 0.42 | 1,499 | 63.65 |
| 8.600 | 0.64 | 16.72 | 17.58 | 0.00 | 0.43 | 1,522 | 63.66 |
| 8.650 | 0.65 | 17.13 | 18.02 | 0.00 | 0.44 | 1,546 | 63.67 |
| 8.700 | 0.67 | 17.54 | 18.46 | 0.00 | 0.46 | 1,570 | 63.68 |
| 8.750 | 0.69 | 17.96 | 18.90 | 0.00 | 0.47 | 1,594 | 63.69 |
| 8.800 | 0.71 | 18.39 | 19.36 | 0.00 | 0.48 | 1,619 | 63.69 |
| 8.850 | 0.72 | 18.83 | 19.82 | 0.00 | 0.50 | 1,644 | 63.70 |
| 8.900 | 0.74 | 19.27 | 20.29 | 0.00 | 0.51 | 1,670 | 63.71 |
| 8.950 | 0.76 | 19.72 | 20.77 | 0.00 | 0.53 | 1,696 | 63.72 |
| 9.000 | 0.78 | 20.17 | 21.26 | 0.00 | 0.54 | 1,722 | 63.73 |
| 9.050 | 0.80 | 20.64 | 21.75 | 0.00 | 0.56 | 1,749 | 63.74 |
| 9.100 | 0.81 | 21.11 | 22.25 | 0.00 | 0.57 | 1,776 | 63.75 |
| 9.150 | 0.83 | 21.58 | 22.75 | 0.00 | 0.59 | 1,804 | 63.76 |
| 9.200 | 0.85 | 22.06 | 23.27 | 0.00 | 0.60 | 1,832 | 63.77 |
| 9.250 | 0.87 | 22.55 | 23.79 | 0.00 | 0.62 | 1,860 | 63.78 |
| 9.300 | 0.89 | 23.04 | 24.31 | 0.00 | 0.63 | 1,889 | 63.79 |
| 9.350 | 0.91 | 23.55 | 24.84 | 0.00 | 0.65 | 1,918 | 63.80 |
| 9.400 | 0.93 | 24.05 | 25.38 | 0.00 | 0.67 | 1,947 | 63.81 |
| 9.450 | 0.95 | 24.56 | 25.93 | 0.00 | 0.68 | 1,977 | 63.82 |
| 9.500 | 0.97 | 25.08 | 26.48 | 0.00 | 0.70 | 2,007 | 63.83 |
| 9.550 | 0.99 | 25.60 | 27.03 | 0.00 | 0.72 | 2,037 | 63.84 |
| 9.600 | 1.01 | 26.13 | 27.60 | 0.00 | 0.73 | 2,068 | 63.85 |
| 9.650 | 1.03 | 26.67 | 28.17 | 0.00 | 0.75 | 2,099 | 63.86 |
| 9.700 | 1.05 | 27.21 | 28.74 | 0.00 | 0.77 | 2,130 | 63.87 |
| 9.750 | 1.07 | 27.75 | 29.32 | 0.00 | 0.78 | 2,162 | 63.88 |
| 9.800 | 1.09 | 28.30 | 29.90 | 0.00 | 0.80 | 2,194 | 63.89 |
| 9.850 | 1.11 | 28.86 | 30.49 | 0.00 | 0.82 | 2,226 | 63.90 |
| 9.900 | 1.13 | 29.41 | 31.09 | 0.00 | 0.84 | 2,294 | 63.91 |
| 9.950 | 1.15 | 29.98 | 31.69 | 0.00 | 0.86 | 2,366 | 63.92 |
| 10.000 | 1.17 | 30.55 | 32.30 | 0.00 | 0.87 | 2,439 | 63.93 |
| 10.050 | 1.19 | 31.12 | 32.91 | 0.00 | 0.89 | 2,512 | 63.94 |
| 10.100 | 1.22 | 31.71 | 33.53 | 0.00 | 0.91 | 2,587 | 63.95 |
| 10.150 | 1.25 | 32.31 | 34.17 | 0.00 | 0.93 | 2,664 | 63.97 |
| 10.200 | 1.28 | 32.93 | 34.83 | 0.00 | 0.95 | 2,743 | 63.98 |
| 10.250 | 1.31 | 33.58 | 35.53 | 0.00 | 0.97 | 2,827 | 63.99 |
| 10.300 | 1.35 | 34.26 | 36.25 | 0.00 | 0.99 | 2,913 | 64.00 |
| 10.350 | 1.39 | 34.97 | 37.00 | 0.00 | 1.02 | 3,004 | 64.02 |
| 10.400 | 1.43 | 35.71 | 37.79 | 0.00 | 1.04 | 3,098 | 64.03 |
| 10.450 | 1.46 | 36.47 | 38.60 | 0.00 | 1.06 | 3,195 | 64.05 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 1.50 | 37.26 | 39.44 | 0.00 | 1.09 | 3,296 | 64.06 |
| 10.550 | 1.54 | 38.07 | 40.30 | 0.00 | 1.11 | 3,400 | 64.08 |
| 10.600 | 1.58 | 38.91 | 41.20 | 0.00 | 1.14 | 3,507 | 64.10 |
| 10.650 | 1.62 | 39.77 | 42.11 | 0.00 | 1.17 | 3,617 | 64.11 |
| 10.700 | 1.66 | 40.66 | 43.05 | 0.00 | 1.20 | 3,730 | 64.13 |
| 10.750 | 1.70 | 41.56 | 44.02 | 0.00 | 1.23 | 3,846 | 64.15 |
| 10.800 | 1.74 | 42.49 | 45.00 | 0.00 | 1.26 | 3,938 | 64.16 |
| 10.850 | 1.78 | 43.44 | 46.01 | 0.00 | 1.29 | 4,026 | 64.17 |
| 10.900 | 1.82 | 44.41 | 47.04 | 0.00 | 1.32 | 4,116 | 64.19 |
| 10.950 | 1.86 | 45.39 | 48.09 | 0.00 | 1.35 | 4,208 | 64.20 |
| 11.000 | 1.90 | 46.40 | 49.16 | 0.00 | 1.38 | 4,302 | 64.22 |
| 11.050 | 1.95 | 47.43 | 50.25 | 0.00 | 1.41 | 4,398 | 64.23 |
| 11.100 | 2.02 | 48.51 | 51.41 | 0.00 | 1.45 | 4,500 | 64.25 |
| 11.150 | 2.11 | 49.69 | 52.65 | 0.00 | 1.48 | 4,609 | 64.26 |
| 11.200 | 2.23 | 50.98 | 54.03 | 0.00 | 1.52 | 4,730 | 64.28 |
| 11.250 | 2.36 | 52.43 | 55.57 | 0.00 | 1.57 | 4,866 | 64.30 |
| 11.300 | 2.49 | 54.05 | 57.29 | 0.00 | 1.62 | 5,016 | 64.33 |
| 11.350 | 2.63 | 55.82 | 59.17 | 0.00 | 1.68 | 5,182 | 64.35 |
| 11.400 | 2.77 | 57.75 | 61.22 | 0.00 | 1.74 | 5,362 | 64.38 |
| 11.450 | 2.91 | 59.83 | 63.44 | 0.00 | 1.80 | 5,555 | 64.41 |
| 11.500 | 3.06 | 62.06 | 65.81 | 0.00 | 1.87 | 5,761 | 64.44 |
| 11.550 | 3.32 | 64.55 | 68.45 | 0.00 | 1.95 | 5,991 | 64.48 |
| 11.600 | 3.84 | 67.62 | 71.71 | 0.00 | 2.05 | 6,274 | 64.52 |
| 11.650 | 4.56 | 71.67 | 76.02 | 0.00 | 2.18 | 6,648 | 64.58 |
| 11.700 | 5.64 | 77.17 | 81.88 | 0.00 | 2.35 | 7,158 | 64.66 |
| 11.750 | 6.83 | 84.37 | 89.64 | 0.00 | 2.64 | 7,836 | 64.77 |
| 11.800 | 8.16 | 93.38 | 99.35 | 0.00 | 2.99 | 8,685 | 64.90 |
| 11.850 | 9.48 | 104.21 | 111.02 | 0.00 | 3.41 | 9,689 | 65.07 |
| 11.900 | 10.94 | 116.73 | 124.63 | 0.00 | 3.95 | 10,868 | 65.26 |
| 11.950 | 13.33 | 131.70 | 141.00 | 0.00 | 4.65 | 12,282 | 65.49 |
| 12.000 | 18.00 | 151.70 | 163.04 | 0.00 | 5.67 | 14,178 | 65.81 |
| 12.050 | 22.25 | 177.64 | 191.95 | 0.00 | 7.16 | 16,645 | 66.25 |
| 12.100 | 24.51 | 206.11 | 224.39 | 0.00 | 9.14 | 19,402 | 66.79 |
| 12.150 | 24.28 | 231.71 | 254.90 | 0.00 | 11.60 | 21,962 | 67.40 |
| 12.200 | 20.71 | 248.82 | 276.70 | 0.00 | 13.94 | 23,648 | 67.96 |
| 12.250 | 16.78 | 256.18 | 286.30 | 0.00 | 15.06 | 24,412 | 68.21 |
| 12.300 | 14.01 | 256.69 | 286.97 | 0.00 | 15.14 | 24,465 | 68.23 |
| 12.350 | 12.05 | 253.47 | 282.76 | 0.00 | 14.64 | 24,130 | 68.12 |
| 12.400 | 10.36 | 248.19 | 275.88 | 0.00 | 13.84 | 23,583 | 67.93 |
| 12.450 | 8.85 | 241.68 | 267.40 | 0.00 | 12.86 | 22,909 | 67.71 |
| 12.500 | 7.36 | 234.12 | 257.89 | 0.00 | 11.89 | 22,187 | 67.47 |
| 12.550 | 6.08 | 225.81 | 247.56 | 0.00 | 10.88 | 21,322 | 67.23 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 5.04 | 216.86 | 236.92 | 0.00 | 10.03 | 20,447 | 67.02 |
| 12.650 | 4.29 | 207.65 | 226.19 | 0.00 | 9.27 | 19,559 | 66.82 |
| 12.700 | 3.85 | 198.72 | 215.80 | 0.00 | 8.54 | 18,655 | 66.64 |
| 12.750 | 3.58 | 190.18 | 206.14 | 0.00 | 7.98 | 17,856 | 66.48 |
| 12.800 | 3.36 | 182.21 | 197.12 | 0.00 | 7.46 | 17,094 | 66.34 |
| 12.850 | 3.19 | 174.82 | 188.77 | 0.00 | 6.97 | 16,368 | 66.20 |
| 12.900 | 3.03 | 167.92 | 181.05 | 0.00 | 6.56 | 15,710 | 66.08 |
| 12.950 | 2.88 | 161.43 | 173.84 | 0.00 | 6.20 | 15,103 | 65.97 |
| 13.000 | 2.73 | 155.31 | 167.05 | 0.00 | 5.87 | 14,527 | 65.87 |
| 13.050 | 2.60 | 149.55 | 160.64 | 0.00 | 5.55 | 13,970 | 65.78 |
| 13.100 | 2.48 | 144.13 | 154.63 | 0.00 | 5.25 | 13,448 | 65.69 |
| 13.150 | 2.39 | 139.03 | 149.01 | 0.00 | 4.99 | 12,965 | 65.61 |
| 13.200 | 2.33 | 134.22 | 143.75 | 0.00 | 4.77 | 12,516 | 65.53 |
| 13.250 | 2.28 | 129.71 | 138.82 | 0.00 | 4.56 | 12,097 | 65.46 |
| 13.300 | 2.23 | 125.51 | 134.23 | 0.00 | 4.36 | 11,704 | 65.39 |
| 13.350 | 2.20 | 121.59 | 129.94 | 0.00 | 4.18 | 11,331 | 65.33 |
| 13.400 | 2.15 | 117.93 | 125.94 | 0.00 | 4.01 | 10,982 | 65.28 |
| 13.450 | 2.12 | 114.51 | 122.20 | 0.00 | 3.85 | 10,656 | 65.22 |
| 13.500 | 2.08 | 111.31 | 118.70 | 0.00 | 3.70 | 10,352 | 65.17 |
| 13.550 | 2.04 | 108.29 | 115.43 | 0.00 | 3.57 | 10,068 | 65.13 |
| 13.600 | 2.00 | 105.42 | 112.33 | 0.00 | 3.46 | 9,802 | 65.08 |
| 13.650 | 1.96 | 102.68 | 109.38 | 0.00 | 3.35 | 9,548 | 65.04 |
| 13.700 | 1.92 | 100.08 | 106.57 | 0.00 | 3.25 | 9,306 | 65.00 |
| 13.750 | 1.89 | 97.58 | 103.88 | 0.00 | 3.15 | 9,074 | 64.97 |
| 13.800 | 1.85 | 95.20 | 101.31 | 0.00 | 3.06 | 8,853 | 64.93 |
| 13.850 | 1.81 | 92.92 | 98.85 | 0.00 | 2.97 | 8,641 | 64.90 |
| 13.900 | 1.77 | 90.73 | 96.49 | 0.00 | 2.88 | 8,435 | 64.86 |
| 13.950 | 1.73 | 88.63 | 94.23 | 0.00 | 2.80 | 8,237 | 64.83 |
| 14.000 | 1.69 | 86.60 | 92.05 | 0.00 | 2.72 | 8,046 | 64.80 |
| 14.050 | 1.65 | 84.66 | 89.95 | 0.00 | 2.65 | 7,863 | 64.77 |
| 14.100 | 1.62 | 82.79 | 87.93 | 0.00 | 2.57 | 7,687 | 64.75 |
| 14.150 | 1.59 | 80.99 | 86.00 | 0.00 | 2.50 | 7,518 | 64.72 |
| 14.200 | 1.57 | 79.28 | 84.16 | 0.00 | 2.44 | 7,357 | 64.69 |
| 14.250 | 1.55 | 77.66 | 82.41 | 0.00 | 2.37 | 7,204 | 64.67 |
| 14.300 | 1.53 | 76.11 | 80.74 | 0.00 | 2.32 | 7,058 | 64.65 |
| 14.350 | 1.51 | 74.62 | 79.15 | 0.00 | 2.27 | 6,920 | 64.62 |
| 14.400 | 1.49 | 73.18 | 77.62 | 0.00 | 2.22 | 6,787 | 64.60 |
| 14.450 | 1.48 | 71.79 | 76.14 | 0.00 | 2.18 | 6,659 | 64.58 |
| 14.500 | 1.46 | 70.44 | 74.72 | 0.00 | 2.14 | 6,535 | 64.56 |
| 14.550 | 1.44 | 69.14 | 73.34 | 0.00 | 2.10 | 6,415 | 64.55 |
| 14.600 | 1.42 | 67.89 | 72.00 | 0.00 | 2.06 | 6,299 | 64.53 |
| 14.650 | 1.40 | 66.67 | 70.71 | 0.00 | 2.02 | 6,187 | 64.51 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 1.38 | 65.49 | 69.45 | 0.00 | 1.98 | 6,078 | 64.49 |
| 14.750 | 1.36 | 64.35 | 68.24 | 0.00 | 1.94 | 5,972 | 64.48 |
| 14.800 | 1.34 | 63.24 | 67.06 | 0.00 | 1.91 | 5,870 | 64.46 |
| 14.850 | 1.33 | 62.16 | 65.91 | 0.00 | 1.88 | 5,770 | 64.44 |
| 14.900 | 1.31 | 61.11 | 64.79 | 0.00 | 1.84 | 5,673 | 64.43 |
| 14.950 | 1.29 | 60.08 | 63.70 | 0.00 | 1.81 | 5,578 | 64.41 |
| 15.000 | 1.27 | 59.08 | 62.64 | 0.00 | 1.78 | 5,486 | 64.40 |
| 15.050 | 1.25 | 58.11 | 61.60 | 0.00 | 1.75 | 5,395 | 64.39 |
| 15.100 | 1.23 | 57.16 | 60.59 | 0.00 | 1.72 | 5,306 | 64.37 |
| 15.150 | 1.21 | 56.23 | 59.60 | 0.00 | 1.69 | 5,220 | 64.36 |
| 15.200 | 1.20 | 55.32 | 58.64 | 0.00 | 1.66 | 5,135 | 64.35 |
| 15.250 | 1.18 | 54.42 | 57.69 | 0.00 | 1.63 | 5,051 | 64.33 |
| 15.300 | 1.16 | 53.55 | 56.76 | 0.00 | 1.60 | 4,970 | 64.32 |
| 15.350 | 1.14 | 52.69 | 55.85 | 0.00 | 1.58 | 4,890 | 64.31 |
| 15.400 | 1.12 | 51.85 | 54.95 | 0.00 | 1.55 | 4,811 | 64.30 |
| 15.450 | 1.10 | 51.03 | 54.08 | 0.00 | 1.53 | 4,734 | 64.28 |
| 15.500 | 1.08 | 50.21 | 53.21 | 0.00 | 1.50 | 4,658 | 64.27 |
| 15.550 | 1.07 | 49.41 | 52.36 | 0.00 | 1.47 | 4,584 | 64.26 |
| 15.600 | 1.05 | 48.63 | 51.52 | 0.00 | 1.45 | 4,510 | 64.25 |
| 15.650 | 1.03 | 47.85 | 50.70 | 0.00 | 1.43 | 4,438 | 64.24 |
| 15.700 | 1.01 | 47.09 | 49.89 | 0.00 | 1.40 | 4,366 | 64.23 |
| 15.750 | 0.99 | 46.33 | 49.08 | 0.00 | 1.38 | 4,296 | 64.22 |
| 15.800 | 0.97 | 45.58 | 48.29 | 0.00 | 1.35 | 4,226 | 64.21 |
| 15.850 | 0.95 | 44.85 | 47.51 | 0.00 | 1.33 | 4,158 | 64.20 |
| 15.900 | 0.93 | 44.12 | 46.73 | 0.00 | 1.31 | 4,090 | 64.18 |
| 15.950 | 0.92 | 43.40 | 45.97 | 0.00 | 1.28 | 4,022 | 64.17 |
| 16.000 | 0.90 | 42.69 | 45.21 | 0.00 | 1.26 | 3,956 | 64.16 |
| 16.050 | 0.88 | 41.98 | 44.46 | 0.00 | 1.24 | 3,890 | 64.15 |
| 16.100 | 0.86 | 41.29 | 43.73 | 0.00 | 1.22 | 3,811 | 64.14 |
| 16.150 | 0.85 | 40.61 | 43.01 | 0.00 | 1.20 | 3,725 | 64.13 |
| 16.200 | 0.84 | 39.95 | 42.31 | 0.00 | 1.18 | 3,640 | 64.12 |
| 16.250 | 0.83 | 39.32 | 41.62 | 0.00 | 1.15 | 3,559 | 64.10 |
| 16.300 | 0.82 | 38.70 | 40.97 | 0.00 | 1.13 | 3,480 | 64.09 |
| 16.350 | 0.81 | 38.10 | 40.33 | 0.00 | 1.12 | 3,404 | 64.08 |
| 16.400 | 0.81 | 37.53 | 39.72 | 0.00 | 1.10 | 3,330 | 64.07 |
| 16.450 | 0.80 | 36.97 | 39.13 | 0.00 | 1.08 | 3,259 | 64.06 |
| 16.500 | 0.79 | 36.43 | 38.56 | 0.00 | 1.06 | 3,190 | 64.05 |
| 16.550 | 0.78 | 35.91 | 38.00 | 0.00 | 1.05 | 3,124 | 64.04 |
| 16.600 | 0.77 | 35.41 | 37.47 | 0.00 | 1.03 | 3,059 | 64.03 |
| 16.650 | 0.76 | 34.92 | 36.94 | 0.00 | 1.01 | 2,997 | 64.02 |
| 16.700 | 0.76 | 34.44 | 36.44 | 0.00 | 1.00 | 2,936 | 64.01 |
| 16.750 | 0.75 | 33.98 | 35.95 | 0.00 | 0.98 | 2,877 | 64.00 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.74 | 33.53 | 35.47 | 0.00 | 0.97 | 2,820 | 63.99 |
| 16.850 | 0.73 | 33.09 | 35.00 | 0.00 | 0.96 | 2,764 | 63.98 |
| 16.900 | 0.72 | 32.66 | 34.55 | 0.00 | 0.94 | 2,709 | 63.97 |
| 16.950 | 0.72 | 32.25 | 34.10 | 0.00 | 0.93 | 2,656 | 63.97 |
| 17.000 | 0.71 | 31.84 | 33.67 | 0.00 | 0.92 | 2,604 | 63.96 |
| 17.050 | 0.70 | 31.44 | 33.25 | 0.00 | 0.90 | 2,553 | 63.95 |
| 17.100 | 0.69 | 31.05 | 32.83 | 0.00 | 0.89 | 2,503 | 63.94 |
| 17.150 | 0.68 | 30.67 | 32.43 | 0.00 | 0.88 | 2,455 | 63.93 |
| 17.200 | 0.67 | 30.30 | 32.03 | 0.00 | 0.87 | 2,407 | 63.93 |
| 17.250 | 0.67 | 29.93 | 31.64 | 0.00 | 0.85 | 2,360 | 63.92 |
| 17.300 | 0.66 | 29.58 | 31.26 | 0.00 | 0.84 | 2,315 | 63.91 |
| 17.350 | 0.65 | 29.22 | 30.89 | 0.00 | 0.83 | 2,270 | 63.91 |
| 17.400 | 0.64 | 28.88 | 30.52 | 0.00 | 0.82 | 2,227 | 63.90 |
| 17.450 | 0.63 | 28.53 | 30.15 | 0.00 | 0.81 | 2,208 | 63.89 |
| 17.500 | 0.63 | 28.20 | 29.79 | 0.00 | 0.80 | 2,188 | 63.89 |
| 17.550 | 0.62 | 27.87 | 29.44 | 0.00 | 0.79 | 2,169 | 63.88 |
| 17.600 | 0.61 | 27.54 | 29.10 | 0.00 | 0.78 | 2,150 | 63.87 |
| 17.650 | 0.60 | 27.22 | 28.75 | 0.00 | 0.77 | 2,131 | 63.87 |
| 17.700 | 0.59 | 26.90 | 28.41 | 0.00 | 0.76 | 2,113 | 63.86 |
| 17.750 | 0.59 | 26.59 | 28.08 | 0.00 | 0.75 | 2,094 | 63.85 |
| 17.800 | 0.58 | 26.28 | 27.75 | 0.00 | 0.74 | 2,076 | 63.85 |
| 17.850 | 0.57 | 25.97 | 27.42 | 0.00 | 0.73 | 2,059 | 63.84 |
| 17.900 | 0.56 | 25.66 | 27.10 | 0.00 | 0.72 | 2,041 | 63.84 |
| 17.950 | 0.55 | 25.36 | 26.78 | 0.00 | 0.71 | 2,023 | 63.83 |
| 18.000 | 0.54 | 25.06 | 26.46 | 0.00 | 0.70 | 2,006 | 63.82 |
| 18.050 | 0.54 | 24.77 | 26.15 | 0.00 | 0.69 | 1,989 | 63.82 |
| 18.100 | 0.53 | 24.48 | 25.83 | 0.00 | 0.68 | 1,972 | 63.81 |
| 18.150 | 0.52 | 24.19 | 25.53 | 0.00 | 0.67 | 1,955 | 63.81 |
| 18.200 | 0.52 | 23.92 | 25.24 | 0.00 | 0.66 | 1,939 | 63.80 |
| 18.250 | 0.52 | 23.65 | 24.96 | 0.00 | 0.65 | 1,924 | 63.80 |
| 18.300 | 0.52 | 23.40 | 24.69 | 0.00 | 0.64 | 1,909 | 63.79 |
| 18.350 | 0.51 | 23.15 | 24.43 | 0.00 | 0.64 | 1,895 | 63.79 |
| 18.400 | 0.51 | 22.92 | 24.18 | 0.00 | 0.63 | 1,882 | 63.78 |
| 18.450 | 0.51 | 22.69 | 23.94 | 0.00 | 0.62 | 1,869 | 63.78 |
| 18.500 | 0.51 | 22.48 | 23.71 | 0.00 | 0.61 | 1,856 | 63.77 |
| 18.550 | 0.50 | 22.27 | 23.49 | 0.00 | 0.61 | 1,844 | 63.77 |
| 18.600 | 0.50 | 22.07 | 23.28 | 0.00 | 0.60 | 1,833 | 63.77 |
| 18.650 | 0.50 | 21.88 | 23.07 | 0.00 | 0.60 | 1,821 | 63.76 |
| 18.700 | 0.50 | 21.70 | 22.88 | 0.00 | 0.59 | 1,811 | 63.76 |
| 18.750 | 0.49 | 21.52 | 22.69 | 0.00 | 0.58 | 1,800 | 63.76 |
| 18.800 | 0.49 | 21.35 | 22.50 | 0.00 | 0.58 | 1,790 | 63.75 |
| 18.850 | 0.49 | 21.18 | 22.33 | 0.00 | 0.57 | 1,781 | 63.75 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.49 | 21.02 | 22.15 | 0.00 | 0.57 | 1,771 | 63.75 |
| 18.950 | 0.48 | 20.86 | 21.99 | 0.00 | 0.56 | 1,762 | 63.74 |
| 19.000 | 0.48 | 20.71 | 21.83 | 0.00 | 0.56 | 1,754 | 63.74 |
| 19.050 | 0.48 | 20.56 | 21.67 | 0.00 | 0.55 | 1,745 | 63.74 |
| 19.100 | 0.48 | 20.42 | 21.52 | 0.00 | 0.55 | 1,737 | 63.73 |
| 19.150 | 0.47 | 20.28 | 21.37 | 0.00 | 0.54 | 1,729 | 63.73 |
| 19.200 | 0.47 | 20.15 | 21.23 | 0.00 | 0.54 | 1,721 | 63.73 |
| 19.250 | 0.47 | 20.02 | 21.09 | 0.00 | 0.54 | 1,713 | 63.73 |
| 19.300 | 0.47 | 19.89 | 20.96 | 0.00 | 0.53 | 1,706 | 63.72 |
| 19.350 | 0.46 | 19.77 | 20.82 | 0.00 | 0.53 | 1,699 | 63.72 |
| 19.400 | 0.46 | 19.64 | 20.69 | 0.00 | 0.52 | 1,692 | 63.72 |
| 19.450 | 0.46 | 19.53 | 20.57 | 0.00 | 0.52 | 1,685 | 63.72 |
| 19.500 | 0.46 | 19.41 | 20.44 | 0.00 | 0.52 | 1,678 | 63.71 |
| 19.550 | 0.45 | 19.30 | 20.32 | 0.00 | 0.51 | 1,671 | 63.71 |
| 19.600 | 0.45 | 19.18 | 20.20 | 0.00 | 0.51 | 1,665 | 63.71 |
| 19.650 | 0.45 | 19.07 | 20.09 | 0.00 | 0.51 | 1,659 | 63.71 |
| 19.700 | 0.45 | 18.97 | 19.97 | 0.00 | 0.50 | 1,652 | 63.71 |
| 19.750 | 0.44 | 18.86 | 19.86 | 0.00 | 0.50 | 1,646 | 63.70 |
| 19.800 | 0.44 | 18.76 | 19.75 | 0.00 | 0.50 | 1,640 | 63.70 |
| 19.850 | 0.44 | 18.65 | 19.64 | 0.00 | 0.49 | 1,634 | 63.70 |
| 19.900 | 0.44 | 18.55 | 19.53 | 0.00 | 0.49 | 1,628 | 63.70 |
| 19.950 | 0.43 | 18.45 | 19.43 | 0.00 | 0.49 | 1,623 | 63.70 |
| 20.000 | 0.43 | 18.36 | 19.32 | 0.00 | 0.48 | 1,617 | 63.69 |
| 20.050 | 0.43 | 18.26 | 19.22 | 0.00 | 0.48 | 1,611 | 63.69 |
| 20.100 | 0.43 | 18.17 | 19.12 | 0.00 | 0.48 | 1,606 | 63.69 |
| 20.150 | 0.43 | 18.07 | 19.02 | 0.00 | 0.47 | 1,600 | 63.69 |
| 20.200 | 0.42 | 17.98 | 18.92 | 0.00 | 0.47 | 1,595 | 63.69 |
| 20.250 | 0.42 | 17.89 | 18.83 | 0.00 | 0.47 | 1,590 | 63.68 |
| 20.300 | 0.42 | 17.80 | 18.73 | 0.00 | 0.47 | 1,585 | 63.68 |
| 20.350 | 0.42 | 17.72 | 18.64 | 0.00 | 0.46 | 1,580 | 63.68 |
| 20.400 | 0.42 | 17.63 | 18.55 | 0.00 | 0.46 | 1,575 | 63.68 |
| 20.450 | 0.41 | 17.55 | 18.46 | 0.00 | 0.46 | 1,570 | 63.68 |
| 20.500 | 0.41 | 17.47 | 18.38 | 0.00 | 0.45 | 1,565 | 63.68 |
| 20.550 | 0.41 | 17.39 | 18.29 | 0.00 | 0.45 | 1,561 | 63.68 |
| 20.600 | 0.41 | 17.31 | 18.21 | 0.00 | 0.45 | 1,556 | 63.67 |
| 20.650 | 0.41 | 17.24 | 18.13 | 0.00 | 0.45 | 1,552 | 63.67 |
| 20.700 | 0.40 | 17.16 | 18.05 | 0.00 | 0.44 | 1,547 | 63.67 |
| 20.750 | 0.40 | 17.08 | 17.97 | 0.00 | 0.44 | 1,543 | 63.67 |
| 20.800 | 0.40 | 17.01 | 17.89 | 0.00 | 0.44 | 1,539 | 63.67 |
| 20.850 | 0.40 | 16.93 | 17.81 | 0.00 | 0.44 | 1,534 | 63.67 |
| 20.900 | 0.40 | 16.86 | 17.73 | 0.00 | 0.43 | 1,530 | 63.66 |
| 20.950 | 0.40 | 16.79 | 17.66 | 0.00 | 0.43 | 1,526 | 63.66 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.39 | 16.72 | 17.58 | 0.00 | 0.43 | 1,522 | 63.66 |
| 21.050 | 0.39 | 16.65 | 17.51 | 0.00 | 0.43 | 1,518 | 63.66 |
| 21.100 | 0.39 | 16.59 | 17.44 | 0.00 | 0.43 | 1,514 | 63.66 |
| 21.150 | 0.39 | 16.52 | 17.37 | 0.00 | 0.42 | 1,510 | 63.66 |
| 21.200 | 0.39 | 16.45 | 17.29 | 0.00 | 0.42 | 1,506 | 63.66 |
| 21.250 | 0.39 | 16.38 | 17.22 | 0.00 | 0.42 | 1,502 | 63.66 |
| 21.300 | 0.38 | 16.32 | 17.15 | 0.00 | 0.42 | 1,499 | 63.65 |
| 21.350 | 0.38 | 16.25 | 17.08 | 0.00 | 0.42 | 1,495 | 63.65 |
| 21.400 | 0.38 | 16.19 | 17.01 | 0.00 | 0.41 | 1,491 | 63.65 |
| 21.450 | 0.38 | 16.12 | 16.95 | 0.00 | 0.41 | 1,487 | 63.65 |
| 21.500 | 0.38 | 16.06 | 16.88 | 0.00 | 0.41 | 1,482 | 63.65 |
| 21.550 | 0.37 | 15.99 | 16.81 | 0.00 | 0.41 | 1,476 | 63.65 |
| 21.600 | 0.37 | 15.92 | 16.74 | 0.00 | 0.41 | 1,470 | 63.64 |
| 21.650 | 0.37 | 15.86 | 16.67 | 0.00 | 0.40 | 1,464 | 63.64 |
| 21.700 | 0.37 | 15.79 | 16.60 | 0.00 | 0.40 | 1,458 | 63.64 |
| 21.750 | 0.37 | 15.73 | 16.53 | 0.00 | 0.40 | 1,451 | 63.64 |
| 21.800 | 0.37 | 15.66 | 16.46 | 0.00 | 0.40 | 1,445 | 63.64 |
| 21.850 | 0.36 | 15.59 | 16.39 | 0.00 | 0.40 | 1,439 | 63.63 |
| 21.900 | 0.36 | 15.53 | 16.32 | 0.00 | 0.40 | 1,433 | 63.63 |
| 21.950 | 0.36 | 15.46 | 16.25 | 0.00 | 0.39 | 1,427 | 63.63 |
| 22.000 | 0.36 | 15.39 | 16.18 | 0.00 | 0.39 | 1,421 | 63.63 |
| 22.050 | 0.36 | 15.33 | 16.11 | 0.00 | 0.39 | 1,414 | 63.63 |
| 22.100 | 0.35 | 15.26 | 16.03 | 0.00 | 0.39 | 1,408 | 63.62 |
| 22.150 | 0.35 | 15.19 | 15.96 | 0.00 | 0.39 | 1,402 | 63.62 |
| 22.200 | 0.35 | 15.12 | 15.89 | 0.00 | 0.39 | 1,396 | 63.62 |
| 22.250 | 0.35 | 15.05 | 15.82 | 0.00 | 0.38 | 1,389 | 63.62 |
| 22.300 | 0.35 | 14.98 | 15.75 | 0.00 | 0.38 | 1,383 | 63.62 |
| 22.350 | 0.34 | 14.91 | 15.67 | 0.00 | 0.38 | 1,376 | 63.61 |
| 22.400 | 0.34 | 14.84 | 15.60 | 0.00 | 0.38 | 1,370 | 63.61 |
| 22.450 | 0.34 | 14.77 | 15.53 | 0.00 | 0.38 | 1,363 | 63.61 |
| 22.500 | 0.34 | 14.70 | 15.45 | 0.00 | 0.37 | 1,357 | 63.61 |
| 22.550 | 0.34 | 14.63 | 15.38 | 0.00 | 0.37 | 1,351 | 63.60 |
| 22.600 | 0.34 | 14.56 | 15.31 | 0.00 | 0.37 | 1,344 | 63.60 |
| 22.650 | 0.33 | 14.50 | 15.23 | 0.00 | 0.37 | 1,338 | 63.60 |
| 22.700 | 0.33 | 14.43 | 15.16 | 0.00 | 0.37 | 1,332 | 63.60 |
| 22.750 | 0.33 | 14.36 | 15.09 | 0.00 | 0.37 | 1,325 | 63.60 |
| 22.800 | 0.33 | 14.29 | 15.02 | 0.00 | 0.36 | 1,319 | 63.59 |
| 22.850 | 0.33 | 14.22 | 14.94 | 0.00 | 0.36 | 1,312 | 63.59 |
| 22.900 | 0.32 | 14.15 | 14.87 | 0.00 | 0.36 | 1,306 | 63.59 |
| 22.950 | 0.32 | 14.08 | 14.79 | 0.00 | 0.36 | 1,299 | 63.59 |
| 23.000 | 0.32 | 14.01 | 14.72 | 0.00 | 0.36 | 1,293 | 63.58 |
| 23.050 | 0.32 | 13.94 | 14.65 | 0.00 | 0.36 | 1,286 | 63.58 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: MC-3500 - 3 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.32 | 13.86 | 14.57 | 0.00 | 0.35 | 1,280 | 63.58 |
| 23.150 | 0.31 | 13.79 | 14.49 | 0.00 | 0.35 | 1,273 | 63.58 |
| 23.200 | 0.31 | 13.72 | 14.42 | 0.00 | 0.35 | 1,266 | 63.58 |
| 23.250 | 0.31 | 13.65 | 14.34 | 0.00 | 0.35 | 1,260 | 63.57 |
| 23.300 | 0.31 | 13.58 | 14.27 | 0.00 | 0.35 | 1,253 | 63.57 |
| 23.350 | 0.31 | 13.51 | 14.19 | 0.00 | 0.34 | 1,247 | 63.57 |
| 23.400 | 0.31 | 13.44 | 14.12 | 0.00 | 0.34 | 1,240 | 63.57 |
| 23.450 | 0.31 | 13.37 | 14.05 | 0.00 | 0.34 | 1,234 | 63.57 |
| 23.500 | 0.30 | 13.30 | 13.97 | 0.00 | 0.34 | 1,227 | 63.56 |
| 23.550 | 0.30 | 13.23 | 13.90 | 0.00 | 0.34 | 1,221 | 63.56 |
| 23.600 | 0.30 | 13.15 | 13.82 | 0.00 | 0.34 | 1,214 | 63.56 |
| 23.650 | 0.30 | 13.08 | 13.75 | 0.00 | 0.33 | 1,207 | 63.56 |
| 23.700 | 0.29 | 13.01 | 13.67 | 0.00 | 0.33 | 1,201 | 63.55 |
| 23.750 | 0.29 | 12.94 | 13.60 | 0.00 | 0.33 | 1,194 | 63.55 |
| 23.800 | 0.29 | 12.87 | 13.52 | 0.00 | 0.33 | 1,188 | 63.55 |
| 23.850 | 0.29 | 12.80 | 13.45 | 0.00 | 0.33 | 1,181 | 63.55 |
| 23.900 | 0.29 | 12.72 | 13.37 | 0.00 | 0.32 | 1,174 | 63.55 |
| 23.950 | 0.28 | 12.65 | 13.30 | 0.00 | 0.32 | 1,168 | 63.54 |
| 24.000 | 0.28 | 12.58 | 13.22 | 0.00 | 0.32 | 1,161 | 63.54 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: MC-3500 - 3 (IN)

Scenario: Post-Development 1 year

Return Event: 1 years

Storm Event: 1 year

Summary for Hydrograph Addition at 'MC-3500 - 3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-3 | 19,897 | 12.150 | 5.21 |
| Flow (In) | MC-3500 - 3 | 19,897 | 12.150 | 5.21 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: MC-3500 - 3 (IN)

Scenario: Post-Development 10 year

Return Event: 10 years

Storm Event: 10 year

Summary for Hydrograph Addition at 'MC-3500 - 3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-3 | 47,606 | 12.150 | 12.08 |
| Flow (In) | MC-3500 - 3 | 47,606 | 12.150 | 12.08 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Label: MC-3500 - 3 (IN)

Scenario: Post-Development 25 year

Return Event: 25 years

Storm Event: 25 year

Summary for Hydrograph Addition at 'MC-3500 - 3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-3 | 64,556 | 12.100 | 16.18 |
| Flow (In) | MC-3500 - 3 | 64,556 | 12.100 | 16.18 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary

Return Event: 100 years

Label: MC-3500 - 3 (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

Summary for Hydrograph Addition at 'MC-3500 - 3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-3 |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-3 | 100,006 | 12.100 | 24.51 |
| Flow (In) | MC-3500 - 3 | 100,006 | 12.100 | 24.51 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 1 years

Label: Stormwater Planters - 2

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 78.81 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.14 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.14 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 78.81 | 0.14 | 0 | 3,050 | 0.00 | 0.14 | 0.14 |
| 78.91 | 0.14 | 305 | 3,050 | 0.00 | 0.14 | 3.53 |
| 79.01 | 0.14 | 610 | 3,050 | 0.00 | 0.14 | 6.92 |
| 79.11 | 0.14 | 915 | 3,050 | 0.00 | 0.14 | 10.31 |
| 79.21 | 0.14 | 1,220 | 3,050 | 0.00 | 0.14 | 13.70 |
| 79.31 | 0.14 | 1,525 | 3,050 | 0.00 | 0.14 | 17.09 |
| 79.41 | 0.14 | 1,830 | 3,050 | 0.00 | 0.14 | 20.47 |
| 79.51 | 0.14 | 2,135 | 3,050 | 0.00 | 0.14 | 23.86 |
| 79.61 | 0.14 | 2,440 | 3,050 | 0.00 | 0.14 | 27.25 |
| 79.71 | 0.14 | 2,745 | 3,050 | 0.00 | 0.14 | 30.64 |
| 79.81 | 0.14 | 3,050 | 3,050 | 0.00 | 0.14 | 34.03 |
| 79.91 | 0.74 | 3,355 | 3,050 | 0.00 | 0.74 | 38.01 |
| 80.01 | 1.83 | 3,660 | 3,050 | 0.00 | 1.83 | 42.49 |
| 80.11 | 3.24 | 3,965 | 3,050 | 0.00 | 3.24 | 47.29 |
| 80.21 | 4.91 | 4,270 | 3,050 | 0.00 | 4.91 | 52.36 |
| 80.31 | 5.49 | 4,575 | 3,050 | 0.00 | 5.49 | 56.32 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 10 years

Label: Stormwater Planters - 2

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 78.81 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.14 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.14 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 78.81 | 0.14 | 0 | 3,050 | 0.00 | 0.14 | 0.14 |
| 78.91 | 0.14 | 305 | 3,050 | 0.00 | 0.14 | 3.53 |
| 79.01 | 0.14 | 610 | 3,050 | 0.00 | 0.14 | 6.92 |
| 79.11 | 0.14 | 915 | 3,050 | 0.00 | 0.14 | 10.31 |
| 79.21 | 0.14 | 1,220 | 3,050 | 0.00 | 0.14 | 13.70 |
| 79.31 | 0.14 | 1,525 | 3,050 | 0.00 | 0.14 | 17.09 |
| 79.41 | 0.14 | 1,830 | 3,050 | 0.00 | 0.14 | 20.47 |
| 79.51 | 0.14 | 2,135 | 3,050 | 0.00 | 0.14 | 23.86 |
| 79.61 | 0.14 | 2,440 | 3,050 | 0.00 | 0.14 | 27.25 |
| 79.71 | 0.14 | 2,745 | 3,050 | 0.00 | 0.14 | 30.64 |
| 79.81 | 0.14 | 3,050 | 3,050 | 0.00 | 0.14 | 34.03 |
| 79.91 | 0.74 | 3,355 | 3,050 | 0.00 | 0.74 | 38.01 |
| 80.01 | 1.83 | 3,660 | 3,050 | 0.00 | 1.83 | 42.49 |
| 80.11 | 3.24 | 3,965 | 3,050 | 0.00 | 3.24 | 47.29 |
| 80.21 | 4.91 | 4,270 | 3,050 | 0.00 | 4.91 | 52.36 |
| 80.31 | 5.49 | 4,575 | 3,050 | 0.00 | 5.49 | 56.32 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 25 years

Label: Stormwater Planters - 2

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 78.81 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.14 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.14 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 78.81 | 0.14 | 0 | 3,050 | 0.00 | 0.14 | 0.14 |
| 78.91 | 0.14 | 305 | 3,050 | 0.00 | 0.14 | 3.53 |
| 79.01 | 0.14 | 610 | 3,050 | 0.00 | 0.14 | 6.92 |
| 79.11 | 0.14 | 915 | 3,050 | 0.00 | 0.14 | 10.31 |
| 79.21 | 0.14 | 1,220 | 3,050 | 0.00 | 0.14 | 13.70 |
| 79.31 | 0.14 | 1,525 | 3,050 | 0.00 | 0.14 | 17.09 |
| 79.41 | 0.14 | 1,830 | 3,050 | 0.00 | 0.14 | 20.47 |
| 79.51 | 0.14 | 2,135 | 3,050 | 0.00 | 0.14 | 23.86 |
| 79.61 | 0.14 | 2,440 | 3,050 | 0.00 | 0.14 | 27.25 |
| 79.71 | 0.14 | 2,745 | 3,050 | 0.00 | 0.14 | 30.64 |
| 79.81 | 0.14 | 3,050 | 3,050 | 0.00 | 0.14 | 34.03 |
| 79.91 | 0.74 | 3,355 | 3,050 | 0.00 | 0.74 | 38.01 |
| 80.01 | 1.83 | 3,660 | 3,050 | 0.00 | 1.83 | 42.49 |
| 80.11 | 3.24 | 3,965 | 3,050 | 0.00 | 3.24 | 47.29 |
| 80.21 | 4.91 | 4,270 | 3,050 | 0.00 | 4.91 | 52.36 |
| 80.31 | 5.49 | 4,575 | 3,050 | 0.00 | 5.49 | 56.32 |

Existing and Proposed Hydrologic Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Return Event: 100 years

Label: Stormwater Planters - 2

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | |
|------------------------------------|-------------------------|
| Infiltration Method (Computed) | No Infiltration |
| Initial Conditions | |
| Elevation (Water Surface, Initial) | 78.81 ft |
| Volume (Initial) | 0 ft ³ |
| Flow (Initial Outlet) | 0.14 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.14 ft ³ /s |
| Time Increment | 0.050 hours |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ft ³) | Area (ft ²) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|----------------------------|-------------------------|-----------------------------------|-----------------------------------|-------------------------------|
| 78.81 | 0.14 | 0 | 3,050 | 0.00 | 0.14 | 0.14 |
| 78.91 | 0.14 | 305 | 3,050 | 0.00 | 0.14 | 3.53 |
| 79.01 | 0.14 | 610 | 3,050 | 0.00 | 0.14 | 6.92 |
| 79.11 | 0.14 | 915 | 3,050 | 0.00 | 0.14 | 10.31 |
| 79.21 | 0.14 | 1,220 | 3,050 | 0.00 | 0.14 | 13.70 |
| 79.31 | 0.14 | 1,525 | 3,050 | 0.00 | 0.14 | 17.09 |
| 79.41 | 0.14 | 1,830 | 3,050 | 0.00 | 0.14 | 20.47 |
| 79.51 | 0.14 | 2,135 | 3,050 | 0.00 | 0.14 | 23.86 |
| 79.61 | 0.14 | 2,440 | 3,050 | 0.00 | 0.14 | 27.25 |
| 79.71 | 0.14 | 2,745 | 3,050 | 0.00 | 0.14 | 30.64 |
| 79.81 | 0.14 | 3,050 | 3,050 | 0.00 | 0.14 | 34.03 |
| 79.91 | 0.74 | 3,355 | 3,050 | 0.00 | 0.74 | 38.01 |
| 80.01 | 1.83 | 3,660 | 3,050 | 0.00 | 1.83 | 42.49 |
| 80.11 | 3.24 | 3,965 | 3,050 | 0.00 | 3.24 | 47.29 |
| 80.21 | 4.91 | 4,270 | 3,050 | 0.00 | 4.91 | 52.36 |
| 80.31 | 5.49 | 4,575 | 3,050 | 0.00 | 5.49 | 56.32 |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 1 years

Label: Stormwater Planters - 2 (IN)

Storm Event: 1 year

Scenario: Post-Development 1 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 78.81 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.14 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.14 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 0.97 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.14 ft ³ /s | Time to Peak (Flow, Outlet) | 11.600 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 79.20 ft | | |
| Volume (Peak) | 1,189 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 3,907 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 3,912 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 5 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 10 years

Label: Stormwater Planters - 2 (IN)

Storm Event: 10 year

Scenario: Post-Development 10 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 78.81 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.14 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.14 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 1.81 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.14 ft ³ /s | Time to Peak (Flow, Outlet) | 10.850 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 79.77 ft | | |
| Volume (Peak) | 2,931 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 7,510 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 7,515 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 5 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 25 years

Label: Stormwater Planters - 2 (IN)

Storm Event: 25 year

Scenario: Post-Development 25 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 78.81 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.14 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.14 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 2.30 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 0.70 ft ³ /s | Time to Peak (Flow, Outlet) | 12.450 hours |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 79.90 ft | | |
| Volume (Peak) | 3,336 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 9,617 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 9,621 ft ³ | | |
| Volume (Retained) | 0 ft ³ | | |
| Volume (Unrouted) | 4 ft ³ | | |
| Error (Mass Balance) | 0.0 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Level Pool Pond Routing Summary

Return Event: 100 years

Label: Stormwater Planters - 2 (IN)

Storm Event: 100 year

Scenario: Post-Development 100 year

| Infiltration | | | |
|------------------------------------|-------------------------|-----------------------------|--------------|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 78.81 ft | | |
| Volume (Initial) | 0 ft ³ | | |
| Flow (Initial Outlet) | 0.14 ft ³ /s | | |
| Flow (Initial Infiltration) | 0.00 ft ³ /s | | |
| Flow (Initial, Total) | 0.14 ft ³ /s | | |
| Time Increment | 0.050 hours | | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 3.30 ft ³ /s | Time to Peak (Flow, In) | 12.100 hours |
| Flow (Peak Outlet) | 2.47 ft ³ /s | Time to Peak (Flow, Outlet) | 12.200 hours |
| Elevation (Water Surface, Peak) | 80.06 ft | | |
| Volume (Peak) | 3,800 ft ³ | | |
| Mass Balance (ft ³) | | | |
| Volume (Initial) | 0 ft ³ | | |
| Volume (Total Inflow) | 13,940 ft ³ | | |
| Volume (Total Infiltration) | 0 ft ³ | | |
| Volume (Total Outlet Outflow) | 13,345 ft ³ | | |
| Volume (Retained) | 577 ft ³ | | |
| Volume (Unrouted) | -19 ft ³ | | |
| Error (Mass Balance) | 0.1 % | | |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 2.500 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.550 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.600 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.700 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.750 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.800 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.850 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 2.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.050 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.100 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.150 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.300 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 3.350 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.400 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.850 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.900 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 3.950 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 4.000 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 4.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 4.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 4.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 4.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 5.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 6.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 6.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 6.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 7.700 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 7.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 7.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 7.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 7.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 7.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 8.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 8.050 | 0.03 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 8.100 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 8.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 8.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 8.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 8.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 8.700 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 8.750 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 8.800 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 8.850 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 8.900 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 8.950 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 9.000 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 9.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.350 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 9.400 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 9.450 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 9.500 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 9.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 9.600 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 9.650 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 9.700 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 9.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 9.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 9.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 9.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 9.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 10.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 10.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 10.100 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 10.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 10.200 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 10.250 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 10.300 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 10.350 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 10.400 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 10.450 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 10.550 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 10.600 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 10.650 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 10.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 10.750 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 10.800 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 10.850 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 10.900 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |
| 10.950 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |
| 11.000 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 11.050 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 11.100 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 11.150 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 11.200 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 11.250 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 11.300 | 0.11 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 11.350 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 11.400 | 0.12 | 0.00 | 0.23 | 0.00 | 0.11 | 0 | 78.81 |
| 11.450 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 11.500 | 0.13 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 78.81 |
| 11.550 | 0.14 | 0.00 | 0.27 | 0.00 | 0.14 | 0 | 78.81 |
| 11.600 | 0.17 | 0.03 | 0.31 | 0.00 | 0.14 | 16 | 78.82 |
| 11.650 | 0.21 | 0.13 | 0.41 | 0.00 | 0.14 | 24 | 78.82 |
| 11.700 | 0.26 | 0.32 | 0.60 | 0.00 | 0.14 | 41 | 78.82 |
| 11.750 | 0.31 | 0.60 | 0.88 | 0.00 | 0.14 | 67 | 78.83 |
| 11.800 | 0.36 | 0.99 | 1.27 | 0.00 | 0.14 | 101 | 78.84 |
| 11.850 | 0.41 | 1.47 | 1.76 | 0.00 | 0.14 | 145 | 78.86 |
| 11.900 | 0.47 | 2.07 | 2.35 | 0.00 | 0.14 | 199 | 78.88 |
| 11.950 | 0.61 | 2.86 | 3.15 | 0.00 | 0.14 | 270 | 78.90 |
| 12.000 | 0.85 | 4.05 | 4.33 | 0.00 | 0.14 | 377 | 78.93 |
| 12.050 | 0.94 | 5.56 | 5.84 | 0.00 | 0.14 | 513 | 78.98 |
| 12.100 | 0.97 | 7.18 | 7.46 | 0.00 | 0.14 | 659 | 79.03 |
| 12.150 | 0.85 | 8.72 | 9.00 | 0.00 | 0.14 | 797 | 79.07 |
| 12.200 | 0.62 | 9.91 | 10.19 | 0.00 | 0.14 | 904 | 79.11 |
| 12.250 | 0.51 | 10.75 | 11.04 | 0.00 | 0.14 | 981 | 79.13 |
| 12.300 | 0.43 | 11.41 | 11.69 | 0.00 | 0.14 | 1,040 | 79.15 |
| 12.350 | 0.38 | 11.94 | 12.23 | 0.00 | 0.14 | 1,088 | 79.17 |
| 12.400 | 0.32 | 12.37 | 12.65 | 0.00 | 0.14 | 1,126 | 79.18 |
| 12.450 | 0.28 | 12.68 | 12.96 | 0.00 | 0.14 | 1,154 | 79.19 |
| 12.500 | 0.22 | 12.89 | 13.18 | 0.00 | 0.14 | 1,173 | 79.19 |
| 12.550 | 0.18 | 13.02 | 13.30 | 0.00 | 0.14 | 1,184 | 79.20 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.15 | 13.07 | 13.35 | 0.00 | 0.14 | 1,189 | 79.20 |
| 12.650 | 0.14 | 13.08 | 13.36 | 0.00 | 0.14 | 1,189 | 79.20 |
| 12.700 | 0.13 | 13.06 | 13.34 | 0.00 | 0.14 | 1,188 | 79.20 |
| 12.750 | 0.12 | 13.02 | 13.31 | 0.00 | 0.14 | 1,185 | 79.20 |
| 12.800 | 0.12 | 12.98 | 13.26 | 0.00 | 0.14 | 1,181 | 79.20 |
| 12.850 | 0.11 | 12.93 | 13.21 | 0.00 | 0.14 | 1,176 | 79.20 |
| 12.900 | 0.10 | 12.86 | 13.14 | 0.00 | 0.14 | 1,170 | 79.19 |
| 12.950 | 0.10 | 12.78 | 13.06 | 0.00 | 0.14 | 1,163 | 79.19 |
| 13.000 | 0.09 | 12.69 | 12.98 | 0.00 | 0.14 | 1,155 | 79.19 |
| 13.050 | 0.09 | 12.60 | 12.88 | 0.00 | 0.14 | 1,146 | 79.19 |
| 13.100 | 0.09 | 12.49 | 12.77 | 0.00 | 0.14 | 1,137 | 79.18 |
| 13.150 | 0.08 | 12.38 | 12.66 | 0.00 | 0.14 | 1,127 | 79.18 |
| 13.200 | 0.08 | 12.27 | 12.55 | 0.00 | 0.14 | 1,117 | 79.18 |
| 13.250 | 0.08 | 12.15 | 12.43 | 0.00 | 0.14 | 1,106 | 79.17 |
| 13.300 | 0.08 | 12.03 | 12.31 | 0.00 | 0.14 | 1,095 | 79.17 |
| 13.350 | 0.08 | 11.90 | 12.18 | 0.00 | 0.14 | 1,084 | 79.17 |
| 13.400 | 0.08 | 11.78 | 12.06 | 0.00 | 0.14 | 1,073 | 79.16 |
| 13.450 | 0.08 | 11.65 | 11.93 | 0.00 | 0.14 | 1,061 | 79.16 |
| 13.500 | 0.07 | 11.51 | 11.80 | 0.00 | 0.14 | 1,049 | 79.15 |
| 13.550 | 0.07 | 11.38 | 11.66 | 0.00 | 0.14 | 1,037 | 79.15 |
| 13.600 | 0.07 | 11.24 | 11.52 | 0.00 | 0.14 | 1,024 | 79.15 |
| 13.650 | 0.07 | 11.10 | 11.38 | 0.00 | 0.14 | 1,012 | 79.14 |
| 13.700 | 0.07 | 10.96 | 11.24 | 0.00 | 0.14 | 999 | 79.14 |
| 13.750 | 0.07 | 10.81 | 11.09 | 0.00 | 0.14 | 986 | 79.13 |
| 13.800 | 0.07 | 10.66 | 10.94 | 0.00 | 0.14 | 972 | 79.13 |
| 13.850 | 0.06 | 10.51 | 10.79 | 0.00 | 0.14 | 958 | 79.12 |
| 13.900 | 0.06 | 10.35 | 10.64 | 0.00 | 0.14 | 945 | 79.12 |
| 13.950 | 0.06 | 10.20 | 10.48 | 0.00 | 0.14 | 930 | 79.12 |
| 14.000 | 0.06 | 10.04 | 10.32 | 0.00 | 0.14 | 916 | 79.11 |
| 14.050 | 0.06 | 9.87 | 10.15 | 0.00 | 0.14 | 901 | 79.11 |
| 14.100 | 0.06 | 9.71 | 9.99 | 0.00 | 0.14 | 886 | 79.10 |
| 14.150 | 0.06 | 9.54 | 9.82 | 0.00 | 0.14 | 871 | 79.10 |
| 14.200 | 0.06 | 9.37 | 9.65 | 0.00 | 0.14 | 856 | 79.09 |
| 14.250 | 0.06 | 9.20 | 9.48 | 0.00 | 0.14 | 841 | 79.09 |
| 14.300 | 0.05 | 9.03 | 9.31 | 0.00 | 0.14 | 825 | 79.08 |
| 14.350 | 0.05 | 8.86 | 9.14 | 0.00 | 0.14 | 810 | 79.08 |
| 14.400 | 0.05 | 8.68 | 8.96 | 0.00 | 0.14 | 794 | 79.07 |
| 14.450 | 0.05 | 8.51 | 8.79 | 0.00 | 0.14 | 778 | 79.07 |
| 14.500 | 0.05 | 8.33 | 8.61 | 0.00 | 0.14 | 762 | 79.06 |
| 14.550 | 0.05 | 8.15 | 8.43 | 0.00 | 0.14 | 746 | 79.05 |
| 14.600 | 0.05 | 7.97 | 8.25 | 0.00 | 0.14 | 730 | 79.05 |
| 14.650 | 0.05 | 7.79 | 8.07 | 0.00 | 0.14 | 714 | 79.04 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.05 | 7.61 | 7.89 | 0.00 | 0.14 | 697 | 79.04 |
| 14.750 | 0.05 | 7.42 | 7.70 | 0.00 | 0.14 | 681 | 79.03 |
| 14.800 | 0.05 | 7.24 | 7.52 | 0.00 | 0.14 | 664 | 79.03 |
| 14.850 | 0.05 | 7.05 | 7.33 | 0.00 | 0.14 | 647 | 79.02 |
| 14.900 | 0.05 | 6.86 | 7.15 | 0.00 | 0.14 | 630 | 79.02 |
| 14.950 | 0.05 | 6.67 | 6.96 | 0.00 | 0.14 | 613 | 79.01 |
| 15.000 | 0.05 | 6.48 | 6.77 | 0.00 | 0.14 | 596 | 79.01 |
| 15.050 | 0.04 | 6.29 | 6.57 | 0.00 | 0.14 | 579 | 79.00 |
| 15.100 | 0.04 | 6.10 | 6.38 | 0.00 | 0.14 | 562 | 78.99 |
| 15.150 | 0.04 | 5.90 | 6.19 | 0.00 | 0.14 | 544 | 78.99 |
| 15.200 | 0.04 | 5.71 | 5.99 | 0.00 | 0.14 | 526 | 78.98 |
| 15.250 | 0.04 | 5.51 | 5.79 | 0.00 | 0.14 | 509 | 78.98 |
| 15.300 | 0.04 | 5.31 | 5.59 | 0.00 | 0.14 | 491 | 78.97 |
| 15.350 | 0.04 | 5.11 | 5.39 | 0.00 | 0.14 | 473 | 78.96 |
| 15.400 | 0.04 | 4.91 | 5.19 | 0.00 | 0.14 | 455 | 78.96 |
| 15.450 | 0.04 | 4.71 | 4.99 | 0.00 | 0.14 | 436 | 78.95 |
| 15.500 | 0.04 | 4.50 | 4.79 | 0.00 | 0.14 | 418 | 78.95 |
| 15.550 | 0.04 | 4.30 | 4.58 | 0.00 | 0.14 | 399 | 78.94 |
| 15.600 | 0.04 | 4.09 | 4.37 | 0.00 | 0.14 | 381 | 78.93 |
| 15.650 | 0.04 | 3.88 | 4.16 | 0.00 | 0.14 | 362 | 78.93 |
| 15.700 | 0.04 | 3.67 | 3.96 | 0.00 | 0.14 | 343 | 78.92 |
| 15.750 | 0.04 | 3.46 | 3.74 | 0.00 | 0.14 | 324 | 78.92 |
| 15.800 | 0.03 | 3.25 | 3.53 | 0.00 | 0.14 | 305 | 78.91 |
| 15.850 | 0.03 | 3.04 | 3.32 | 0.00 | 0.14 | 286 | 78.90 |
| 15.900 | 0.03 | 2.82 | 3.10 | 0.00 | 0.14 | 267 | 78.90 |
| 15.950 | 0.03 | 2.61 | 2.89 | 0.00 | 0.14 | 247 | 78.89 |
| 16.000 | 0.03 | 2.39 | 2.67 | 0.00 | 0.14 | 228 | 78.88 |
| 16.050 | 0.03 | 2.17 | 2.45 | 0.00 | 0.14 | 208 | 78.88 |
| 16.100 | 0.03 | 1.95 | 2.23 | 0.00 | 0.14 | 188 | 78.87 |
| 16.150 | 0.03 | 1.73 | 2.01 | 0.00 | 0.14 | 168 | 78.87 |
| 16.200 | 0.03 | 1.51 | 1.79 | 0.00 | 0.14 | 148 | 78.86 |
| 16.250 | 0.03 | 1.28 | 1.57 | 0.00 | 0.14 | 128 | 78.85 |
| 16.300 | 0.03 | 1.06 | 1.34 | 0.00 | 0.14 | 108 | 78.85 |
| 16.350 | 0.03 | 0.84 | 1.12 | 0.00 | 0.14 | 88 | 78.84 |
| 16.400 | 0.03 | 0.61 | 0.90 | 0.00 | 0.14 | 68 | 78.83 |
| 16.450 | 0.03 | 0.39 | 0.67 | 0.00 | 0.14 | 48 | 78.83 |
| 16.500 | 0.03 | 0.16 | 0.45 | 0.00 | 0.14 | 28 | 78.82 |
| 16.550 | 0.03 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 16.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 16.650 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 16.700 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 16.750 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 16.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 16.900 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 16.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 17.000 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 17.050 | 0.02 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 17.100 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.150 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.200 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.400 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.450 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 17.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 17.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 18.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 18.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.600 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.650 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.700 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.750 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.800 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.850 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.900 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 19.950 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.000 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.050 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 20.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 20.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.250 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.300 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.350 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.400 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.450 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.500 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.550 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.600 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.650 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 21.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 22.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 22.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 22.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 22.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 22.200 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 22.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 22.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 1 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 1 year

Scenario: Post-Development 1 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 23.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 24.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.900 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.950 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.000 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 1.200 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.250 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.300 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.350 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.400 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.450 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.500 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.550 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.600 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.650 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.800 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.050 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.150 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.200 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.250 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 2.700 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.750 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.800 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 3.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 3.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 3.100 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 3.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.550 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 3.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 4.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.600 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.650 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.700 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 4.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 5.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 5.050 | 0.03 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 5.100 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.250 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.300 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.350 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.400 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.450 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.500 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.550 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 5.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.800 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.850 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.900 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 5.950 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.000 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.050 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.100 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.150 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.200 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.250 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 6.350 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 6.400 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 6.450 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 6.500 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 6.550 | 0.04 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 6.600 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 6.650 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 6.700 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 6.750 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 6.800 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.850 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 7.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 7.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 7.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 7.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 7.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 7.250 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 7.300 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 7.350 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 7.400 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 7.450 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 7.500 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 7.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 7.600 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 7.650 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 7.700 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 8.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 8.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 8.100 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 8.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 8.200 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 8.250 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 8.300 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 8.350 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 8.450 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 8.500 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 8.550 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 8.600 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 8.650 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 8.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.750 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.800 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.850 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.900 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 8.950 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 9.000 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |
| 9.050 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |
| 9.100 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 9.150 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 9.200 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 9.250 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 9.300 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 9.350 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 9.400 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 9.450 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 9.500 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 9.550 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 9.600 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 9.650 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 9.700 | 0.09 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 78.81 |
| 9.750 | 0.10 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 78.81 |
| 9.800 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 9.850 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 9.900 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 9.950 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 10.000 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 10.050 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 10.100 | 0.11 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 78.81 |
| 10.150 | 0.11 | 0.00 | 0.21 | 0.00 | 0.11 | 0 | 78.81 |
| 10.200 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 10.250 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 10.300 | 0.12 | 0.00 | 0.23 | 0.00 | 0.11 | 0 | 78.81 |
| 10.350 | 0.12 | 0.00 | 0.23 | 0.00 | 0.12 | 0 | 78.81 |
| 10.400 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 10.450 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.13 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 78.81 |
| 10.550 | 0.13 | 0.00 | 0.25 | 0.00 | 0.13 | 0 | 78.81 |
| 10.600 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 10.650 | 0.13 | 0.00 | 0.27 | 0.00 | 0.13 | 0 | 78.81 |
| 10.700 | 0.14 | 0.00 | 0.27 | 0.00 | 0.14 | 0 | 78.81 |
| 10.750 | 0.14 | 0.00 | 0.28 | 0.00 | 0.14 | 0 | 78.81 |
| 10.800 | 0.14 | 0.00 | 0.28 | 0.00 | 0.14 | 0 | 78.81 |
| 10.850 | 0.14 | 0.00 | 0.29 | 0.00 | 0.14 | 13 | 78.81 |
| 10.900 | 0.15 | 0.01 | 0.30 | 0.00 | 0.14 | 14 | 78.81 |
| 10.950 | 0.15 | 0.03 | 0.31 | 0.00 | 0.14 | 15 | 78.82 |
| 11.000 | 0.15 | 0.05 | 0.33 | 0.00 | 0.14 | 17 | 78.82 |
| 11.050 | 0.16 | 0.08 | 0.36 | 0.00 | 0.14 | 20 | 78.82 |
| 11.100 | 0.16 | 0.12 | 0.40 | 0.00 | 0.14 | 23 | 78.82 |
| 11.150 | 0.17 | 0.17 | 0.45 | 0.00 | 0.14 | 28 | 78.82 |
| 11.200 | 0.18 | 0.24 | 0.52 | 0.00 | 0.14 | 34 | 78.82 |
| 11.250 | 0.19 | 0.33 | 0.61 | 0.00 | 0.14 | 42 | 78.82 |
| 11.300 | 0.20 | 0.44 | 0.72 | 0.00 | 0.14 | 52 | 78.83 |
| 11.350 | 0.21 | 0.57 | 0.85 | 0.00 | 0.14 | 64 | 78.83 |
| 11.400 | 0.22 | 0.72 | 1.00 | 0.00 | 0.14 | 77 | 78.84 |
| 11.450 | 0.23 | 0.89 | 1.17 | 0.00 | 0.14 | 93 | 78.84 |
| 11.500 | 0.24 | 1.08 | 1.36 | 0.00 | 0.14 | 110 | 78.85 |
| 11.550 | 0.27 | 1.31 | 1.59 | 0.00 | 0.14 | 131 | 78.85 |
| 11.600 | 0.32 | 1.63 | 1.91 | 0.00 | 0.14 | 159 | 78.86 |
| 11.650 | 0.39 | 2.07 | 2.35 | 0.00 | 0.14 | 199 | 78.88 |
| 11.700 | 0.49 | 2.67 | 2.95 | 0.00 | 0.14 | 253 | 78.89 |
| 11.750 | 0.58 | 3.46 | 3.74 | 0.00 | 0.14 | 324 | 78.92 |
| 11.800 | 0.68 | 4.44 | 4.72 | 0.00 | 0.14 | 412 | 78.95 |
| 11.850 | 0.77 | 5.61 | 5.89 | 0.00 | 0.14 | 518 | 78.98 |
| 11.900 | 0.88 | 6.98 | 7.26 | 0.00 | 0.14 | 641 | 79.02 |
| 11.950 | 1.15 | 8.73 | 9.01 | 0.00 | 0.14 | 798 | 79.07 |
| 12.000 | 1.60 | 11.19 | 11.47 | 0.00 | 0.14 | 1,020 | 79.14 |
| 12.050 | 1.76 | 14.27 | 14.55 | 0.00 | 0.14 | 1,297 | 79.24 |
| 12.100 | 1.81 | 17.55 | 17.83 | 0.00 | 0.14 | 1,592 | 79.33 |
| 12.150 | 1.59 | 20.66 | 20.95 | 0.00 | 0.14 | 1,872 | 79.42 |
| 12.200 | 1.16 | 23.13 | 23.41 | 0.00 | 0.14 | 2,094 | 79.50 |
| 12.250 | 0.95 | 24.95 | 25.23 | 0.00 | 0.14 | 2,258 | 79.55 |
| 12.300 | 0.81 | 26.42 | 26.70 | 0.00 | 0.14 | 2,390 | 79.59 |
| 12.350 | 0.71 | 27.65 | 27.93 | 0.00 | 0.14 | 2,501 | 79.63 |
| 12.400 | 0.60 | 28.68 | 28.96 | 0.00 | 0.14 | 2,594 | 79.66 |
| 12.450 | 0.51 | 29.51 | 29.79 | 0.00 | 0.14 | 2,668 | 79.68 |
| 12.500 | 0.41 | 30.15 | 30.43 | 0.00 | 0.14 | 2,726 | 79.70 |
| 12.550 | 0.34 | 30.62 | 30.90 | 0.00 | 0.14 | 2,768 | 79.72 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.28 | 30.96 | 31.24 | 0.00 | 0.14 | 2,799 | 79.73 |
| 12.650 | 0.25 | 31.21 | 31.49 | 0.00 | 0.14 | 2,821 | 79.74 |
| 12.700 | 0.24 | 31.42 | 31.70 | 0.00 | 0.14 | 2,840 | 79.74 |
| 12.750 | 0.23 | 31.60 | 31.88 | 0.00 | 0.14 | 2,857 | 79.75 |
| 12.800 | 0.22 | 31.76 | 32.04 | 0.00 | 0.14 | 2,871 | 79.75 |
| 12.850 | 0.21 | 31.90 | 32.18 | 0.00 | 0.14 | 2,883 | 79.76 |
| 12.900 | 0.19 | 32.02 | 32.30 | 0.00 | 0.14 | 2,894 | 79.76 |
| 12.950 | 0.19 | 32.12 | 32.40 | 0.00 | 0.14 | 2,903 | 79.76 |
| 13.000 | 0.17 | 32.20 | 32.48 | 0.00 | 0.14 | 2,910 | 79.76 |
| 13.050 | 0.17 | 32.26 | 32.54 | 0.00 | 0.14 | 2,916 | 79.77 |
| 13.100 | 0.16 | 32.30 | 32.58 | 0.00 | 0.14 | 2,920 | 79.77 |
| 13.150 | 0.16 | 32.34 | 32.62 | 0.00 | 0.14 | 2,923 | 79.77 |
| 13.200 | 0.15 | 32.37 | 32.65 | 0.00 | 0.14 | 2,926 | 79.77 |
| 13.250 | 0.15 | 32.39 | 32.67 | 0.00 | 0.14 | 2,928 | 79.77 |
| 13.300 | 0.15 | 32.40 | 32.69 | 0.00 | 0.14 | 2,929 | 79.77 |
| 13.350 | 0.15 | 32.42 | 32.70 | 0.00 | 0.14 | 2,930 | 79.77 |
| 13.400 | 0.14 | 32.42 | 32.70 | 0.00 | 0.14 | 2,931 | 79.77 |
| 13.450 | 0.14 | 32.42 | 32.70 | 0.00 | 0.14 | 2,931 | 79.77 |
| 13.500 | 0.14 | 32.42 | 32.70 | 0.00 | 0.14 | 2,930 | 79.77 |
| 13.550 | 0.13 | 32.41 | 32.69 | 0.00 | 0.14 | 2,929 | 79.77 |
| 13.600 | 0.13 | 32.39 | 32.68 | 0.00 | 0.14 | 2,928 | 79.77 |
| 13.650 | 0.13 | 32.37 | 32.66 | 0.00 | 0.14 | 2,926 | 79.77 |
| 13.700 | 0.13 | 32.35 | 32.63 | 0.00 | 0.14 | 2,924 | 79.77 |
| 13.750 | 0.12 | 32.32 | 32.60 | 0.00 | 0.14 | 2,921 | 79.77 |
| 13.800 | 0.12 | 32.28 | 32.56 | 0.00 | 0.14 | 2,918 | 79.77 |
| 13.850 | 0.12 | 32.24 | 32.52 | 0.00 | 0.14 | 2,914 | 79.77 |
| 13.900 | 0.12 | 32.20 | 32.48 | 0.00 | 0.14 | 2,910 | 79.76 |
| 13.950 | 0.11 | 32.14 | 32.43 | 0.00 | 0.14 | 2,906 | 79.76 |
| 14.000 | 0.11 | 32.09 | 32.37 | 0.00 | 0.14 | 2,901 | 79.76 |
| 14.050 | 0.11 | 32.03 | 32.31 | 0.00 | 0.14 | 2,895 | 79.76 |
| 14.100 | 0.11 | 31.96 | 32.24 | 0.00 | 0.14 | 2,889 | 79.76 |
| 14.150 | 0.11 | 31.89 | 32.17 | 0.00 | 0.14 | 2,883 | 79.76 |
| 14.200 | 0.10 | 31.82 | 32.10 | 0.00 | 0.14 | 2,876 | 79.75 |
| 14.250 | 0.10 | 31.74 | 32.03 | 0.00 | 0.14 | 2,870 | 79.75 |
| 14.300 | 0.10 | 31.67 | 31.95 | 0.00 | 0.14 | 2,863 | 79.75 |
| 14.350 | 0.10 | 31.59 | 31.87 | 0.00 | 0.14 | 2,855 | 79.75 |
| 14.400 | 0.10 | 31.50 | 31.79 | 0.00 | 0.14 | 2,848 | 79.74 |
| 14.450 | 0.10 | 31.42 | 31.70 | 0.00 | 0.14 | 2,840 | 79.74 |
| 14.500 | 0.10 | 31.33 | 31.61 | 0.00 | 0.14 | 2,832 | 79.74 |
| 14.550 | 0.10 | 31.24 | 31.52 | 0.00 | 0.14 | 2,824 | 79.74 |
| 14.600 | 0.09 | 31.15 | 31.43 | 0.00 | 0.14 | 2,816 | 79.73 |
| 14.650 | 0.09 | 31.05 | 31.34 | 0.00 | 0.14 | 2,807 | 79.73 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.09 | 30.96 | 31.24 | 0.00 | 0.14 | 2,799 | 79.73 |
| 14.750 | 0.09 | 30.86 | 31.14 | 0.00 | 0.14 | 2,790 | 79.72 |
| 14.800 | 0.09 | 30.75 | 31.04 | 0.00 | 0.14 | 2,780 | 79.72 |
| 14.850 | 0.09 | 30.65 | 30.93 | 0.00 | 0.14 | 2,771 | 79.72 |
| 14.900 | 0.09 | 30.54 | 30.82 | 0.00 | 0.14 | 2,761 | 79.72 |
| 14.950 | 0.09 | 30.43 | 30.71 | 0.00 | 0.14 | 2,751 | 79.71 |
| 15.000 | 0.08 | 30.32 | 30.60 | 0.00 | 0.14 | 2,741 | 79.71 |
| 15.050 | 0.08 | 30.20 | 30.48 | 0.00 | 0.14 | 2,731 | 79.71 |
| 15.100 | 0.08 | 30.09 | 30.37 | 0.00 | 0.14 | 2,720 | 79.70 |
| 15.150 | 0.08 | 29.97 | 30.25 | 0.00 | 0.14 | 2,710 | 79.70 |
| 15.200 | 0.08 | 29.84 | 30.12 | 0.00 | 0.14 | 2,699 | 79.69 |
| 15.250 | 0.08 | 29.72 | 30.00 | 0.00 | 0.14 | 2,687 | 79.69 |
| 15.300 | 0.08 | 29.59 | 29.87 | 0.00 | 0.14 | 2,676 | 79.69 |
| 15.350 | 0.08 | 29.46 | 29.74 | 0.00 | 0.14 | 2,664 | 79.68 |
| 15.400 | 0.07 | 29.33 | 29.61 | 0.00 | 0.14 | 2,652 | 79.68 |
| 15.450 | 0.07 | 29.19 | 29.47 | 0.00 | 0.14 | 2,640 | 79.68 |
| 15.500 | 0.07 | 29.05 | 29.34 | 0.00 | 0.14 | 2,628 | 79.67 |
| 15.550 | 0.07 | 28.91 | 29.20 | 0.00 | 0.14 | 2,615 | 79.67 |
| 15.600 | 0.07 | 28.77 | 29.05 | 0.00 | 0.14 | 2,602 | 79.66 |
| 15.650 | 0.07 | 28.63 | 28.91 | 0.00 | 0.14 | 2,589 | 79.66 |
| 15.700 | 0.07 | 28.48 | 28.76 | 0.00 | 0.14 | 2,576 | 79.65 |
| 15.750 | 0.07 | 28.33 | 28.61 | 0.00 | 0.14 | 2,562 | 79.65 |
| 15.800 | 0.06 | 28.17 | 28.46 | 0.00 | 0.14 | 2,548 | 79.65 |
| 15.850 | 0.06 | 28.02 | 28.30 | 0.00 | 0.14 | 2,534 | 79.64 |
| 15.900 | 0.06 | 27.86 | 28.14 | 0.00 | 0.14 | 2,520 | 79.64 |
| 15.950 | 0.06 | 27.70 | 27.98 | 0.00 | 0.14 | 2,506 | 79.63 |
| 16.000 | 0.06 | 27.54 | 27.82 | 0.00 | 0.14 | 2,491 | 79.63 |
| 16.050 | 0.06 | 27.37 | 27.66 | 0.00 | 0.14 | 2,476 | 79.62 |
| 16.100 | 0.06 | 27.21 | 27.49 | 0.00 | 0.14 | 2,461 | 79.62 |
| 16.150 | 0.06 | 27.04 | 27.32 | 0.00 | 0.14 | 2,446 | 79.61 |
| 16.200 | 0.06 | 26.87 | 27.15 | 0.00 | 0.14 | 2,431 | 79.61 |
| 16.250 | 0.05 | 26.70 | 26.98 | 0.00 | 0.14 | 2,415 | 79.60 |
| 16.300 | 0.05 | 26.52 | 26.81 | 0.00 | 0.14 | 2,400 | 79.60 |
| 16.350 | 0.05 | 26.35 | 26.63 | 0.00 | 0.14 | 2,384 | 79.59 |
| 16.400 | 0.05 | 26.18 | 26.46 | 0.00 | 0.14 | 2,369 | 79.59 |
| 16.450 | 0.05 | 26.00 | 26.28 | 0.00 | 0.14 | 2,353 | 79.58 |
| 16.500 | 0.05 | 25.82 | 26.11 | 0.00 | 0.14 | 2,337 | 79.58 |
| 16.550 | 0.05 | 25.65 | 25.93 | 0.00 | 0.14 | 2,321 | 79.57 |
| 16.600 | 0.05 | 25.47 | 25.75 | 0.00 | 0.14 | 2,305 | 79.57 |
| 16.650 | 0.05 | 25.29 | 25.57 | 0.00 | 0.14 | 2,289 | 79.56 |
| 16.700 | 0.05 | 25.11 | 25.39 | 0.00 | 0.14 | 2,272 | 79.55 |
| 16.750 | 0.05 | 24.92 | 25.21 | 0.00 | 0.14 | 2,256 | 79.55 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.05 | 24.74 | 25.02 | 0.00 | 0.14 | 2,239 | 79.54 |
| 16.850 | 0.05 | 24.56 | 24.84 | 0.00 | 0.14 | 2,223 | 79.54 |
| 16.900 | 0.05 | 24.37 | 24.65 | 0.00 | 0.14 | 2,206 | 79.53 |
| 16.950 | 0.05 | 24.18 | 24.47 | 0.00 | 0.14 | 2,189 | 79.53 |
| 17.000 | 0.05 | 24.00 | 24.28 | 0.00 | 0.14 | 2,172 | 79.52 |
| 17.050 | 0.05 | 23.81 | 24.09 | 0.00 | 0.14 | 2,155 | 79.52 |
| 17.100 | 0.05 | 23.62 | 23.90 | 0.00 | 0.14 | 2,138 | 79.51 |
| 17.150 | 0.05 | 23.43 | 23.71 | 0.00 | 0.14 | 2,121 | 79.51 |
| 17.200 | 0.04 | 23.24 | 23.52 | 0.00 | 0.14 | 2,104 | 79.50 |
| 17.250 | 0.04 | 23.04 | 23.32 | 0.00 | 0.14 | 2,086 | 79.49 |
| 17.300 | 0.04 | 22.85 | 23.13 | 0.00 | 0.14 | 2,069 | 79.49 |
| 17.350 | 0.04 | 22.65 | 22.93 | 0.00 | 0.14 | 2,051 | 79.48 |
| 17.400 | 0.04 | 22.46 | 22.74 | 0.00 | 0.14 | 2,034 | 79.48 |
| 17.450 | 0.04 | 22.26 | 22.54 | 0.00 | 0.14 | 2,016 | 79.47 |
| 17.500 | 0.04 | 22.06 | 22.34 | 0.00 | 0.14 | 1,998 | 79.47 |
| 17.550 | 0.04 | 21.86 | 22.14 | 0.00 | 0.14 | 1,980 | 79.46 |
| 17.600 | 0.04 | 21.66 | 21.94 | 0.00 | 0.14 | 1,962 | 79.45 |
| 17.650 | 0.04 | 21.46 | 21.74 | 0.00 | 0.14 | 1,944 | 79.45 |
| 17.700 | 0.04 | 21.25 | 21.54 | 0.00 | 0.14 | 1,926 | 79.44 |
| 17.750 | 0.04 | 21.05 | 21.33 | 0.00 | 0.14 | 1,907 | 79.44 |
| 17.800 | 0.04 | 20.85 | 21.13 | 0.00 | 0.14 | 1,889 | 79.43 |
| 17.850 | 0.04 | 20.64 | 20.92 | 0.00 | 0.14 | 1,870 | 79.42 |
| 17.900 | 0.04 | 20.43 | 20.71 | 0.00 | 0.14 | 1,852 | 79.42 |
| 17.950 | 0.04 | 20.22 | 20.51 | 0.00 | 0.14 | 1,833 | 79.41 |
| 18.000 | 0.04 | 20.01 | 20.30 | 0.00 | 0.14 | 1,814 | 79.40 |
| 18.050 | 0.04 | 19.80 | 20.09 | 0.00 | 0.14 | 1,795 | 79.40 |
| 18.100 | 0.03 | 19.59 | 19.87 | 0.00 | 0.14 | 1,776 | 79.39 |
| 18.150 | 0.03 | 19.38 | 19.66 | 0.00 | 0.14 | 1,757 | 79.39 |
| 18.200 | 0.03 | 19.17 | 19.45 | 0.00 | 0.14 | 1,738 | 79.38 |
| 18.250 | 0.03 | 18.96 | 19.24 | 0.00 | 0.14 | 1,719 | 79.37 |
| 18.300 | 0.03 | 18.74 | 19.02 | 0.00 | 0.14 | 1,699 | 79.37 |
| 18.350 | 0.03 | 18.53 | 18.81 | 0.00 | 0.14 | 1,680 | 79.36 |
| 18.400 | 0.03 | 18.31 | 18.60 | 0.00 | 0.14 | 1,661 | 79.35 |
| 18.450 | 0.03 | 18.10 | 18.38 | 0.00 | 0.14 | 1,642 | 79.35 |
| 18.500 | 0.03 | 17.89 | 18.17 | 0.00 | 0.14 | 1,622 | 79.34 |
| 18.550 | 0.03 | 17.67 | 17.95 | 0.00 | 0.14 | 1,603 | 79.34 |
| 18.600 | 0.03 | 17.46 | 17.74 | 0.00 | 0.14 | 1,584 | 79.33 |
| 18.650 | 0.03 | 17.24 | 17.52 | 0.00 | 0.14 | 1,564 | 79.32 |
| 18.700 | 0.03 | 17.03 | 17.31 | 0.00 | 0.14 | 1,545 | 79.32 |
| 18.750 | 0.03 | 16.81 | 17.09 | 0.00 | 0.14 | 1,526 | 79.31 |
| 18.800 | 0.03 | 16.59 | 16.88 | 0.00 | 0.14 | 1,506 | 79.30 |
| 18.850 | 0.03 | 16.38 | 16.66 | 0.00 | 0.14 | 1,487 | 79.30 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.03 | 16.16 | 16.44 | 0.00 | 0.14 | 1,467 | 79.29 |
| 18.950 | 0.03 | 15.94 | 16.22 | 0.00 | 0.14 | 1,447 | 79.28 |
| 19.000 | 0.03 | 15.72 | 16.01 | 0.00 | 0.14 | 1,428 | 79.28 |
| 19.050 | 0.03 | 15.51 | 15.79 | 0.00 | 0.14 | 1,408 | 79.27 |
| 19.100 | 0.03 | 15.29 | 15.57 | 0.00 | 0.14 | 1,389 | 79.27 |
| 19.150 | 0.03 | 15.07 | 15.35 | 0.00 | 0.14 | 1,369 | 79.26 |
| 19.200 | 0.03 | 14.85 | 15.13 | 0.00 | 0.14 | 1,349 | 79.25 |
| 19.250 | 0.03 | 14.63 | 14.91 | 0.00 | 0.14 | 1,330 | 79.25 |
| 19.300 | 0.03 | 14.41 | 14.69 | 0.00 | 0.14 | 1,310 | 79.24 |
| 19.350 | 0.03 | 14.19 | 14.47 | 0.00 | 0.14 | 1,290 | 79.23 |
| 19.400 | 0.03 | 13.97 | 14.25 | 0.00 | 0.14 | 1,270 | 79.23 |
| 19.450 | 0.03 | 13.75 | 14.03 | 0.00 | 0.14 | 1,250 | 79.22 |
| 19.500 | 0.03 | 13.53 | 13.81 | 0.00 | 0.14 | 1,230 | 79.21 |
| 19.550 | 0.03 | 13.31 | 13.59 | 0.00 | 0.14 | 1,210 | 79.21 |
| 19.600 | 0.03 | 13.09 | 13.37 | 0.00 | 0.14 | 1,191 | 79.20 |
| 19.650 | 0.03 | 12.87 | 13.15 | 0.00 | 0.14 | 1,171 | 79.19 |
| 19.700 | 0.03 | 12.64 | 12.93 | 0.00 | 0.14 | 1,151 | 79.19 |
| 19.750 | 0.03 | 12.42 | 12.70 | 0.00 | 0.14 | 1,131 | 79.18 |
| 19.800 | 0.03 | 12.20 | 12.48 | 0.00 | 0.14 | 1,110 | 79.17 |
| 19.850 | 0.03 | 11.97 | 12.26 | 0.00 | 0.14 | 1,090 | 79.17 |
| 19.900 | 0.03 | 11.75 | 12.03 | 0.00 | 0.14 | 1,070 | 79.16 |
| 19.950 | 0.03 | 11.53 | 11.81 | 0.00 | 0.14 | 1,050 | 79.15 |
| 20.000 | 0.03 | 11.30 | 11.58 | 0.00 | 0.14 | 1,030 | 79.15 |
| 20.050 | 0.03 | 11.08 | 11.36 | 0.00 | 0.14 | 1,010 | 79.14 |
| 20.100 | 0.03 | 10.85 | 11.14 | 0.00 | 0.14 | 990 | 79.13 |
| 20.150 | 0.03 | 10.63 | 10.91 | 0.00 | 0.14 | 969 | 79.13 |
| 20.200 | 0.03 | 10.40 | 10.68 | 0.00 | 0.14 | 949 | 79.12 |
| 20.250 | 0.03 | 10.18 | 10.46 | 0.00 | 0.14 | 929 | 79.11 |
| 20.300 | 0.03 | 9.95 | 10.23 | 0.00 | 0.14 | 908 | 79.11 |
| 20.350 | 0.03 | 9.73 | 10.01 | 0.00 | 0.14 | 888 | 79.10 |
| 20.400 | 0.03 | 9.50 | 9.78 | 0.00 | 0.14 | 868 | 79.09 |
| 20.450 | 0.03 | 9.27 | 9.55 | 0.00 | 0.14 | 847 | 79.09 |
| 20.500 | 0.03 | 9.05 | 9.33 | 0.00 | 0.14 | 827 | 79.08 |
| 20.550 | 0.03 | 8.82 | 9.10 | 0.00 | 0.14 | 806 | 79.07 |
| 20.600 | 0.03 | 8.59 | 8.87 | 0.00 | 0.14 | 786 | 79.07 |
| 20.650 | 0.03 | 8.36 | 8.65 | 0.00 | 0.14 | 765 | 79.06 |
| 20.700 | 0.03 | 8.14 | 8.42 | 0.00 | 0.14 | 745 | 79.05 |
| 20.750 | 0.03 | 7.91 | 8.19 | 0.00 | 0.14 | 724 | 79.05 |
| 20.800 | 0.03 | 7.68 | 7.96 | 0.00 | 0.14 | 704 | 79.04 |
| 20.850 | 0.03 | 7.45 | 7.73 | 0.00 | 0.14 | 683 | 79.03 |
| 20.900 | 0.03 | 7.22 | 7.50 | 0.00 | 0.14 | 663 | 79.03 |
| 20.950 | 0.03 | 6.99 | 7.28 | 0.00 | 0.14 | 642 | 79.02 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.03 | 6.76 | 7.05 | 0.00 | 0.14 | 621 | 79.01 |
| 21.050 | 0.03 | 6.53 | 6.82 | 0.00 | 0.14 | 601 | 79.01 |
| 21.100 | 0.03 | 6.31 | 6.59 | 0.00 | 0.14 | 580 | 79.00 |
| 21.150 | 0.03 | 6.08 | 6.36 | 0.00 | 0.14 | 559 | 78.99 |
| 21.200 | 0.03 | 5.84 | 6.13 | 0.00 | 0.14 | 539 | 78.99 |
| 21.250 | 0.03 | 5.61 | 5.90 | 0.00 | 0.14 | 518 | 78.98 |
| 21.300 | 0.03 | 5.38 | 5.67 | 0.00 | 0.14 | 497 | 78.97 |
| 21.350 | 0.03 | 5.15 | 5.43 | 0.00 | 0.14 | 476 | 78.97 |
| 21.400 | 0.03 | 4.92 | 5.20 | 0.00 | 0.14 | 456 | 78.96 |
| 21.450 | 0.03 | 4.69 | 4.97 | 0.00 | 0.14 | 435 | 78.95 |
| 21.500 | 0.02 | 4.46 | 4.74 | 0.00 | 0.14 | 414 | 78.95 |
| 21.550 | 0.02 | 4.23 | 4.51 | 0.00 | 0.14 | 393 | 78.94 |
| 21.600 | 0.02 | 3.99 | 4.28 | 0.00 | 0.14 | 372 | 78.93 |
| 21.650 | 0.02 | 3.76 | 4.04 | 0.00 | 0.14 | 351 | 78.93 |
| 21.700 | 0.02 | 3.53 | 3.81 | 0.00 | 0.14 | 330 | 78.92 |
| 21.750 | 0.02 | 3.30 | 3.58 | 0.00 | 0.14 | 309 | 78.91 |
| 21.800 | 0.02 | 3.06 | 3.34 | 0.00 | 0.14 | 288 | 78.90 |
| 21.850 | 0.02 | 2.83 | 3.11 | 0.00 | 0.14 | 267 | 78.90 |
| 21.900 | 0.02 | 2.60 | 2.88 | 0.00 | 0.14 | 246 | 78.89 |
| 21.950 | 0.02 | 2.36 | 2.64 | 0.00 | 0.14 | 225 | 78.88 |
| 22.000 | 0.02 | 2.13 | 2.41 | 0.00 | 0.14 | 204 | 78.88 |
| 22.050 | 0.02 | 1.89 | 2.17 | 0.00 | 0.14 | 183 | 78.87 |
| 22.100 | 0.02 | 1.66 | 1.94 | 0.00 | 0.14 | 162 | 78.86 |
| 22.150 | 0.02 | 1.42 | 1.70 | 0.00 | 0.14 | 141 | 78.86 |
| 22.200 | 0.02 | 1.19 | 1.47 | 0.00 | 0.14 | 120 | 78.85 |
| 22.250 | 0.02 | 0.95 | 1.23 | 0.00 | 0.14 | 98 | 78.84 |
| 22.300 | 0.02 | 0.72 | 1.00 | 0.00 | 0.14 | 77 | 78.84 |
| 22.350 | 0.02 | 0.48 | 0.76 | 0.00 | 0.14 | 56 | 78.83 |
| 22.400 | 0.02 | 0.24 | 0.53 | 0.00 | 0.14 | 35 | 78.82 |
| 22.450 | 0.02 | 0.01 | 0.29 | 0.00 | 0.14 | 13 | 78.81 |
| 22.500 | 0.02 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 22.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 22.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 10 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 10 year

Scenario: Post-Development 10 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.250 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 23.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 24.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.650 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.700 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.750 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.800 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.850 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.900 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 0.950 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.000 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.050 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 1.100 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.150 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.200 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.250 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 1.300 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.350 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.400 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.450 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.500 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.550 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.600 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.650 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.700 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.750 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.850 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 1.900 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 1.950 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.000 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.150 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 2.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 2.300 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 2.350 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 2.400 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 2.450 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 2.500 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 2.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.700 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.750 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.800 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.850 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.900 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 2.950 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.000 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.050 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.100 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.150 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.200 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 3.250 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.300 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.350 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.400 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.450 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.500 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.550 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 3.600 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.650 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.700 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.750 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.800 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.850 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.900 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 3.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 4.000 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.050 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.100 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.150 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.250 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.750 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 4.800 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 4.850 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 4.900 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 4.950 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 5.000 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 5.050 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 5.100 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 5.150 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 5.200 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 5.250 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.300 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.350 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.400 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.450 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.500 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.550 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.600 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.650 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 5.700 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 5.750 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 5.800 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 5.850 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 5.900 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 5.950 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.000 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.050 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.100 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.150 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.200 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 6.350 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 6.400 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 6.450 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 6.500 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 6.550 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 6.600 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 6.650 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 6.700 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 6.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 6.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 6.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 6.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 6.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 7.050 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 7.100 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 7.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 7.200 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 7.250 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 7.300 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 7.350 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.400 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.450 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.500 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.550 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.600 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.650 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 7.700 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 7.750 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 7.800 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 7.850 | 0.07 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 7.900 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 7.950 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 8.000 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 8.050 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.100 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.150 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.200 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 8.250 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 8.300 | 0.08 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 8.350 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 8.450 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 8.500 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 8.550 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 8.600 | 0.09 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 8.650 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 8.700 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 8.750 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 8.800 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 8.850 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 8.900 | 0.09 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 78.81 |
| 8.950 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 9.000 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 9.050 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 9.100 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 9.150 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 9.200 | 0.10 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 78.81 |
| 9.250 | 0.11 | 0.00 | 0.21 | 0.00 | 0.11 | 0 | 78.81 |
| 9.300 | 0.11 | 0.00 | 0.21 | 0.00 | 0.11 | 0 | 78.81 |
| 9.350 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 9.400 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 9.450 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 9.500 | 0.11 | 0.00 | 0.23 | 0.00 | 0.11 | 0 | 78.81 |
| 9.550 | 0.12 | 0.00 | 0.23 | 0.00 | 0.12 | 0 | 78.81 |
| 9.600 | 0.12 | 0.00 | 0.23 | 0.00 | 0.12 | 0 | 78.81 |
| 9.650 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 9.700 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 9.750 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 9.800 | 0.12 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 78.81 |
| 9.850 | 0.13 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 78.81 |
| 9.900 | 0.13 | 0.00 | 0.25 | 0.00 | 0.13 | 0 | 78.81 |
| 9.950 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 10.000 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 10.050 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 10.100 | 0.14 | 0.00 | 0.27 | 0.00 | 0.13 | 0 | 78.81 |
| 10.150 | 0.14 | 0.00 | 0.27 | 0.00 | 0.14 | 0 | 78.81 |
| 10.200 | 0.14 | 0.00 | 0.28 | 0.00 | 0.14 | 0 | 78.81 |
| 10.250 | 0.14 | 0.00 | 0.29 | 0.00 | 0.14 | 13 | 78.81 |
| 10.300 | 0.15 | 0.01 | 0.30 | 0.00 | 0.14 | 14 | 78.81 |
| 10.350 | 0.15 | 0.03 | 0.31 | 0.00 | 0.14 | 16 | 78.82 |
| 10.400 | 0.15 | 0.06 | 0.34 | 0.00 | 0.14 | 18 | 78.82 |
| 10.450 | 0.16 | 0.09 | 0.37 | 0.00 | 0.14 | 20 | 78.82 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.16 | 0.12 | 0.40 | 0.00 | 0.14 | 24 | 78.82 |
| 10.550 | 0.16 | 0.17 | 0.45 | 0.00 | 0.14 | 28 | 78.82 |
| 10.600 | 0.17 | 0.22 | 0.50 | 0.00 | 0.14 | 32 | 78.82 |
| 10.650 | 0.17 | 0.27 | 0.56 | 0.00 | 0.14 | 37 | 78.82 |
| 10.700 | 0.17 | 0.34 | 0.62 | 0.00 | 0.14 | 43 | 78.82 |
| 10.750 | 0.18 | 0.41 | 0.69 | 0.00 | 0.14 | 50 | 78.83 |
| 10.800 | 0.18 | 0.49 | 0.77 | 0.00 | 0.14 | 56 | 78.83 |
| 10.850 | 0.18 | 0.57 | 0.85 | 0.00 | 0.14 | 64 | 78.83 |
| 10.900 | 0.19 | 0.66 | 0.94 | 0.00 | 0.14 | 72 | 78.83 |
| 10.950 | 0.19 | 0.76 | 1.04 | 0.00 | 0.14 | 81 | 78.84 |
| 11.000 | 0.19 | 0.86 | 1.15 | 0.00 | 0.14 | 90 | 78.84 |
| 11.050 | 0.20 | 0.98 | 1.26 | 0.00 | 0.14 | 101 | 78.84 |
| 11.100 | 0.21 | 1.10 | 1.39 | 0.00 | 0.14 | 112 | 78.85 |
| 11.150 | 0.22 | 1.25 | 1.53 | 0.00 | 0.14 | 125 | 78.85 |
| 11.200 | 0.23 | 1.42 | 1.70 | 0.00 | 0.14 | 140 | 78.86 |
| 11.250 | 0.24 | 1.61 | 1.89 | 0.00 | 0.14 | 157 | 78.86 |
| 11.300 | 0.26 | 1.83 | 2.11 | 0.00 | 0.14 | 177 | 78.87 |
| 11.350 | 0.27 | 2.07 | 2.35 | 0.00 | 0.14 | 199 | 78.88 |
| 11.400 | 0.28 | 2.34 | 2.62 | 0.00 | 0.14 | 223 | 78.88 |
| 11.450 | 0.29 | 2.63 | 2.91 | 0.00 | 0.14 | 250 | 78.89 |
| 11.500 | 0.31 | 2.95 | 3.23 | 0.00 | 0.14 | 278 | 78.90 |
| 11.550 | 0.35 | 3.33 | 3.61 | 0.00 | 0.14 | 312 | 78.91 |
| 11.600 | 0.41 | 3.81 | 4.09 | 0.00 | 0.14 | 355 | 78.93 |
| 11.650 | 0.50 | 4.44 | 4.72 | 0.00 | 0.14 | 412 | 78.95 |
| 11.700 | 0.63 | 5.29 | 5.57 | 0.00 | 0.14 | 489 | 78.97 |
| 11.750 | 0.74 | 6.37 | 6.66 | 0.00 | 0.14 | 586 | 79.00 |
| 11.800 | 0.87 | 7.70 | 7.98 | 0.00 | 0.14 | 706 | 79.04 |
| 11.850 | 0.98 | 9.27 | 9.55 | 0.00 | 0.14 | 847 | 79.09 |
| 11.900 | 1.12 | 11.08 | 11.36 | 0.00 | 0.14 | 1,010 | 79.14 |
| 11.950 | 1.46 | 13.38 | 13.66 | 0.00 | 0.14 | 1,217 | 79.21 |
| 12.000 | 2.03 | 16.59 | 16.87 | 0.00 | 0.14 | 1,506 | 79.30 |
| 12.050 | 2.24 | 20.57 | 20.85 | 0.00 | 0.14 | 1,864 | 79.42 |
| 12.100 | 2.30 | 24.82 | 25.11 | 0.00 | 0.14 | 2,247 | 79.55 |
| 12.150 | 2.01 | 28.85 | 29.13 | 0.00 | 0.14 | 2,609 | 79.67 |
| 12.200 | 1.47 | 32.05 | 32.34 | 0.00 | 0.14 | 2,898 | 79.76 |
| 12.250 | 1.20 | 34.24 | 34.73 | 0.00 | 0.24 | 3,103 | 79.83 |
| 12.300 | 1.02 | 35.45 | 36.46 | 0.00 | 0.50 | 3,236 | 79.87 |
| 12.350 | 0.90 | 36.09 | 37.37 | 0.00 | 0.64 | 3,306 | 79.89 |
| 12.400 | 0.76 | 36.36 | 37.75 | 0.00 | 0.70 | 3,335 | 79.90 |
| 12.450 | 0.65 | 36.37 | 37.77 | 0.00 | 0.70 | 3,336 | 79.90 |
| 12.500 | 0.52 | 36.21 | 37.54 | 0.00 | 0.67 | 3,319 | 79.90 |
| 12.550 | 0.43 | 35.94 | 37.16 | 0.00 | 0.61 | 3,290 | 79.89 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.36 | 35.64 | 36.73 | 0.00 | 0.54 | 3,257 | 79.88 |
| 12.650 | 0.32 | 35.36 | 36.32 | 0.00 | 0.48 | 3,226 | 79.87 |
| 12.700 | 0.30 | 35.11 | 35.98 | 0.00 | 0.43 | 3,199 | 79.86 |
| 12.750 | 0.29 | 34.92 | 35.70 | 0.00 | 0.39 | 3,178 | 79.85 |
| 12.800 | 0.27 | 34.77 | 35.48 | 0.00 | 0.36 | 3,161 | 79.85 |
| 12.850 | 0.26 | 34.64 | 35.30 | 0.00 | 0.33 | 3,147 | 79.84 |
| 12.900 | 0.25 | 34.53 | 35.15 | 0.00 | 0.31 | 3,136 | 79.84 |
| 12.950 | 0.24 | 34.44 | 35.01 | 0.00 | 0.29 | 3,125 | 79.83 |
| 13.000 | 0.22 | 34.36 | 34.90 | 0.00 | 0.27 | 3,116 | 79.83 |
| 13.050 | 0.21 | 34.28 | 34.79 | 0.00 | 0.25 | 3,108 | 79.83 |
| 13.100 | 0.20 | 34.22 | 34.70 | 0.00 | 0.24 | 3,101 | 79.83 |
| 13.150 | 0.20 | 34.16 | 34.62 | 0.00 | 0.23 | 3,095 | 79.82 |
| 13.200 | 0.19 | 34.12 | 34.55 | 0.00 | 0.22 | 3,090 | 79.82 |
| 13.250 | 0.19 | 34.08 | 34.50 | 0.00 | 0.21 | 3,086 | 79.82 |
| 13.300 | 0.19 | 34.05 | 34.46 | 0.00 | 0.20 | 3,083 | 79.82 |
| 13.350 | 0.18 | 34.02 | 34.42 | 0.00 | 0.20 | 3,080 | 79.82 |
| 13.400 | 0.18 | 34.00 | 34.39 | 0.00 | 0.19 | 3,077 | 79.82 |
| 13.450 | 0.18 | 33.98 | 34.36 | 0.00 | 0.19 | 3,075 | 79.82 |
| 13.500 | 0.17 | 33.96 | 34.33 | 0.00 | 0.19 | 3,073 | 79.82 |
| 13.550 | 0.17 | 33.94 | 34.30 | 0.00 | 0.18 | 3,071 | 79.82 |
| 13.600 | 0.17 | 33.92 | 34.28 | 0.00 | 0.18 | 3,069 | 79.82 |
| 13.650 | 0.16 | 33.91 | 34.25 | 0.00 | 0.17 | 3,067 | 79.82 |
| 13.700 | 0.16 | 33.89 | 34.23 | 0.00 | 0.17 | 3,065 | 79.82 |
| 13.750 | 0.16 | 33.87 | 34.21 | 0.00 | 0.17 | 3,064 | 79.81 |
| 13.800 | 0.15 | 33.86 | 34.19 | 0.00 | 0.16 | 3,062 | 79.81 |
| 13.850 | 0.15 | 33.84 | 34.16 | 0.00 | 0.16 | 3,060 | 79.81 |
| 13.900 | 0.15 | 33.83 | 34.14 | 0.00 | 0.16 | 3,058 | 79.81 |
| 13.950 | 0.14 | 33.81 | 34.12 | 0.00 | 0.15 | 3,057 | 79.81 |
| 14.000 | 0.14 | 33.79 | 34.10 | 0.00 | 0.15 | 3,055 | 79.81 |
| 14.050 | 0.14 | 33.78 | 34.07 | 0.00 | 0.15 | 3,053 | 79.81 |
| 14.100 | 0.14 | 33.76 | 34.05 | 0.00 | 0.14 | 3,052 | 79.81 |
| 14.150 | 0.13 | 33.75 | 34.03 | 0.00 | 0.14 | 3,050 | 79.81 |
| 14.200 | 0.13 | 33.73 | 34.02 | 0.00 | 0.14 | 3,049 | 79.81 |
| 14.250 | 0.13 | 33.72 | 34.00 | 0.00 | 0.14 | 3,047 | 79.81 |
| 14.300 | 0.13 | 33.69 | 33.97 | 0.00 | 0.14 | 3,045 | 79.81 |
| 14.350 | 0.13 | 33.67 | 33.95 | 0.00 | 0.14 | 3,043 | 79.81 |
| 14.400 | 0.13 | 33.64 | 33.92 | 0.00 | 0.14 | 3,040 | 79.81 |
| 14.450 | 0.12 | 33.61 | 33.89 | 0.00 | 0.14 | 3,037 | 79.81 |
| 14.500 | 0.12 | 33.57 | 33.85 | 0.00 | 0.14 | 3,034 | 79.80 |
| 14.550 | 0.12 | 33.53 | 33.81 | 0.00 | 0.14 | 3,031 | 79.80 |
| 14.600 | 0.12 | 33.49 | 33.77 | 0.00 | 0.14 | 3,027 | 79.80 |
| 14.650 | 0.12 | 33.45 | 33.73 | 0.00 | 0.14 | 3,023 | 79.80 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.12 | 33.40 | 33.68 | 0.00 | 0.14 | 3,018 | 79.80 |
| 14.750 | 0.11 | 33.35 | 33.63 | 0.00 | 0.14 | 3,014 | 79.80 |
| 14.800 | 0.11 | 33.29 | 33.57 | 0.00 | 0.14 | 3,009 | 79.80 |
| 14.850 | 0.11 | 33.23 | 33.52 | 0.00 | 0.14 | 3,004 | 79.79 |
| 14.900 | 0.11 | 33.17 | 33.46 | 0.00 | 0.14 | 2,998 | 79.79 |
| 14.950 | 0.11 | 33.11 | 33.39 | 0.00 | 0.14 | 2,993 | 79.79 |
| 15.000 | 0.11 | 33.04 | 33.32 | 0.00 | 0.14 | 2,987 | 79.79 |
| 15.050 | 0.10 | 32.97 | 33.25 | 0.00 | 0.14 | 2,980 | 79.79 |
| 15.100 | 0.10 | 32.90 | 33.18 | 0.00 | 0.14 | 2,974 | 79.78 |
| 15.150 | 0.10 | 32.82 | 33.10 | 0.00 | 0.14 | 2,967 | 79.78 |
| 15.200 | 0.10 | 32.74 | 33.02 | 0.00 | 0.14 | 2,959 | 79.78 |
| 15.250 | 0.10 | 32.66 | 32.94 | 0.00 | 0.14 | 2,952 | 79.78 |
| 15.300 | 0.10 | 32.57 | 32.85 | 0.00 | 0.14 | 2,944 | 79.78 |
| 15.350 | 0.10 | 32.48 | 32.76 | 0.00 | 0.14 | 2,936 | 79.77 |
| 15.400 | 0.09 | 32.39 | 32.67 | 0.00 | 0.14 | 2,928 | 79.77 |
| 15.450 | 0.09 | 32.29 | 32.58 | 0.00 | 0.14 | 2,919 | 79.77 |
| 15.500 | 0.09 | 32.20 | 32.48 | 0.00 | 0.14 | 2,910 | 79.76 |
| 15.550 | 0.09 | 32.09 | 32.38 | 0.00 | 0.14 | 2,901 | 79.76 |
| 15.600 | 0.09 | 31.99 | 32.27 | 0.00 | 0.14 | 2,892 | 79.76 |
| 15.650 | 0.09 | 31.88 | 32.16 | 0.00 | 0.14 | 2,882 | 79.75 |
| 15.700 | 0.08 | 31.77 | 32.05 | 0.00 | 0.14 | 2,872 | 79.75 |
| 15.750 | 0.08 | 31.65 | 31.93 | 0.00 | 0.14 | 2,861 | 79.75 |
| 15.800 | 0.08 | 31.53 | 31.82 | 0.00 | 0.14 | 2,851 | 79.74 |
| 15.850 | 0.08 | 31.41 | 31.70 | 0.00 | 0.14 | 2,840 | 79.74 |
| 15.900 | 0.08 | 31.29 | 31.57 | 0.00 | 0.14 | 2,829 | 79.74 |
| 15.950 | 0.08 | 31.16 | 31.44 | 0.00 | 0.14 | 2,817 | 79.73 |
| 16.000 | 0.07 | 31.03 | 31.31 | 0.00 | 0.14 | 2,805 | 79.73 |
| 16.050 | 0.07 | 30.90 | 31.18 | 0.00 | 0.14 | 2,793 | 79.73 |
| 16.100 | 0.07 | 30.76 | 31.04 | 0.00 | 0.14 | 2,781 | 79.72 |
| 16.150 | 0.07 | 30.62 | 30.90 | 0.00 | 0.14 | 2,769 | 79.72 |
| 16.200 | 0.07 | 30.48 | 30.76 | 0.00 | 0.14 | 2,756 | 79.71 |
| 16.250 | 0.07 | 30.34 | 30.62 | 0.00 | 0.14 | 2,743 | 79.71 |
| 16.300 | 0.07 | 30.20 | 30.48 | 0.00 | 0.14 | 2,730 | 79.71 |
| 16.350 | 0.07 | 30.05 | 30.33 | 0.00 | 0.14 | 2,717 | 79.70 |
| 16.400 | 0.07 | 29.91 | 30.19 | 0.00 | 0.14 | 2,704 | 79.70 |
| 16.450 | 0.07 | 29.76 | 30.04 | 0.00 | 0.14 | 2,691 | 79.69 |
| 16.500 | 0.07 | 29.61 | 29.89 | 0.00 | 0.14 | 2,678 | 79.69 |
| 16.550 | 0.07 | 29.46 | 29.74 | 0.00 | 0.14 | 2,664 | 79.68 |
| 16.600 | 0.06 | 29.31 | 29.59 | 0.00 | 0.14 | 2,651 | 79.68 |
| 16.650 | 0.06 | 29.16 | 29.44 | 0.00 | 0.14 | 2,637 | 79.67 |
| 16.700 | 0.06 | 29.00 | 29.29 | 0.00 | 0.14 | 2,623 | 79.67 |
| 16.750 | 0.06 | 28.85 | 29.13 | 0.00 | 0.14 | 2,609 | 79.67 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.06 | 28.69 | 28.97 | 0.00 | 0.14 | 2,595 | 79.66 |
| 16.850 | 0.06 | 28.53 | 28.81 | 0.00 | 0.14 | 2,581 | 79.66 |
| 16.900 | 0.06 | 28.37 | 28.66 | 0.00 | 0.14 | 2,566 | 79.65 |
| 16.950 | 0.06 | 28.21 | 28.49 | 0.00 | 0.14 | 2,552 | 79.65 |
| 17.000 | 0.06 | 28.05 | 28.33 | 0.00 | 0.14 | 2,537 | 79.64 |
| 17.050 | 0.06 | 27.89 | 28.17 | 0.00 | 0.14 | 2,522 | 79.64 |
| 17.100 | 0.06 | 27.72 | 28.00 | 0.00 | 0.14 | 2,508 | 79.63 |
| 17.150 | 0.06 | 27.55 | 27.84 | 0.00 | 0.14 | 2,493 | 79.63 |
| 17.200 | 0.06 | 27.39 | 27.67 | 0.00 | 0.14 | 2,477 | 79.62 |
| 17.250 | 0.06 | 27.22 | 27.50 | 0.00 | 0.14 | 2,462 | 79.62 |
| 17.300 | 0.06 | 27.05 | 27.33 | 0.00 | 0.14 | 2,447 | 79.61 |
| 17.350 | 0.05 | 26.87 | 27.16 | 0.00 | 0.14 | 2,431 | 79.61 |
| 17.400 | 0.05 | 26.70 | 26.98 | 0.00 | 0.14 | 2,416 | 79.60 |
| 17.450 | 0.05 | 26.53 | 26.81 | 0.00 | 0.14 | 2,400 | 79.60 |
| 17.500 | 0.05 | 26.35 | 26.63 | 0.00 | 0.14 | 2,384 | 79.59 |
| 17.550 | 0.05 | 26.17 | 26.45 | 0.00 | 0.14 | 2,368 | 79.59 |
| 17.600 | 0.05 | 25.99 | 26.28 | 0.00 | 0.14 | 2,352 | 79.58 |
| 17.650 | 0.05 | 25.81 | 26.09 | 0.00 | 0.14 | 2,336 | 79.58 |
| 17.700 | 0.05 | 25.63 | 25.91 | 0.00 | 0.14 | 2,319 | 79.57 |
| 17.750 | 0.05 | 25.45 | 25.73 | 0.00 | 0.14 | 2,303 | 79.57 |
| 17.800 | 0.05 | 25.26 | 25.55 | 0.00 | 0.14 | 2,286 | 79.56 |
| 17.850 | 0.05 | 25.08 | 25.36 | 0.00 | 0.14 | 2,270 | 79.55 |
| 17.900 | 0.05 | 24.89 | 25.17 | 0.00 | 0.14 | 2,253 | 79.55 |
| 17.950 | 0.05 | 24.70 | 24.98 | 0.00 | 0.14 | 2,236 | 79.54 |
| 18.000 | 0.05 | 24.51 | 24.79 | 0.00 | 0.14 | 2,219 | 79.54 |
| 18.050 | 0.04 | 24.32 | 24.60 | 0.00 | 0.14 | 2,201 | 79.53 |
| 18.100 | 0.04 | 24.13 | 24.41 | 0.00 | 0.14 | 2,184 | 79.53 |
| 18.150 | 0.04 | 23.93 | 24.22 | 0.00 | 0.14 | 2,167 | 79.52 |
| 18.200 | 0.04 | 23.74 | 24.02 | 0.00 | 0.14 | 2,149 | 79.51 |
| 18.250 | 0.04 | 23.55 | 23.83 | 0.00 | 0.14 | 2,132 | 79.51 |
| 18.300 | 0.04 | 23.35 | 23.63 | 0.00 | 0.14 | 2,114 | 79.50 |
| 18.350 | 0.04 | 23.16 | 23.44 | 0.00 | 0.14 | 2,097 | 79.50 |
| 18.400 | 0.04 | 22.96 | 23.24 | 0.00 | 0.14 | 2,079 | 79.49 |
| 18.450 | 0.04 | 22.77 | 23.05 | 0.00 | 0.14 | 2,062 | 79.49 |
| 18.500 | 0.04 | 22.57 | 22.85 | 0.00 | 0.14 | 2,044 | 79.48 |
| 18.550 | 0.04 | 22.37 | 22.65 | 0.00 | 0.14 | 2,026 | 79.47 |
| 18.600 | 0.04 | 22.18 | 22.46 | 0.00 | 0.14 | 2,008 | 79.47 |
| 18.650 | 0.04 | 21.98 | 22.26 | 0.00 | 0.14 | 1,991 | 79.46 |
| 18.700 | 0.04 | 21.78 | 22.06 | 0.00 | 0.14 | 1,973 | 79.46 |
| 18.750 | 0.04 | 21.58 | 21.86 | 0.00 | 0.14 | 1,955 | 79.45 |
| 18.800 | 0.04 | 21.38 | 21.66 | 0.00 | 0.14 | 1,937 | 79.45 |
| 18.850 | 0.04 | 21.18 | 21.47 | 0.00 | 0.14 | 1,919 | 79.44 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.04 | 20.98 | 21.27 | 0.00 | 0.14 | 1,901 | 79.43 |
| 18.950 | 0.04 | 20.78 | 21.07 | 0.00 | 0.14 | 1,883 | 79.43 |
| 19.000 | 0.04 | 20.58 | 20.87 | 0.00 | 0.14 | 1,865 | 79.42 |
| 19.050 | 0.04 | 20.38 | 20.66 | 0.00 | 0.14 | 1,847 | 79.42 |
| 19.100 | 0.04 | 20.18 | 20.46 | 0.00 | 0.14 | 1,829 | 79.41 |
| 19.150 | 0.04 | 19.98 | 20.26 | 0.00 | 0.14 | 1,811 | 79.40 |
| 19.200 | 0.04 | 19.78 | 20.06 | 0.00 | 0.14 | 1,793 | 79.40 |
| 19.250 | 0.04 | 19.57 | 19.86 | 0.00 | 0.14 | 1,774 | 79.39 |
| 19.300 | 0.04 | 19.37 | 19.65 | 0.00 | 0.14 | 1,756 | 79.39 |
| 19.350 | 0.04 | 19.17 | 19.45 | 0.00 | 0.14 | 1,738 | 79.38 |
| 19.400 | 0.04 | 18.96 | 19.25 | 0.00 | 0.14 | 1,720 | 79.37 |
| 19.450 | 0.04 | 18.76 | 19.04 | 0.00 | 0.14 | 1,701 | 79.37 |
| 19.500 | 0.04 | 18.56 | 18.84 | 0.00 | 0.14 | 1,683 | 79.36 |
| 19.550 | 0.04 | 18.35 | 18.63 | 0.00 | 0.14 | 1,664 | 79.36 |
| 19.600 | 0.04 | 18.15 | 18.43 | 0.00 | 0.14 | 1,646 | 79.35 |
| 19.650 | 0.04 | 17.94 | 18.22 | 0.00 | 0.14 | 1,627 | 79.34 |
| 19.700 | 0.04 | 17.73 | 18.02 | 0.00 | 0.14 | 1,609 | 79.34 |
| 19.750 | 0.04 | 17.53 | 17.81 | 0.00 | 0.14 | 1,590 | 79.33 |
| 19.800 | 0.04 | 17.32 | 17.60 | 0.00 | 0.14 | 1,571 | 79.33 |
| 19.850 | 0.04 | 17.11 | 17.39 | 0.00 | 0.14 | 1,553 | 79.32 |
| 19.900 | 0.04 | 16.90 | 17.19 | 0.00 | 0.14 | 1,534 | 79.31 |
| 19.950 | 0.04 | 16.70 | 16.98 | 0.00 | 0.14 | 1,515 | 79.31 |
| 20.000 | 0.04 | 16.49 | 16.77 | 0.00 | 0.14 | 1,497 | 79.30 |
| 20.050 | 0.04 | 16.28 | 16.56 | 0.00 | 0.14 | 1,478 | 79.29 |
| 20.100 | 0.04 | 16.07 | 16.35 | 0.00 | 0.14 | 1,459 | 79.29 |
| 20.150 | 0.04 | 15.86 | 16.14 | 0.00 | 0.14 | 1,440 | 79.28 |
| 20.200 | 0.04 | 15.65 | 15.93 | 0.00 | 0.14 | 1,421 | 79.28 |
| 20.250 | 0.04 | 15.44 | 15.72 | 0.00 | 0.14 | 1,402 | 79.27 |
| 20.300 | 0.04 | 15.23 | 15.51 | 0.00 | 0.14 | 1,383 | 79.26 |
| 20.350 | 0.04 | 15.02 | 15.30 | 0.00 | 0.14 | 1,364 | 79.26 |
| 20.400 | 0.04 | 14.80 | 15.09 | 0.00 | 0.14 | 1,345 | 79.25 |
| 20.450 | 0.03 | 14.59 | 14.87 | 0.00 | 0.14 | 1,326 | 79.24 |
| 20.500 | 0.03 | 14.38 | 14.66 | 0.00 | 0.14 | 1,307 | 79.24 |
| 20.550 | 0.03 | 14.17 | 14.45 | 0.00 | 0.14 | 1,288 | 79.23 |
| 20.600 | 0.03 | 13.96 | 14.24 | 0.00 | 0.14 | 1,269 | 79.23 |
| 20.650 | 0.03 | 13.74 | 14.02 | 0.00 | 0.14 | 1,250 | 79.22 |
| 20.700 | 0.03 | 13.53 | 13.81 | 0.00 | 0.14 | 1,230 | 79.21 |
| 20.750 | 0.03 | 13.32 | 13.60 | 0.00 | 0.14 | 1,211 | 79.21 |
| 20.800 | 0.03 | 13.10 | 13.38 | 0.00 | 0.14 | 1,192 | 79.20 |
| 20.850 | 0.03 | 12.89 | 13.17 | 0.00 | 0.14 | 1,173 | 79.19 |
| 20.900 | 0.03 | 12.67 | 12.95 | 0.00 | 0.14 | 1,153 | 79.19 |
| 20.950 | 0.03 | 12.46 | 12.74 | 0.00 | 0.14 | 1,134 | 79.18 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.03 | 12.24 | 12.52 | 0.00 | 0.14 | 1,114 | 79.18 |
| 21.050 | 0.03 | 12.03 | 12.31 | 0.00 | 0.14 | 1,095 | 79.17 |
| 21.100 | 0.03 | 11.81 | 12.09 | 0.00 | 0.14 | 1,076 | 79.16 |
| 21.150 | 0.03 | 11.60 | 11.88 | 0.00 | 0.14 | 1,056 | 79.16 |
| 21.200 | 0.03 | 11.38 | 11.66 | 0.00 | 0.14 | 1,037 | 79.15 |
| 21.250 | 0.03 | 11.16 | 11.44 | 0.00 | 0.14 | 1,017 | 79.14 |
| 21.300 | 0.03 | 10.94 | 11.23 | 0.00 | 0.14 | 998 | 79.14 |
| 21.350 | 0.03 | 10.73 | 11.01 | 0.00 | 0.14 | 978 | 79.13 |
| 21.400 | 0.03 | 10.51 | 10.79 | 0.00 | 0.14 | 959 | 79.12 |
| 21.450 | 0.03 | 10.29 | 10.57 | 0.00 | 0.14 | 939 | 79.12 |
| 21.500 | 0.03 | 10.07 | 10.36 | 0.00 | 0.14 | 919 | 79.11 |
| 21.550 | 0.03 | 9.85 | 10.14 | 0.00 | 0.14 | 900 | 79.10 |
| 21.600 | 0.03 | 9.64 | 9.92 | 0.00 | 0.14 | 880 | 79.10 |
| 21.650 | 0.03 | 9.42 | 9.70 | 0.00 | 0.14 | 860 | 79.09 |
| 21.700 | 0.03 | 9.20 | 9.48 | 0.00 | 0.14 | 840 | 79.09 |
| 21.750 | 0.03 | 8.98 | 9.26 | 0.00 | 0.14 | 821 | 79.08 |
| 21.800 | 0.03 | 8.76 | 9.04 | 0.00 | 0.14 | 801 | 79.07 |
| 21.850 | 0.03 | 8.54 | 8.82 | 0.00 | 0.14 | 781 | 79.07 |
| 21.900 | 0.03 | 8.32 | 8.60 | 0.00 | 0.14 | 761 | 79.06 |
| 21.950 | 0.03 | 8.09 | 8.38 | 0.00 | 0.14 | 741 | 79.05 |
| 22.000 | 0.03 | 7.87 | 8.15 | 0.00 | 0.14 | 721 | 79.05 |
| 22.050 | 0.03 | 7.65 | 7.93 | 0.00 | 0.14 | 701 | 79.04 |
| 22.100 | 0.03 | 7.43 | 7.71 | 0.00 | 0.14 | 681 | 79.03 |
| 22.150 | 0.03 | 7.21 | 7.49 | 0.00 | 0.14 | 661 | 79.03 |
| 22.200 | 0.03 | 6.98 | 7.27 | 0.00 | 0.14 | 641 | 79.02 |
| 22.250 | 0.03 | 6.76 | 7.04 | 0.00 | 0.14 | 621 | 79.01 |
| 22.300 | 0.03 | 6.54 | 6.82 | 0.00 | 0.14 | 601 | 79.01 |
| 22.350 | 0.03 | 6.31 | 6.60 | 0.00 | 0.14 | 581 | 79.00 |
| 22.400 | 0.03 | 6.09 | 6.37 | 0.00 | 0.14 | 561 | 78.99 |
| 22.450 | 0.03 | 5.87 | 6.15 | 0.00 | 0.14 | 541 | 78.99 |
| 22.500 | 0.03 | 5.64 | 5.92 | 0.00 | 0.14 | 520 | 78.98 |
| 22.550 | 0.03 | 5.42 | 5.70 | 0.00 | 0.14 | 500 | 78.97 |
| 22.600 | 0.03 | 5.19 | 5.47 | 0.00 | 0.14 | 480 | 78.97 |
| 22.650 | 0.03 | 4.97 | 5.25 | 0.00 | 0.14 | 460 | 78.96 |
| 22.700 | 0.03 | 4.74 | 5.02 | 0.00 | 0.14 | 439 | 78.95 |
| 22.750 | 0.03 | 4.51 | 4.80 | 0.00 | 0.14 | 419 | 78.95 |
| 22.800 | 0.03 | 4.29 | 4.57 | 0.00 | 0.14 | 399 | 78.94 |
| 22.850 | 0.03 | 4.06 | 4.34 | 0.00 | 0.14 | 378 | 78.93 |
| 22.900 | 0.03 | 3.83 | 4.12 | 0.00 | 0.14 | 358 | 78.93 |
| 22.950 | 0.03 | 3.61 | 3.89 | 0.00 | 0.14 | 337 | 78.92 |
| 23.000 | 0.03 | 3.38 | 3.66 | 0.00 | 0.14 | 317 | 78.91 |
| 23.050 | 0.03 | 3.15 | 3.43 | 0.00 | 0.14 | 296 | 78.91 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 25 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 25 year

Scenario: Post-Development 25 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.03 | 2.92 | 3.20 | 0.00 | 0.14 | 276 | 78.90 |
| 23.150 | 0.03 | 2.69 | 2.97 | 0.00 | 0.14 | 255 | 78.89 |
| 23.200 | 0.03 | 2.46 | 2.75 | 0.00 | 0.14 | 234 | 78.89 |
| 23.250 | 0.03 | 2.24 | 2.52 | 0.00 | 0.14 | 214 | 78.88 |
| 23.300 | 0.03 | 2.01 | 2.29 | 0.00 | 0.14 | 193 | 78.87 |
| 23.350 | 0.03 | 1.78 | 2.06 | 0.00 | 0.14 | 172 | 78.87 |
| 23.400 | 0.03 | 1.55 | 1.83 | 0.00 | 0.14 | 152 | 78.86 |
| 23.450 | 0.03 | 1.32 | 1.60 | 0.00 | 0.14 | 131 | 78.85 |
| 23.500 | 0.03 | 1.08 | 1.37 | 0.00 | 0.14 | 110 | 78.85 |
| 23.550 | 0.03 | 0.85 | 1.14 | 0.00 | 0.14 | 89 | 78.84 |
| 23.600 | 0.03 | 0.62 | 0.90 | 0.00 | 0.14 | 69 | 78.83 |
| 23.650 | 0.02 | 0.39 | 0.67 | 0.00 | 0.14 | 48 | 78.83 |
| 23.700 | 0.02 | 0.16 | 0.44 | 0.00 | 0.14 | 27 | 78.82 |
| 23.750 | 0.02 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 78.81 |
| 23.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 23.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 23.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 23.950 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 24.000 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 0.000 | 0.00 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 0.050 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.100 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.150 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.200 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.250 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.300 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.350 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.400 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.450 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.500 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.550 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.600 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0 | 78.81 |
| 0.650 | 0.00 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 0.700 | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0 | 78.81 |
| 0.750 | 0.01 | 0.00 | 0.01 | 0.00 | 0.01 | 0 | 78.81 |
| 0.800 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 0.850 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 0.900 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 0.950 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.000 | 0.01 | 0.00 | 0.02 | 0.00 | 0.01 | 0 | 78.81 |
| 1.050 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 1.100 | 0.01 | 0.00 | 0.03 | 0.00 | 0.01 | 0 | 78.81 |
| 1.150 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 1.200 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 1.250 | 0.02 | 0.00 | 0.03 | 0.00 | 0.02 | 0 | 78.81 |
| 1.300 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.350 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.400 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.450 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.500 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.550 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.600 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.650 | 0.02 | 0.00 | 0.04 | 0.00 | 0.02 | 0 | 78.81 |
| 1.700 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 1.750 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 1.800 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 1.850 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 1.900 | 0.02 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 1.950 | 0.03 | 0.00 | 0.05 | 0.00 | 0.02 | 0 | 78.81 |
| 2.000 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 2.050 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 2.100 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 2.150 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 2.200 | 0.03 | 0.00 | 0.05 | 0.00 | 0.03 | 0 | 78.81 |
| 2.250 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.300 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.350 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.400 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.450 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.500 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.550 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.600 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.650 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.700 | 0.03 | 0.00 | 0.06 | 0.00 | 0.03 | 0 | 78.81 |
| 2.750 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 2.800 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 2.850 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 2.900 | 0.03 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 2.950 | 0.04 | 0.00 | 0.07 | 0.00 | 0.03 | 0 | 78.81 |
| 3.000 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 3.050 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 3.100 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 3.150 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 3.200 | 0.04 | 0.00 | 0.07 | 0.00 | 0.04 | 0 | 78.81 |
| 3.250 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.300 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.350 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.400 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.450 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.500 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.550 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.600 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.650 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.700 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.750 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.800 | 0.04 | 0.00 | 0.08 | 0.00 | 0.04 | 0 | 78.81 |
| 3.850 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 3.900 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 3.950 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 4.000 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 4.050 | 0.04 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 4.100 | 0.05 | 0.00 | 0.09 | 0.00 | 0.04 | 0 | 78.81 |
| 4.150 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 4.200 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 4.250 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 4.300 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 4.350 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 4.400 | 0.05 | 0.00 | 0.09 | 0.00 | 0.05 | 0 | 78.81 |
| 4.450 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.500 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.550 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.600 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.650 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.700 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.750 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.800 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.850 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.900 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 4.950 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 5.000 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 5.050 | 0.05 | 0.00 | 0.10 | 0.00 | 0.05 | 0 | 78.81 |
| 5.100 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.150 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.200 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.250 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.300 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.350 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.400 | 0.05 | 0.00 | 0.11 | 0.00 | 0.05 | 0 | 78.81 |
| 5.450 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.500 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.550 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.600 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.650 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.700 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.750 | 0.06 | 0.00 | 0.11 | 0.00 | 0.06 | 0 | 78.81 |
| 5.800 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 5.850 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 5.900 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 5.950 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 6.000 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 6.050 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 6.100 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 6.150 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 6.200 | 0.06 | 0.00 | 0.12 | 0.00 | 0.06 | 0 | 78.81 |
| 6.250 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 6.300 | 0.06 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 6.350 | 0.07 | 0.00 | 0.13 | 0.00 | 0.06 | 0 | 78.81 |
| 6.400 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 6.450 | 0.07 | 0.00 | 0.13 | 0.00 | 0.07 | 0 | 78.81 |
| 6.500 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 6.550 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 6.600 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 6.650 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 6.700 | 0.07 | 0.00 | 0.14 | 0.00 | 0.07 | 0 | 78.81 |
| 6.750 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 6.800 | 0.07 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 6.850 | 0.08 | 0.00 | 0.15 | 0.00 | 0.07 | 0 | 78.81 |
| 6.900 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |
| 6.950 | 0.08 | 0.00 | 0.15 | 0.00 | 0.08 | 0 | 78.81 |
| 7.000 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 7.050 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 7.100 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 7.150 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 7.200 | 0.08 | 0.00 | 0.16 | 0.00 | 0.08 | 0 | 78.81 |
| 7.250 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 7.300 | 0.08 | 0.00 | 0.17 | 0.00 | 0.08 | 0 | 78.81 |
| 7.350 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 7.400 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 7.450 | 0.09 | 0.00 | 0.17 | 0.00 | 0.09 | 0 | 78.81 |
| 7.500 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 7.550 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 7.600 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 7.650 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 7.700 | 0.09 | 0.00 | 0.18 | 0.00 | 0.09 | 0 | 78.81 |
| 7.750 | 0.09 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 78.81 |
| 7.800 | 0.09 | 0.00 | 0.19 | 0.00 | 0.09 | 0 | 78.81 |
| 7.850 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 7.900 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 7.950 | 0.10 | 0.00 | 0.19 | 0.00 | 0.10 | 0 | 78.81 |
| 8.000 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 8.050 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 8.100 | 0.10 | 0.00 | 0.20 | 0.00 | 0.10 | 0 | 78.81 |
| 8.150 | 0.10 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 78.81 |
| 8.200 | 0.11 | 0.00 | 0.21 | 0.00 | 0.10 | 0 | 78.81 |
| 8.250 | 0.11 | 0.00 | 0.21 | 0.00 | 0.11 | 0 | 78.81 |
| 8.300 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |
| 8.350 | 0.11 | 0.00 | 0.22 | 0.00 | 0.11 | 0 | 78.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 8.400 | 0.12 | 0.00 | 0.23 | 0.00 | 0.11 | 0 | 78.81 |
| 8.450 | 0.12 | 0.00 | 0.23 | 0.00 | 0.12 | 0 | 78.81 |
| 8.500 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 8.550 | 0.12 | 0.00 | 0.24 | 0.00 | 0.12 | 0 | 78.81 |
| 8.600 | 0.12 | 0.00 | 0.25 | 0.00 | 0.12 | 0 | 78.81 |
| 8.650 | 0.13 | 0.00 | 0.25 | 0.00 | 0.13 | 0 | 78.81 |
| 8.700 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 8.750 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 8.800 | 0.13 | 0.00 | 0.26 | 0.00 | 0.13 | 0 | 78.81 |
| 8.850 | 0.14 | 0.00 | 0.27 | 0.00 | 0.13 | 0 | 78.81 |
| 8.900 | 0.14 | 0.00 | 0.27 | 0.00 | 0.14 | 0 | 78.81 |
| 8.950 | 0.14 | 0.00 | 0.28 | 0.00 | 0.14 | 0 | 78.81 |
| 9.000 | 0.14 | 0.00 | 0.28 | 0.00 | 0.14 | 13 | 78.81 |
| 9.050 | 0.14 | 0.01 | 0.29 | 0.00 | 0.14 | 13 | 78.81 |
| 9.100 | 0.15 | 0.02 | 0.30 | 0.00 | 0.14 | 14 | 78.81 |
| 9.150 | 0.15 | 0.03 | 0.32 | 0.00 | 0.14 | 16 | 78.82 |
| 9.200 | 0.15 | 0.05 | 0.34 | 0.00 | 0.14 | 18 | 78.82 |
| 9.250 | 0.15 | 0.08 | 0.36 | 0.00 | 0.14 | 20 | 78.82 |
| 9.300 | 0.16 | 0.11 | 0.39 | 0.00 | 0.14 | 22 | 78.82 |
| 9.350 | 0.16 | 0.14 | 0.42 | 0.00 | 0.14 | 25 | 78.82 |
| 9.400 | 0.16 | 0.18 | 0.46 | 0.00 | 0.14 | 29 | 78.82 |
| 9.450 | 0.16 | 0.22 | 0.51 | 0.00 | 0.14 | 33 | 78.82 |
| 9.500 | 0.17 | 0.27 | 0.55 | 0.00 | 0.14 | 37 | 78.82 |
| 9.550 | 0.17 | 0.32 | 0.61 | 0.00 | 0.14 | 42 | 78.82 |
| 9.600 | 0.17 | 0.38 | 0.66 | 0.00 | 0.14 | 47 | 78.83 |
| 9.650 | 0.17 | 0.44 | 0.72 | 0.00 | 0.14 | 53 | 78.83 |
| 9.700 | 0.18 | 0.51 | 0.79 | 0.00 | 0.14 | 58 | 78.83 |
| 9.750 | 0.18 | 0.58 | 0.86 | 0.00 | 0.14 | 65 | 78.83 |
| 9.800 | 0.18 | 0.66 | 0.94 | 0.00 | 0.14 | 72 | 78.83 |
| 9.850 | 0.18 | 0.74 | 1.02 | 0.00 | 0.14 | 79 | 78.84 |
| 9.900 | 0.18 | 0.82 | 1.10 | 0.00 | 0.14 | 87 | 78.84 |
| 9.950 | 0.19 | 0.91 | 1.19 | 0.00 | 0.14 | 95 | 78.84 |
| 10.000 | 0.19 | 1.00 | 1.29 | 0.00 | 0.14 | 103 | 78.84 |
| 10.050 | 0.19 | 1.10 | 1.39 | 0.00 | 0.14 | 112 | 78.85 |
| 10.100 | 0.20 | 1.21 | 1.49 | 0.00 | 0.14 | 121 | 78.85 |
| 10.150 | 0.20 | 1.32 | 1.60 | 0.00 | 0.14 | 132 | 78.85 |
| 10.200 | 0.20 | 1.44 | 1.73 | 0.00 | 0.14 | 143 | 78.86 |
| 10.250 | 0.21 | 1.58 | 1.86 | 0.00 | 0.14 | 155 | 78.86 |
| 10.300 | 0.21 | 1.72 | 2.00 | 0.00 | 0.14 | 167 | 78.86 |
| 10.350 | 0.22 | 1.87 | 2.15 | 0.00 | 0.14 | 181 | 78.87 |
| 10.400 | 0.22 | 2.03 | 2.31 | 0.00 | 0.14 | 195 | 78.87 |
| 10.450 | 0.23 | 2.20 | 2.48 | 0.00 | 0.14 | 211 | 78.88 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 10.500 | 0.23 | 2.38 | 2.66 | 0.00 | 0.14 | 227 | 78.88 |
| 10.550 | 0.24 | 2.57 | 2.85 | 0.00 | 0.14 | 244 | 78.89 |
| 10.600 | 0.24 | 2.77 | 3.05 | 0.00 | 0.14 | 262 | 78.90 |
| 10.650 | 0.25 | 2.97 | 3.26 | 0.00 | 0.14 | 280 | 78.90 |
| 10.700 | 0.25 | 3.19 | 3.47 | 0.00 | 0.14 | 300 | 78.91 |
| 10.750 | 0.26 | 3.42 | 3.70 | 0.00 | 0.14 | 320 | 78.92 |
| 10.800 | 0.26 | 3.66 | 3.94 | 0.00 | 0.14 | 342 | 78.92 |
| 10.850 | 0.27 | 3.90 | 4.18 | 0.00 | 0.14 | 364 | 78.93 |
| 10.900 | 0.27 | 4.16 | 4.44 | 0.00 | 0.14 | 387 | 78.94 |
| 10.950 | 0.28 | 4.42 | 4.71 | 0.00 | 0.14 | 411 | 78.94 |
| 11.000 | 0.28 | 4.70 | 4.98 | 0.00 | 0.14 | 436 | 78.95 |
| 11.050 | 0.29 | 4.99 | 5.27 | 0.00 | 0.14 | 462 | 78.96 |
| 11.100 | 0.30 | 5.30 | 5.58 | 0.00 | 0.14 | 489 | 78.97 |
| 11.150 | 0.31 | 5.63 | 5.91 | 0.00 | 0.14 | 519 | 78.98 |
| 11.200 | 0.33 | 6.00 | 6.28 | 0.00 | 0.14 | 552 | 78.99 |
| 11.250 | 0.35 | 6.40 | 6.68 | 0.00 | 0.14 | 588 | 79.00 |
| 11.300 | 0.37 | 6.84 | 7.12 | 0.00 | 0.14 | 628 | 79.02 |
| 11.350 | 0.39 | 7.31 | 7.59 | 0.00 | 0.14 | 671 | 79.03 |
| 11.400 | 0.41 | 7.82 | 8.10 | 0.00 | 0.14 | 717 | 79.04 |
| 11.450 | 0.42 | 8.37 | 8.65 | 0.00 | 0.14 | 766 | 79.06 |
| 11.500 | 0.44 | 8.95 | 9.24 | 0.00 | 0.14 | 819 | 79.08 |
| 11.550 | 0.50 | 9.62 | 9.90 | 0.00 | 0.14 | 878 | 79.10 |
| 11.600 | 0.60 | 10.43 | 10.71 | 0.00 | 0.14 | 952 | 79.12 |
| 11.650 | 0.72 | 11.47 | 11.75 | 0.00 | 0.14 | 1,045 | 79.15 |
| 11.700 | 0.90 | 12.82 | 13.10 | 0.00 | 0.14 | 1,166 | 79.19 |
| 11.750 | 1.06 | 14.50 | 14.78 | 0.00 | 0.14 | 1,318 | 79.24 |
| 11.800 | 1.25 | 16.53 | 16.81 | 0.00 | 0.14 | 1,500 | 79.30 |
| 11.850 | 1.41 | 18.90 | 19.19 | 0.00 | 0.14 | 1,714 | 79.37 |
| 11.900 | 1.60 | 21.64 | 21.92 | 0.00 | 0.14 | 1,960 | 79.45 |
| 11.950 | 2.10 | 25.06 | 25.34 | 0.00 | 0.14 | 2,268 | 79.55 |
| 12.000 | 2.91 | 29.80 | 30.08 | 0.00 | 0.14 | 2,695 | 79.69 |
| 12.050 | 3.21 | 35.08 | 35.93 | 0.00 | 0.42 | 3,195 | 79.86 |
| 12.100 | 3.30 | 38.38 | 41.59 | 0.00 | 1.61 | 3,598 | 79.99 |
| 12.150 | 2.89 | 39.69 | 44.56 | 0.00 | 2.43 | 3,792 | 80.05 |
| 12.200 | 2.11 | 39.75 | 44.69 | 0.00 | 2.47 | 3,800 | 80.06 |
| 12.250 | 1.73 | 39.29 | 43.58 | 0.00 | 2.15 | 3,729 | 80.03 |
| 12.300 | 1.47 | 38.84 | 42.48 | 0.00 | 1.82 | 3,659 | 80.01 |
| 12.350 | 1.29 | 38.38 | 41.59 | 0.00 | 1.61 | 3,599 | 79.99 |
| 12.400 | 1.09 | 37.95 | 40.76 | 0.00 | 1.40 | 3,542 | 79.97 |
| 12.450 | 0.93 | 37.55 | 39.98 | 0.00 | 1.21 | 3,489 | 79.95 |
| 12.500 | 0.74 | 37.16 | 39.23 | 0.00 | 1.03 | 3,438 | 79.94 |
| 12.550 | 0.62 | 36.81 | 38.53 | 0.00 | 0.86 | 3,390 | 79.92 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 12.600 | 0.51 | 36.49 | 37.94 | 0.00 | 0.73 | 3,349 | 79.91 |
| 12.650 | 0.46 | 36.16 | 37.46 | 0.00 | 0.65 | 3,313 | 79.90 |
| 12.700 | 0.43 | 35.86 | 37.05 | 0.00 | 0.59 | 3,281 | 79.89 |
| 12.750 | 0.41 | 35.63 | 36.71 | 0.00 | 0.54 | 3,255 | 79.88 |
| 12.800 | 0.39 | 35.43 | 36.43 | 0.00 | 0.50 | 3,234 | 79.87 |
| 12.850 | 0.37 | 35.27 | 36.20 | 0.00 | 0.46 | 3,216 | 79.86 |
| 12.900 | 0.35 | 35.13 | 36.00 | 0.00 | 0.43 | 3,201 | 79.86 |
| 12.950 | 0.34 | 35.00 | 35.82 | 0.00 | 0.41 | 3,187 | 79.85 |
| 13.000 | 0.32 | 34.89 | 35.66 | 0.00 | 0.38 | 3,175 | 79.85 |
| 13.050 | 0.31 | 34.79 | 35.52 | 0.00 | 0.36 | 3,164 | 79.85 |
| 13.100 | 0.29 | 34.70 | 35.39 | 0.00 | 0.34 | 3,154 | 79.84 |
| 13.150 | 0.28 | 34.62 | 35.28 | 0.00 | 0.33 | 3,145 | 79.84 |
| 13.200 | 0.28 | 34.56 | 35.19 | 0.00 | 0.31 | 3,139 | 79.84 |
| 13.250 | 0.27 | 34.51 | 35.11 | 0.00 | 0.30 | 3,133 | 79.84 |
| 13.300 | 0.27 | 34.46 | 35.05 | 0.00 | 0.29 | 3,128 | 79.84 |
| 13.350 | 0.26 | 34.43 | 35.00 | 0.00 | 0.29 | 3,124 | 79.83 |
| 13.400 | 0.26 | 34.39 | 34.95 | 0.00 | 0.28 | 3,120 | 79.83 |
| 13.450 | 0.26 | 34.36 | 34.91 | 0.00 | 0.27 | 3,117 | 79.83 |
| 13.500 | 0.25 | 34.34 | 34.87 | 0.00 | 0.27 | 3,114 | 79.83 |
| 13.550 | 0.25 | 34.31 | 34.83 | 0.00 | 0.26 | 3,111 | 79.83 |
| 13.600 | 0.24 | 34.29 | 34.80 | 0.00 | 0.26 | 3,109 | 79.83 |
| 13.650 | 0.24 | 34.26 | 34.76 | 0.00 | 0.25 | 3,106 | 79.83 |
| 13.700 | 0.23 | 34.24 | 34.73 | 0.00 | 0.25 | 3,103 | 79.83 |
| 13.750 | 0.23 | 34.21 | 34.69 | 0.00 | 0.24 | 3,101 | 79.83 |
| 13.800 | 0.22 | 34.19 | 34.66 | 0.00 | 0.24 | 3,098 | 79.83 |
| 13.850 | 0.22 | 34.17 | 34.63 | 0.00 | 0.23 | 3,096 | 79.83 |
| 13.900 | 0.21 | 34.15 | 34.60 | 0.00 | 0.23 | 3,093 | 79.82 |
| 13.950 | 0.21 | 34.12 | 34.56 | 0.00 | 0.22 | 3,091 | 79.82 |
| 14.000 | 0.20 | 34.10 | 34.53 | 0.00 | 0.22 | 3,089 | 79.82 |
| 14.050 | 0.20 | 34.08 | 34.50 | 0.00 | 0.21 | 3,086 | 79.82 |
| 14.100 | 0.19 | 34.06 | 34.47 | 0.00 | 0.21 | 3,084 | 79.82 |
| 14.150 | 0.19 | 34.04 | 34.44 | 0.00 | 0.20 | 3,082 | 79.82 |
| 14.200 | 0.19 | 34.02 | 34.42 | 0.00 | 0.20 | 3,080 | 79.82 |
| 14.250 | 0.19 | 34.01 | 34.40 | 0.00 | 0.20 | 3,078 | 79.82 |
| 14.300 | 0.18 | 33.99 | 34.38 | 0.00 | 0.19 | 3,077 | 79.82 |
| 14.350 | 0.18 | 33.98 | 34.36 | 0.00 | 0.19 | 3,075 | 79.82 |
| 14.400 | 0.18 | 33.97 | 34.34 | 0.00 | 0.19 | 3,074 | 79.82 |
| 14.450 | 0.18 | 33.95 | 34.32 | 0.00 | 0.18 | 3,073 | 79.82 |
| 14.500 | 0.18 | 33.94 | 34.31 | 0.00 | 0.18 | 3,071 | 79.82 |
| 14.550 | 0.17 | 33.93 | 34.29 | 0.00 | 0.18 | 3,070 | 79.82 |
| 14.600 | 0.17 | 33.92 | 34.28 | 0.00 | 0.18 | 3,069 | 79.82 |
| 14.650 | 0.17 | 33.91 | 34.26 | 0.00 | 0.18 | 3,068 | 79.82 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 14.700 | 0.17 | 33.90 | 34.25 | 0.00 | 0.17 | 3,066 | 79.82 |
| 14.750 | 0.16 | 33.89 | 34.23 | 0.00 | 0.17 | 3,065 | 79.82 |
| 14.800 | 0.16 | 33.88 | 34.21 | 0.00 | 0.17 | 3,064 | 79.81 |
| 14.850 | 0.16 | 33.87 | 34.20 | 0.00 | 0.17 | 3,063 | 79.81 |
| 14.900 | 0.16 | 33.86 | 34.18 | 0.00 | 0.16 | 3,062 | 79.81 |
| 14.950 | 0.16 | 33.85 | 34.17 | 0.00 | 0.16 | 3,061 | 79.81 |
| 15.000 | 0.15 | 33.83 | 34.15 | 0.00 | 0.16 | 3,059 | 79.81 |
| 15.050 | 0.15 | 33.82 | 34.14 | 0.00 | 0.16 | 3,058 | 79.81 |
| 15.100 | 0.15 | 33.81 | 34.12 | 0.00 | 0.15 | 3,057 | 79.81 |
| 15.150 | 0.15 | 33.80 | 34.11 | 0.00 | 0.15 | 3,056 | 79.81 |
| 15.200 | 0.14 | 33.79 | 34.09 | 0.00 | 0.15 | 3,055 | 79.81 |
| 15.250 | 0.14 | 33.78 | 34.08 | 0.00 | 0.15 | 3,054 | 79.81 |
| 15.300 | 0.14 | 33.77 | 34.06 | 0.00 | 0.15 | 3,052 | 79.81 |
| 15.350 | 0.14 | 33.76 | 34.05 | 0.00 | 0.14 | 3,051 | 79.81 |
| 15.400 | 0.13 | 33.75 | 34.03 | 0.00 | 0.14 | 3,050 | 79.81 |
| 15.450 | 0.13 | 33.73 | 34.02 | 0.00 | 0.14 | 3,049 | 79.81 |
| 15.500 | 0.13 | 33.71 | 34.00 | 0.00 | 0.14 | 3,047 | 79.81 |
| 15.550 | 0.13 | 33.69 | 33.97 | 0.00 | 0.14 | 3,045 | 79.81 |
| 15.600 | 0.13 | 33.66 | 33.94 | 0.00 | 0.14 | 3,042 | 79.81 |
| 15.650 | 0.12 | 33.63 | 33.91 | 0.00 | 0.14 | 3,039 | 79.81 |
| 15.700 | 0.12 | 33.59 | 33.87 | 0.00 | 0.14 | 3,036 | 79.81 |
| 15.750 | 0.12 | 33.55 | 33.83 | 0.00 | 0.14 | 3,032 | 79.80 |
| 15.800 | 0.12 | 33.50 | 33.78 | 0.00 | 0.14 | 3,028 | 79.80 |
| 15.850 | 0.11 | 33.45 | 33.73 | 0.00 | 0.14 | 3,023 | 79.80 |
| 15.900 | 0.11 | 33.39 | 33.67 | 0.00 | 0.14 | 3,018 | 79.80 |
| 15.950 | 0.11 | 33.33 | 33.61 | 0.00 | 0.14 | 3,012 | 79.80 |
| 16.000 | 0.11 | 33.27 | 33.55 | 0.00 | 0.14 | 3,007 | 79.80 |
| 16.050 | 0.11 | 33.20 | 33.48 | 0.00 | 0.14 | 3,000 | 79.79 |
| 16.100 | 0.10 | 33.12 | 33.40 | 0.00 | 0.14 | 2,994 | 79.79 |
| 16.150 | 0.10 | 33.05 | 33.33 | 0.00 | 0.14 | 2,987 | 79.79 |
| 16.200 | 0.10 | 32.97 | 33.25 | 0.00 | 0.14 | 2,980 | 79.79 |
| 16.250 | 0.10 | 32.89 | 33.17 | 0.00 | 0.14 | 2,973 | 79.78 |
| 16.300 | 0.10 | 32.80 | 33.09 | 0.00 | 0.14 | 2,965 | 79.78 |
| 16.350 | 0.10 | 32.72 | 33.00 | 0.00 | 0.14 | 2,957 | 79.78 |
| 16.400 | 0.10 | 32.63 | 32.91 | 0.00 | 0.14 | 2,950 | 79.78 |
| 16.450 | 0.10 | 32.54 | 32.83 | 0.00 | 0.14 | 2,942 | 79.77 |
| 16.500 | 0.10 | 32.45 | 32.74 | 0.00 | 0.14 | 2,933 | 79.77 |
| 16.550 | 0.09 | 32.36 | 32.64 | 0.00 | 0.14 | 2,925 | 79.77 |
| 16.600 | 0.09 | 32.27 | 32.55 | 0.00 | 0.14 | 2,917 | 79.77 |
| 16.650 | 0.09 | 32.17 | 32.45 | 0.00 | 0.14 | 2,908 | 79.76 |
| 16.700 | 0.09 | 32.07 | 32.35 | 0.00 | 0.14 | 2,899 | 79.76 |
| 16.750 | 0.09 | 31.97 | 32.25 | 0.00 | 0.14 | 2,890 | 79.76 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 16.800 | 0.09 | 31.87 | 32.15 | 0.00 | 0.14 | 2,881 | 79.75 |
| 16.850 | 0.09 | 31.76 | 32.04 | 0.00 | 0.14 | 2,871 | 79.75 |
| 16.900 | 0.09 | 31.66 | 31.94 | 0.00 | 0.14 | 2,862 | 79.75 |
| 16.950 | 0.09 | 31.55 | 31.83 | 0.00 | 0.14 | 2,852 | 79.75 |
| 17.000 | 0.08 | 31.44 | 31.72 | 0.00 | 0.14 | 2,842 | 79.74 |
| 17.050 | 0.08 | 31.32 | 31.61 | 0.00 | 0.14 | 2,832 | 79.74 |
| 17.100 | 0.08 | 31.21 | 31.49 | 0.00 | 0.14 | 2,822 | 79.74 |
| 17.150 | 0.08 | 31.09 | 31.38 | 0.00 | 0.14 | 2,811 | 79.73 |
| 17.200 | 0.08 | 30.98 | 31.26 | 0.00 | 0.14 | 2,800 | 79.73 |
| 17.250 | 0.08 | 30.85 | 31.14 | 0.00 | 0.14 | 2,790 | 79.72 |
| 17.300 | 0.08 | 30.73 | 31.01 | 0.00 | 0.14 | 2,779 | 79.72 |
| 17.350 | 0.08 | 30.61 | 30.89 | 0.00 | 0.14 | 2,767 | 79.72 |
| 17.400 | 0.08 | 30.48 | 30.76 | 0.00 | 0.14 | 2,756 | 79.71 |
| 17.450 | 0.08 | 30.35 | 30.63 | 0.00 | 0.14 | 2,744 | 79.71 |
| 17.500 | 0.08 | 30.22 | 30.50 | 0.00 | 0.14 | 2,733 | 79.71 |
| 17.550 | 0.07 | 30.09 | 30.37 | 0.00 | 0.14 | 2,721 | 79.70 |
| 17.600 | 0.07 | 29.96 | 30.24 | 0.00 | 0.14 | 2,709 | 79.70 |
| 17.650 | 0.07 | 29.82 | 30.10 | 0.00 | 0.14 | 2,696 | 79.69 |
| 17.700 | 0.07 | 29.68 | 29.96 | 0.00 | 0.14 | 2,684 | 79.69 |
| 17.750 | 0.07 | 29.54 | 29.82 | 0.00 | 0.14 | 2,671 | 79.69 |
| 17.800 | 0.07 | 29.40 | 29.68 | 0.00 | 0.14 | 2,658 | 79.68 |
| 17.850 | 0.07 | 29.25 | 29.54 | 0.00 | 0.14 | 2,645 | 79.68 |
| 17.900 | 0.07 | 29.11 | 29.39 | 0.00 | 0.14 | 2,632 | 79.67 |
| 17.950 | 0.07 | 28.96 | 29.24 | 0.00 | 0.14 | 2,619 | 79.67 |
| 18.000 | 0.07 | 28.81 | 29.09 | 0.00 | 0.14 | 2,605 | 79.66 |
| 18.050 | 0.06 | 28.66 | 28.94 | 0.00 | 0.14 | 2,592 | 79.66 |
| 18.100 | 0.06 | 28.50 | 28.78 | 0.00 | 0.14 | 2,578 | 79.66 |
| 18.150 | 0.06 | 28.35 | 28.63 | 0.00 | 0.14 | 2,564 | 79.65 |
| 18.200 | 0.06 | 28.19 | 28.47 | 0.00 | 0.14 | 2,550 | 79.65 |
| 18.250 | 0.06 | 28.04 | 28.32 | 0.00 | 0.14 | 2,536 | 79.64 |
| 18.300 | 0.06 | 27.88 | 28.16 | 0.00 | 0.14 | 2,522 | 79.64 |
| 18.350 | 0.06 | 27.72 | 28.00 | 0.00 | 0.14 | 2,508 | 79.63 |
| 18.400 | 0.06 | 27.56 | 27.85 | 0.00 | 0.14 | 2,493 | 79.63 |
| 18.450 | 0.06 | 27.40 | 27.69 | 0.00 | 0.14 | 2,479 | 79.62 |
| 18.500 | 0.06 | 27.25 | 27.53 | 0.00 | 0.14 | 2,465 | 79.62 |
| 18.550 | 0.06 | 27.09 | 27.37 | 0.00 | 0.14 | 2,450 | 79.61 |
| 18.600 | 0.06 | 26.93 | 27.21 | 0.00 | 0.14 | 2,436 | 79.61 |
| 18.650 | 0.06 | 26.76 | 27.05 | 0.00 | 0.14 | 2,421 | 79.60 |
| 18.700 | 0.06 | 26.60 | 26.88 | 0.00 | 0.14 | 2,407 | 79.60 |
| 18.750 | 0.06 | 26.44 | 26.72 | 0.00 | 0.14 | 2,392 | 79.59 |
| 18.800 | 0.06 | 26.28 | 26.56 | 0.00 | 0.14 | 2,378 | 79.59 |
| 18.850 | 0.06 | 26.11 | 26.40 | 0.00 | 0.14 | 2,363 | 79.58 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 18.900 | 0.06 | 25.95 | 26.23 | 0.00 | 0.14 | 2,348 | 79.58 |
| 18.950 | 0.06 | 25.79 | 26.07 | 0.00 | 0.14 | 2,333 | 79.58 |
| 19.000 | 0.06 | 25.62 | 25.90 | 0.00 | 0.14 | 2,319 | 79.57 |
| 19.050 | 0.06 | 25.46 | 25.74 | 0.00 | 0.14 | 2,304 | 79.57 |
| 19.100 | 0.06 | 25.29 | 25.57 | 0.00 | 0.14 | 2,289 | 79.56 |
| 19.150 | 0.06 | 25.12 | 25.40 | 0.00 | 0.14 | 2,274 | 79.56 |
| 19.200 | 0.06 | 24.95 | 25.24 | 0.00 | 0.14 | 2,259 | 79.55 |
| 19.250 | 0.06 | 24.79 | 25.07 | 0.00 | 0.14 | 2,243 | 79.55 |
| 19.300 | 0.06 | 24.62 | 24.90 | 0.00 | 0.14 | 2,228 | 79.54 |
| 19.350 | 0.06 | 24.45 | 24.73 | 0.00 | 0.14 | 2,213 | 79.54 |
| 19.400 | 0.06 | 24.28 | 24.56 | 0.00 | 0.14 | 2,198 | 79.53 |
| 19.450 | 0.06 | 24.11 | 24.39 | 0.00 | 0.14 | 2,182 | 79.53 |
| 19.500 | 0.06 | 23.94 | 24.22 | 0.00 | 0.14 | 2,167 | 79.52 |
| 19.550 | 0.05 | 23.76 | 24.05 | 0.00 | 0.14 | 2,151 | 79.52 |
| 19.600 | 0.05 | 23.59 | 23.87 | 0.00 | 0.14 | 2,136 | 79.51 |
| 19.650 | 0.05 | 23.42 | 23.70 | 0.00 | 0.14 | 2,120 | 79.51 |
| 19.700 | 0.05 | 23.25 | 23.53 | 0.00 | 0.14 | 2,105 | 79.50 |
| 19.750 | 0.05 | 23.07 | 23.35 | 0.00 | 0.14 | 2,089 | 79.49 |
| 19.800 | 0.05 | 22.90 | 23.18 | 0.00 | 0.14 | 2,073 | 79.49 |
| 19.850 | 0.05 | 22.72 | 23.00 | 0.00 | 0.14 | 2,058 | 79.48 |
| 19.900 | 0.05 | 22.55 | 22.83 | 0.00 | 0.14 | 2,042 | 79.48 |
| 19.950 | 0.05 | 22.37 | 22.65 | 0.00 | 0.14 | 2,026 | 79.47 |
| 20.000 | 0.05 | 22.19 | 22.47 | 0.00 | 0.14 | 2,010 | 79.47 |
| 20.050 | 0.05 | 22.01 | 22.30 | 0.00 | 0.14 | 1,994 | 79.46 |
| 20.100 | 0.05 | 21.84 | 22.12 | 0.00 | 0.14 | 1,978 | 79.46 |
| 20.150 | 0.05 | 21.66 | 21.94 | 0.00 | 0.14 | 1,962 | 79.45 |
| 20.200 | 0.05 | 21.48 | 21.76 | 0.00 | 0.14 | 1,946 | 79.45 |
| 20.250 | 0.05 | 21.30 | 21.58 | 0.00 | 0.14 | 1,930 | 79.44 |
| 20.300 | 0.05 | 21.12 | 21.40 | 0.00 | 0.14 | 1,913 | 79.44 |
| 20.350 | 0.05 | 20.94 | 21.22 | 0.00 | 0.14 | 1,897 | 79.43 |
| 20.400 | 0.05 | 20.76 | 21.04 | 0.00 | 0.14 | 1,881 | 79.43 |
| 20.450 | 0.05 | 20.58 | 20.86 | 0.00 | 0.14 | 1,865 | 79.42 |
| 20.500 | 0.05 | 20.39 | 20.68 | 0.00 | 0.14 | 1,848 | 79.42 |
| 20.550 | 0.05 | 20.21 | 20.49 | 0.00 | 0.14 | 1,832 | 79.41 |
| 20.600 | 0.05 | 20.03 | 20.31 | 0.00 | 0.14 | 1,815 | 79.41 |
| 20.650 | 0.05 | 19.85 | 20.13 | 0.00 | 0.14 | 1,799 | 79.40 |
| 20.700 | 0.05 | 19.66 | 19.94 | 0.00 | 0.14 | 1,782 | 79.39 |
| 20.750 | 0.05 | 19.48 | 19.76 | 0.00 | 0.14 | 1,766 | 79.39 |
| 20.800 | 0.05 | 19.29 | 19.57 | 0.00 | 0.14 | 1,749 | 79.38 |
| 20.850 | 0.05 | 19.11 | 19.39 | 0.00 | 0.14 | 1,732 | 79.38 |
| 20.900 | 0.05 | 18.92 | 19.20 | 0.00 | 0.14 | 1,716 | 79.37 |
| 20.950 | 0.05 | 18.74 | 19.02 | 0.00 | 0.14 | 1,699 | 79.37 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - 0 (ft ³ /s) | 2S/t + 0 (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 21.000 | 0.05 | 18.55 | 18.83 | 0.00 | 0.14 | 1,682 | 79.36 |
| 21.050 | 0.05 | 18.36 | 18.65 | 0.00 | 0.14 | 1,665 | 79.36 |
| 21.100 | 0.05 | 18.18 | 18.46 | 0.00 | 0.14 | 1,649 | 79.35 |
| 21.150 | 0.05 | 17.99 | 18.27 | 0.00 | 0.14 | 1,632 | 79.34 |
| 21.200 | 0.05 | 17.80 | 18.08 | 0.00 | 0.14 | 1,615 | 79.34 |
| 21.250 | 0.05 | 17.61 | 17.89 | 0.00 | 0.14 | 1,598 | 79.33 |
| 21.300 | 0.05 | 17.42 | 17.71 | 0.00 | 0.14 | 1,581 | 79.33 |
| 21.350 | 0.05 | 17.23 | 17.52 | 0.00 | 0.14 | 1,564 | 79.32 |
| 21.400 | 0.05 | 17.04 | 17.33 | 0.00 | 0.14 | 1,547 | 79.32 |
| 21.450 | 0.05 | 16.85 | 17.14 | 0.00 | 0.14 | 1,530 | 79.31 |
| 21.500 | 0.05 | 16.66 | 16.94 | 0.00 | 0.14 | 1,512 | 79.31 |
| 21.550 | 0.04 | 16.47 | 16.75 | 0.00 | 0.14 | 1,495 | 79.30 |
| 21.600 | 0.04 | 16.28 | 16.56 | 0.00 | 0.14 | 1,478 | 79.29 |
| 21.650 | 0.04 | 16.09 | 16.37 | 0.00 | 0.14 | 1,461 | 79.29 |
| 21.700 | 0.04 | 15.89 | 16.18 | 0.00 | 0.14 | 1,443 | 79.28 |
| 21.750 | 0.04 | 15.70 | 15.98 | 0.00 | 0.14 | 1,426 | 79.28 |
| 21.800 | 0.04 | 15.51 | 15.79 | 0.00 | 0.14 | 1,408 | 79.27 |
| 21.850 | 0.04 | 15.31 | 15.60 | 0.00 | 0.14 | 1,391 | 79.27 |
| 21.900 | 0.04 | 15.12 | 15.40 | 0.00 | 0.14 | 1,374 | 79.26 |
| 21.950 | 0.04 | 14.93 | 15.21 | 0.00 | 0.14 | 1,356 | 79.25 |
| 22.000 | 0.04 | 14.73 | 15.01 | 0.00 | 0.14 | 1,338 | 79.25 |
| 22.050 | 0.04 | 14.53 | 14.82 | 0.00 | 0.14 | 1,321 | 79.24 |
| 22.100 | 0.04 | 14.34 | 14.62 | 0.00 | 0.14 | 1,303 | 79.24 |
| 22.150 | 0.04 | 14.14 | 14.42 | 0.00 | 0.14 | 1,285 | 79.23 |
| 22.200 | 0.04 | 13.94 | 14.23 | 0.00 | 0.14 | 1,268 | 79.23 |
| 22.250 | 0.04 | 13.75 | 14.03 | 0.00 | 0.14 | 1,250 | 79.22 |
| 22.300 | 0.04 | 13.55 | 13.83 | 0.00 | 0.14 | 1,232 | 79.21 |
| 22.350 | 0.04 | 13.35 | 13.63 | 0.00 | 0.14 | 1,214 | 79.21 |
| 22.400 | 0.04 | 13.15 | 13.43 | 0.00 | 0.14 | 1,196 | 79.20 |
| 22.450 | 0.04 | 12.95 | 13.23 | 0.00 | 0.14 | 1,178 | 79.20 |
| 22.500 | 0.04 | 12.75 | 13.03 | 0.00 | 0.14 | 1,160 | 79.19 |
| 22.550 | 0.04 | 12.55 | 12.83 | 0.00 | 0.14 | 1,142 | 79.18 |
| 22.600 | 0.04 | 12.35 | 12.63 | 0.00 | 0.14 | 1,124 | 79.18 |
| 22.650 | 0.04 | 12.15 | 12.43 | 0.00 | 0.14 | 1,106 | 79.17 |
| 22.700 | 0.04 | 11.95 | 12.23 | 0.00 | 0.14 | 1,088 | 79.17 |
| 22.750 | 0.04 | 11.75 | 12.03 | 0.00 | 0.14 | 1,070 | 79.16 |
| 22.800 | 0.04 | 11.54 | 11.83 | 0.00 | 0.14 | 1,052 | 79.15 |
| 22.850 | 0.04 | 11.34 | 11.62 | 0.00 | 0.14 | 1,033 | 79.15 |
| 22.900 | 0.04 | 11.14 | 11.42 | 0.00 | 0.14 | 1,015 | 79.14 |
| 22.950 | 0.04 | 10.93 | 11.22 | 0.00 | 0.14 | 997 | 79.14 |
| 23.000 | 0.04 | 10.73 | 11.01 | 0.00 | 0.14 | 978 | 79.13 |
| 23.050 | 0.04 | 10.53 | 10.81 | 0.00 | 0.14 | 960 | 79.12 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Routing Calculations (Total Out)

Return Event: 100 years

Label: Stormwater Planters - 2 (OUT)

Storm Event: 100 year

Scenario: Post-Development 100 year

Pond Routing Calculations (Total Out)

| Time (hours) | Flow (Total In) (ft ³ /s) | 2S/t - O (ft ³ /s) | 2S/t + O (ft ³ /s) | Infiltration (ft ³ /s) | Flow (Outlet) (ft ³ /s) | Volume (ft ³) | Elevation (ft) |
|--------------|--------------------------------------|-------------------------------|-------------------------------|-----------------------------------|------------------------------------|---------------------------|----------------|
| 23.100 | 0.04 | 10.32 | 10.60 | 0.00 | 0.14 | 942 | 79.12 |
| 23.150 | 0.04 | 10.11 | 10.40 | 0.00 | 0.14 | 923 | 79.11 |
| 23.200 | 0.04 | 9.91 | 10.19 | 0.00 | 0.14 | 904 | 79.11 |
| 23.250 | 0.04 | 9.70 | 9.98 | 0.00 | 0.14 | 886 | 79.10 |
| 23.300 | 0.04 | 9.50 | 9.78 | 0.00 | 0.14 | 867 | 79.09 |
| 23.350 | 0.04 | 9.29 | 9.57 | 0.00 | 0.14 | 849 | 79.09 |
| 23.400 | 0.04 | 9.08 | 9.36 | 0.00 | 0.14 | 830 | 79.08 |
| 23.450 | 0.04 | 8.87 | 9.15 | 0.00 | 0.14 | 811 | 79.08 |
| 23.500 | 0.04 | 8.66 | 8.95 | 0.00 | 0.14 | 792 | 79.07 |
| 23.550 | 0.04 | 8.45 | 8.74 | 0.00 | 0.14 | 774 | 79.06 |
| 23.600 | 0.04 | 8.24 | 8.53 | 0.00 | 0.14 | 755 | 79.06 |
| 23.650 | 0.04 | 8.03 | 8.32 | 0.00 | 0.14 | 736 | 79.05 |
| 23.700 | 0.04 | 7.82 | 8.11 | 0.00 | 0.14 | 717 | 79.05 |
| 23.750 | 0.04 | 7.61 | 7.89 | 0.00 | 0.14 | 698 | 79.04 |
| 23.800 | 0.04 | 7.40 | 7.68 | 0.00 | 0.14 | 679 | 79.03 |
| 23.850 | 0.03 | 7.19 | 7.47 | 0.00 | 0.14 | 660 | 79.03 |
| 23.900 | 0.03 | 6.98 | 7.26 | 0.00 | 0.14 | 641 | 79.02 |
| 23.950 | 0.03 | 6.76 | 7.05 | 0.00 | 0.14 | 621 | 79.01 |
| 24.000 | 0.03 | 6.55 | 6.83 | 0.00 | 0.14 | 602 | 79.01 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: Stormwater Planters - 2 (IN)
 Scenario: Post-Development 1 year

Return Event: 1 years
 Storm Event: 1 year

Summary for Hydrograph Addition at 'Stormwater Planters - 2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2B |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|----------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2B | 3,907 | 12.100 | 0.97 |
| Flow (In) | Stormwater Planters - 2 | 3,907 | 12.100 | 0.97 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: Stormwater Planters - 2 (IN)
 Scenario: Post-Development 10 year

Return Event: 10 years
 Storm Event: 10 year

Summary for Hydrograph Addition at 'Stormwater Planters - 2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2B |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|----------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2B | 7,510 | 12.100 | 1.81 |
| Flow (In) | Stormwater Planters - 2 | 7,510 | 12.100 | 1.81 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: Stormwater Planters - 2 (IN)
 Scenario: Post-Development 25 year

Return Event: 25 years
 Storm Event: 25 year

Summary for Hydrograph Addition at 'Stormwater Planters - 2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2B |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|-------------------------|---------------------------|----------------------|----------------------------------|
| Flow (From) | PDA-2B | 9,617 | 12.100 | 2.30 |
| Flow (In) | Stormwater Planters - 2 | 9,617 | 12.100 | 2.30 |

Existing and Proposed Hydrologic Calculations

Subsection: Pond Inflow Summary
 Label: Stormwater Planters - 2 (IN)
 Scenario: Post-Development 100 year

Return Event: 100 years
 Storm Event: 100 year

Summary for Hydrograph Addition at 'Stormwater Planters - 2'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | PDA-2B |

Node Inflows

| Inflow Type | Element | Volume (ft ³) | Time to Peak (hours) | Flow (Peak) (ft ³ /s) |
|-------------|----------------------------|------------------------------|-------------------------|-------------------------------------|
| Flow (From) | PDA-2B | 13,940 | 12.100 | 3.30 |
| Flow (In) | Stormwater Planters - 2 | 13,940 | 12.100 | 3.30 |

APPENDIX B

NYSDEC STORMWATER SIZING CALCULATIONS

**RUNOFF REDUCTION VOLUME, WATER QUALITY VOLUME AND
STREAM CHANNEL PROTECTION SIZING CALCULATIONS**

Multi-Family Development Albany Post Road
3119 Albany Post Road
Village of Buchanan, NY

JMC Project: **22062**

Drawing Reference: **DA-1, DA-2**

Computed by: **MT**

Checked by: **XX**

Date Printed: 11/6/2023

WATER QUALITY VOLUME WORKSHEET

JMC Project: **22062**
 Design Point: **SITE**

Multi-Family Development Albany Post Road Drainage Area: **SITE**

| Initial Water Quality Treatment Volume | | | | | | |
|--|---|------|-----------------|--------------------|--------------------|--------------------------|
| DESCRIPTION | Design Storm | Area | Impervious Area | Percent Impervious | Runoff Coefficient | Total Required WQ Volume |
| SYMBOL | P | A | I | %I | R _V | WQ _V |
| VALUE | 1.5 | 3.87 | 2.53 | 65.48 | 0.639285587 | 13,461 |
| UNITS | In | Ac | Ac | % | CF | CF |
| VALUE | Enhanced Phosphorus Removal (WQ _V = 1-yr Storm Runoff) | | | | | |

| Runoff Reduction Techniques (Area) | | | |
|--|------------|-----------------|--|
| DESCRIPTION | Total Area | Impervious Area | |
| SYMBOL | A | I | |
| Conservation of Natural Areas | | | |
| Sheetflow to Riparian Buffers or Filter Strips | | | |
| Vegetated Swale | | | |
| Tree Planting / Tree Pit | | | |
| Disconnection of Rooftop Runoff | | | |
| Stream Daylighting | | | |
| TOTAL | | | |
| UNITS | Ac | Ac | |

| Adjusted Water Quality Treatment Volume | | | | | | |
|---|---|------|-----------------|--------------------|--------------------|--------------------------|
| DESCRIPTION | Design Storm | Area | Impervious Area | Percent Impervious | Runoff Coefficient | Total Required WQ Volume |
| SYMBOL | P | A | I | %I | R _V | WQ _V |
| VALUE | 1.5 | 3.87 | 2.53 | 65.48 | 0.639285587 | 13,461 |
| UNITS | In | Ac | Ac | % | CF | CF |
| VALUE | Enhanced Phosphorus Removal (WQ _V = 1-yr Storm Runoff) | | | | | |

| Net Water Quality Treatment Volume = Adjusted WQ _V - Provided RR _V | | |
|--|--------------|----|
| Initial Water Quality Treatment Volume | 13,461 | CF |
| Adjusted Water Quality Treatment Volume | 13,461 | CF |
| Provided Runoff Reduction Volume | 3,792 | CF |
| Net Water Quality Treatment Volume | 9,669 | CF |

RUNOFF REDUCTION VOLUME WORKSHEET

JMC Project: **22062**

Design Point: **X**

| | | |
|--|----------------|------------|
| Multi-Family Development Albany Post Road | Drainage Area: | XXX |
|--|----------------|------------|

| Total Water Quality Treatment Volume | | | |
|--------------------------------------|-----------------|---------------|-------|
| DESCRIPTION | SYMBOL | VALUE | UNITS |
| Initial Water Quality Volume | WQ _v | 13,461 | CF |
| Adjusted Water Quality Volume | WQ _v | 13,461 | CF |

| Minimum Runoff Reduction Volume | | | |
|---|-----------------------|--------------|-----------|
| DESCRIPTION | SYMBOL | VALUE | UNITS |
| Design Storm [90% Rainfall Event Number] or [1-yr Storm Depth] | P | 1.5 | In |
| Total Area of <i>new</i> Impervious Cover | Aic | 2.53 | Ac |
| Hydrologic Soil Group (HSG) Specific Reduction Factor | S | 0.20 | |
| Runoff Coefficient [0.05 + 0.009 x %I] | R _v | 0.95 | CF |
| Impervious Cover targeted for Runoff Reduction [S x Aic] | Ai | 0.51 | Ac |
| TOTAL VOLUME Required [RR_v = (P x R_v x Ai) / 12] | RR_v | 2,619 | CF |

| Runoff Reduction Techniques (Volume) | | | |
|--------------------------------------|-----------------------|--------------|-----------|
| GREEN INFRASTRUCTURE PRACTICE / SMP | SYMBOL | VALUE | UNITS |
| Stormwater Planter #1 | RR _v | 481 | CF |
| Stormwater Planter #2 | RR _v | 182 | CF |
| Green Roof #1 | RR _v | 923 | CF |
| Green Roof #2 | RR _v | 133 | CF |
| Green Roof #3 | RR _v | 153 | CF |
| Green Roof #4 | RR _v | 781 | CF |
| Green Roof #5 | RR _v | 210 | CF |
| Green Roof #6 | RR _v | 311 | CF |
| Green Roof #7 | RR _v | 62 | CF |
| Green Roof #8 | RR _v | 22 | CF |
| Green Roof #9 | RR _v | 271 | CF |
| Green Roof #10 | RR _v | 82 | CF |
| Green Roof #11 | RR _v | 83 | CF |
| Green Roof #12 | RR _v | 98 | CF |
| TOTAL | RR_v | 3,792 | CF |

| Runoff Reduction | |
|---|------------|
| Is Total RR _v > Adjusted WQ _v ? | NO |
| Is Total RR _v > Minimum RR _v ? | YES |

STORMWATER PLANTER WORKSHEET

JMC Project: **22062**

Design Point: **2**

Stormwater Planter #1

Drainage Area: PDA-2B

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|-----------------|--------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I | 0.31 | Ac |
| Area | A | 0.31 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Coefficient [0.05 + 0.009 x %I] | R _v | 0.95 | CF |
| TOTAL VOLUME Required [WQ _v = (P x R _v x A) / 12] | WQ _v | 1,603 | CF |
| Design Storm [1-yr Storm Depth] | P | | In |
| TOTAL VOLUME Required (TMDL) [WQ _v = 1-yr Storm Runoff] | WQ _v | | CF |

Minimum Planter Bed Area

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|-----------------|-----------------|----------|
| Water Quality Volume | WQ _v | 1,603 | CF |
| Coefficient of permeability of filter media (hydraulic conductivity) | k | 4.00 | Ft / Day |
| Planter bed Depth (soil media) | d _f | 1.50 | Ft |
| Average Height of water above planter bed | h _f | 0.50 | Ft |
| Design planter bed drain Time | t _f | 4.00 | Hours |
| Required Surface Area of Planter Bed [A _f = (WQ _v x d _f) / (k x (h _f + d _f) x t _f)] | A _f | 1,803.52 | SF |

Proposed Area

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|----------------|-----------------|-------|
| Calculated planter bed area (Length x Width) | | | SF |
| Surface Area of Planter Bed Provided | A _f | 1,838.00 | SF |
| Actual Volume Provided | | 919 | CF |

Runoff Reduction

| DESCRIPTION | VALUE | UNITS |
|--|---------------------|-------|
| Is Proposed Af > Required Af ? | YES | |
| Type of Planter | FLOW-THROUGH | |
| RR _v Provided for Infiltration Planter | 1,603 | CF |
| RR _v Provided for Flow-Through Planter in HSG 'C' Soils | 721 | CF |
| RR _v Provided for Flow-Through Planter in HSG 'D' Soils | 481 | CF |

STORMWATER PLANTER WORKSHEET

JMC Project: **22062**

Design Point: **2**

Stormwater Planter #2

Drainage Area: PDA-2B

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|-----------------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I | 0.12 | Ac |
| Area | A | 0.12 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Coefficient [0.05 + 0.009 x %I] | R _v | 0.95 | CF |
| TOTAL VOLUME Required [WQ _v = (P x R _v x A) / 12] | WQ _v | 608 | CF |
| Design Storm [1-yr Storm Depth] | P | | In |
| TOTAL VOLUME Required (TMDL) [WQ _v = 1-yr Storm Runoff] | WQ _v | | CF |

Minimum Planter Bed Area

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|-----------------|---------------|----------|
| Water Quality Volume | WQ _v | 608 | CF |
| Coefficient of permeability of filter media (hydraulic conductivity) | k | 4.00 | Ft / Day |
| Planter bed Depth (soil media) | d _f | 1.50 | Ft |
| Average Height of water above planter bed | h _f | 0.50 | Ft |
| Design planter bed drain Time | t _f | 4.00 | Hours |
| Required Surface Area of Planter Bed [A _f = (WQ _v x d _f) / (k x (h _f + d _f) x t _f)] | A _f | 684.27 | SF |

Proposed Area

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|----------------|-----------------|-------|
| Calculated planter bed area (Length x Width) | | | SF |
| Surface Area of Planter Bed Provided | A _f | 1,212.00 | SF |
| Actual Volume Provided | | 606 | CF |

Runoff Reduction

| DESCRIPTION | VALUE | UNITS |
|--|---------------------|-------|
| Is Proposed Af > Required Af ? | YES | |
| Type of Planter | FLOW-THROUGH | |
| RR _v Provided for Infiltration Planter | 608 | CF |
| RR _v Provided for Flow-Through Planter in HSG 'C' Soils | 274 | CF |
| RR _v Provided for Flow-Through Planter in HSG 'D' Soils | 182 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2C**

Green Roof #1

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.18 | |
| Area | A | 0.18 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [0.05 + 0.009 x %I] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 920 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 852.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 2.00 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 852.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 35.50 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 35.50 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 923 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 923 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2C**

Green Roof #2

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.03 | |
| Area | A | 0.03 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 131 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 123.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 2.00 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 123.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 5.13 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 5.13 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 133 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 133 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2C**

Green Roof #3

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.03 | |
| Area | A | 0.03 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 151 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 141.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 2.00 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 141.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 5.88 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 5.88 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 153 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 153 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2C**

Green Roof #4

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.15 | |
| Area | A | 0.15 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 781 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 721.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 2.00 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 721.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 30.04 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 30.04 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 781 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 781 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2C**

Green Roof #5

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.03 | |
| Area | A | 0.03 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [0.05 + 0.009 x %I] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 176 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 194.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 2.00 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 194.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 8.08 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 8.08 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 210 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 210 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #6

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.06 | |
| Area | A | 0.06 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 309 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 933.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 233.25 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{DL} \times n_{DL}$] | V_{DL} | 38.88 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 38.88 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 311 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 311 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #7

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|-----------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.01 | |
| Area | A | 0.01 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [0.05 + 0.009 x %I] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 59 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|-----------|-------|
| Green Roof surface AREA | A_{RG} | 185.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 46.25 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 7.71 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 7.71 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 62 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|-----------|-------|
| Runoff Reduction volume provided | RR_V | 62 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #8

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|-----------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.00 | |
| Area | A | 0.00 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 18 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|-----------|-------|
| Green Roof surface AREA | A_{RG} | 66.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 16.50 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{DL} \times n_{DL}$] | V_{DL} | 2.75 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 2.75 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 22 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|-----------|-------|
| Runoff Reduction volume provided | RR_V | 22 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #9

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|------------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.05 | |
| Area | A | 0.05 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 270 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|------------|-------|
| Green Roof surface AREA | A_{RG} | 812.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 203.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 33.83 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 33.83 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 271 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|------------|-------|
| Runoff Reduction volume provided | RR_V | 271 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #10

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|-----------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.01 | |
| Area | A | 0.01 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 77 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|-----------|-------|
| Green Roof surface AREA | A_{RG} | 246.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 61.50 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{DL} \times n_{DL}$] | V_{DL} | 10.25 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 10.25 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 82 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|-----------|-------|
| Runoff Reduction volume provided | RR_V | 82 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #11

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|-----------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.02 | |
| Area | A | 0.02 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [$0.05 + 0.009 \times \%I$] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 80 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|-----------|-------|
| Green Roof surface AREA | A_{RG} | 248.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 62.00 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 10.33 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 10.33 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 83 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|-----------|-------|
| Runoff Reduction volume provided | RR_V | 83 | CF |

GREEN ROOF WORKSHEET

JMC Project: **22062**

Design Point: **2**

Drainage Area: **PDA-2D**

Green Roof #12

Site Data for Drainage Area to be Treated by Practice

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|--|--------|-----------|-------|
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I_N | 0.02 | |
| Area | A | 0.02 | Ac |
| Percent Impervious | %I | 100.00 | % |
| Runoff Volume [0.05 + 0.009 x %I] | R_V | 0.95 | CF |
| TOTAL VOLUME Required [$WQ_V = (P \times R_V \times A) / 12$] | WQ_V | 95 | CF |

Proposed Green Roof

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|---|----------|-----------|-------|
| Green Roof surface AREA | A_{RG} | 294.00 | SF |
| DEPTH of the Soil Media | D_{SM} | 0.50 | Ft |
| DEPTH of the Drainage Layer | D_{DL} | 0.17 | Ft |
| DEPTH of Ponding above surface | D_P | 0.04 | Ft |
| Porosity of the Soil Media | n_{SM} | 50% | % |
| Porosity of the Drainage Layer | n_{DL} | 25% | % |
| VOLUME provided in Soil Media [$V_{SM} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{SM} | 73.50 | CF |
| VOLUME provided in Drainage Layer [$V_{DL} = A_{RG} \times D_{SM} \times n_{SM}$] | V_{DL} | 12.25 | CF |
| VOLUME provided in Ponding Area [$D_P \times A_{RG}$] | | 12.25 | CF |
| TOTAL VOLUME Provided [$WQ_V \leq V_{SM} + V_{DL} + (D_P \times A_{RG})$] | WQ_V | 98 | CF |

Runoff Reduction

| DESCRIPTION | SYMBOL | VALUE | UNITS |
|----------------------------------|--------|-----------|-------|
| Runoff Reduction volume provided | RR_V | 98 | CF |

PROPRIETARY PRACTICE WORKSHEET

JMC Project: **22062**

Design Point: **3**

Drainage Area: **PDA-3**

Water Quality Structure

Rainfall Distribution Type: **III**

| | | A | B | C |
|---|-------|---------|---------|---------|
| Coefficients for the equation unit peak | C_0 | -1.774 | 0.3301 | 2.4577 |
| $[R = I_a / P]$ | C_1 | 1.8622 | -0.7397 | -0.4627 |
| $[C_i = A \times R^2 + B \times R + C]$ | C_2 | -0.0648 | 0.2276 | -0.1932 |

| Site Data for Drainage Area to be Treated by Practice | | | |
|---|--------|--------------|-------|
| DESCRIPTION | SYMBOL | VALUE | UNITS |
| Design Storm [90% Rainfall Event Number] | P | 1.5 | In |
| Impervious Area | I | 1.59 | Ac |
| Area | A | 3.61 | Ac |
| Percent Impervious | %I | 44.14 | % |
| Runoff Coefficient $[0.05 + 0.009 \times \%I]$ | R_v | 0.45 | CF |
| TOTAL VOLUME Required $[WQ_v = (P \times R_v \times A) / 12]$ | WQ_v | 8,781 | CF |
| Design Storm [1-yr Storm Depth] | P | | In |
| TOTAL VOLUME Required (TMDL) $[WQ_v = 1\text{-yr Storm Runoff}]$ | WQ_v | | CF |

| Water Quality Peak Flow Calculation | | | |
|--|--------|-------------|-------------------------|
| DESCRIPTION | SYMBOL | VALUE | UNITS |
| Water Quality Volume | WQ_v | 8,781 | CF |
| Design Storm [90% Rainfall Event Number] or [1-yr Storm Depth] | P | 1.5 | In |
| Time of Concentration | t_c | 0.1560 | Hr |
| Runoff Volume $[Q = WQ_v / (A \times 3630)]$ | Q | 0.67 | In |
| Curve Number $[CN = 1000 / (10 + 5P + 10Q - 10 \times (Q^2 + 1.25 QP)^{1/2})]$ | CN | 89.77 | |
| Curve Number | CN | 90 | |
| Initial Abstraction $[I_a = 200 / CN - 2]$ | I_a | 0.23 | In |
| Ratio $[R = I_a / P]$ | R | 0.15 | |
| $C_0 = A \times R^2 + B \times R + C$ | C_0 | 2.47 | |
| $C_1 = A \times R^2 + B \times R + C$ | C_1 | -0.53 | |
| $C_2 = A \times R^2 + B \times R + C$ | C_2 | -0.16 | |
| Unit Peak Discharge | q_u | 619.44 | cfs/mi ² /in |
| Peak Discharge $[Q_p = q_u \times A \times Q / 640]$ | Q_p | 2.34 | cfs |

| Proposed Device | | | |
|--|--------|---------------|-------|
| DESCRIPTION | SYMBOL | VALUE | UNITS |
| Water Quality Peak Flow Provided | Q_p | 2.9 | cfs |
| Water Quality Volume Provided $[WQ_v = 640 \times 3600 \times Q_p / q_u]$ | WQ_v | 10,935 | CF |
| Model Designation | | JFPD0808 | |
| Quantity | | 1 | |

APPENDIX C

SOIL TESTING DATA



CARLIN • SIMPSON & ASSOCIATES, LLC

Consulting Geotechnical and Environmental Engineers

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16 August 2023

AMS Acquisitions
One Bridge Plaza North
Suite 840
Fort Lee, NJ 07024

Attn: Mr. Ryan Sutherland, AIA LEED AP BD&C
Director of Design and Development

Re: Preliminary Report on Subsurface Soil and Foundation Investigation
Proposed 4 Story Building
Albany Post Road and Craft Lane
Buchanan, NY (CSA Job #23-34)

Dear Mr. Sutherland:

In accordance with our proposal dated 6 March 2023 and your subsequent authorization, we have completed a Preliminary Subsurface Soil and Foundation Investigation for the referenced site. The purpose of this study was to determine the nature and engineering properties of the subsurface soil and groundwater conditions for the new construction, to recommend a practical foundation scheme, to determine the allowable bearing capacity of the site soils, and to preliminary determine the subsurface conditions in the new stormwater management areas.

We understand that the planned construction will consist of a new 4 story building with 1 level of below-grade parking. The proposed construction will also include site retaining walls, stormwater management areas, new underground utilities, and new asphalt-paved driveways and parking areas. To guide us in our study, you have provided us with plans that indicate the existing site conditions and the conceptual location of the proposed construction.

Our scope of work for this project included the following:

1. Reviewed the proposed layout, the existing site conditions, the expected soil conditions, and planned this study.
2. Retained Environmental Technical Drilling Inc. to advance 13 test borings at the subject site.
3. Retained American Tree and Landscape Corp. to excavate 12 test pits at the subject site.

4. Laid out the boring and test pit locations in the field, provided full time inspection of the explorations, obtained soil samples, and prepared detailed logs and a Boring & Test Pit Location Plan.
5. Performed soil identification tests on selected soil samples in our laboratory.
6. Analyzed the field and laboratory test data and prepared this report containing the results of this study.

1.0 SITE DESCRIPTION

The subject property is located behind 3115 and 3119 Albany Post Road at the intersection with Craft Lane in Buchanan, Westchester County, New York. The property is currently undeveloped and wooded with varying (sparse to dense) vegetation. The site grades generally slope down from east to west and vary from approximately +120.0 to +66.0.

There is a pond on the adjacent property to the south that extends into the southern portion of the subject site. Historic aerial photographs indicate that the pond was larger at one time and extended further to the north into the area of the proposed building. The pond was filled sometime between 1964 and 1974.

2.0 PROPOSED CONSTRUCTION

We understand that the planned construction will consist of a new 4 story building with 1 level of below-grade parking. Preliminarily, the finished floor elevation for the new building will be at elevation +79.5. Based on the existing site conditions, we anticipate that cuts up to 16 feet will be required in the southeast and northeast corners of the building and fills up to 2 feet will be required on the west side of the building to achieve the finished floor elevation. Based on the preliminary plans, we understand that the proposed construction will also include two new retaining walls, stormwater management areas, underground utilities, and asphalt-paved driveways and parking areas.

The recommendations within this report are preliminary in nature and have been generalized for the anticipated development. The recommendations below are intended for planning purposes only and are not intended for final design and construction. Additional subsurface investigation (i.e. borings) is also required for the subject site, as discussed later in this report. The recommendations provided within this report are subject to change pending the supplemental subsurface investigation as well as the final site layout and grading. Once the site and building plans are further developed, a copy of the plans should be forwarded to our office so that we can review them along with the recommendations in this report. At that time, any changes or additional recommendations can be provided, if required.

3.0 SUBSURFACE CONDITIONS

To determine the subsurface soil and groundwater conditions at the site 13 borings and 12 test pits were performed for the referenced project. The borings were performed by

Environmental Technical Drilling Inc. using hollow stem augers and split spoon sampling. The test pits were excavated by American Tree and Landscape Corp. using a backhoe. Detailed boring and test pit logs have been prepared and are included in this report.

The borings were completed in July 2023 and the test pits were excavated in June 2023 under the full-time inspection of Carlin-Simpson & Associates. Our field engineer visually identified all of the soil samples obtained during the boring and test pit operations and select samples were tested in our laboratory.

3.1 Soil and Rock

The soil descriptions shown on the boring and test pit logs are based on the Burmister Classification System. In this system, the soil is divided into three components: Sand (S), Silt (\$) and Gravel (G). The major component is indicated in all capital letters, the lesser in lower case letters. The following modifiers indicate the quantity of each lesser component:

| <u>Modifier</u> | <u>Quantity</u> |
|------------------------|------------------------|
| trace (t) | 0 -10% |
| little (l) | 10% - 20% |
| some (s) | 20% - 35% |
| and (a) | 35% - 50% |

The subsurface soil and rock conditions encountered in the borings and test pits can be summarized as follows:

Stratum 1A Topsoil The surface layer in 9 borings and in each of the test pits consists of dark brown or black topsoil that ranges from approximately 0'2" to 1'4" in thickness.

Stratum 1B Asphalt At the surface in the remaining 4 borings is asphalt pavement that ranges from approximately 0'2" to 0'8" in thickness.

Stratum 2 Existing Fill Beneath the surface layers in 8 borings and 6 test pits is existing fill that generally consists of loose to dense brown, gray, black coarse to fine Sand, trace (to some) Silt, trace (to some) coarse to fine Gravel, with varying amounts of cobbles, boulders, organic material, and debris. Organic material and/or debris was noted in 3 of the test pits and 4 of the borings and consisted of roots, buried topsoil, plastic, wood, concrete, brick, and asphalt. The existing fill was encountered to depths ranging from 1'6" to more than 27'0" below the existing ground surface at the boring and test pit locations.

Stratum 3 Sand, Silty Sand, or Sandy Gravel Below the surface layers and existing fill in many locations is a shallow layer of medium dense to dense brown, gray coarse to fine SAND, trace (to and) Silt, trace (to and) coarse to fine Gravel or coarse to fine GRAVEL some (to and), coarse to fine Sand, trace Silt. Many cobbles and boulders were encountered in this stratum. This layer was encountered to depth ranging from 1'0" to 8'3" below the existing ground surface at the boring and test pit locations.

Stratum 4
Clayey Silt

Underlying the above layers in borings B-8 and B-12 and in test pit TP-12 is medium stiff to stiff brown, gray or mottled red brown, brown, gray Clayey SILT, trace coarse to fine Sand. Boring B-8 was terminated in this stratum at a depth of 29'0" below the ground surface and test pit TP-12 was terminated in this stratum at a depth of 9'6" below the surface. At boring B-12, this stratum continued to a depth of 10'2" below the ground surface.

Stratum 5
Weathered
Bedrock

Beneath the existing fill and virgin soil layers is weathered bedrock. In some test pit locations, the upper few feet of the bedrock was completely weathered and rippable. However, the completely weathered rock quickly transitioned to harder rock. Auger or bucket refusal on probable harder bedrock was encountered in 16 of the boring and test pit locations at depths ranging from 1'0" to 6'8" below the existing ground surface. At boring B-12, spoon refusal on possible bedrock was encountered at a depth of 10'2" below the ground surface.

At boring B-9, the upper 5 feet of the bedrock was cored. The rock generally consisted of gray Gneiss or Norite, was moderately jointed, and was slightly to moderately weathered. The rock core recovery ranged from 95% to 100% and the rock quality designation (RQD) of the recovered cores was 39% and 70%. Based on the rock core RQD values and visual inspection, the upper portion of the bedrock in the area of B-9 can be described as poor to fair quality ranging from a shattered condition to a blocky and seamy condition.

3.2 Bedrock

Bedrock or refusal on probable bedrock was encountered at depths ranging from 1'0" to 10'2" below the existing ground surface (elevation +63.5 to +90.0) at many of the boring and test pit locations. Based on our experience, the bedrock will generally transition from completely or highly weathered rock to harder bedrock with increasing depth. The bedrock observations are summarized in Table 1 below.

Based on the preliminary grading plan, cuts are planned for portions of the site. Based on the proposed construction and boring data, some of these excavations will extend into bedrock. Only limited bedrock core samples were obtained during this preliminary investigation. We recommend that additional borings be performed with rock coring to determine the rock quality, degree of weathering, and consistency of fractures in the deeper cut areas for the proposed building and in the proposed retaining wall areas.

Penetration into the bedrock and completely weathered rock with excavation equipment will depend on the degree of weathering and fracturing in the rock. The upper few feet of rock may be "rippable" by using large construction equipment, but we anticipate that the "rippability" of the bedrock will be variable and very limited. It should not be assumed that the completely weathered rock (very dense material in a soil-like state) can be excavated with conventional equipment. Zones of harder rock will be encountered within the completely weathered rock layer. Where harder rock is encountered in the site excavations, the use of hydraulic hammers and/or rock blasting will be required to excavate the harder bedrock.

3.3 Groundwater

During this investigation, groundwater was encountered in 8 of the boring and test pit locations at depths ranging from 3'0" to 14'0" (elevations +75.5 to +62.8) below the ground surface. In some locations, the observed groundwater may be trapped in the fill layer or perched on the bedrock surface. The groundwater observations are summarized in Table 1 below.

During construction, we expect that perched or trapped water may be encountered within the existing fill, in the silty site soils, and/or along the soil/rock interface, especially during wet periods. Groundwater on the subject site will be controlled by the topography and the underlying bedrock surface. Proper groundwater control measures will be required where water is encountered in the site excavations.

Variations in the location of the long-term water table may occur as a result of changes in precipitation, evaporation, surface water runoff, and other factors not immediately apparent at the time of this exploration.

3.4 Summary of Boring and Test Pit Observations

A summary of the boring and test pit observations is provided in Table 1 below. Borings B-2 through B-8, B-10, B-12, and B-13 were performed within the proposed building area.

Table 1 – Summary of Boring and Test Pit Observations

| Boring or Test Pit No. | Approximate Existing Ground Surface Elevation | Depth to Bottom of Existing Fill (Elevation) | Depth to Groundwater (Elevation) | Depth to Bedrock (Elevation) |
|------------------------|---|--|----------------------------------|------------------------------|
| B-1 | +70.0 | 4'0" (+66.0) | NE to 4'0" | AR @ 4'0" (+66.0) |
| B-2 | +78.0 | >9'0" (+69.0) | 7'0 (+71.0) | NE to 9'0" |
| B-3 | +81.0 | 1'6" (+79.5) | NE to 5'3" | AR @ 5'3" (+75.8) |
| B-4 | +79.0 | 3'7" (+75.4) | NE to 3'7" | AR @ 3'7" (+75.4) |
| B-5 | +79.5 | 5'6" (+74.0) | NE to 6'8" | AR @ 6'8" (+72.8) |
| B-6 | +78.5 | 2'5" (+76.1) | NE to 2'5" | AR @ 2'5" (+76.1) |
| B-7 | +80.0 | NE | NE to 1'2" | AR @ 1'2" (+78.8) |
| B-8 | +79.0 | 5'6" (+73.5) | 14'0" (+65.0) | NE to 29'0" |
| B-9 | +88.0 | NE | NE to 1'0" | C @ 1'0" (+87.0) |
| B-10 | +78.5 | >27'0" (+51.5) | 3'0" (+75.5) | NE to 27'0" |
| B-11 | +79.0 | NE | NE to 1'9" | AR @ 1'9" (+77.3) |
| B-12 | +79.0 | 8'0" (+71.0) | 4'7" (+74.4) | SR @ 10'2" (+68.8) |
| B-13 | +79.0 | NE | NE to 1'4" | AR @ 1'4" (+77.7) |
| | | | | |
| TP-1 | +68.0 | 7'9" (+60.3) | 5'3" (+62.8) | NE to 8'3" |
| TP-2 | +71.0 | 5'9" (+65.3) | 8'3" (+62.8) | NE to 8'6" |
| TP-3 | +80.0 | NE | NE to 1'0" | BR@ 1'0" (+79.0) |
| TP-4 | +78.5 | NE | NE to 1'0" | BR @ 1'0" (+77.5) |
| TP-5 | +77.0 | >7'6" (+69.5) | 6'9" (+70.3) | NE to 7'6" |
| TP-6 | +95.0 | NE | NE to 5'0" | BR @ 5'0" (+90.0) |
| TP-7 | +70.0 | 3'0" (+67.0) | NE to 3'0" | BR @ 3'0" (+67.0) |
| TP-8 | +68.0 | 4'6" (+63.5) | NE to 4'6" | BR @ 4'6" (+63.5) |

| Boring or Test Pit No. | Approximate Existing Ground Surface Elevation | Depth to Bottom of Existing Fill (Elevation) | Depth to Groundwater (Elevation) | Depth to Bedrock (Elevation) |
|------------------------|---|--|----------------------------------|------------------------------|
| TP-9 | +82.0 | NE | NE to 1'3" | BR @ 1'3" (+80.8) |
| TP-10 | +88.0 | NE | NE to 1'1" | BR @ 1'1" (+86.9) |
| TP-11 | +87.0 | NE | NE to 2'8" | BR @ 2'8" (+84.3) |
| TP-12 | +72.0 | 8'2" (+63.8) | 7'6" (+64.5) | NE to 9'6" |

NE – Not Encountered

C – Cored Bedrock

AR/BR – Auger or Bucket Refusal on Probable Bedrock

SR – Spoon Refusal on Possible Bedrock

4.0 SUMMARY OF DESIGN RECOMMENDATIONS

Below is a summary of the major design and construction considerations for this project. Additional recommendations are provided in the following sections of this report.

- Subsurface Conditions (Section 3.0)
 - Existing fill was encountered in 15 of the 25 test locations to depths ranging from 1'6" to more than 27'0" below the existing ground surface (elevations +79.5 to +51.5).
 - A pond was formerly present in the southwest portion of the proposed building. Borings B-2, B-4, B-10, and B-12 as well as test pit TP-5 encountered fill with boulders, debris (concrete, brick, plastic, brick), and organic material (roots and topsoil) that had been used to previously fill the pond. The fill in this area extended to depths ranging from 3'7" to more than 27'0" below the ground surface. Existing fill outside the pond area extended to depths ranging from 1'6" to 8'2" below the ground surface.
 - Groundwater was encountered in 8 of the 25 test locations at depths ranging from 3'0" to 14'0" below the ground surface (elevations +75.5 to +62.8).
 - Weathered bedrock was encountered in 18 of the 25 test locations at depths ranging from 1'0" to 10'2" below the existing ground surface (elevations +90.0 to +63.5). The use of hydraulic hammers and/or blasting will likely be required to achieve subgrade elevations in portions of the site.
 - A summary of the subsurface observations is provided in Table 1.
- Building Evaluation (Section 5.0)
 - The existing fill is not suitable for support of the proposed building foundations or floor slab. In addition, the boring and test pit data indicates that there are abrupt changes from deep soil to shallow bedrock within the building area. To eliminate the potential for damaging differential settlements, micropiles shall be used in areas that are underlain by existing fill or virgin soil. Where bedrock is at or above the foundation elevation, shallow spread footings may bear directly on bedrock.
 - Drilled micropiles foundations capable of supporting axial capacities of 100 to 125 tons can be used for the new building. A load test will be required to confirm the micropile capacity.
 - Where shallow spread footings can be constructed directly on bedrock, the net design bearing pressure shall be 8,000 psf.
 - The building floor slab shall be designed as a structural slab for the entire building.
 - Sub-slab drainage may be required for portions of the building.

- Seismic Site Class is C or Very Dense Soil or Soft Rock Profile.
- ***Supplemental borings are required to further evaluate the existing fill and bedrock conditions in the proposed building area.***
- *Additional Site Recommendations (Section 6.0)*
 - *New Retaining Walls (Section 6.2)*
 - A cast-in-place steel reinforced concrete wall, a large segmental block wall, and a soil/rock nail and shotcrete wall can be considered for this project.
 - ***Additional borings are required to further evaluate the subsurface conditions and to complete the retaining wall recommendations.***
 - *Utilities (Section 6.3) and Pavement (Section 6.4)*
 - Densified existing fill, virgin soil, new compacted fill, and weathered rock may be used to support the new utilities and pavement.
 - The use of hydraulic hammers and/or blasting may be required in areas to achieve the proposed subgrade elevations.

5.0 **BUILDING EVALUATION**

We understand that the planned construction will consist of a new 4 story building with 1 level of below-grade parking. Preliminarily, the finished floor elevation of the new building will be at +79.5. Based on existing and proposed grades, we anticipate cuts up to 16 feet will be required in the southeast and northeast corners of the building and fills up to 2 feet will be required on the west side of the building. The southeast and northeast cuts will require rock excavation to achieve the planned finished floor elevation. The use of hydraulic hammers and/or blasting (if permitted) will likely be required.

As discussed above, there was previously a pond located in the proposed building area that was filled sometime between 1964 and 1974. The approximate pond limits are shown on the attached Boring & Test Pit Location Plan. The boring data indicates that the existing fill material within the proposed building area extends to depths ranging from 1'6" to more than 27'0" below the existing ground surface (elevations +79.5 to +51.5). The depth and extent of the existing fill are variable, and the fill may be deeper in unexplored areas of the site. The existing fill is not an acceptable bearing material for the new building foundations or floor slab. The consistency and density of the fill are not predictable. Certain areas may contain clean dense soil while other areas may contain loose material, void spaces, and/or debris, as shown by the boring and test pit data. The existing fill creates the possibility of intolerable differential settlements under loading. In addition, the boring and test pit data indicates that there are abrupt changes from deep soil to shallow bedrock within the proposed building area.

To eliminate the potential for damaging differential settlements, micropiles shall be used in areas that are underlain by existing fill or virgin soil. Preliminarily, we anticipate that micropiles will be required in the central and southwestern portions of the building. Where bedrock is at or above the foundation elevation, which is expected in the northern and southeastern portions of the building, shallow spread footings may bear directly on bedrock. ***Supplemental borings are required to further evaluate the existing fill and bedrock conditions within the proposed building area. The borings must extend through numerous boulders in areas and shall include rock coring to evaluate the quality of the underlying bedrock.***

Preliminary recommendations for preparation of the building area are provided in Section 5.1 below. Micropile foundation recommendations are provided in Section 5.2. Recommendations for foundations bearing on bedrock are provided in Section 5.3 below. Floor slab and foundation wall recommendations can be found in Section 5.4 and Section 5.5 below, respectively.

5.1 Building Area Preparation

In order to prepare the site for construction, all surface materials such as surface vegetation, topsoil, and asphalt shall be removed from the planned building areas, extending at least 10 feet beyond the new construction limits, where practical.

Rock Removal - Blasting

In order to develop the site, rock or weathered rock cuts will be required in areas. Based on our experience, the in-situ bedrock will be variable, ranging from completely weathered rock to harder intact bedrock. The top 1 to 5 feet of rock may be “rippable” by using large construction equipment. However, we anticipate that the “rippability” of the bedrock will be variable and very limited. The use of hydraulic hammers and/or blasting will be required to excavate the harder bedrock and zones of harder rock within the completely weathered rock stratum. Additional blasting requirements and details will be provided once the project plans have been further developed and the supplemental borings have been completed.

Handling Groundwater and Wet Subgrades

Based on the boring and test pit data, groundwater is not expected to be encountered above the planned finished floor elevation during construction. However, perched or trapped groundwater may be present in the existing fill, in the silty site soils, along the soil/rock interface, and/or in the bedrock fractures. In the event that perched or trapped groundwater is encountered in the site excavations, proper groundwater control measures (i.e. construction dewatering) will be required.

Where required, temporary groundwater control measures shall consist of 1 or more sumps and pumps. The sumps shall consist of a perforated pipe at least 8 inches in diameter, surrounded by crushed stone and filter fabric. The sump pits must be installed just outside the planned excavation area and at least 2 feet below the lowest anticipated subgrade elevation. The sumps and pumps must be set and in operation prior to excavating below the water table. The pumps shall be used to temporarily lower the surrounding groundwater level and keep the excavation relatively dry.

In the event that the exposed subgrade soil within the excavation becomes wet or soft, stabilizing the subgrade surface may be required. The subgrade may be stabilized with geotextile filter fabric and crushed stone. The geotextile filter fabric shall consist of Mirafi 500X or equivalent. Adjacent layers of geotextile filter fabric should be overlapped a minimum of 6 inches. As necessary, approximately 12 inches of 3/4-inch clean crushed stone will be installed on top of the filter fabric layer to provide a firm working surface, provide protection for the geotextile filter fabric, minimize pumping, and to stabilize the subgrade soil. Carlin Simpson &

Associates will determine the need for subgrade stabilization and will direct the contractor during construction.

Installation of New Structural Fill

New fill required to achieve final grades shall consist of either engineer-approved on-site soil or imported sand and gravel. The new fill shall be placed in layers not exceeding one (1) foot in thickness and each layer shall be compacted to at least 95% of its Maximum Modified Dry Density (ASTM D1557). Each layer must be compacted, tested, and approved by the Carlin-Simpson & Associates field representative prior to placing subsequent layers. The suitability of the on-site soil and rock for reuse as compacted fill is discussed in Section 6.6 below.

If imported structural fill will be required during construction, the imported structural fill shall meet the following specified gradation:

| <u>US Standard Sieve Size</u> | <u>Percent Finer By Weight</u> |
|-------------------------------|--------------------------------|
| 3-inch | 100 |
| No. 4 | 30-80 |
| No. 40 | 10-50 |
| No. 200 | 0-20 |

Based on the preliminary grading plans, rock cuts are also required at the site to achieve proposed grades. We anticipate that excavated boulders and rock material will be processed onsite for use of backfill material. Refer to section 6.6 below for recommendations regarding use of excavated cobbles, boulders, and rock material.

5.2 Micropile Foundations

For this project, drilled in-place grout-filled steel pipe piles (micropiles) can be used to support the new building foundations and the floor slab in the existing fill and deep virgin soil areas. Preliminarily, we expect that micropiles will be required for the central and southwestern portions of the proposed building. The piles must extend through the existing fill and soil layers and develop their load carrying capacity with a bond zone formed in the underlying bedrock. To accomplish this, the piles must be cased through the existing fill and soil layers.

The depth to bedrock within the anticipated micropile areas of the building varies significantly. Based on the boring and test pit observations, we expect bedrock to be encountered approximately 3'7" to more than 29'0" below the existing ground surface. As discussed above, supplemental borings are required to further evaluate the existing fill and bedrock conditions within the proposed building area.

The project structural engineer shall determine the number of piles required and their locations. The micropiles shall be designed by a micropile contractor to meet the specified loading conditions as shown on the structural drawings. The piles must also be designed and installed in accordance with the New York State Building Code.

For this project, we recommend that the steel pipe casing have a minimum nominal diameter of 8 inches and a wall thickness of at least 0.408 inches. The casing shall extend at least

1 foot into the bond zone upon the completion of the grouting and shall remain in place permanently. The micropiles shall be filled with cement grout having a minimum 28-day compressive strength of at least 5,000 psi. The grout mix shall be designed and proportioned so as to produce a pumpable mixture. A maximum water/cement ratio of 0.44, by weight is recommended. Center to center spacing shall be at least three times the outside diameter of the steel casing but not less than 30 inches.

Preliminarily, 8-inch diameter piles with an allowable capacity of 100 to 125 tons could be considered for the proposed building. This would require a rock socket length of approximately 8 to 12 feet. The preliminary estimated pile lengths, assuming a finished floor elevation at +79.5, can be found in Table 2 below. Additional borings are required to finalize the anticipated pile depths. The structural engineer shall select the required allowable pile capacity based on the design loads of the proposed structure.

Table 2 – Pile Recommendations

| Pile Capacity | Estimated Cased Length | Rock Socket Length | Estimated Total Length |
|----------------------|-------------------------------|---------------------------|-------------------------------|
| 100 | 4 to >29 feet | 8 to 10 feet | 12 to >39 feet |
| 125 | 4 to >29 feet | 10 to 12 feet | 14 to >41 feet |

Reinforcing steel extending to the bond zone shall be placed in the casing to the bottom of the bond zone prior to placing grout. The full length of the micropile shall contain either a steel pipe and/or steel reinforcement. Reinforcement steel shall be in accordance with ASTM A615 Grade 60 or 75 or ASTM A722 Grade 150. Preliminarily, we anticipate that the core reinforcement steel will consist of a single steel threaded bar, ASTM A615 Grade 150 (150 ksi yield strength), extending the full length of the pile. As required for structural design, steel reinforcement bars shall extend from the micropile and up into the pile cap, grade beam, and/or floor slab.

The pile to pile cap or grade beam connection shall be designed by the project structural engineer. The top of the pile should be embedded into the grade beam or pile cap a minimum of 6 inches and should be at least 6 inches from the edges of the grade beam or cap. Typically, the top of the pile is terminated with a bearing plate that extends into the pile cap or grade beam to transfer the applied load. Structural steel plates shall conform to ASTM A36 or ASTM A572 Grade 50.

Based on the boring observations, obstructions and debris (i.e. cobbles, boulders, brick, concrete, etc.) are present within the existing fill layer. Depending upon the depth of the obstruction below the bottom of the pile cap or grade beam, the contractor shall either remove the obstruction or clear away the obstruction by excavating or other means, or abandon the pile and install an additional pile at the locations determined by the project structural engineer.

Micropile Submittals

For this project, the pile contractor will design the individual pile elements and select the pile construction process and installation equipment. The foundation specialty contractor shall

submit shop drawings and design calculations to Carlin-Simpson & Associates and the project structural engineer for review and approval.

At a minimum the contractor's submittal should include the following: 1) pile design calculations and shop drawings for all structural steel and pile components prepared and stamped by a New York State registered Professional Engineer; 2) a detailed description of the construction procedure proposed, including type of equipment to be used for installing the piles; 3) a pile location and numbering plan; 4) the proposed concrete or cement grout mix design(s) and procedures for placing the concrete or cement grout; and 5) detailed plans and procedures for the pile load test(s), including load test apparatus set-up for the pile load testing and current calibration report for the hydraulic jack and gauges.

Micropile Load Tests and Inspection

A compressional load test will be required to confirm the micropile contractor's pile design. The test may be performed on either a production pile or a sacrificial pile. However, production piles shall not be used as reaction piles. The pile load test(s) must be performed under the full time inspection of a Carlin-Simpson & Associates representative. Piles used for the pile load test should be installed at least 1 week prior to testing to allow time for the grout to obtain adequate strength for testing.

The piles shall be installed under the full time inspection of a representative from Carlin-Simpson & Associates. At the completion of the pile installation, Carlin-Simpson & Associates will provide a letter of compliance stating that the piles have been installed in accordance with our recommendations and the project specifications, and that they are capable of supporting the design loads.

5.3 New Building Foundations on Bedrock

Where bedrock is near or above the foundation subgrade elevation, which is expected in the northern and southeastern portions of the building, shallow spread footings may bear directly on the bedrock surface. The new building foundations in these areas may be designed as shallow spread footings using a net design bearing pressure as listed in Table 3 below. As discussed above, additional borings are required to further evaluate the existing fill and bedrock conditions within the proposed building area.

All of the exterior and interior footings shall bear directly on bedrock, which is not susceptible to frost. In some areas, however, we expect that the footings may have to step down approximately 1 to 3 feet below the subgrade elevation to bear on the bedrock surface. Care must be taken during rock excavation to not disturb the bedrock that will remain and support the new foundations. If the bedrock is disturbed/over-blasted, either the unsuitable bearing material will have to be over-excavated and replaced with concrete or micropiles will be required.

The excavations for the new foundations shall be performed under the full-time inspection of Carlin-Simpson & Associates. The on-site representative shall confirm that the foundation bearing material is capable of supporting the design bearing pressure.

Table 3 – Foundation Design Parameters for Rock

| Description | Value |
|-----------------------------|--------------|
| Foundation Bearing Material | Bedrock |
| Net Design Bearing Pressure | 8,000 psf |
| Minimum Column Dimension | 30 inches |
| Minimum Wall Dimension | 18 inches |

5.4 Floor Slab

The existing fill is not suitable for support of the proposed floor slab. Where a new floor slab will be constructed as part of the proposed construction, we recommend that it be designed as a structural slab. Pile recommendations are discussed in the previous section of this report.

Floor Slab Underdrains

Preliminarily, we believe that a permanent dewatering system consisting of a sub-slab drainage system may be required for the southeast and/or northeast portions of the proposed building where substantial cuts are needed to achieve the planned finished floor elevation. We expect that an underdrain system can be drained by gravity to the stormwater management system, but a sump pit and pump system could be required. Carlin-Simpson & Associates will determine the need for and the extent of the sub-slab drainage system as the project plans are further developed and after the supplemental investigation is completed.

5.5 Foundation Walls

Where foundation walls are required, the soil adjacent to the building walls will exert a horizontal pressure against the wall. This pressure is based on the soil density and Coefficient of Earth Pressure at Rest (k_0), which is applicable to non-yielding building walls. Foundation wall design parameters are listed in Table 4 below.

Table 4 – Foundation Wall Design Parameters

| Soil Type | On-Site Soils |
|---|----------------------|
| Moist Unit Weight (γ) | 130 pcf |
| Coefficient of Earth Pressure at Rest (k_0) | 0.5 |
| Equivalent Fluid Pressure | 65 psf/ft |
| Foundation Sliding Coefficient. | |
| Virgin Soils or New Structural Fill: | 0.45 |
| Clean Sound Rock: | 0.55 |

Where foundation walls are required, we recommend that a footing drain be placed around the exterior of the new building to prevent water from accumulating against the foundation wall. This drain may consist of a minimum 4-inch diameter, rigid wall perforated PVC pipe surrounded by at least 12 inches of 3/4-inch clean crushed stone. The stone shall be wrapped in a geotextile fabric, such as Mirafi 140N or equivalent. The foundation drainpipe should be extended to daylight, if possible, or to the stormwater collection system. The outside face of the foundation wall, where it extends below grade, shall be waterproofed.

Outside the building, the backfill placed adjacent to the foundation walls and above the footing drain shall consist of either clean crushed stone or an imported sand and gravel mixture containing less than 10% by weight passing a No. 200 sieve and placed in layers not exceeding 12 inches in thickness. This clean sand and gravel or crushed stone backfill shall extend a minimum of 12 inches horizontally from the back face of the foundation walls, and shall extend vertically up the wall face to 2 feet below the finished ground surface elevation. Where retained soils are not covered by concrete or pavement and are exposed to weather, the top 2 feet of backfill should consist of low permeable soil. This will help to minimize water infiltration behind the wall. Surface grades should be sloped away from the building to prevent water from accumulating adjacent to the wall.

Beyond this point, the foundation walls should be backfilled with suitable soil placed in layers up to 12 inches in thickness. The suitability of the on-site soil for reuse as compacted fill is discussed in a separate section below. The new fill should be compacted with a vibratory drum trench compactor (i.e. Wacker Model RT560), a heavy vibratory plate tamper (i.e. Wacker BPU 3545A or equivalent), or “jumping jack” style tamper (i.e. Wacker Model BS 600) to at least 92% of its Maximum Modified Dry Density (ASTM D1557). Heavy equipment should not be operated near the building walls as damage to the walls could occur.

5.6 Seismic Design Considerations

From site-specific test boring data, the Site Class was determined from New York State Building Code Section 1613.2.2. The site-specific data used to determine the Site Class typically includes soil test borings to determine Standard Penetration resistances (N-values). Based on estimated average N-values in the upper 100 feet of soil profile, the site can be classified as Site Class C – Very Dense Soil and Soft Rock Profile.

New structures should be designed to resist stress produced by lateral forces computed in accordance with Section 1613 of the New York State Building Code. The values in Table 5 shall be used for this project.

Table 5– Seismic Design Values

| Description | Value |
|--|-----------------|
| Mapped Spectral Response Acceleration for Short Periods, [Fig 1613.2.1 (1)] | $S_S=0.284g$ |
| Mapped Spectral Response Acceleration at 1-Second Period, [Fig 1613.2.1 (2)] | $S_1=0.061g$ |
| Site Coefficient [Table 1613.2.3 (1)] | $F_a= 1.3$ |
| Site Coefficient [Table 1613.2.3 (2)] | $F_v= 1.5$ |
| Max Considered Earthquake Spectral Response for Short Periods [Eq 16-36] | $S_{MS}=0.37g$ |
| Max Considered Earthquake Spectral Response at 1-Second Period [Eq 16-37] | $S_{M1}=0.091g$ |
| Design Spectral Response Acceleration for Short Periods [Eq 16-38] | $S_{DS}=0.246g$ |
| Design Spectral Response Acceleration for 1-Second Period [Eq 16-39] | $S_{D1}=0.061g$ |

We expect that the proposed building will have a Risk Category of II. Based on this assumption, the Seismic Design Category (SDC) is B. The Risk Category and SDC should be verified by the project structural engineer. In the event that the structure has a different Risk

Category, the SDC should be updated in accordance with Section 1613 of the New York State Building Code

Liquefaction Potential

Liquefaction is a phenomenon in which saturated or partially saturated soils lose strength and stiffness when subjected to earthquake-induced ground shaking. Ground shaking of sufficient duration results in the loss of grain-to-grain contact and collapse of the soil skeleton which causes stresses in the soil to be completely transferred to the pore water fluid. Liquefaction is most often observed in saturated, loose sandy soils at depths shallower than 50 feet below the ground surface. Factors known to influence liquefaction potential include composition and thickness of soil layers, grain size, relative density, groundwater level, degree of saturation, and both intensity and duration of ground shaking.

The liquefaction potential was evaluated with the available boring data, including the SPT blow counts, soil classification, total unit weight, soil fines content, and depth to groundwater. We have determined the potential for liquefaction of the non-cohesive soils below the groundwater table and less than 50 feet below the ground surface is considered unlikely. Therefore, a liquefaction evaluation is not required for the site.

6.0 SITE EVALUATION

Our recommendations for the proposed site development including new stormwater management areas, retaining walls, new underground utilities, pavement for new driveways and parking areas, temporary construction excavations, and the suitability of the existing site soils for reuse as structural fill are provided below. A summary of the boring and test pit observations for the site are provided in Table 1 above.

6.1 Stormwater Management Areas

We understand that the planned construction will include new stormwater management areas. During this study, test pits were excavated to determine the subsurface conditions within the proposed stormwater management areas. The locations were determined by the project Site Engineer. The types of systems, planned locations, and invert elevations were not finalized at the time of this report.

Infiltration tests had been planned for select locations, but were eliminated due to shallow bedrock, existing fill, and/or shallow groundwater conditions. The results of the test pit observations are summarized in Table 1 above.

Stormwater management areas should be a minimum of 3 feet above confining layers, seasonal high groundwater, or the existing groundwater table. Should stormwater management areas be planned in other portions of the property, they should be evaluated on a case-by-case basis. The stormwater management systems must be designed in accordance with the applicable New York State Department of Environmental Conservation (NYSDEC) regulations and the New York State Stormwater Management Design Manual (January 2015). The testing requirements for infiltration systems are outlined in Appendix D of the manual.

6.2 New Site Retaining Walls

We understand that site retaining walls will be required to achieve the planned site grades for the parking and roadway area in the northern portion of the site. The type of retaining walls for this project and the final wall heights were unknown at the time of this report. Preliminary design options for this site could include cast-in-place steel reinforced concrete walls, large segmental block gravity walls, or soil/rock nail and shotcrete walls. The following is a preliminary evaluation of the types of retaining wall systems that may be used for this project. This evaluation is meant to give guidance during the design process.

Based on the preliminary grading plan, the two walls will range up to approximately 6 feet and 11 feet in height, respectively. The walls will primarily be “cut walls” where site grades are being lowered in front of the wall. The preliminary boring and test data indicates that the excavations in the retaining wall areas will consist of mostly weathered bedrock with a small amount of overburden soil. Soil/rock nail and shotcrete walls are preferable in this type of “cut wall” condition, but other wall types may also be feasible.

The following evaluation is based on preliminary information that has been provided to our office as of the date of this report. Once the project plans have been further developed, a copy of the plans should be forwarded to our office so that we can review them along with the recommendations in this report. In addition, supplemental borings with rock coring will be required for the retaining wall areas. Further retaining wall recommendations and design parameters will be provided after the project plans are further developed and the supplemental subsurface investigation has been completed.

Soil/Rock Nail and Shotcrete Walls

A soil/rock nail wall is constructed using a top-down construction sequence, where the ground is excavated in stages (or lifts) of limited height. Soil/rock nails and a temporary shotcrete facing shall be installed at each excavation stage to provide temporary stability and protection. Upon completion, a final shotcrete facing shall be constructed over the initial facing to provide structural continuity for the entire wall. The final facing may also include an aesthetic finish if desired. Preliminarily a finished slope of 1.0 horizontal to 4.0 vertical (1H:4V) or flatter can be considered for this project. Additional borings with rock coring will be required to determine the allowable finished slope.

Soil/rock nails typically consist of solid threaded bars with corrosion protection. Nails are typically installed at a horizontal and vertical spacing in the range of 4 to 8 feet. The nail vertical spacing is comparable to the typical height of a stable, excavation lift, which is commonly 3 to 5 feet. Nail inclination is typically 10 to 20 degrees from horizontal.

Where applicable, additional surcharge loads, such as structures, tiered retaining walls, vehicle loads, snow loads, construction equipment, temporary materials storage, etc. are also incorporated into the soil/rock nail and shotcrete wall design.

The soil/rock nail wall design engineer shall prepare a complete wall design (i.e. drawings, specifications, and calculations), which shall be designed and sealed by a Professional Engineer registered in the State of New York and submitted to the Carlin-Simpson & Associates

for review and approval. Carlin-Simpson & Associates can prepare a wall design as an additional service upon request.

Reinforced Concrete Walls and Segmental Block Retaining Walls

A reinforced concrete wall consists of cast-in-place concrete that can be designed as a gravity retaining wall or cantilevered retaining wall. In a gravity wall design, the weight of the concrete alone is used to prevent movement and overturning in the wall. In a cantilevered design, the stem wall is thinner and the base of the wall is wider than that of a gravity wall. However, the cantilevered design utilizes the weight of the soil above the base and steel reinforcing in the concrete to counteract the lateral forces of the retained soil wall.

A segmental block wall, such as Redi-Rock or equivalent, consists of large segmental concrete block units. The wall would be designed as a gravity retaining wall where the weight of the concrete blocks is used to prevent movement and overturning in the wall. Gravity Redi-Rock walls with backslope conditions are typically feasible for retained wall heights up to approximately 9 to 10 feet. In this case, the anticipated maximum retained wall height is 11 feet. Additional borings with rock coring are required to determine the extent and quality of the rock in the wall area and confirm the feasibility for a Redi-Rock retaining wall.

The wall design engineer shall prepare a complete wall design (i.e. drawings, specifications, and calculations), which shall be designed and sealed by a Professional Engineer registered in the State of New York and submitted to Carlin-Simpson & Associates for review. Segmental block retaining walls shall be designed in accordance with the recommendations of the NCMA Design Manual for Segmental Retaining Walls (Current Edition) and in accordance with AASHTO standards. The design shall be completed in accordance with acceptable engineering practice, including the evaluation of sliding, overturning, and bearing, as well as global stability. Where applicable, surcharge loads, such as structures, tiered retaining walls, vehicle loads, snow loads, construction equipment, temporary materials storage, etc. must also be incorporated into the wall design. Carlin-Simpson & Associates can prepare a large segmental block wall design as an additional service upon request.

6.3 Utilities

New utilities may bear in the densified existing fill, virgin site soils, new compacted fill, completely weathered rock, or bedrock. The bottom of all trenches should be excavated clean and shaped so a hard bottom is provided for the pipe support. If any soft or unsuitable soil conditions are encountered during construction, the unsuitable materials must be removed and replaced with new compacted fill.

Trench hammering or blasting may be required to install the new utilities in portions of the site where weathered rock is encountered above the planned utility invert elevation. Where rock is encountered in the utility excavations, it must be removed to at least 6 inches below planned pipe invert. The over-excavated 6 inches shall then be filled with new sandy fill and compacted to at least 92% of its Maximum Modified Dry Density (ASTM D1557) to act as a cushion on the rock.

For areas where existing fill is encountered within the utility excavations, the subgrade at bottom of the utility excavation shall be compacted in place with a vibratory drum trench compactor or “jumping jack” style tamper. Carlin-Simpson & Associates must evaluate these areas for the presence of soft or unsuitable material within the existing fill matrix. If instability is observed, portions of this fill may have to be removed and replaced with new compacted fill. Carlin-Simpson & Associates will determine this during construction.

In the event that the trench bottom becomes soft due to the inflow of surface or trapped water, the soft soil shall be removed and the excavation filled with a minimum of 6 inches of 3/4-inch clean crushed stone to provide a firm base for support of the pipe. Sump pits and pumps should be adequate to keep the excavations dry.

Any utility pipes below the pile-supported portion of the new building should be attached to the structural floor slab with hangers. This is required so that the utilities do not become damaged due to differential settlement. We also recommend that all of the utility pipes that connect to the new structure be designed with flexible connections.

After the utility is installed, the trench must be backfilled with compacted fill. The fill shall consist of suitable on-site soil or imported sand and gravel. Imported fill shall contain less than 20% by weight passing a No. 200 sieve. Large rock fragments and boulders must not be placed directly against the pipe. Controlled compacted fill shall be placed in 12 inch loose layers and each layer shall be compacted to at least 92% of its Maximum Modified Dry Density (ASTM D1557). The backfill must be free of topsoil, debris, and large boulders or rock fragments.

6.4 Pavement

We understand that the proposed construction will also include new paved driveways and parking areas. Based on the preliminary site plan, we expect that cuts up to approximately 10 feet and fills up to approximately 4 feet will be required to achieve the planned subgrade elevations in the new pavement areas. The densified existing fill, virgin soil, completely weathered bedrock, bedrock, and new compacted fill may be used to support the pavement.

To prepare the new pavement areas, the existing surface materials (i.e. topsoil, vegetation, etc.) must be removed from the planned pavement areas. In the proposed pavement areas, the existing structures and debris resulting from the demolition of these structures must be completely removed from the new pavement area, extending at least 5 feet beyond the new paving limits, where practical. After all debris has been removed, the exposed subgrade soil that is either at or below the planned subgrade elevation shall be proofrolled with a large vibratory drum roller (i.e. Dynapac 250 or equivalent) to densify the underlying soils. The on-site representative from Carlin-Simpson & Associates shall witness the proofrolling operation. If any excessive movement is noted during the proofrolling, the soft or unsuitable soil shall be removed and replaced with new compacted fill.

Areas, where existing fill is encountered, it shall be compacted in place. Carlin-Simpson & Associates must evaluate these areas for the presence of soft or unsuitable material within the existing fill matrix. Portions of this fill may have to be removed and replaced with new compacted fill. Carlin-Simpson & Associates will determine this during construction.

Where new fill is required to achieve final grades, it shall consist of either suitable on-site soil or imported sand and gravel. Imported sand and gravel shall contain less than 20% by weight passing a No. 200 sieve. New fill shall be placed in layers not exceeding 12 inches in loose thickness and each layer shall be compacted to at least 92% of its Maximum Modified Dry Density (ASTM D1557).

After the planned subgrade has been proofrolled and new compacted fill has been placed as required, the new pavement subbase may be placed on the existing site soils, bedrock, and new compacted fill. A layer of densely graded aggregate (DGA) is recommended as a subbase layer for drainage and additional pavement support. See the recommended thicknesses for the pavement sections below.

Where rock is encountered at the subgrade elevation in the cut areas, the subgrade stone should be increased to a depth of 12-inches. In addition, to provide additional drainage, finger drains extending from the catch basins, may be required. This must be evaluated by Carlin-Simpson & Associates at the time of construction. A typical finger drain section consists of an 18 to 24 inch wide trench excavated 12 to 18 inches below the subgrade surface. Each drain should extend 20 to 30 feet from the catch basin and should be sloped toward the catch basin. Geotextile non-woven filter fabric (i.e. Mirafi 140N or equivalent) is placed on the subgrade and up the sidewalls of the excavation, completely lining the excavation. After the trench has been lined with filter fabric, a 4-inch diameter, rigid wall perforated PVC drainpipe is installed and the trench is backfilled with 3/4-inch clean crushed stone. Once the trench is backfilled to the subgrade elevation, the filter fabric is wrapped over the clean crushed stone. The asphalt pavement section is then installed directly over the filter fabric.

We recommend that the following pavement sections be used for the parking lots and driveways. These pavement sections are subject to local government approval.

Light Duty Areas – Parking Areas

| | | |
|------|--|-----------------|
| 1 ½" | Asphalt Top Course | NYSDOT, Type 6F |
| 2 ½" | Asphalt Base Course | NYSDOT, Type 3 |
| 6" | Stone Subbase (DGA) | NYSDOT, Type 1 |
| | Approved Compacted Subgrade (Minimum CBR = 10) | |

Heavy Duty Areas – Driveways

| | | |
|----|--|-----------------|
| 2" | Asphalt Top Course | NYSDOT, Type 6F |
| 3" | Asphalt Base Course | NYSDOT, Type 3 |
| 8" | Stone Subbase (DGA) | NYSDOT, Type 1 |
| | Approved Compacted Subgrade (Minimum CBR = 10) | |

Based on the boring and test pit data, we anticipate that the densified existing site soils, weathered bedrock, and new compacted fill will provide a CBR value that is equal to or greater than 10, which can adequately support the above pavement sections.

6.5 Temporary Construction Excavations and Excavation Protection

Temporary construction excavations shall be conducted in accordance with the most recent OSHA guidelines or applicable federal, state or local codes. A qualified person should evaluate the excavations at the time of construction to determine the appropriate soil or rock type and the allowable slope configuration. Based on the boring data, we believe the site soil and bedrock would have the following classifications as defined by the OSHA guidelines.

| <u>Soil/ Rock Type</u> | <u>Possible Classification</u> | <u>Maximum Slope or Bench</u> |
|------------------------|--------------------------------|-------------------------------|
| Existing Fill | “C” | 1½H:1V |
| Virgin Soil | “B” or “C” | 1H:1V or 1½H:1V |
| Weathered Rock | “B” | 1H:1V |
| Intact Bedrock | “A” | 3/4H:1V |

Temporary support (i.e. trench boxes, sheeting and shoring, etc.) should be used for any excavation that cannot be sloped or benched in accordance with the applicable regulations, where necessary to protect adjacent property, utilities, driveways, and/or structures, or where saturated soils or water seepage is encountered within the excavation. In the event that water is encountered within the excavation, an evaluation of the excavation’s stability must be performed. Perched water or groundwater encountered within the excavation will destabilize the sides of the excavation. Temporary support will be required to stabilize the excavation. Dewatering of the excavation will also be required.

A New York State licensed professional engineer must design all temporary and permanent support systems. The contractor will select the shoring type and submit design calculations for the proposed shoring method to Carlin-Simpson & Associates for review.

The soil adjacent to the temporary support system will exert a horizontal pressure against the system. This pressure is based on the soil unit weight, coefficient of active earth pressure, and depth of the excavation. In addition, the surcharge loads from adjacent driveways, construction equipment, or stored materials near the excavation must be incorporated into the design of the support system, as applicable. The design parameters for temporary excavation support systems are listed in Table 6 below.

Table 6 – Temporary Sheet piling and Shoring Design Parameters

| Description | Soil | Highly Weathered Rock |
|---|-------------|------------------------------|
| Moist Unit Weight (pcf) | 130 | 140 |
| Friction Angle (ϕ , deg) | 30 | 36-38 |
| Cohesion (c, psf) | 0 | 0 |
| Active Earth Pressure Coefficient (k_a) ¹ | 0.33 | 0.26-0.24 |
| Equivalent Fluid Pressure (pcf) | 42.9 | 36.4-33.6 |
| Passive Earth Pressure Coefficient (k_p) ¹ | 3.0 | 3.9-4.2 |

6.6 Suitability of the In-Situ Soil and Rock for Use as Compacted Fill

The suitability of each stratum for use as compacted fill is discussed below.

- Stratum 1A**
Topsoil
Topsoil is not suitable for use as compacted fill. During construction, it shall be stripped from the construction areas. The topsoil may be reused in non-structural, non-sloped landscape areas or be hauled offsite.
- Stratum 1B**
Asphalt
Asphalt is not suitable for use as compacted fill in the proposed building area. However, the existing asphalt pavement may be reused as subgrade material and mixed with soil for use in the parking lot and driveway areas. The asphalt should be stripped from the work area and stockpiled if to be reused or hauled off site for disposal. Prior to using the asphalt for compacted fill, the material shall be crushed into pieces smaller than 4 inches and mixed with soil.
- Stratum 2**
Existing Fill
The existing fill generally consists of brown, gray, black coarse to fine Sand, trace (to some) Silt, trace (to some) coarse to fine Gravel, with varying amounts of cobbles, boulders, organic material, and debris. The organic material and debris consisted of roots, buried topsoil, plastic, wood, concrete, brick, and asphalt. The existing fill will only be suitable for reuse if it remains relatively dry for optimum compaction and all of the debris and organic material is removed prior to reuse as compacted fill.
- Stratum 3**
Sand, Silty Sand, or Sandy Gravel
The virgin soil consists of brown, gray coarse to fine SAND, trace (to and) Silt, trace (to and) coarse to fine Gravel or coarse to fine GRAVEL some (to and), coarse to fine Sand, trace Silt. Many cobbles and boulders were encountered in this stratum. This stratum is generally suitable for reuse as compacted fill, provided that it remains relatively dry for optimum compaction. See below for requirements for reuse of cobbles and boulders.
- Stratum 4**
Clayey Silt
In select areas of the site, the virgin soil consists of brown, gray or mottled red brown, brown, gray Clayey SILT, trace coarse to fine Sand. This stratum has a high percentage of silt and will be very moisture sensitive. If the soil becomes too wet, it will be difficult to achieve adequate compaction. In the event that this material is encountered within the site excavations, it will only be suitable for reuse as compacted fill if it remains relatively dry for optimum compaction prior to its use.
- Stratum 5**
Weathered Bedrock
Excavated rock may be used as fill material provided that the material is well graded and has been approved prior to use by Carlin-Simpson & Associates.
- All rock fill (including large cobbles and boulders) must be well blended with smaller rock fragments and/or soil. Gradation limits (i.e. maximum particle size for rock placed) will depend on the location of placement as shown in Table 7 below. Excavated rock (and boulders) that are too large for use as structural fill should be processed through a crusher to provide suitable fill material.

Rock fill shall be placed in maximum 12 inch thick layers and compacted with multiple passes of a large vibratory roller to a firm and non-yielding state as determined by the on-site representative from Carlin-Simpson & Associates. Rock fill should not be used where it will interfere with the installation of foundations, pile foundations, or utilities. Also, it shall not be used as backfill directly against concrete walls or utilities.

The boring and test pit data indicates that the on-site soils contain a varying percentage of silt (5% to >50%). The higher silt content soils will be moisture sensitive. If the soil becomes too wet, it will be difficult to achieve adequate compaction. In addition, the site soils that extend below the groundwater table are completely saturated and therefore, unsuitable for reuse.

Proper moisture conditioning of the soil will be required. New compacted fill should be within 2% (+/-) of its optimum moisture content at the time of placement. In the event that the on-site material is too wet at the time of placement and cannot be adequately compacted, the soil should be aerated and allowed to dry or the material removed and a drier cleaner fill material used. In the event that the on-site material is too dry at the time of placement and cannot be adequately compacted, water may be needed to increase the soil moisture content for proper compaction.

The in-situ soils which exist throughout the site may become soft and weave if exposed to excessive moisture and construction traffic. The instability will occur quickly when exposed to these elements and it will be difficult to stabilize the subgrade. We recommend that adequate site drainage be implemented early in the construction schedule and if the subgrade becomes wet, the contractor should limit construction activity until the soil has dried.

Excavated boulders, weathered rock, and rock may be used as fill material in designated areas, provided that the material conforms to the required gradation, is well graded, and has been approved prior to use by Carlin-Simpson & Associates. All rock fill must be well blended with smaller rock fragments and/or soil. The recommended maximum particle size for rock placed as fill is shown in Table 7 below. Excavated rock, too large for use as structural fill, should be processed through a crusher to provide suitable fill material.

Table 7 – Rock Fill Gradation Limitations

| Location | | Maximum Particle Size |
|--|--|------------------------------|
| Building Area | Within 2 feet of Finished Floor | 3 inches |
| | More than 2 feet below Finished Floor | 6 inches |
| | More than 6 feet below Finished Floor | 12 inches |
| Outside Building Area (i.e. Pavement and Sidewalk Areas) | Within 18 inches of Finished Grade | 3 inches |
| | More than 18 inches below Finished Grade | 6 inches |
| | More than 3 feet below Finished Grade | 12 inches |

The minimum compaction requirements for the various areas of the site are summarized in Table 8 below.

Table 8 – Minimum Compaction Requirements

| Area | Maximum Modified Dry Density (ASTM D1557) |
|------------------------------------|--|
| Below Foundations | 95% |
| Below Floor Slabs | 92% |
| Retaining Wall Subgrade | 95% |
| Retaining Wall Backfill | 92% |
| Pavement Areas | 92% |
| Exterior Slabs and Sidewalks | 92% |
| Utility Trenches | 92% |
| Landscape Areas (Non-Sloped Areas) | 90% |

Debris Fill and Potential Environmental Concerns

Debris was encountered within the existing fill stratum during this subsurface investigation. In the event that the debris fill is encountered in any of the site excavations, the excavated material will generally not be suitable for reuse as compacted fill unless the debris can be sufficiently separated and removed from the soil fill. The possibility of not being able to reuse all of the excavated existing fill material should be taken into consideration by the project team. This should also be included in the project specifications.

In the event that the debris fill material needs to be hauled off site, environmental testing will likely be required to export the debris fill material. An environmental evaluation of the site was beyond the scope of this study. Proper disposal of all soil must be performed in accordance with applicable federal and state regulations. An environmental engineering firm should be retained by the owner to address these potential issues. The possibility of having to haul off materials should be taken into consideration by the project team.

Additional Subsurface Investigation

As discussed above, additional testing is required to complete the recommendations in this report. The borings will be performed for the building, retaining walls, and large cut areas. We also recommend that rock coring be performed at select boring locations to understand the quality of bedrock across the site. One or two monitoring wells may also be installed in the cut areas to better assess the expected groundwater conditions. The additional borings will aid in determining the following: 1) depth and extent of existing fill within the building area; 2) extent of bedrock at the foundation bearing elevation; 3) depth to bedrock and quality of rock in cut areas; 4) determining an appropriate retaining wall system and design parameters; and 5) determining if sub-slab drainage is needed for the building.

7.0 GENERAL

The findings, conclusions and recommendations presented in this report represent our professional opinions concerning subsurface conditions at the site. The opinions presented are relative to the dates of our site work and should not be relied on to represent conditions at later dates or at locations not explored. The opinions included herein are based on information

provided to us, the data obtained at specific locations during the study and our past experience. If additional information becomes available that might impact our geotechnical opinions, it will be necessary for Carlin-Simpson & Associates to review the information, reassess the potential concerns, and re-evaluate our conclusions and recommendations.

Regardless of the thoroughness of a geotechnical exploration, there is the possibility that conditions between borings and test pits will differ from those encountered at specific boring or test pit locations, that conditions are not as anticipated by the designers and/or the contractors, or that either natural events or the construction process have altered the subsurface conditions. These variations are an inherent risk associated with subsurface conditions in this region and the approximate methods used to obtain the data. These variations may not be apparent until construction.

The professional opinions presented in this geotechnical report are not final. Field observations and foundation installation monitoring by the geotechnical engineer, as well as soil density testing and other quality assurance functions associated with site earthwork and foundation construction, are an extension of this report. Therefore, Carlin-Simpson & Associates should be retained by the owner to observe all earthwork and foundation construction, to document that the conditions anticipated in this study actually exist, and to finalize or amend our conclusions and recommendations. Carlin-Simpson & Associates is not responsible or liable for the conclusions and recommendations presented in this report if Carlin-Simpson & Associates does not perform the observation and testing services.

Therefore, in order to preserve continuity in this project, the owner shall retain the services of Carlin-Simpson & Associates to provide full time geotechnical related monitoring and testing during construction. At a minimum, this shall include the observation and testing of the following: 1) the removal of existing fill and unsuitable soil, where required; 2) the proofrolling of the subgrade soil prior to the placement of new compacted fill; 3) the placement and compaction of controlled fill; 4) the installation of pile foundations; 5) the excavation for new foundations bearing on rock; 6) the construction of retaining walls, soil slopes, and rock slopes; and 7) the preparation of the subgrade for the floor slab and pavement areas.

This report has been prepared in accordance with generally accepted geotechnical engineering practice. No other warranty is expressed or implied. The evaluations and recommendations presented in this report are based on the available project information, as well as on the results of the exploration. Carlin-Simpson & Associates should be given the opportunity to review the final drawings and site plans for this project to determine if changes to the recommendations outlined in this report are needed. Should the nature of the project change, these recommendations should be re-evaluated.

This report is provided for the exclusive use of AMS Acquisitions and the project specific design team and may not be used or relied upon in connection with other projects or by other third parties. Carlin-Simpson & Associates disclaims liability for any such third-party use or reliance without express written permission. Use of this report or the findings, conclusions or recommendations by others will be at the sole risk of the user. Carlin-Simpson & Associates is not responsible or liable for the interpretation by others of the data in this report, nor their conclusions, recommendations or opinions.

If the conditions encountered during construction vary significantly from those stated in this report, this office should be notified immediately so that additional recommendations can be made.

Thank you for allowing us to assist you with this project. Should you have any questions or comments, please contact this office.

Very truly yours,

CARLIN-SIMPSON & ASSOCIATES, LLC



MEREDITH R. ANKE, P.E.
Senior Project Engineer



ROBERT B. SIMPSON, P.E.
Principal



File No. 23-34

| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | | BORING NUMBER B-1 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|------|-------------------|---|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | | SHEET NO.: 1 of 1 | | |
| Client: AMS Acquisitions | | | | | | | | JOB NUMBER: 23-34 | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | | ELEVATION: +70.0 | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 5/Jul/23 | |
| No groundwater encountered | | | | DIA. | 3 1/4" | 1 3/8" | | | FINISH DATE: 5/Jul/23 | |
| | | | | WGHT | | 140# | | | DRILLER: Collin | |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS | |
| 1 | | S-1 | 3 | | <u>Dark brown topsoil</u> 0'3" | | | | Rec = 16" moist | |
| | | | 4 | | FILL (Br cf S, l \$, t mf G) | | | | | |
| 2 | | | 5 | | <u>FILL (Brown coarse to fine SAND, little Silt, trace medium to fine Gravel)</u> | | | | Rec = 8" moist | |
| | | | 4 | | | | | | | |
| 3 | | S-2 | 6 | | FILL (same, l mf G, w/ fine roots) | | | | | |
| | | | 17 | | | | | | | |
| 4 | | | 26 | | 4'0" | | | | | |
| | | | 50/1" | | <u>End of Boring @ 4'0"</u> | | | | Auger refusal 4'0" Moved hole 5' east Auger refusal 3'9" on probable bedrock | |
| 5 | | | | | | | | | | |
| 6 | | | | | | | | | | |
| 7 | | | | | | | | | | |
| 8 | | | | | | | | | | |
| 9 | | | | | | | | | | |
| 10 | | | | | | | | | | |
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| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | | BORING NUMBER B-2 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|------|-----------------------|---|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | | SHEET NO.: 1 of 1 | | |
| Client: AMS Acquisitions | | | | | | | | JOB NUMBER: 23-34 | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | | ELEVATION: +78.0 | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | START DATE: 5/Jul/23 | | |
| 5/Jul/23 | | 7'0" | Open | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 5/Jul/23 | | |
| | | | | WGHT | | 140# | | DRILLER: Collin | | |
| | | | | FALL | | 30" | | INSPECTOR: Mike C | | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS | |
| | | | 6 | | Black topsoil | | | | 0'3" | |
| 1 | | S-1 | 9 | | FILL (Br cf S, l (-) \$, a cf G, w/many cobbles, boulders) | | | | Rec = 11" moist | |
| | | | 24 | | | | | | Boulder @ 1'0" | |
| 2 | | | 17 | | | | | | Auger refusal 2'0", moved hole 2' north | |
| 3 | | | | | | | | | Concrete @ 4'0" | |
| | | | 5 | | FILL (same, s \$, w/roots, topsoil) | | | | Rec = 12" moist | |
| 4 | | S-2 | 10 | | | | | | | |
| | | | 29 | | FILL (Brown coarse to fine SAND, little Silt, and coarse to fine Gravel, with cobbles, boulders, debris, roots, topsoil) | | | | | |
| 5 | | | 26 | | | | | | | |
| | | | 5 | | | | | | | |
| 6 | | S-3 | 4 | | FILL (same, br, g w/concrete, plastic, fine roots, mixed topsoil) | | | | Rec = 9" moist | |
| | | | 4 | | | | | | | |
| 7 | | | 11 | | | | | | | |
| | | | 11 | | | | | | | |
| 8 | | S-4 | 12 | | FILL (Dk gr, br \$ s (+), cf S, t f G, w/concrete, wood, fine roots) | | | | Rec = 8" moist to wet | |
| | | | 25 | | | | | | | |
| 9 | | | 13 | | | | | | 9'0" | |
| | | | | | End of Boring @ 9'0" | | | | | |
| 10 | | | | | | | | | Auger refusal 8'0" on boulder | |
| 11 | | | | | | | | | move hole 5' north. Start mud rotary, lost water in existing fill. Could not continue mud rotary. Abandoned boring. | |
| 12 | | | | | | | | | | |
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| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-3 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|-------------------|--|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | SHEET NO.: 1 of 1 | | |
| Client: AMS Acquisitions | | | | | | | JOB NUMBER: 23-34 | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | ELEVATION: +81.0 | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | START DATE: 5/Jul/23 | |
| No groundwater encountered | | | | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 5/Jul/23 | |
| | | | | WGHT | | 140# | | DRILLER: Collin | |
| | | | | FALL | | 30" | | INSPECTOR: Mike C | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | REMARKS | |
| 1 | | S-1 | 2 | | <u>Black topsoil</u> | | | 0'5" | |
| | | | 6 | | <u>FILL (Gray coarse to fine GRAVEL and, coarse to fine Sand, little (-) Silt)</u> | | | 1'6" | |
| 2 | | | 12 | | Gr cf G a, cf S, t \$, w/many cobbles, boulders | | | Rec = 7" moist | |
| | | | 9 | | | | | | |
| 3 | | S-2 | 12 | | | | | Rec = 7" moist | |
| | | | 32 | | | | | | |
| 4 | | | 43 | | <u>Gray coarse to fine GRAVEL and, coarse to fine Sand, trace Silt, with many cobbles, boulders</u> | | | Auger refusal 5'0" possible boulder, moved hole 5' north | |
| | | | 14/3" | | | | | Rec = 8" moist | |
| 5 | | S-3 | 18 | | same, highly fractured bedrock | | | 5'3" | |
| | | | 27 | | | | | | |
| | | | 30/3" | | | | | | |
| 6 | | | | | <u>End of Boring @5'3"</u> | | | Spoon bouncing on possible bedrock 5'3" | |
| 7 | | | | | | | | Auger refusal 5'3" on probable bedrock | |
| 8 | | | | | | | | | |
| 9 | | | | | | | | | |
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| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-4 | |
|--|-----------------------|---------------|------------------------------|-----------------|--|-------------------|--------|----------------------|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | SHEET NO.: 1 of 1 | | | |
| Client: AMS Acquisitions | | | | | | JOB NUMBER: 23-34 | | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | ELEVATION: +79.0 | | | |
| GROUNDWATER | | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 6/Jul/23 |
| No groundwater encountered | | | | | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 6/Jul/23 |
| | | | | WGHT | | 140# | | | DRILLER: Collin |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS |
| 1 | | S-1 | 4 | | Black Asphalt 0'3" | | | | Rec = 8" moist |
| | | | 12 | | FILL (Lt br gr cf S, t \$, l (-) mf G, shattered boulder) | | | | |
| 2 | | | 20 | | FILL (Light brown, gray coarse to fine SAND, trace Silt, little (-) medium to fine Gravel, shattered boulder) | | | | Rec = 3" moist Auger refusal 4'0", moved 3' N Auger refusal 2'0", moved 8' S Auger refusal 2'6" on possible bedrock |
| | | | 8 | | | | | | |
| 3 | | S-2 | 10 | | FILL (Br cf S, l (-) \$, a cf G) | | | | |
| | | | 7 | | | | | | |
| 4 | | | 15/1" | | 3'7" | | | | |
| 5 | | | | | End of Boring @ 3'7" | | | | |
| 6 | | | | | | | | | |
| 7 | | | | | | | | | |
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| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-5 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|-------------------|--------|----------------------|---|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | SHEET NO.: 1 of 1 | | | |
| Client: AMS Acquisitions | | | | | | JOB NUMBER: 23-34 | | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | ELEVATION: +79.5 | | | |
| GROUNDWATER | | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 6/Jul/23 |
| No groundwater encountered | | | | | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 6/Jul/23 |
| | | | | WGHT | | 140# | | | DRILLER: Collin |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS |
| | | | 5 | | Black Asphalt 0'2" | | | | |
| 1 | | S-1 | 15 | | FILL (Lt br cf S, l (+) \$, a cf G, boulder) | | | | Rec = 6" moist |
| | | | 15 | | | | | | Boulders @ 2'0" |
| 2 | | | 9 | | | | | | |
| | | | 7 | | | | | | |
| 3 | | S-2 | 4 | | FILL (Dk br cf S, s (-) \$, l mf G, w/some roots) | | | | Rec = 7" moist |
| | | | 4 | | FILL (Brown coarse to fine SAND, little (+) Silt, and coarse to fine Gravel, boulder, roots) | | | | Auger breakthrough 4' |
| 4 | | | 3 | | | | | | |
| 5 | | | | | | | | | |
| | | | 1 | | FILL (same, s \$, t (+) mf G, w/some roots) 5'6" | | | | |
| 6 | | S-3 | 1 | | Lt br cf S, a \$, t (-) mf G | | | | Rec = 18" moist |
| | | | 15 | | Light brown coarse to fine SAND, and Silt, trace (-) medium to fine Gravel 6'8" | | | | |
| 7 | | | 10/0" | | End of Boring @ 6'8" | | | | Auger refusal 6'8" on probable bedrock |
| 8 | | | | | | | | | |
| 9 | | | | | | | | | |
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| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-6 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|-------------------|----------------------|---|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | SHEET NO.: 1 of 1 | | |
| Client: AMS Acquisitions | | | | | | | JOB NUMBER: 23-34 | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | ELEVATION: +78.5 | | |
| GROUNDWATER | | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 6/Jul/23 |
| No groundwater encountered | | | | | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 6/Jul/23 |
| | | | | WGHT | | 140# | | | DRILLER: Collin |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS |
| 1 | | S-1 | 27 | | <u>Black topsoil</u> 0'4" | | | | Rec = 12" Refusal 0'7", moved hole 3' west Auger refusal 2'2" Auger refusal 2'5" on probable bedrock |
| 2 | | | 15 | | <u>Light brown, gray coarse to fine SAND, little Silt, a coarse to fine Gravel, with rock fragments</u> | | | | |
| 3 | | S-2 | 23/5"10/0" | same | 2'5" | | | | |
| 4 | | | | | <u>End of Boring @ 2'5"</u> | | | | |
| 5 | | | | | | | | | |
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| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-7 | |
|--|-----------------------|---------------|------------------------------|-----------------|--|--------|-------------------|----------------------|---|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | SHEET NO.: 1 of 2 | | |
| Client: AMS Acquisitions | | | | | | | JOB NUMBER: 23-34 | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | ELEVATION: +80.0 | | |
| GROUNDWATER | | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 6/Jul/23 |
| No groundwater encountered | | | | | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 6/Jul/23 |
| | | | | WGHT | | 140# | | | DRILLER: Collin |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS |
| 1 | | S-1 | 9 | | Black topsoil | | | | 0'3" |
| 2 | | | 7 | | Gray coarse to fine SAND, trace Silt, some (+) coarse to fine Gravel, with rock fragments. | | | | 1'2" |
| 3 | | | 8/0" | | <u>End of Boring @ 1'2"</u> | | | | Rec = 7" moist |
| 4 | | | | | | | | | Auger refusal 1'0", moved 3' south, auger refusal 0'10", moved 3' west, |
| 5 | | | | | | | | | Auger refusal 1'2" on probable bedrock |
| 6 | | | | | | | | | |
| 7 | | | | | | | | | |
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| CARLIN - SIMPSON & ASSOCIATES Sayreville, N.J. | | | | TEST BORING LOG | | | | BORING NUMBER B-8 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|---|------|----------------------|-----------------------|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | SHEET NO.: | | 1 of 2 | | | |
| Client: AMS Acquisitions | | | | JOB NUMBER: | | 23-34 | | | |
| Drilling Contractor: Environmental Technical Drilling | | | | ELEVATION: | | +79.0 | | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 6/Jul/23 |
| 6/Jul/23 | | 14'0" | | DIA. | 3 1/4" | 1 3/8" | | | FINISH DATE: 7/Jul/23 |
| | | | | WGHT | | 140# | | | DRILLER: Collin |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS |
| 1 | | S-1 | 5 | | | | | | Layer of rip rap |
| | | | 4 | | Black asphalt | | | 0'8" | |
| 2 | | S-2 | 6 | | FILL (Dk br cf S, l \$, s cf G) | | | | Rec = 10" moist |
| | | | 4 | | | | | | |
| 3 | | S-3 | 4 | | FILL (same, l (+) \$) | | | | Rec = 2" moist |
| | | | 7 | | FILL (Dark brown coarse to fine SAND, little Silt, some coarse to fine Gravel) | | | | |
| 4 | | S-4 | 8 | | | | | | |
| | | | 6 | | | | | | |
| 5 | | S-5 | 5 | | | | | | Rec = 6" moist |
| | | | 6 | | | | | 5'6" | |
| 6 | | S-6 | 9 | | Lt br cf S, s (+) \$, s cf G | | | | |
| | | | 9 | | same | Light brown coarse to fine SAND, some (+) Silt, some coarse to fine Gravel | | | |
| 7 | | S-7 | 10 | | | | | | Rec = 2" moist |
| | | | 9 | | | | | 8'0" | |
| 8 | | S-8 | 10 | | | | | | |
| | | | 12 | | | | | | |
| 9 | | S-9 | 14 | | Lt br, gr Cy \$ | | | | Rec = 24" moist |
| | | | 13 | | | | | | |
| 10 | | S-10 | 13 | | | | | | |
| | | | 7 | | | | | | |
| 11 | | S-11 | 11 | | same | | | | Rec = 10" moist |
| | | | 12 | | | | | | |
| 12 | | S-12 | 11 | | | | | | |
| | | | 8 | | | | | | |
| 13 | | S-13 | 10 | | same | | | | Rec = 24" moist |
| | | | 12 | | | | | | |
| 14 | | S-14 | 13 | | Light brown, gray Clayey SILT | | | | |
| | | | 12 | | | | | | |
| 15 | | S-15 | 11 | | same | | | | Rec = 24" wet |
| | | | 11 | | | | | | |
| 16 | | S-16 | 20 | | | | | | |
| | | | 7 | | | | | | |
| 17 | | S-17 | 9 | | same, gr | | | | Rec = 24" wet |
| | | | 10 | | | | | | |
| 18 | | S-18 | 10 | | | | | | |
| | | | 4 | | | | | | |
| 19 | | S-19 | 5 | | same | | | | Rec = 24" wet |
| | | | 6 | | | | | | |
| 20 | | S-20 | 6 | | | | | | |
| | | | 3 | | | | | | |
| 21 | | S-21 | 2 | | same | | | | Rec = 7" wet |
| | | | 3 | | | | | | |
| 22 | | S-22 | 3 | | | | | | |

| CARLIN - SIMPSON & ASSOCIATES Sayreville, N.J. | | TEST BORING LOG | | BORING NUMBER B-8 | | |
|--|-----------------------|-----------------|------------------------------|----------------------|--------------------------------------|------------------|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | SHEET NO.: 2 of 2 | | |
| Client: AMS Acquisitions | | | | JOB NUMBER: 23-34 | | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | Soil | IDENTIFICATION | REMARKS |
| 23 | | S-12 | 4 | | Lt br, gr Cy \$ | Rec = 24" wet |
| | | | 5 | | | |
| 24 | | | 6 | | <u>Light brown, gray Clayey SILT</u> | Rec = 20" wet |
| | | | 5 | | | |
| 25 | | S-13 | 3 | same | | |
| | | | 4 | | | |
| 26 | | | 4 | | same | Rec = 24" wet |
| | | | 5 | | | |
| 27 | | S-14 | 4 | | | |
| | | | 5 | | | |
| 28 | | | 5 | | | |
| 29 | | | | | | 29'0" |
| 30 | | | | | <u>End of Boring @ 29'0"</u> | |
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| CARLIN - SIMPSON & ASSOCIATES Sayreville, N.J. | | | | TEST BORING LOG | | | | BORING NUMBER B-9 | |
|--|-----------------------|---------------|------------------------------|--|--------|--------|------|----------------------|-----------------------|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | SHEET NO.: 1 of 1 | | | | JOB NUMBER: 23-34 | |
| Client: AMS Acquisitions | | | | ELEVATION: +88.0 | | | | DATUM: Topo | |
| Drilling Contractor: Environmental Technical Drilling | | | | GROUNDWATER | | | | START DATE: 7/Jul/23 | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | CORE | TUBE | FINISH DATE: 7/Jul/23 |
| No Water Reading | | | | DIA. | 3 1/4" | 1 3/8" | | | DRILLER: Collin |
| | | | | WGHT | | 140# | | | INSPECTOR: Mike C |
| | | | | FALL | | 30" | | | |
| Depth (ft.) | Casing Blows pre Foot | Sample Number | Blows on Sample Spoon per 6" | IDENTIFICATION | | | | REMARKS | |
| 1 | | S-1 | 3 | <u>Black asphalt</u> | | | | 0'2" Rec = 4" | |
| | | | 4 | <u>Orange brown coarse to fine SAND, and Silt, little medium to fine Gravel</u> | | | | 1'0" moist | |
| 2 | Run #1 | | 10/2" | | | | | Run #1 1'0"-2'6" | |
| 3 | | | | | | | | Run = 18" | |
| 4 | Run #2 | | | <u>Gray Gneiss or Norite, massive moderately jointed, slightly to moderately weathered</u> | | | | Rec = 18" = 100% | |
| 5 | | | | | | | | RQD = 39% | |
| 6 | | | | | | | | Run #2 2'6"-6'0" | |
| | | | | | | | | Run = 42" | |
| | | | | | | | | Rec = 40" = 95% | |
| | | | | | | | | 6'0" RQD = 70% | |
| 7 | | | | <u>End of Boring @ 6'0"</u> | | | | | |
| 8 | | | | | | | | | |
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| 18 | | | | | | | | | |
| 19 | | | | | | | | | |
| 20 | | | | | | | | | |
| 21 | | | | | | | | | |
| 22 | | | | | | | | | |

| CARLIN - SIMPSON & ASSOCIATES Sayreville, N.J. | | | | TEST BORING LOG | | | | BORING NUMBER B-10 | | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|------|---|-----------|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | SHEET NO.: | | 1 of 2 | | | | |
| Client: AMS Acquisitions | | | | JOB NUMBER: | | 23-34 | | | | |
| Drilling Contractor: Environmental Technical Drilling | | | | ELEVATION: | | +78.5 | | | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | START DATE: | 10/Jul/23 | |
| 11/Jul/23 | | 3'0" | | DIA. | 3 1/4" | 1 3/4" | | FINISH DATE: | 11/Jul/23 | |
| | | | | WGHT | | 140# | | DRILLER: | Collin | |
| | | | | FALL | | 30" | | INSPECTOR: | Mike C | |
| Depth (ft.) | Casing Blows pre Foot | Sample Number | Blows on Sample Spoon per 6" | S Y M | IDENTIFICATION | | | REMARKS | | |
| 1 | | S-1 | 8 | | Black topsoil | | | 0'3" | | |
| | | | 11 | | FILL (Br cf S, t (+) \$, s cf G, w/rk frg) | | | Rec = 9" moist | | |
| | | | 10 | | | | | | | |
| 2 | | | 5 | | | | | | | |
| | | | 6 | | | | | | | |
| 3 | | S-2 | 8 | | FILL (same, l \$, a cf G) | | | Rec = 8" wet | | |
| | | | 15 | | | | | | | |
| 4 | | | 20 | | <u>FILL (Brown coarse to fine SAND, little Silt, some coarse to fine Gravel, with rock fragments, asphalt)</u> | | | | | |
| 5 | | | | | | | | | | |
| | | | 19 | | | | | | | |
| 6 | | S-3 | 22 | | FILL (same, bk cf S, l (-) \$, a cf G, w/asphalt) | | | Rec = 13" wet | | |
| | | | 13 | | | | | | | |
| 7 | | | 8 | | | | | | | |
| | | | 7 | | | | | | | |
| 8 | | S-4 | 3 | | FILL (Gr, br cf S, a \$, l cf G) | | | Rec = 20" wet | | |
| | | | 6 | | | | | | | |
| 9 | | | 45/4" | | | | | | | |
| 10 | | | | | | | | 10'0" | | |
| 11 | | | | | | | | | | |
| 12 | | Run #1 | | | <u>FILL (Boulders)</u> | | | | | |
| 13 | | | | | | | | | | |
| 14 | | | | | | | | | | |
| 15 | | | | | | | | 15'0" | | |
| 16 | | S-5 | 45 | | FILL (Dk br, gr cf S, a \$, l mf G) | | | Rec = 8" wet | | |
| | | | 38/4" | | | | | | | |
| 17 | | | | | <u>FILL (Dark brown, gray coarse to fine SAND, and Silt, little medium to fine Gravel)</u> | | | Pea gravel in tip of spoon Refusal on boulders | | |
| 18 | | | | | | | | | | |
| 19 | | | | | | | | 19'0" | | |
| 20 | | S-6 | 5/0" | | | | | Rec = 5" bouncing refusal | | |
| | | Run #2 | | | <u>FILL (Boulders)</u> | | | | | |
| 21 | | | | | | | | | | |
| 22 | | | | | | | | | | |

| | |
|--|-------------------|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | SHEET NO.: 2 of 2 |
| Client: AMS Acquisitions | JOB NUMBER: 23-34 |

| Depth (ft.) | Casing Blows pre Foot | Sample Number | Blows on Sample Spoon per 6" | Sym | IDENTIFICATION | REMARKS |
|-------------|-----------------------|---------------|------------------------------|-----|-------------------------------------|---|
| 23 | | | | | | |
| 24 | | | | | | |
| 25 | | Run #3 | | | <u>FILL (Boulders)</u> | |
| 26 | | | | | | |
| 27 | | | | | 27'0" | Rollerbit to 27'0" encountered additional boulders. |
| 28 | | | | | <u>End of Boring @ 27'0"</u> | Abandoned boring. |
| 29 | | | | | | |
| 30 | | | | | | |
| 31 | | | | | | |
| 32 | | | | | | |
| 33 | | | | | | |
| 34 | | | | | | |
| 35 | | | | | | |
| 36 | | | | | | |
| 37 | | | | | | |
| 38 | | | | | | |
| 39 | | | | | | |
| 40 | | | | | | |
| 41 | | | | | | |
| 42 | | | | | | |
| 43 | | | | | | |
| 44 | | | | | | |
| 45 | | | | | | |
| 46 | | | | | | |
| 47 | | | | | | |

| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-11 | | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|-------------------|-----------------------|--|------------------------|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | SHEET NO.: 1 of 1 | | | |
| Client: AMS Acquisitions | | | | | | | JOB NUMBER: 23-34 | | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | ELEVATION: +79.0 | | | |
| GROUNDWATER | | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 12/Jul/23 | |
| No groundwater encountered | | | | | DIA. | 3 1/4" | 1 3/8" | | | FINISH DATE: 12/Jul/23 |
| | | | | WGHT | | 140# | | | DRILLER: Collin | |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | | REMARKS | |
| 1 | | S-1 | 4 | | <u>Black topsoil</u> 0'2" | | | | Rec = 12" moist Spoon refusal 1'9" moved NW 3' Auger refusal 1'7" moved NW 5' Auger refusal 1'3" on probable bedrock | |
| | | | 13 | | <u>Gray, brown coarse to fine SAND, little Silt, some coarse to fine Gravel, with rock fragments</u> 1'9" | | | | | |
| 2 | | | 20 | | <u>End of Boring @ 1'9"</u> | | | | | |
| | | | 25/3" | | | | | | | |
| 3 | | | | | | | | | | |
| 4 | | | | | | | | | | |
| 5 | | | | | | | | | | |
| 6 | | | | | | | | | | |
| 7 | | | | | | | | | | |
| 8 | | | | | | | | | | |
| 9 | | | | | | | | | | |
| 10 | | | | | | | | | | |
| 11 | | | | | | | | | | |
| 12 | | | | | | | | | | |
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| 16 | | | | | | | | | | |
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| 19 | | | | | | | | | | |
| 20 | | | | | | | | | | |
| 21 | | | | | | | | | | |
| 22 | | | | | | | | | | |

| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-12 | | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|-------------------|-----------------------|--|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | SHEET NO.: 1 of 1 | | | |
| Client: AMS Acquisitions | | | | | | | JOB NUMBER: 23-34 | | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | ELEVATION: +79.0 | | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | | START DATE: 12/Jul/23 | |
| 12/Jul/23 | | 4'7" | | DIA. | 3 1/4" | 1 3/8" | | | FINISH DATE: 12/Jul/23 | |
| | | | | WGHT | | 140# | | | DRILLER: Collin | |
| | | | | FALL | | 30" | | | INSPECTOR: Mike C | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | Sym | IDENTIFICATION | | | | REMARKS | |
| | | | 7 | | <u>Black topsoil</u> | | | | 0'3" | |
| 1 | | S-1 | 14 | | FILL (Gr, br cf S, t \$, s cf G, w/boulder) | | | | Rec = 16" moist | |
| | | | 19 | | | | | | | |
| 2 | | | 16 | | | | | | | |
| | | | 9 | | | | | | | |
| 3 | | S-2 | 26 | | FILL (same) | | | | Rec = 4" moist | |
| | | | 11 | | <u>FILL (Gray, brown coarse to fine SAND, trace Silt, some coarse to fine Gravel, with boulder)</u> | | | | | |
| 4 | | | 8 | | | | | | | |
| | | | 18 | | | | | | | |
| 5 | | S-3 | 18 | | FILL (same, s \$) | | | | Rec = 1" wet | |
| | | | 10 | | | | | | | |
| 6 | | | 5 | | | | | | | |
| | | | 3 | | | | | | | |
| 7 | | S-4 | 5 | | FILL (Br cf S, a \$, s cf G, w/Cy \$ pockets) | | | | Rec = 4" wet | |
| | | | 9 | | | | | | | |
| 8 | | | 5 | | | | | | 8'0" | |
| | | | 13 | | | | | | | |
| 9 | | S-5 | 8 | | Br, gr Cy \$, w/t cf S | | | | Rec = 14" wet | |
| | | | 5 | | <u>Brown, gray Clayey SILT, with trace coarse to fine Sand</u> | | | | | |
| 10 | | | 4 | | | | | | | |
| | | S-6 | 13/2" | | same | | | | 10'2" | |
| 11 | | | | | <u>End of Boring @ 10'2"</u> | | | | Rec = 3" wet | |
| 12 | | | | | | | | | Spoon refusal 10'2" on possible bedrock | |
| 13 | | | | | | | | | | |
| 14 | | | | | | | | | | |
| 15 | | | | | | | | | | |
| 16 | | | | | | | | | | |
| 17 | | | | | | | | | | |
| 18 | | | | | | | | | | |
| 19 | | | | | | | | | | |
| 20 | | | | | | | | | | |
| 21 | | | | | | | | | | |
| 22 | | | | | | | | | | |

| CARLIN-SIMPSON & ASSOCIATES Sayreville, NJ | | | | TEST BORING LOG | | | | BORING NUMBER B-13 | |
|--|-----------------------|---------------|------------------------------|-----------------|---|--------|-------------------|------------------------|--|
| Project: Proposed 4 Story Building, Albany Post Rd & Craft Ln, Buchanan NY | | | | | | | SHEET NO.: 1 of 1 | | |
| Client: AMS Acquisitions | | | | | | | JOB NUMBER: 23-34 | | |
| Drilling Contractor: Environmental Technical Drilling | | | | | | | ELEVATION: +79.0 | | |
| GROUNDWATER | | | | CASING | SAMPLE | CORE | TUBE | DATUM: Topo | |
| DATE | TIME | DEPTH | CASING | TYPE | HSA | SS | | START DATE: 12/Jul/23 | |
| No groundwater encountered | | | | DIA. | 3 1/4" | 1 3/8" | | FINISH DATE: 12/Jul/23 | |
| | | | | WGHT | | 140# | | DRILLER: Collin | |
| | | | | FALL | | 30" | | INSPECTOR: Mike C | |
| Depth (ft.) | Casing Blows per Foot | Sample Number | Blows on Sample Spoon per 6" | S y m | IDENTIFICATION | | | REMARKS | |
| 1 | | S-1 | 4 | | <u>Black topsoil</u> | | | 0'3" | |
| | | | 14 | | <u>Gray brown coarse to fine SAND,</u> | | | | |
| 2 | | | 18/4" | | <u>little (+) Silt, and coarse to fine Gravel</u> | | | 1'4" | |
| 3 | | | | | <u>End of Boring @ 1'6"</u> | | | | |
| 4 | | | | | | | | Auger refusal 1'4" | |
| 5 | | | | | | | | moved 3' west | |
| 6 | | | | | | | | Auger refusal 1'2" | |
| 7 | | | | | | | | moved 3' west | |
| 8 | | | | | | | | Auger refusal 0'8" | |
| 9 | | | | | | | | on probable bedrock | |
| 10 | | | | | | | | | |
| 11 | | | | | | | | | |
| 12 | | | | | | | | | |
| 13 | | | | | | | | | |
| 14 | | | | | | | | | |
| 15 | | | | | | | | | |
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| 17 | | | | | | | | | |
| 18 | | | | | | | | | |
| 19 | | | | | | | | | |
| 20 | | | | | | | | | |
| 21 | | | | | | | | | |
| 22 | | | | | | | | | |

CARLIN-SIMPSON & ASSOCIATES, LLC

Consulting Engineers
Geotechnical & Environmental

Proposed 4-Story Building
Albany Post Rd. & Craft Ln.
Buchanan, NY
23-34

28 June 2023

TP-1 (Elev. +68.0)

| | | |
|------------|--|----------------------------|
| 0'0"-0'4" | Black topsoil | |
| 0'4"-0'10" | FILL (Gravel, 1" road base) | dense, moist |
| 0'10"-5'3" | FILL (Gray, brown coarse to fine SAND, little Silt, and (-) coarse to fine Gravel, with many cobbles and boulders) | medium dense, dense, moist |
| 5'3"-7'9" | FILL (Dark gray coarse to fine SAND, some (+) Silt, trace (-) fine Gravel, with wood) | loose, moist to wet |
| 7'9"-8'3" | Light gray coarse to fine SAND, and (+) Silt, little (-) medium to fine Gravel) | medium dense, wet |
| | Groundwater encountered @ 5'3" | |

TP-2 (Elev. +71.0)

| | | |
|-----------|--|---------------------|
| 0'0"-1'0" | Black topsoil | |
| 1'0"-4'9" | FILL (Light brown coarse to fine SAND, little (+) Silt, some (+) coarse to fine Gravel, with many large cobbles boulders, many fine roots) | medium dense, moist |
| 4'9"-5'9" | FILL (Dark gray coarse to fine SAND, little (+) Silt, with trace organics, old topsoil layer) | loose, moist |
| 5'9"-6'9" | Brown coarse to fine SAND, little Silt, some (-) coarse to fine Gravel, with cobbles | medium dense, moist |
| 6'9"-8'6" | Stacked packed boulders. Bucket refusal on large boulder. | dense, moist to wet |
| | Groundwater encountered @ 8'3" | |

28 June 2023

TP-3 (Elev. +80.0)

| | | |
|-----------|-----------------------------|-----------------|
| 0'0"-0'4" | Black topsoil | |
| 0'4"-1'0" | Boulders with seams of soil | rippable, moist |
| 1'0" | Refusal on Bedrock | unrippable |
| | No groundwater encountered | |

TP-4 (Elev. +78.5)

| | | |
|-----------|-----------------------------|------------|
| 0'0"-0'3" | Black topsoil | |
| 0'3"-1'0" | Boulders with seams of soil | rippable |
| 1'0" | Refusal on Bedrock | unrippable |
| | No groundwater encountered | |

TP-5 (Elev. +77.0)

| | | |
|-----------|--|------------------------|
| 0'0"-0'6" | Black topsoil | |
| 0'6"-2'6" | FILL (Brown coarse to fine SAND, little Silt, some coarse to fine Gravel, with many cobbles, boulders) | loose-med dense, moist |
| 2'6"-4'0" | FILL (Gray, brown coarse to fine SAND, little (+) Silt, little medium to fine Gravel) | dense, moist |
| 4'0"-5'6" | Asphalt | |
| 5'6"-7'6" | FILL (Brown, gray coarse to fine SAND, little (+) Silt, some (+) coarse to fine Gravel, with many cobbles, boulders, with brick) | dense, moist to wet |
| 7'6" | Refusal on boulders (probable fill) | |
| | Groundwater encountered @ 6'9" | |

28 June 2023

TP-6 (Elev. +95.0)

| | | |
|-----------|---|---------------------|
| 0'0"-0'4" | Black topsoil | |
| 0'4"-1'3" | Brown coarse to fine SAND, little (-) Silt, little (+) coarse to fine Gravel, with many boulders | medium dense, moist |
| 1'3"-5'0" | Brown coarse to fine GRAVEL some (-), coarse to fine Sand, trace (+) Silt, with many cobbles, boulders | dense, moist |
| 5'0" | Refusal on Bedrock, highly fractured and weathered, with soil seams | rippable |
| | No groundwater encountered | |

TP-7 (Elev. +70.0)

| | | |
|-----------|--|--------------|
| 0'0"-0'6" | Black topsoil | |
| 0'6"-3'0" | FILL (Brown coarse to fine SAND, little Silt, some (-) coarse to fine Gravel, with a few boulders | dense, moist |
| 3'0" | Refusal on Bedrock | |
| | No groundwater encountered | |

TP-8 (Elev. +68.0)

| | | |
|------------|--|--------------|
| 0'0"-0'10" | Black topsoil | |
| 0'10"-4'6" | FILL (Dark brown coarse to fine SAND, little (+) Silt, some (-) coarse to fine Gravel, with boulders) | loose, moist |
| 4'6" | Refusal on Bedrock | |
| | No groundwater encountered | |

28 June 2023

TP-9 (Elev. +82.0)

0'0"-0'3" Black topsoil

0'3"-1'3" Rippable rock with soil seams (Brown coarse to fine SAND, some (+) Silt, little (-) coarse to fine Gravel) dense, moist

1'3" Refusal on Bedrock

No groundwater encountered

TP-10 (Elev. +88.0)

0'0"-0'2" Black topsoil

0'2"-1'1" Rippable rock with soil seams (Brown coarse to fine SAND, some (-) Silt, little coarse to fine Gravel) dense, moist

1'1" Refusal on Bedrock

No groundwater encountered

TP-11 (Elev. +87.0)

0'0"-0'5" Black topsoil

0'5"-2'8" Rippable rock with soil seams (Brown coarse to fine SAND, some (-) Silt, little (+) coarse to fine Gravel) dense, moist

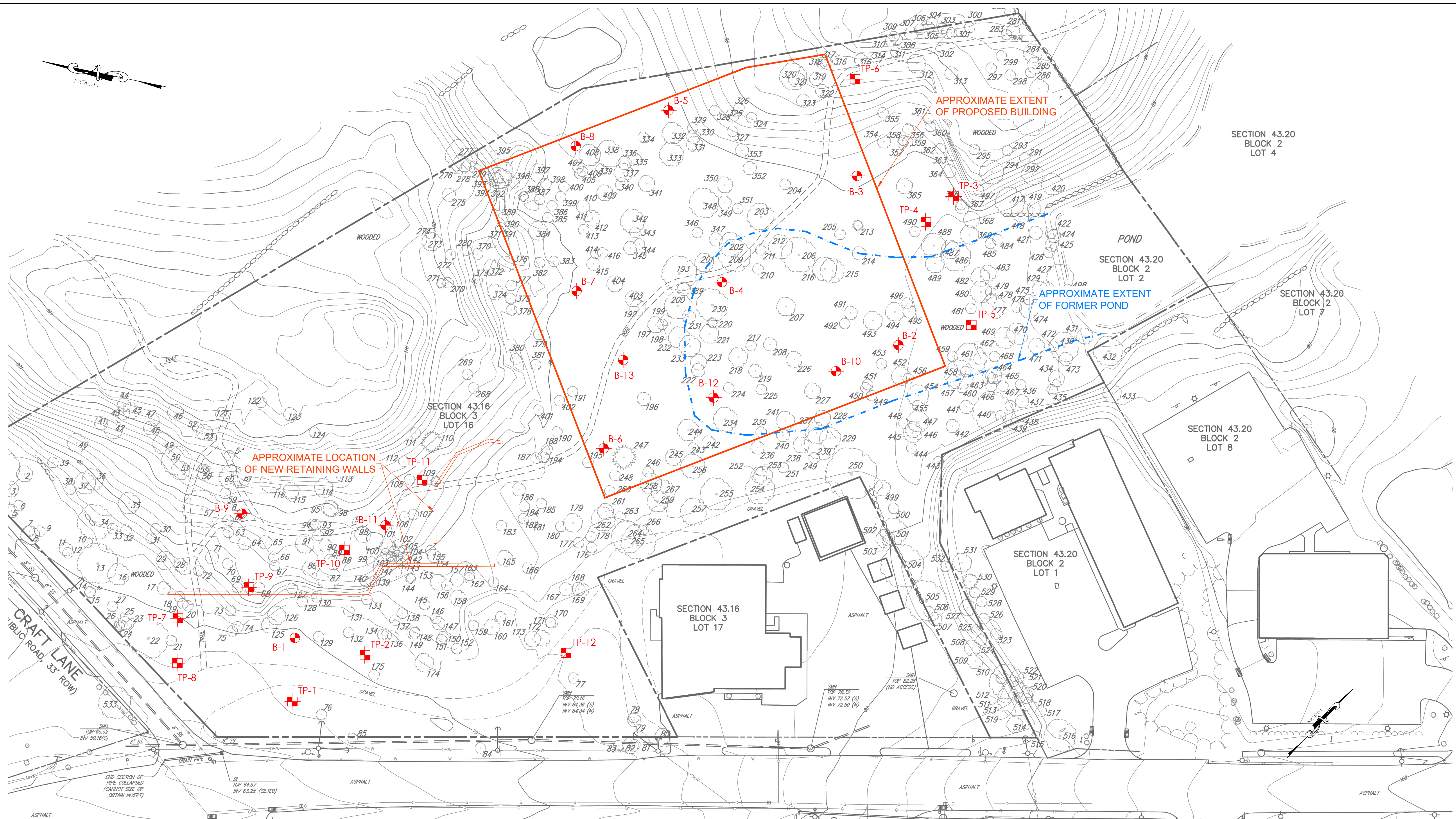
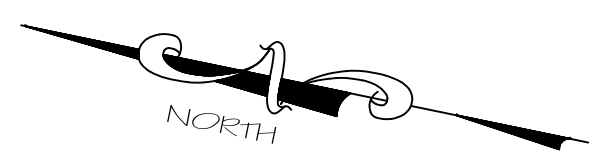
2'8" Refusal on Bedrock

No groundwater encountered

28 June 2023

TP-12 (Elev. +72.0)

| | | |
|-----------|---|-------------------------|
| 0'0"-1'4" | Black topsoil | |
| 1'4"-4'0" | FILL (Dark brown coarse to fine SAND, and Silt, some coarse to fine Gravel, with boulders, clay pockets, and construction debris) | loose, moist |
| 4'0"-8'2" | FILL (Gray Clayey SILT) | moist-wet, organic odor |
| 8'2"-9'6" | Mottled red brown, brown, gray Clayey SILT | very dense, moist |
| | Groundwater encountered @ 7'6" | |



CRAFT LANE
(PUBLIC ROAD, 33' ROW)

NEW YORK AND ALBANY POST ROAD (NYS ROUTE 9W)
(PUBLIC ROAD)

- GENERAL NOTES:**
- GENERAL LAYOUT WAS OBTAINED FROM DRAWINGS PREPARED BY JMC PLLC, ENTITLED "TREE SURVEY" DATED 1/27/2023 AND "CONCEPTUAL SITE PLAN" DATED 4/7/2023.
 - BORING AND TEST PIT LOCATIONS WERE LAID OUT IN THE FIELD BY CARLIN-SIMPSON & ASSOCIATES (CSA).
 - BORINGS (B-1 THRU B-13) WERE PERFORMED BY ENVIRONMENTAL TECHNICAL DRILLING INC. IN JULY 2023 UNDER THE FULL TIME INSPECTION OF CSA.
 - TEST PITS (TP-1 THRU TP-12) WERE PERFORMED BY AMERICAN TREE AND LANDSCAPE CORP. IN JUNE 2023 UNDER THE FULL TIME INSPECTION OF CSA.
 - ALL LOCATIONS ARE APPROXIMATE.

- LEGEND:**
- BORING LOCATION
 - TEST PIT LOCATION


ROBERT B. SIMPSON, P.E.
PROFESSIONAL ENGINEER

BORING & TEST PIT LOCATION PLAN

PROPOSED 4-STORY BUILDING
ALBANY POST ROAD & CRAFT LANE
BUCHANAN, NEW YORK

| | | | |
|-------------|--------|----------|------------|
| DRAWN | SR/MRA | SCALE | 1" = 30' |
| CHECKED | RBS | DATE | 08-15-2023 |
| PROJECT NO. | 23-34 | DWG. NO. | BTLP-1 |
| APPROVED | | | |

CARLIN-SIMPSON & ASSOCIATES, LLC
61 Main Street
Sayreville, NJ 08872
Consulting Geotechnical and
Environmental Engineers



APPENDIX D

TEMPORARY & PERMANENT EROSION AND SEDIMENT CONTROL INSPECTION AND MAINTENANCE CHECKLISTS

Temporary Erosion and Sediment Control Inspection and Maintenance Checklist

| Erosion and Sediment Control Measure | Inspection/Maintenance Intervals | Inspection/Maintenance Requirements |
|---|---|--|
| Stabilized Construction Entrance | Daily | <ul style="list-style-type: none"> • Periodic top dressing with additional aggregate as required • Clean sediment in public right-of-ways immediately |
| Silt Fence | Weekly + After Each Rain | <ul style="list-style-type: none"> • Remove & redistribute sediment when bulges develop in the silt fence. |
| Inlet Protection | Weekly + After Each Rain | <ul style="list-style-type: none"> • Remove sediment as necessary and replace filter fabric, crushed stone etc. • Any broken and damaged components should be replaced. • Check all materials for proper anchorage and secure as necessary. |
| Concrete Washout | Daily | <ul style="list-style-type: none"> • Damaged or leaking facilities shall be deactivated and repaired or replaced immediately. |
| | After Each Rain | <ul style="list-style-type: none"> • Pump excess rainwater that has accumulated over hardened concrete to a stabilized area. |
| | | <ul style="list-style-type: none"> • Remove accumulated hardened material when 75% of the storage capacity of the structure is filled. Replace plastic liner with each cleaning of the washout facility. |

Permanent Stormwater Management Practice Inspection and Maintenance Checklist

| Stormwater Management Practice | Inspection/Maintenance Intervals | Inspection/Maintenance Requirements |
|---|--|---|
| Drain Inlets | Monthly | <ul style="list-style-type: none"> • Check for blockage and/or erosion at top of each inlet. Repair/remove as necessary. • Check for sediment and debris collected within sumps and clean out as necessary. |
| Subsurface Stormwater Management Detention Facility | Annually + After Major Storms | <ul style="list-style-type: none"> • Check level of sediment and debris accumulated within the system. • Check structural integrity of the system pipes, structures, etc. for cracking, bulging or deterioration. Repair/remove as necessary. • Confirm all inlets and outlet structures/pipes are operating properly. |
| Up-Flo Filter Water Quality Structure | (See Maintenance Guidelines in Appendix) | <ul style="list-style-type: none"> • Check primary manhole for sediment, debris, trash, etc. Confirm Bay Separator Unit inlet/outlet pipes from primary manhole to the Bay separator Unit are not clogged. • Check storage manhole for sediment, debris, trash, etc. Clean out after 2 feet have accumulated. • Remove any noticeable oil from the water surfaces within the primary and storage manholes. |

Permanent Stormwater Management Practice Inspection and Maintenance Checklist (Cont'd)

| Stormwater Management Practice | Inspection/Maintenance Intervals | • Inspection/Maintenance Requirements |
|---------------------------------------|---|---|
| Green Roof | Spring | <ul style="list-style-type: none"> • Annual Soil Test by removing small soil quantities and sending to a testing laboratory for nutrient content, etc. • Begin biweekly weed inspection and removal. • Judiciously apply phosphorus free fertilizer if needed based on the annual soil test results. • Biweekly check for displaced soil, inspect roof drains, remove debris and check for pests. |
| | Summer | <ul style="list-style-type: none"> • Continue biweekly weed inspection and removal. • Continue biweekly inspection for soil displacement, roof drains, debris, pest control, etc. • Irrigation may be required every 2 or 3 weeks during prolonged hot, dry weather. |
| | Fall | <ul style="list-style-type: none"> • Continue biweekly weed inspection and removal. • Continue biweekly inspection for soil displacement, roof drains, debris, pest control, etc. |
| | Winter | <ul style="list-style-type: none"> • Remove snow as needed from access walkways. |

Permanent Stormwater Management Practice Inspection and Maintenance Checklist (Cont'd)

| Stormwater Management Practice | Inspection/Maintenance Intervals | Inspection/Maintenance Requirements |
|--|---|--|
| Stormwater Planters Stormwater Planters | Early Spring (before new growth is 3 inches high) | <ul style="list-style-type: none"> • Cut and remove dead stalks and seed heads remaining from previous season. • Remove sticks and debris. • Prune shrubs if necessary. • Divide and move perennials if they are too crowded. • Replenish mulch layer to maintain a • 3 inch layer of shredded bark. |
| | Late Spring | <ul style="list-style-type: none"> • Remove weeds. • Water as needed during periods of drought. |
| | Fall | <ul style="list-style-type: none"> • Removed weeds and diseased plants. • Remove excess leaves. • If fall is dry, continue to water trees and shrubs until ground begins to freeze (later October). These woody plants need moisture entering winter to ensure survival. |

The owner/operator responsible for inspection and maintenance as outlined above:

Buchanan Dev AMS LLC
Mr. Ryan Sutherland
86 Main Street, Suite 200
Yonkers, NY 10701
Phone: 212-695-7585
Fax:
Email: RSutherland@amsacquisitions.com

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APPENDIX E

CONTRACTOR'S CERTIFICATION



Site Planning
 Civil Engineering
 Landscape Architecture
 Land Surveying
 Transportation Engineering

Environmental Studies
 Entitlements
 Construction Services
 3D Visualization
 Laser Scanning

JMC Project 22062
 AMS BUCHANAN
 ALBANY POST ROAD & CRAFT LANE
 VILLAGE OF BUCHANAN, NY

CONTRACTOR'S CERTIFICATION

“I hereby certify under penalty of law that I understand and agree to comply with the terms and conditions of the SWPPP and agree to implement any corrective actions identified by the qualified inspector during a site inspection. I also understand that the owner or operator must comply with the terms and conditions of the most current version of the New York State Pollutant Discharge Elimination System ("SPDES") general permit for stormwater discharges from construction activities and that it is unlawful for any person to cause or contribute to a violation of water quality standards. Furthermore, I am aware that there are significant penalties for submitting false information, that I do not believe to be true, including the possibility of fine and imprisonment for knowing violations.”

Company Name: _____

Address: _____

Telephone Number: _____

Name and Title: _____

Signature: _____ Date: _____

Permit Identification No.: _____

Name and Title of Trained Contractor: _____

Elements of the SWPPP Contractor is responsible for: _____

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APPENDIX F

DRAWINGS

EXISTING DRAINAGE LEGEND

| | |
|--|-----------------------------|
| | EXISTING GRADE |
| | SURVEYED WETLANDS |
| | EXISTING STONE WALL |
| | WATERSHED BOUNDARY LINE |
| | BOUNDARY OF COVER TYPE LINE |
| | LIMIT OF SOIL GROUPS LINE |
| | FLOW PATH LINE |
| | HYDROLOGIC SOIL GROUP 'C' |
| | HYDROLOGIC SOIL GROUP 'B' |

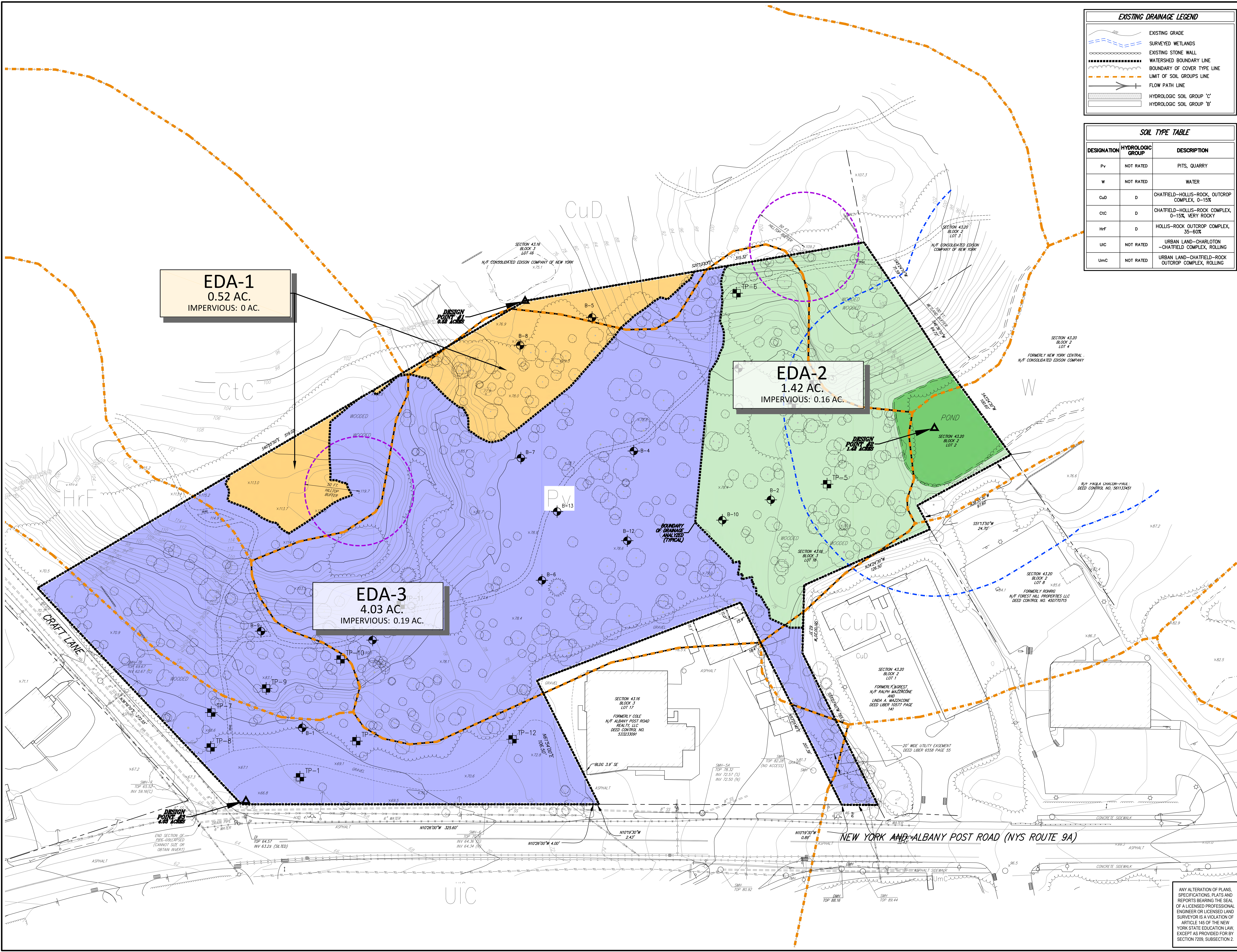
SOIL TYPE TABLE

| DESIGNATION | HYDROLOGIC GROUP | DESCRIPTION |
|-------------|------------------|--|
| Pv | NOT RATED | PITS, QUARRY |
| W | NOT RATED | WATER |
| CuD | D | CHATFIELD-HOLLIS-ROCK, OUTCROP COMPLEX, 0-15% |
| CtC | D | CHATFIELD-HOLLIS-ROCK COMPLEX, 0-15%, VERY ROCKY |
| HrF | D | HOLLIS-ROCK OUTCROP COMPLEX, 35-60% |
| UIC | NOT RATED | URBAN LAND-CHARLTON-CHATFIELD COMPLEX, ROLLING |
| UmC | NOT RATED | URBAN LAND-CHATFIELD-ROCK OUTCROP COMPLEX, ROLLING |

EDA-1
0.52 AC.
IMPERVIOUS: 0 AC.

EDA-2
1.42 AC.
IMPERVIOUS: 0.16 AC.

EDA-3
4.03 AC.
IMPERVIOUS: 0.19 AC.



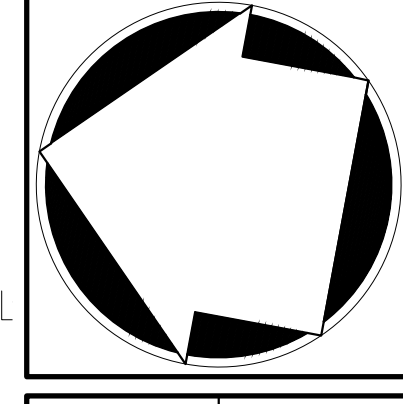
| | |
|----------|--|
| No. | |
| Revision | |
| Date | |

BUCHANAN DEV AMS LLC
ONE BRIDGE PLAZA NORTH, SUITE 640
FORT LEE, NJ 07024

PERKINS EASTMAN
677 WASHINGTON BOULEVARD, SUITE 101
STAMFORD, CT 06901

JMC Planning, Engineering, Landscape Architecture & Land Surveying, PLLC
JMC Site Development Consultants, LLC
John Mayer Consulting, Inc.

120 BEDFORD ROAD • BRIDGEVILLE, NY 10504
voice 914.273.5225 • fax 914.273.2192
www.jmcpllc.com



EXISTING DRAINAGE AREA MAP

AMS BUCHANAN
ALBANY POST ROAD & CRAFT LANE
VILLAGE OF BUCHANAN, NEW YORK

| | | | |
|-------------|------------|----------|----|
| Drawn | EJK | Approved | AN |
| Scale | 1" = 30' | | |
| Date | 11/08/2023 | | |
| Project No. | 22062 | | |
| 2006-AMMAGE | EDA | | |
| DA-1 | | | |

ANY ALTERATION OF PLANS, SPECIFICATIONS, PLATS AND REPORTS BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER OR LICENSED LAND SURVEYOR IS A VIOLATION OF ARTICLE 145 OF THE NEW YORK STATE EDUCATION LAW, EXCEPT AS PROVIDED FOR BY SECTION 7209, SUBSECTION 2.

NOT FOR CONSTRUCTION

NOT FOR CONSTRUCTION



PROPOSED DRAINAGE LEGEND

- EXISTING GRADE
- PROPOSED FINISHED GRADE
- SURVEYED WETLANDS
- EXISTING STONE WALL
- WATERSHED BOUNDARY LINE
- LIMIT OF SOIL GROUPS LINE
- FLOW PATH LINE
- PROPOSED BUILDING LINE
- PROPOSED CONCRETE CURB
- PROPOSED MANHOLE (MH)
- EXISTING DRAIN INLET
- PROPOSED DRAIN INLET (DI)
- PROPOSED COMBINATION INLET (CI)
- PROPOSED END SECTION (ES)
- PROPOSED WATER QUALITY STRUCTURE
- RIP RAP ENERGY DISSIPATOR

SOIL TYPE TABLE

| DESIGNATION | HYDROLOGIC GROUP | DESCRIPTION |
|-------------|------------------|--|
| Pv | NOT RATED | PITS, QUARRY |
| W | NOT RATED | WATER |
| CuD | D | CHATFIELD-HOLLIS-ROCK, OUTCROP COMPLEX, 0-15% |
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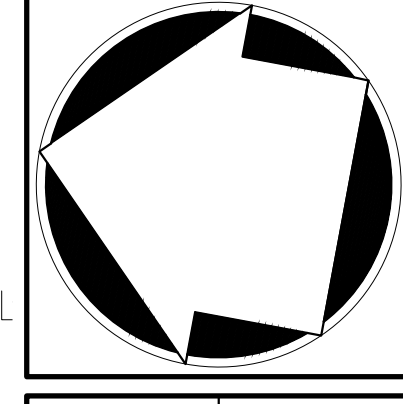
| | | | |
|-----|----------|------|----|
| No. | Revision | Date | By |
| | | | |

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PROPOSED DRAINAGE AREA MAP

AMS BUCHANAN
 ALBANY POST ROAD & CRAFT LANE
 VILLAGE OF BUCHANAN, NEW YORK

| | | | |
|-------------|----------|--------------|------------|
| Drawn: | EJK | Approved: | AN |
| Scale: | 1" = 30' | Date: | 11/08/2023 |
| Project No: | 22062 | Zone/Agency: | POA |
| Drawing No: | DA-2 | | |

ANY ALTERATION OF PLANS, SPECIFICATIONS, PLATS AND REPORTS BEARING THE SEAL OF A LICENSED PROFESSIONAL ENGINEER OR LICENSED LAND SURVEYOR IS A VIOLATION OF ARTICLE 145 OF THE NEW YORK STATE EDUCATION LAW, EXCEPT AS PROVIDED FOR BY SECTION 7209, SUBSECTION 2.